

# Distributed Illumination Control

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**Abstract**—This project aims to control a small-scale model of an office space (3-LED illumination system) in a distributed manner, maximizing the user (desk) comfort and minimizing the energy spent. A consensus algorithm was applied to a control system, in which an agent network finds a consensus about the optimal solution, trying to respect the system's reference (input). If those references are not achievable, the network should be able to determine the closest best solution. We could not implement some parts of the project: the PC application and the energy consumption control. However, we did manage to obtain the illuminance distributed control which was the main goal.

**Index Terms**—

## I. INTRODUCTION

The last decade brought a new way of lighting - LEDs (Light Emitting Diodes). They outlast conventional light bulbs and have a much lower energy consumption. Besides, LED's have no danger associated with handling mercury and other metals. They also allow for an easier integration with sensors, computers, controllers and all kinds of other electronics. With that said, there are still some challenges with LED's regarding optimization.

This project aims to tackle those challenges. In order to do so, the system is defined as an agent network in which each agent tries to respect minimum specifications, taking into account its neighbors' interference and trying to achieve the best global situation. Such compromise is managed with a communication system. This network could be centralized, but it would take more processing (and hardware) power since centralized control needs to make all operations in the same place. It would also make the system's response slower overall.

The main goal is to simulate an office floor, where minimum illuminance levels must be guaranteed at each desk. The desk's occupancy is also taken into account, meaning it is not necessary to illuminate an empty desk. Of course, day/night cycles (outside interference) are a factor to consider as well as the other desk's light interferences.

Everything was implemented through a distributed control system with a coordinated agent network (based on the consensus algorithm). The system can be monitored and changes can be made by the user, regarding illuminance levels and interferences. All the code developed is available in the delivered folder.

## II. PROBLEM DEFINITION

To simulate the office floor, 3 luminaires (LED's) were set up inside a shoe box. This box was "coated" with white paper on the inside to maximize reflection, and cuts were made to simulate an open/closed window. Each luminaire is

attached to a PCB (printed circuit board). Each PCB also has an LDR (Light Detection Resistor) attached, in order to monitor our illuminance levels reflected. The 3 PCBs simulate the 3 desks. In figure 1 is shown a picture of such setup and figure 2 shows the electrical configuration (connections) in each PCB. 2 resistors ( $100\Omega$  and  $10k\Omega$ ) and 1 capacitor were used per PCB (besides the LED and LDR).

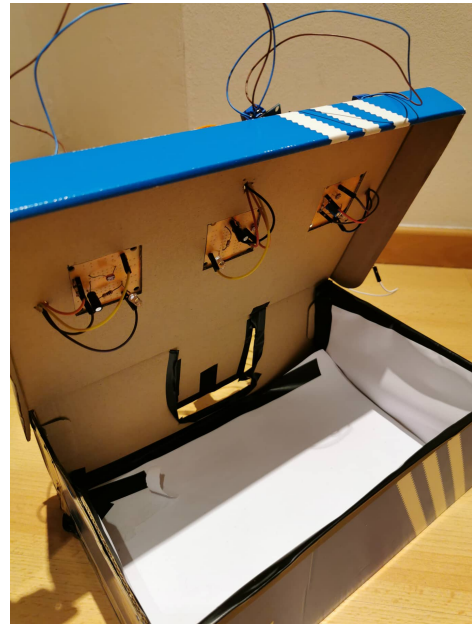


Fig. 1: Luminaire setup

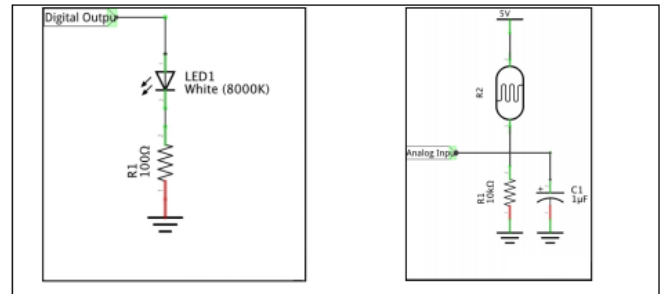


Fig. 2: LED driving circuit (left) and LDR Illuminance Reading circuit

One arduino Uno is connected to each one of the PCB's and all 3 arduinos are connected through a CAN-BUS setup, which is shown in figure 3.

