

Chapter Two *Basic fiber theory*

2.1 The basic equations of fiber optics

2.2 Waveguide field equation and eigen solution of guided modes

2.3 Fiber loss and the measurement methods

2.4 Fiber dispersion and the measurement methods

Approaches

Two main **approaches** are commonly used to analyze the mode characteristics in the optical fiber.

- (1) Ray theory — **Geometrical Optics**
- (2) Wave theory — **Wave optics**

Ray theory

- Fiber **core** is much **larger** than optical **wavelength** λ_0
- The light wave can be regarded as some **beams**
- Therefore, the ray theory can be employed to investigate the light **incidence**, propagation **path**, time **delay**, etc.

Advantages:

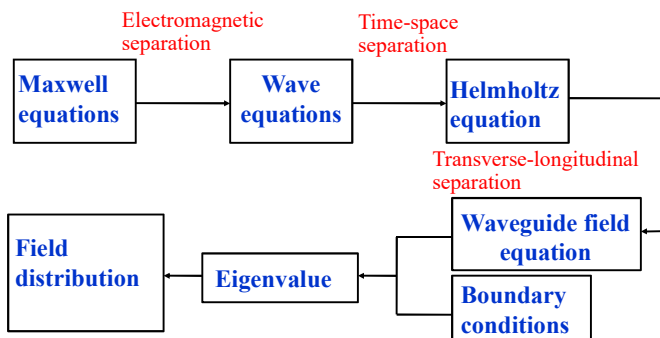
- Simple**
- Available for **large core (multimode)** fiber

Disadvantages:

- Unable** to explain some cases: mode **distribution**, **cladding modes**, mode **coupling**, etc.
- Significantly large **deviations** in the case of analyzing **single mode fiber** (fiber core comparable to λ_0).

The path of wave theory

Here we focus on investigating **wave theory** ?



The path of wave theory

a) Maxwell equations $\nabla \cdot \vec{D} = \rho$ Gauss' Law of electric fields
 In differential form: $\nabla \cdot \vec{B} = 0$ Gauss' Law of magnetic fields
 (static electric field and magnetic field)

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad \text{Faraday' Law of electromagnetic induction}$$

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \quad \text{The Law of total currents}$$

(The relationship between dynamic electric field and magnetic field)

where E , D , B , H are electric field intensity, electric induction intensity, magnetic induction intensity and magnetic field intensity, respectively. ρ is electric charge volume density. J is surface current density.

Fiber modes

Optical fiber: a kind of **waveguide**

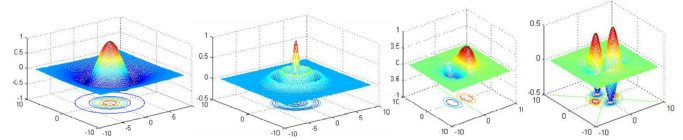
- There are some certain field **distributions** which remain **unchanged** during propagation.
- Such field distributions are called **modes** of the fiber.
- Each mode corresponds to one **solution** of **Maxwell equations**.

TE₀₁;TM₀₁ mode

TE₀₄;TM₀₄ mode

EH₁₁ mode

EH₂₁ mode



Wave theory

- Performed by a **rigorous** analysis
- To solve the **Maxwell equations**
- Originating from electromagnetic wave thus deriving the **field distribution** of electromagnetic wave.

Advantage: It is available for analyzing **both single-** and **multi-mode** optical fibers with different refractive index profiles because of **not** making any **approximations**

Disadvantage: the analysis is comparatively **complex**

Comparison of two above theories

	Ray theory	Wave theory
Condition	$\lambda_0 \ll d$	all
Subject	Beams	Modes
Basic equation	Ray equation	Waveguide equation
Method	Refraction/ reflection law	Boundary condition
Content	Ray trace	Modal distribution