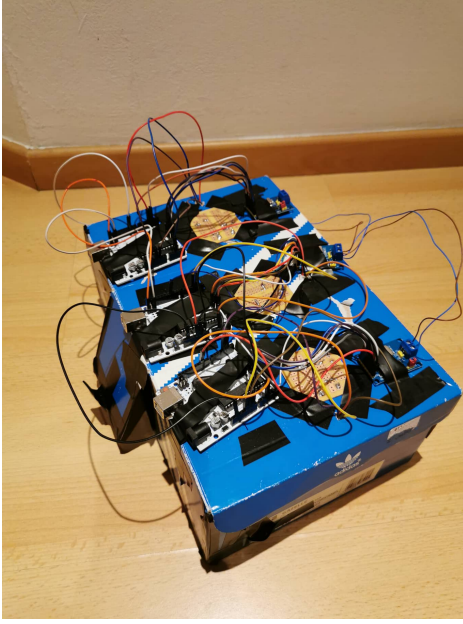


Fig. 3: Arduino communication setup

The LDR is a resistor that changes its resistance values according to the illuminance level, according to figure 4.

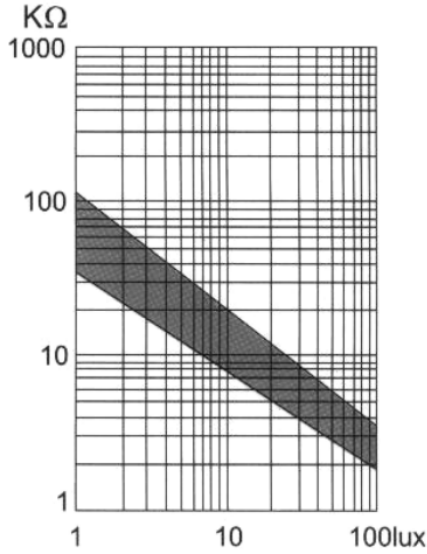


Fig. 4: Resistance values vs Lux values (log scale)

The LED's output illuminance level is determined by its duty cycle - the bigger the duty cycle, the higher the illuminance level (Lux). The duty cycle levels vary from 0 (min) to 255 (max), and are set by the arduino's PWM (Pulse Width Modulation).

For this problem, a consistent way of correlating the variables [*duty cycle*] and [*illuminance*] is needed, so the following is obtained:

$$[Lux] = K * [DutyCycle]. \quad (1)$$

So, in other words,  $K$  must be determined, so illuminance levels are set by adjusting duty cycle levels.

The communication system between arduinos, with the consensus algorithm alongside individual feedback control for stability simulates a smart illuminance system for an office space according to illuminance criteria set by the user.

In this case, the illumination system can be seen as a constrained optimization problem, since the illuminance value of each desk is influenced not only by the duty cycle of the LED above it, but also by the illuminance values of the other desks and external interferences. Given the set of variables:

- $i$  - index of the desk/node,
- $l_i$  - illuminance at desk  $i$ ,
- $L_i$  - lower bound of illuminance at desk  $i$ ,
- $d_i$  - dimming level (duty cycle) of each LED (mapped from 0 to 100),
- $K_{ij}$  - influence of the illuminance of led  $j$  in the irradiance at desk  $i$ ,
- $o_i$  - effect of external illumination at desk  $i$ ,
- $n$  - number of nodes,

and the objective of minimizing all  $d_i$  while guaranteeing that all  $l_i$  are equal or greater than  $L_i$ , this optimization problem can be exposed as:

$$\begin{aligned} \min_{d_1, \dots, d_n} \quad & f(d_1, \dots, d_n) \\ \text{s.t.} \quad & 0 \leq d_i \leq 100 \\ & l_i = \sum_{j=1}^n d_j K_{ij} + o_i \geq L_i, \forall i \end{aligned} \quad (2)$$

So, in this case, all  $K_{ij}$  and  $o_i$  values must be determined.

### III. PROPOSED APPROACH

As mentioned, the problem addressed was solved using a decentralized control system in which each arduino acts as a local controller to each luminaire, in order to achieve a global goal. Two different approaches were used: cooperative and non-cooperative control. Considering the set objective of energy minimization for the total system, it was necessary to implement a cooperative mode. Regarding the non-cooperative solution, it was implemented as a means of canceling fluctuations around the first approach solution.

Due to decentralization of the control system, communications had to be implemented to make sure the arduinos shared information, which was critical to achieve the goal. The protocol used between arduinos was CAN-Bus, which uses serial asynchronous communication, offers bit rate up to 1 Mb/s, and gives the possibility of filtering received messages (through buffer filters) in order to decide if they're important to this arduino or not. This protocol also allows for communications without a master or a slave, which is ideal for decentralized system. This communication protocol is made connecting 7 wires from each CAN-Bus device to each arduino, and 2 wires both between CAN-Bus's and Arduinos, according to figure 5.

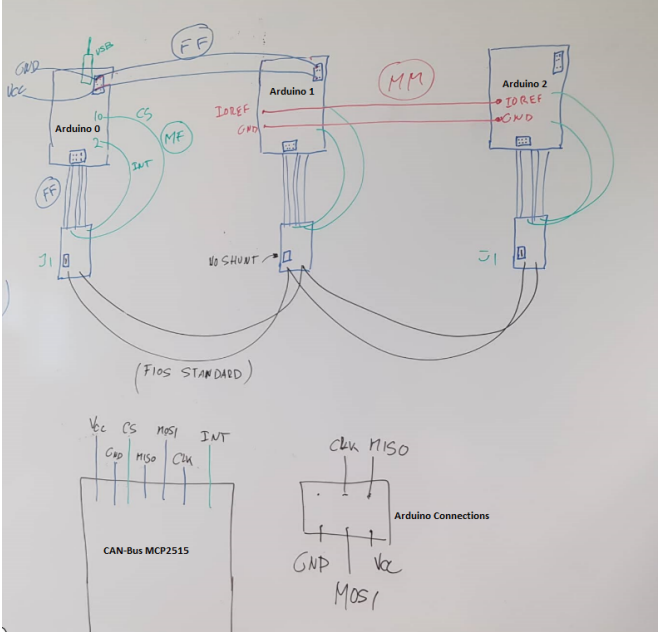


Fig. 5: Serial CAN-Bus Arduino communication configuration

Regarding cooperative control, it was demonstrated that this system can initially be formulated as a constrained global optimization problem. This problem can be manipulated and transformed in an equivalent optimization problem with a quadratic function and a convex set of constraints, as will be discussed later. Besides, it is possible to decompose this problem so that each arduino performs individual computations to reach the global solution. As such, the consensus algorithm becomes a possible and desirable implementation. The consensus algorithm provides a distributed way to compute the solution by the different luminaires so that each one has to respect a smaller set of constraints by introducing a new global variable that all of them have to "agree". For each variable to be determined (the ducty cycles to apply), each luminaire saves two different values. One which results from its computations and another one that is the average of those computations of all the system's luminaires. The algorythm tries to achieve the minimization solution while converging these two values. If the problem is feasible, it guarantees that all luminaires' variables converge to the same value.

The non-cooperative control system is implemented as a PID control, that follows the reference given by the consensus algorithm. The PID acts in order to achieve its own objective, and thus making the system resistant to external disturbances. Note that the reference that the PID controller follows already takes into consideration the gains  $K_{ij}$  regarding other arduinos duty cycle to each LED.

#### IV. DEVELOPMENT

A simplified diagram of the project is presented in figure 6. A detailed discussion of its modules is presented in the next sections, starting from isolated components to the fully integrated form.

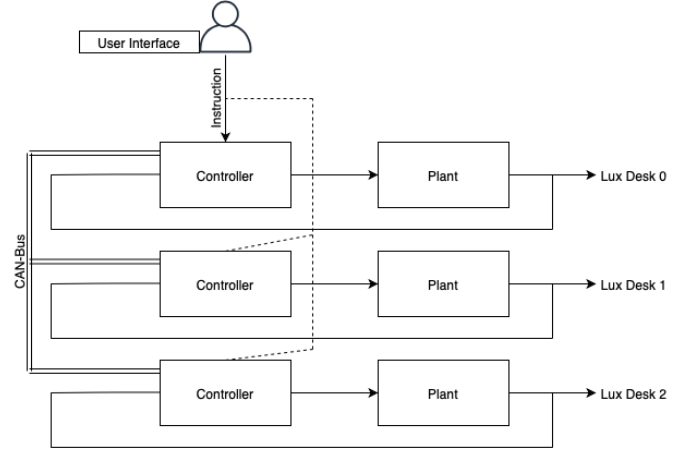


Fig. 6: Overall System Diagram

#### A. Plant - The luminaire: construction and modeling

The basic functionality of each luminaire is to ensure an illuminance treshold by selecting adequate duty cycles for its LED. However, this illuminnace is not read directly from an arduino port. All measurements from the arduinos are digital scaled voltages (between 0 and 1023), therefore, there is a need to determine the relations between the variables of interest and the available measurements.