The path of wave theory

Hamilton operator $\nabla = \vec{i} \frac{\partial}{\partial x} + \vec{j} \frac{\partial}{\partial y} + \vec{k} \frac{\partial}{\partial z}$

divergence $\nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$

curl $\nabla \times \vec{A} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix}$

$$\nabla \times (\nabla \times \vec{A}) = \nabla(\nabla \cdot \vec{A}) - (\nabla \cdot \nabla) \vec{A}$$

The path of wave theory

Optical fiber is one type of optical waveguides having the following characteristics:

- ① **no conduction current:** $J=0$
- ② **no free charge:** $\rho=0$
- ③ **linear isotropic** 线性各向同性

$$\nabla \cdot \vec{D} = 0 \quad \nabla \cdot \vec{B} = 0 \quad \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad \nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t}$$

b) material equations

$$\vec{D} = \epsilon \vec{E} = \epsilon_0 \epsilon_r \vec{E}$$

$$\vec{B} = \mu \vec{H} = \mu_0 \mu_r \vec{H}$$

ϵ_0 is the dielectric constant in vacuum ($8.8542 \times 10^{-12} \text{Fm}^{-1}$)

ϵ_r is the relative dielectric constant

μ_0 is the magnetic conductivity in vacuum ($4\pi \times 10^{-7} \text{Hm}^{-1}$)

μ_r is the relative magnetic conductivity

c) Boundary conditions

$$\begin{aligned}
 \vec{n} \cdot (\vec{D}_1 - \vec{D}_2) &= \rho \\
 \vec{n} \cdot (\vec{B}_1 - \vec{B}_2) &= 0 \\
 \vec{n} \times (\vec{E}_1 - \vec{E}_2) &= 0 \\
 \vec{n} \times (\vec{H}_1 - \vec{H}_2) &= \vec{J}
 \end{aligned}
 \quad \xrightarrow[\text{At the dielectric surface}]{J=0, \rho=0}
 \quad
 \begin{aligned}
 \vec{n} \cdot (\vec{D}_1 - \vec{D}_2) &= 0 \\
 \vec{n} \cdot (\vec{B}_1 - \vec{B}_2) &= 0 \\
 \vec{n} \times (\vec{E}_1 - \vec{E}_2) &= 0 \\
 \vec{n} \times (\vec{H}_1 - \vec{H}_2) &= 0
 \end{aligned}$$

- The **tangential** components of **H** and **E** are continuous
切向分量
- The **normal** components of **B** and **D** are continuous

$$\begin{aligned}
 \nabla \times (\nabla \times \vec{E}) &= \nabla(\nabla \cdot \vec{E}) - (\nabla \cdot \nabla) \vec{E} \\
 &= \nabla(\nabla \cdot \vec{E}) - \nabla^2 \vec{E} \dots\dots(b)
 \end{aligned}$$

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \quad \text{Laplace operator}$$

$$\nabla \cdot \vec{E} = \nabla \cdot \left(\frac{\vec{D}}{\epsilon} \right) = \frac{1}{\epsilon} \nabla \cdot \vec{D} + \vec{D} \cdot \nabla \left(\frac{1}{\epsilon} \right) = -\vec{E} \cdot \frac{\nabla \epsilon}{\epsilon}$$

Therefore

$$\nabla^2 \vec{E} + \nabla \left(\vec{E} \cdot \frac{\nabla \epsilon}{\epsilon} \right) = \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2}$$

2.1.2 Helmholtz equation

Wave equations \longrightarrow Helmholtz equation
Time-space separation

set $\Phi(x, y, z, t) = \Psi(x, y, z)e^{i\omega t}$

$$\begin{aligned}
 \nabla^2 \vec{E} &= \epsilon \mu \frac{\partial^2 \vec{E}}{\partial t^2} \\
 \nabla^2 \vec{H} &= \epsilon \mu \frac{\partial^2 \vec{H}}{\partial t^2}
 \end{aligned}
 \quad \text{scalar wave equations}$$

$$\nabla^2 \Psi(x, y, z) + k^2 \Psi(x, y, z) = 0$$

This is the **Helmholtz equation**

k is the wave number $k = 2\pi / \lambda = \omega \sqrt{\epsilon \mu_0} = n \omega \sqrt{\epsilon_0 \mu_0} = nk_0$,
 $k_0 = \omega \sqrt{\epsilon_0 \mu_0} = 2\pi / \lambda_0$ is the wave number in vacuum