Let us first consider the LDR component. Figure 7 shows the LDR circuit in analysis:

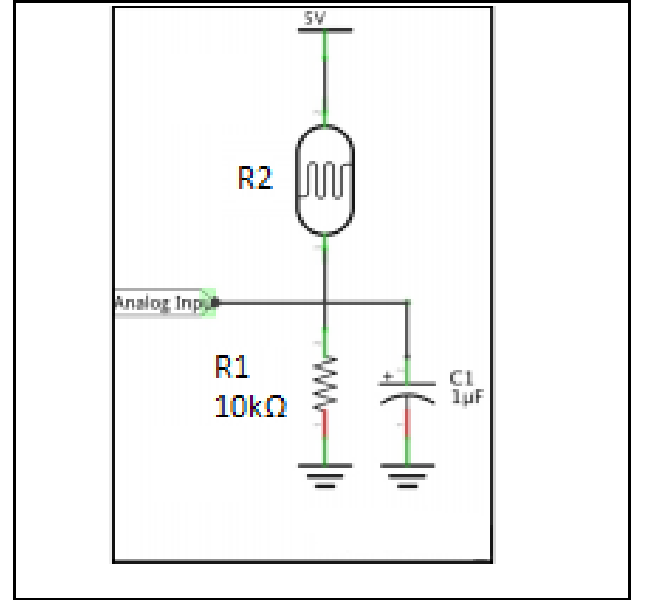


Fig. 7: LDR Illuminance Reading circuit

As previously said, it is possible to calculate the desk's illuminance knowing the LDR resistance value. Analysing figure 4, it is now possible to calculate such resistance considering the voltage divider in steady state:

$$U = 5 \frac{R_1}{R_1 + R_2}. \quad (3)$$

The value of  $U$  is read by the arduino as a digital voltage and the resistor  $R_1$  is known ( $10k\omega$ ), which leads to

$$R_2 = \frac{5R_1}{U} - R_1. \quad (4)$$

The only thing left is to determine the parameters that characterise the LDR properties expressed in figure 4. The illuminance values can be linearized in the form  $y = mx + b$ , in which  $y$  is the LDR resistance value and  $x$  is the illuminance. Applying the logarithmic scale to the equation, we obtain:

$$\log_{10}(R) = m\log_{10}(L) + b, \quad (5)$$

which results in

$$L = 10^{\frac{\log_{10}(R) - b}{m}}. \quad (6)$$

Now that there is a clear relation between illuminance values and resistance values, the calibration process starts, with the goal of determining values for  $m$  and  $b$  -  $b$  being the illuminance value at PMW = 0.

We put a single luminarie inside a closed box, set the PWM duty cycle to a value and record the LDR voltage that is read after a certain time to ignore the transient state. This process is repeated for duty cycles varying from 0 (minimum value) to 255 (maximum value) with increments of 5. This was done for each luminaires.

Since the objective is to have the illuminance values expressed by  $L = K * DutyCycle$ , the only relation between them that is acceptable is a linear one. A matlab algorithm was made to test several  $m$  and  $b$  values, using the Least Square method, allowing it to find the values of  $m$  and  $b$  that make the relation between Lux and duty cycle the "most linear". It was observed that this linearity depended only on the  $m$  paramether. The other one only influenced the gain  $K$ . As so, the later paramether was selected such that the three LDR read equal values for equal duty cycles and that for the maximum duty cycle they read an illuminance of aproximately 500 Lux.

With the optimal values of  $m$  and  $b$  found, we obtained the gain between illuminance and duty cycle -  $K$ . The matlab algorithm was run through for each of the other LDR. Figure 8 shows the best regression for one of the luminaires, which resulted in  $K=1.94$ .

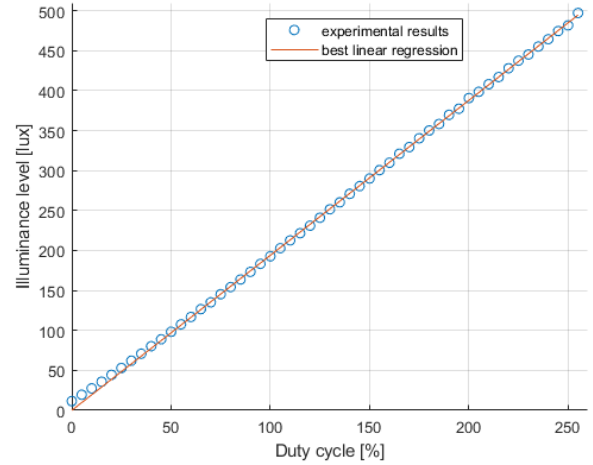


Fig. 8: Illuminance read by one of the luminaires as a function of the PWM duty cycles, for  $m = -0.630$  and  $b = 2.3150$

On a first approach, the information gathered up to now should be sufficient to design a controller that met the requirements. Only the steady state is being considered, but since the transient state is fast compared to the human perception and the system is projected to work over long and continuous periods without sudden variations, there is no major problem. However, for a more rigorous approach, the transient state must be studied. For this, the necessity for changing the system's model arises.