2.1.3 Waveguide field equation

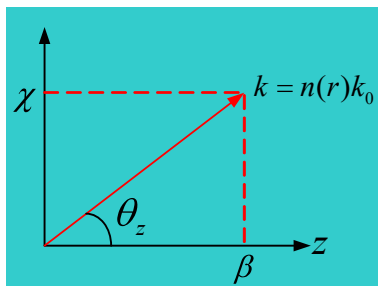
$$\nabla_t^2 \psi(x, y) + \chi^2 \psi(x, y) = 0$$

χ propagation constant at **transverse direction**

β propagation constant at **longitudinal direction**

$$\chi^2 = k^2 - \beta^2 = n^2 k_0^2 - \beta^2$$

$$\beta = nk_0 \cos \theta_z$$



Electromagnetic separation

Maxwell equations \longrightarrow wave equations

$$\nabla \cdot \vec{D} = 0$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t} \longrightarrow \nabla \times (\nabla \times \vec{E}) = -\mu \frac{\partial (\nabla \times \vec{H})}{\partial t}$$

$$\nabla \times \vec{H} = \epsilon \frac{\partial \vec{E}}{\partial t} \longrightarrow \nabla \times (\nabla \times \vec{E}) = -\mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} \dots\dots(a)$$

Similarly, we can derive the wave equation relating to **H** and obtain

$$\nabla^2 \vec{E} + \nabla \left(\vec{E} \cdot \frac{\nabla \epsilon}{\epsilon} \right) = \epsilon \mu \frac{\partial^2 \vec{E}}{\partial t^2}$$

Vector wave equations:

$$\nabla^2 \vec{H} + \frac{\nabla \epsilon}{\epsilon} \times (\nabla \times \vec{H}) = \epsilon \mu \frac{\partial^2 \vec{H}}{\partial t^2}$$

- The **precise** equations of electromagnetic wave.
- In fiber, the refractive index variation is significantly moderate, thus $\nabla \epsilon \approx 0$. The above vector wave equations can be simplified to **scalar wave equations**

$$\nabla^2 \vec{E} = \epsilon \mu \frac{\partial^2 \vec{E}}{\partial t^2}, \quad \nabla^2 \vec{H} = \epsilon \mu \frac{\partial^2 \vec{H}}{\partial t^2}$$

The formulas are valid for each component of $\vec{E}(\underline{x}, y, z, t)$ and $\vec{H}(\underline{x}, y, z, t)$

Notice: These equations are the **approximated** results only valid for solving the **general problems** in fiber.

If more **precise analysis** is required, the **vector equations** are needed.

2.1.3 Waveguide field equation

Helmholtz equation \longrightarrow Waveguide field equation
Transverse-longitudinal separation

Light transmission characteristics in optical fibers:

In the **transverse direction**: **standing wave**

In the **longitudinal direction**: **travelling wave**

Only **phase** without amplitude **variations** exists for the field distribution along longitudinal direction

Transverse-longitudinal separation

set $\Psi(x, y, z) = \psi(x, y)e^{-i\beta z}$

Substituting the formula into the Helmholtz equation

$$\nabla^2 \Psi(x, y, z) + k^2 \Psi(x, y, z) = 0$$

$$\nabla_t^2 \psi(x, y) + \chi^2 \psi(x, y) = 0$$

$$\nabla_t^2 = \nabla^2 - \frac{\partial^2}{\partial z^2} \quad \text{Laplacian operator at transverse direction}$$

2.1.3 Waveguide field equation

The **transverse distribution** of electric field **E** and magnetic field **H** should meet **waveguide field equation**

$$\nabla_t^2 \begin{bmatrix} \vec{E}(x, y) \\ \vec{H}(x, y) \end{bmatrix} + \chi^2 \begin{bmatrix} \vec{E}(x, y) \\ \vec{H}(x, y) \end{bmatrix} = 0$$

It is the **basic equation** of **wave theory** and also a typical **eigen equation**, the **eigenvalue** is χ or β .

If the **boundary condition** is given, the **eigen solution** and its corresponding **eigenvalue** can be obtained. In general, the eigen solution is defined as the **mode**.

2.1.4 Mode and its basic properties

Field distribution (i.e., **eigen solution**)

- The mode field distribution is uniquely determined by six field components:

rectangular coordinate system: $E_x, E_y, E_z, H_x, H_y, H_z$

cylindrical coordinate system: $E_r, E_\phi, E_z, H_r, H_\phi, H_z$

Time-space separation:

$$\text{Maxwell equations: } \begin{cases} \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \\ \nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} \end{cases} \Rightarrow \begin{cases} \nabla \times \vec{E} = i\omega\mu_0 \vec{H} \\ \nabla \times \vec{H} = i\omega\epsilon \vec{E} \end{cases}$$

According to :

$$\nabla \times \vec{A} = \begin{vmatrix} \vec{e}_x & \vec{e}_y & \vec{e}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix} \quad \nabla \times \vec{A} = \frac{1}{r} \begin{vmatrix} \vec{e}_r & r\vec{e}_\phi & \vec{e}_z \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ A_r & rA_\phi & A_z \end{vmatrix}$$

2.1.4 Mode and its basic properties

In **rectangular coordinate** system, the relationship between **transverse** and **longitudinal** coordinates

$$\begin{aligned} \chi^2 E_x &= -i \left(\omega\mu \frac{\partial H_z}{\partial y} + \beta \frac{\partial E_z}{\partial x} \right) \\ \chi^2 E_y &= -i \left(-\omega\mu \frac{\partial H_z}{\partial x} + \beta \frac{\partial E_z}{\partial y} \right) \\ \chi^2 H_x &= -i \left(-\omega\epsilon \frac{\partial E_z}{\partial y} + \beta \frac{\partial H_z}{\partial x} \right) \\ \chi^2 H_y &= -i \left(\omega\epsilon \frac{\partial E_z}{\partial x} + \beta \frac{\partial H_z}{\partial y} \right) \end{aligned} \Rightarrow \begin{aligned} E_x &= f_1(E_z, H_z) \\ E_y &= f_2(E_z, H_z) \\ H_x &= f_3(E_z, H_z) \\ H_y &= f_4(E_z, H_z) \end{aligned} \Rightarrow \psi_{x,y} = f \begin{bmatrix} E_z \\ H_z \end{bmatrix}$$

2.1.4 Mode and its basic properties

In **cylindrical coordinate** system, the relationship between **transverse** and **longitudinal** coordinates

$$\begin{aligned} \chi^2 H_\phi &= -i \left(\omega\epsilon \frac{\partial E_z}{\partial x} + \beta \frac{1}{r} \frac{\partial H_z}{\partial \phi} \right) \\ \chi^2 E_r &= -i \left(\omega\mu \frac{1}{r} \frac{\partial H_z}{\partial \phi} + \beta \frac{\partial E_z}{\partial r} \right) \\ \chi^2 E_\phi &= -i \left(-\omega\mu \frac{\partial H_z}{\partial r} + \beta \frac{1}{r} \frac{\partial E_z}{\partial \phi} \right) \\ \chi^2 H_r &= -i \left(-\omega\epsilon \frac{1}{r} \frac{\partial E_z}{\partial \phi} + \beta \frac{\partial H_z}{\partial r} \right) \end{aligned} \Rightarrow \begin{aligned} E_r &= f_1(E_z, H_z) \\ E_\phi &= f_2(E_z, H_z) \\ H_r &= f_3(E_z, H_z) \\ H_\phi &= f_4(E_z, H_z) \end{aligned} \Rightarrow \psi_{r,\phi} = f \begin{bmatrix} E_z \\ H_z \end{bmatrix}$$

(1) The name of modes

- According to that whether **longitudinal component** E_z and H_z exist or not, the modes can be named as:

(1) **TEM**: $E_z = H_z = 0$;

(2) **TE**: $E_z = 0, H_z \neq 0$;

(3) **TM**: $E_z \neq 0, H_z = 0$;

(4) **HE or EH**: $E_z \neq 0, H_z \neq 0$.