Analysing figure 7, being  $x$  the illuminance value obtained in the static state ( $Lux = K * DutyCycle$ ). Now, taking into account the transient state:

$$\dot{v}\tau(x) = -v + V_{cc} \frac{R_1}{R_1 + R_2(x)}, \quad (7)$$

where  $v$  is the LDR's voltage, while  $\dot{v}$  is its variation in time.  $\tau$  is the time constant relative to this system, which is obtained from:

$$\tau(x) = R_{eq}(x)C_1, \quad (8)$$

$C_1$  being the capacitor's capacitance and

$$R_{eq} = \frac{R_1 R_2(x)}{R_1 + R_2(x)}, \quad (9)$$

is the circuit's equivalent resistance value, where  $R_2$  is the resistance value of the LDR, described by:

$$R_2(x) = 10^{m\log_{10}(x) + b}. \quad (10)$$

The value of  $\tau$  was obtained through tests, running an algorithm through the arduino that increased the duty cycle from 10 in steps of 30, while reading the LDR voltage value "continuously". Once it reached a duty cycle of 250, the same steps were decreased with the same frequency, untill it reached the initial duty cycle.

The data was exported and processed through a matlab algorithm, producing this graph of voltage vs time (s), shown in figure 9.

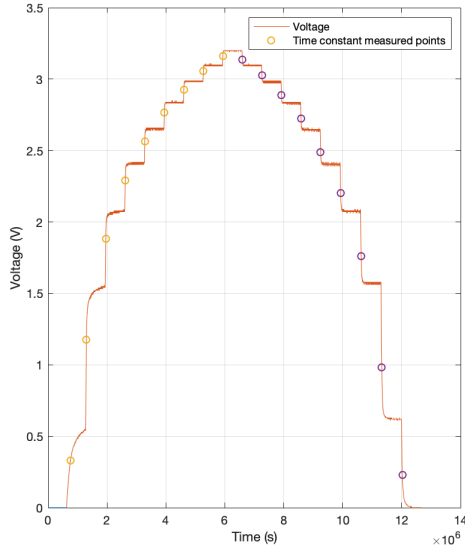


Fig. 9: Voltage of the LDR vs time (step analysis)

From the data structure the value of  $\tau$  is found:

- For the positive steps, by selecting the time instant that corresponds to  $0.66(V_{final} - V_{initial})$  in each step,
- For the negative steps, by selecting the time instant corresponding to  $V_{initial} - 0.66(V_{initial} - V_{final})$  in each step,

being  $V_{initial}$  and  $V_{final}$  the voltage values in the beginning of the step and at the end, respectively.

Those time instants ( $\tau$ ) are then compared to their corresponding illuminance values (obtained through the voltage value), and the following graph is made - figure 10, showing the evolution of  $\tau$  along the illuminance values.

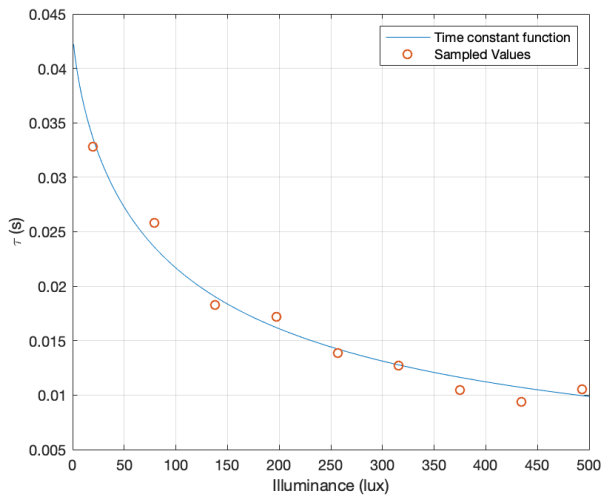


Fig. 10:  $\tau$  vs Lux Values

With the experimental values (red dots) of  $\tau$  obtained, it's possible to approximate the  $\tau$  vs  $Lux$  relation to equation 7, as the blue line seen in figure 10. The approximation obtained is defined by:

$$\tau(x) = \frac{A \cdot 10^{m \log_{10}(x) + b} \cdot 10^3}{B + 10^{m \log_{10}(x) + b} \cdot 10^3}, \quad (11)$$

where  $m$  and  $b$  are already known, and:

- $A = 0.0435$ ,
- $B = 17360.74$ .

The multiplication by  $10^3$  on the numerator and denominator are due to unit adjustments relating resistance values.

There is also a delay associated with the transient state that needs to be included in the model, which is essentially the time it takes for the LDR to "enter" the transient state, in other words, the time it takes for the LDR to "react". The illuminance system model for transient state should be in the form:

$$y(t) = f(v(t - \theta)), \quad (12)$$

$y$  being the illuminance according to the model, which is given by a function of voltage( $v$ ) through time.

A test was compiled to detect how much time it would take in transient state for the LDR voltage value to change. Once the delay  $\theta$  was known, it was added to the expression 11, computing:

$$\tau(x) = \frac{A \cdot 10^{m \log_{10}(x) + b} \cdot 10^3}{B + 10^{m \log_{10}(x) + b} \cdot 10^3} - \theta, \quad (13)$$

with a delay  $\theta = 660 \mu s$

The approximated model obtained can thus be used to further approximate our system's response to the real one.

### B. The local controller

The feedback control system implemented in which both the PID controller and the reference value are controlled by the arduino. The reference value is the feedforward's output. The PID controller was implemented in C++ enabling duty cycle changes to correct any overshoot or any outside disturbances. Figure 11 shows the feedback control scheme.

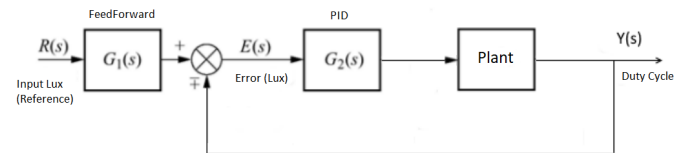


Fig. 11: Feedback control scheme

Figure 12 shows the PID controller configuration scheme.



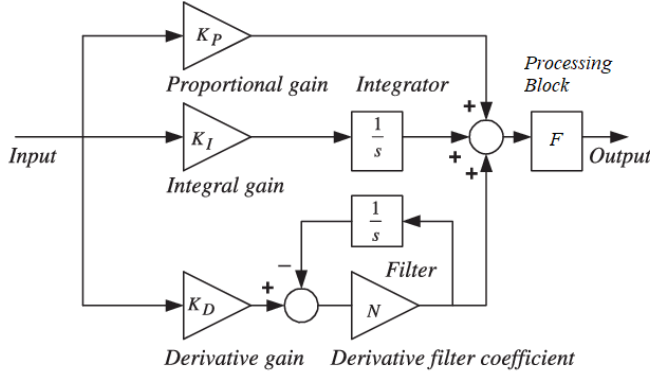


Fig. 12: PID controller scheme

The PID algorithm was implemented as a class in c++. It receives as input the current duty cycle of the LED, the error between reference lux and measured lux, and calculates the proportional, integral and derivative contributions. Then, the processing block will convert the sum of the contributions to duty cycle units, and add or subtract it to the current duty cycle. An anti wind-up and saturation function was then made in c++, that limits the duty cycle to  $[0, 255]$  and resets the integral contribution whenever saturation occurs.

The gains  $K_p$ ,  $K_i$  and  $K_d$  were manually tuned, until a reasonable performance was found.

### C. The cooperative controller

As explained previously, the cooperative controller was designed using the consensus algorithm. A detailed explanation on this method can be consulted [2] if needed as this article will only focus on the fundamental aspects that allow the understanding of the discussed topics. The original problem is manipulated and decomposed so that each luminaire only has to focus on its local properties/variables:

- "The local illuminance lower bound (occupancy state)  $L_i$ .
- The local external illuminance influence  $o_i$
- The local cost  $c_i$ .
- The local actuator bounds (in our case are all the same, 0 and 100).
- The coupling gains from the other luminaires to itself,  $k_i$ .
- The global optimization parameter  $\rho$ ." [2]

At a certain point, this manipulation leads to an Augmented Lagrangean which requires three iterative action to solve the minimization problem:

- the computation of the primal (original) variables to determine, the duty cycles (based on said Lagrangean),
- the computation of the average of those duty cycles of all luminaires,
- the computation of the dual variables (Lagrange multipliers).