- Most modes in fiber are HE (EH) modes, sometimes there are some TE (TM) modes

2.1.4 Mode and its basic properties

In **rectangular coordinate** system, each component can be expressed as the following

$$\begin{aligned} x \text{ component} & \quad \frac{\partial H_z}{\partial y} - \frac{\partial H_y}{\partial z} = i\omega\epsilon E_x, \quad \frac{\partial E_z}{\partial y} - \frac{\partial E_y}{\partial z} = -i\omega\mu H_x \\ y \text{ component} & \quad \frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = i\omega\epsilon E_y, \quad \frac{\partial E_z}{\partial z} - \frac{\partial E_z}{\partial x} = -i\omega\mu H_y \\ z \text{ component} & \quad \frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} = i\omega\epsilon E_z, \quad \frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} = -i\omega\mu H_z \end{aligned}$$

After space separation

$$\Psi(x, y, z) = \psi(x, y)e^{-i\beta z} \Rightarrow \frac{\partial \Psi}{\partial z} = -i\beta \Psi(x, y, z)$$

Take E_x component as an example

$$\begin{aligned} i\omega\epsilon E_x &= \frac{\partial H_z}{\partial y} + i\beta H_y = \frac{\partial H_z}{\partial y} + i\beta \frac{1}{-i\omega\mu} (-i\beta E_x - \frac{\partial E_z}{\partial x}) \\ \Rightarrow \chi^2 E_x &= -i \left(\omega\mu \frac{\partial H_z}{\partial y} + \beta \frac{\partial E_z}{\partial x} \right) \end{aligned}$$

2.1.4 Mode and its basic properties

In **cylindrical coordinate** system

$$\begin{cases} \frac{1}{r} \frac{\partial E_z}{\partial \phi} - \frac{\partial E_\phi}{\partial z} = -i\omega\mu_0 H_r \\ \frac{\partial E_z}{\partial z} - \frac{\partial E_z}{\partial r} = -i\omega\mu_0 H_\phi \\ \frac{\partial E_\phi}{\partial r} + \frac{1}{r} E_\phi - \frac{1}{r} \frac{\partial E_z}{\partial \phi} = -i\omega\mu_0 H_z \end{cases} \quad \begin{cases} \frac{1}{r} \frac{\partial H_z}{\partial \phi} - \frac{\partial H_\phi}{\partial z} = i\omega\epsilon E_r \\ \frac{\partial H_r}{\partial z} - \frac{\partial H_z}{\partial r} = i\omega\epsilon E_\phi \\ \frac{\partial H_\phi}{\partial r} + \frac{1}{r} H_\phi - \frac{1}{r} \frac{\partial H_z}{\partial \phi} = i\omega\epsilon E_z \end{cases}$$

2.1.4 Mode and its basic properties

- The **transverse components** can be obtained from the **longitudinal components**, thus the 6 field components can be simplified to 2 longitudinal components
- E_z and H_z satisfy **waveguide field equation** independently

$$\nabla_t^2 \begin{bmatrix} E_z \\ H_z \end{bmatrix} + \chi^2 \begin{bmatrix} E_z \\ H_z \end{bmatrix} = 0$$