In between, it is also necessary to share those duty cycles among the luminaires. As so, a fourth action is required after the first one to ensure the correct transmission of information and its synchronazation.

The first computation is the hardest one

In terms of implementation, this variables, as well as the methods further explained, are condensed in a C++ class.

### D. Initialization and calibration

#### 1) Initialization

During the design of each controller, a sampling rate of 100Hz was imposed, using arduino *TIMER1* interrupts. When an interrupt is triggered, a flag is used to inform system to sample and control reference. This way, an initialization of *TIMER1* interrupt had to be done. To do so, the following arduino registers had to be changed:

- *OCR1A* (Output compare register A for timer 1) - The interrupt will trigger when *TIMER1* reaches *OCR1A* count.
- *TCCR1B* (Timer 1 counter control register) - Sets operation mode to *Clear on Compare*, and sets prescaler to maximum in order to minimize flickering.
- *TIMSK1* (Timer 1 interrupt mask register) - Enables timer1 compare interrupts.

The information provided by the system modelling of each luminaire was stored in each arduino EEPROM. Then, during initialization, a function that reads data from arduino EEPROM is called, and values are stored as global variables in a data structure.

The network is built by the individual systems described previously. Now with 3 arduinos, each arduino's individual gains  $K_{ii}$  is the same, but there are relative gains  $K_{ij}$  that need to be determined, so that each desk's illuminance level is described by:

$$\begin{bmatrix} L_1 \\ L_2 \\ L_3 \end{bmatrix} = \begin{bmatrix} K_{11} & K_{12} & K_{13} \\ K_{21} & K_{22} & K_{23} \\ K_{31} & K_{32} & K_{33} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} + \begin{bmatrix} o_1 \\ o_2 \\ o_3 \end{bmatrix}. \quad (14)$$

- $u_i$  - duty cycle applied in desk  $i$ ,
- $L_i$  - illuminance level in desk  $i$ ,
- $o_i$  - outside disturbance level (lux) in desk  $i$ ,

To provide CAN-Bus communications, the mcp2515 was connected to each arduino via serial peripheral interface (SPI) communication. Thus, SPI communications had to be initialized, to allow mcp2515 to trigger an interrupt on the arduino each time a CAN message was received. Then, the used interrupt number was attached to an interrupt handler function, which reads messages from buffers that had the incoming message flag ON, and puts them into the adequate CAN frame stream. Masks were used to separate User Instruction into one CAN frame stream, and messages regarding luminaire crucial information into another CAN frame stream. This way, a clear separation between messages is done, and is easier to process each message received.

The consensus algorithm also needs an initialization to pass values read from arduino EEPROM, gains  $K_{ij}$  (provided by the calibration explained in the next section) and the external interference into variables stored inside consensus class.

## 2) Calibration

The calibration function has to calculate in each arduino gains corresponding to its own luminaire and to other arduino luminaires. To simplify the analysis, fluxogram (13) was made to illustrate how the function was implemented.