The relationship between **transverse** and **longitudinal** components

If the **transverse components** are known, the **longitudinal components** can be solved In **rectangular** coordinate system In **cylindrical** coordinate system

$$\begin{aligned} H_z &= -j \frac{1}{\beta} \left(\frac{\partial H_x}{\partial x} + \frac{\partial H_y}{\partial y} \right) = \frac{i}{\omega\mu} \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right) \\ E_z &= -j \frac{1}{\omega\epsilon} \left(\frac{\partial H_y}{\partial x} - \frac{\partial H_x}{\partial y} \right) \\ E_x &= -i \frac{1}{\omega\epsilon} \left[\frac{1}{r} \cdot \frac{\partial}{\partial r} (r H_\phi) - \frac{1}{r} \cdot \frac{\partial H_r}{\partial \phi} \right] \\ H_x &= -i \frac{1}{\beta} \left[\frac{1}{r} \cdot \frac{\partial}{\partial r} (r H_r) + \frac{1}{r} \cdot \frac{\partial H_\phi}{\partial \phi} \right] = \frac{1}{\omega\mu} \left[\frac{1}{r} \cdot \frac{\partial}{\partial r} (r E_\phi) - \frac{1}{r} \cdot \frac{\partial E_r}{\partial \phi} \right] \end{aligned}$$

(2) Longitudinal propagation constant (β)

Phase variation rate per **unit length** along z direction

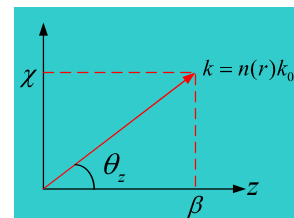
The **component** of wave vector k along z direction

$$\beta = \vec{k} \cdot \vec{e}_z = nk_0 \cos \theta_z$$

- The values of b are **separated** and **correspond** to a group of guided **modes**

- If different guided **modes** correspond to a **same** b , they are **degenerate**

$$n_2 k_0 < \beta < n_1 k_0$$



(3) Normalized frequency (V)

In a given fiber, the **allowed guided modes** are determined by the **structure parameter** which is characterized by **normalized frequency V** . Larger V leads to **more** guided modes.

$$V = \frac{2\pi}{\lambda_0} a \sqrt{n_1^2 - n_2^2} = k_0 a \cdot NA = k_0 a n_1 \sqrt{2\Delta}$$

$$NA = \sqrt{n_1^2 - n_2^2} = n_1 \sqrt{\frac{(n_1 + n_2)(n_1 - n_2)}{n_1^2}} \approx n_1 \sqrt{\frac{2(n_1 - n_2)}{n_1}} = n_1 \sqrt{2\Delta}$$

Numerical aperture

$$\Delta = \frac{n_1 - n_2}{n_1}$$

Relative refractive index difference

(3) Normalized frequency (V)

Guided mode cutoff: For a certain V , the modes except fundamental mode maybe not allowed and the **guided mode** will be **converted** to **radiation mode**. This V (labeled V_c) is called the **cutoff frequency** for a specific guided mode.

Different guided modes have different V_c

$$V < V_c \text{ or } \lambda > \lambda_c \implies \text{Guided mode cutoff}$$

Guided mode far from cutoff: If the guided mode **eigen value β** approaches $n_1 k_0$, the guided mode field will be **restricted tightly** within the **core**. This is called as guided mode far from cutoff condition.

(4) Transverse propagation constant (U, W)

Transverse propagation constant :

$$\chi_d = \sqrt{n_1^2 k_0^2 - \beta^2} \quad (\text{core})$$

$$\chi_c = \sqrt{n_2^2 k_0^2 - \beta^2} \quad (\text{cladding})$$

Transverse constant:

$$U = a \chi_d = \sqrt{n_1^2 k_0^2 - \beta^2} \cdot a$$

$$W = -i a \chi_c = \sqrt{\beta^2 - n_2^2 k_0^2} \cdot a$$

Satisfy: $V^2 = U^2 + W^2$

Normalized propagation constant:

$$b = \frac{W^2}{V^2} = \frac{\beta^2 - n_2^2 k_0^2}{n_1^2 k_0^2 - n_2^2 k_0^2}$$