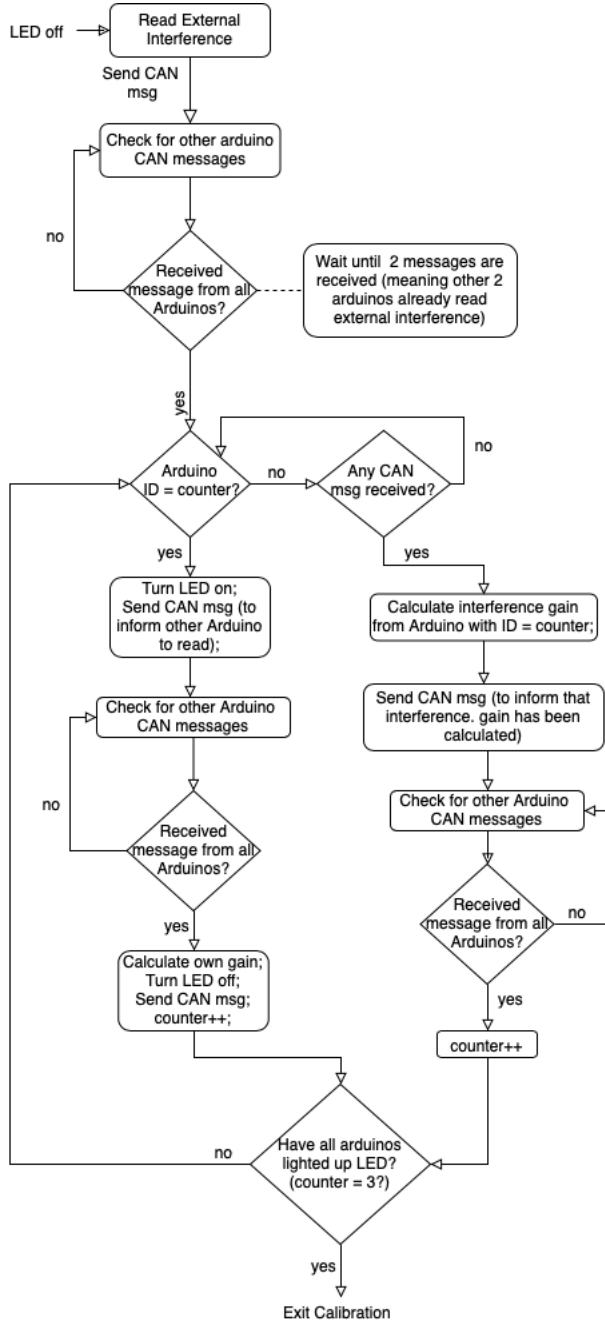


Fig. 13: Fluxogram Calibration

The previous control method must also be revised. As it stands, the global system is non cooperative, since each module tries to reach the reference illuminance, not taking into account the evolution of its surrounding modules. As previously said, one of the goals is to optimize the energy consumption, thus requiring communication between the components.

## E. CAN-Bus Communication System

Work in progress...

## F. UI Application

Work in progress...

## V. EXPERIMENTS

### A. Individual feedback + feedforward control system

In order to test our individual control system, an individual luminaire was placed inside the shoe box. The code implemented for this experiment asked the user (serial) to input an integer between 0 and 500, which was our range of values of illuminance in that setting. With no disturbances (closed box), a duty cycle of 0 should produce 0 lux of illuminance, and a duty cycle of 255 should produce around 500Lux of illuminance. The experiment was conducted, imposing an operation timer on the arduino in order keep the results consistent, as discussed earlier.

When a valid input was detected, the algorithm applied:

- Conversion from illuminance to duty cycle considering static state -  $L = K * DutyCycle$ ,
- Feedforward control, taking into account the transient state model with the delay, mentioned earlier, in order to simulate the step more accurately,
- Feedback control with anti-windup and deadzone, to:
  - Reduce overshoot,
  - Keep the Lux value "stable" at the reference (input) value,
  - Be able to correct for outside disturbances (when the shoe was opened)

We also tested the systems ability to change its reference value from 200Lux to a low reference value of 20Lux (no disturbances applied). This allows for a more thorough PID testing.

The results are shown in the next section.

### B. Cooperative decentralized control system

This experiment had many goals:

- Verify if the cooperative calibration was in accordance to the theoretical results,
- Test the effectiveness and speed of the communication system,
- Test the consensus algorithm implemented,
- Verify if the local controllers (PID's) were working as intended,
- Test the system's capability of handling user requests while running

Regarding setup and calibration,

## VI. RESULTS

### A. Individual System

After the aforementioned manual PID tuning, the system behaved in a very stable way, showing very little oscillations, but also fast corrections to disturbances with minimal overshoot. Regarding these criteria, the feedforward controller had minimal to no effect, since its purpose is

only related to the transient state (which is very fast). Every individual arduino behaved more or less the same way, with no differences worth pointing out.

Figure 14 shows a graph exported from the serial plotter showing the system's behaviour, given a reference, with no disturbances.

Fig. 14: System behaviour to a given reference value of  $200Lux$  with no disturbances

The anti-windup feature is quite valuable here, since it stops most of the overshoot in rising steps (as well as falling steps). We can also see that the deadzone implemented helps the system behave more "calmly", as the line is not too "spiky".

Figure 15 shows a graph of the same system's behaviour, given the same reference, but with some disturbances.

Fig. 15: System behaviour to a given reference value of  $200Lux$ , with disturbances

This helps us see how fast the local controller acts, correcting disturbances, but also if the system stays accurate after the correction.

Some individual systems showed some difficulty in changing their reference values from a medium/high value to a low value, as showed in figure 16. This was usually solved by repeating the individual calibration process for the luminaire.

Fig. 16: System behaviour while changing reference values from  $200Lux$  to  $20Lux$ , with no disturbances

## B. Cooperative System

## VII. CONCLUSIONS AND FUTURE

## VIII. BIBLIOGRAPHY

## IX. APPENDICES

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