# ME 599/699 Robot Modeling & Control Fall 2021

#### **Drive Trains**

Hasan A. Poonawala

Department of Mechanical Engineering University of Kentucky

Email: hasan.poonawala@uky.edu Web: https://www.engr.uky.edu/~hap

# **Permanent Magnet DC motors**

We consider permanent magnet DC motors. Other kinds include *AC* motors and brushless *DC* motors.

A model for the motor torque is  $\tau = K_m i_a$ , if the flux in the motor is constant. The current is generated by a voltage source, and has dynamics

$$L\frac{d}{dt}i_a + Ri_a = V - V_b, \tag{1}$$

where L is the motor inductance, R is the winding resistance,  $V_b$  is the back EMF and is proportional to  $\omega_m$ , the motor speed.

### **PMDC** Model

The dynamics governing  $\theta_m$  are

$$J_m \ddot{\theta}_m + B_m \dot{\theta}_m = \tau_m - \tau_I / r \tag{2}$$

$$= K_m i_a - \tau_I / r \tag{3}$$

We can rewrite (1) and (5) as

$$(Ls+R)I_a(s)=V(s)-K_b\ s\Theta_m(s), \tag{4}$$

$$(J_m s^2 + B_m s)\Theta_m(s) = K_m I_a(s) - \tau_I(s)/r$$
 (5)

We combine these equations to obtain

$$s\left((Ls+R)(J_ms+B_m)+K_bK_m\right)\Theta_m(s)=K_mV(s)-\frac{(Ls+R)}{r}\tau_I(s). \tag{6}$$

# **Fast Electrical Dynamics**

The electrical time constant L/R is much smaller than the mechanical time constant  $J_m/B_m$ . So, we can divide by R and set L/R to zero, obtaining.

$$s\left(\left(J_ms+B_m\right)+rac{K_bK_m}{R}\right)\Theta_m(s)=rac{K_m}{R}V(s)-rac{1}{r}\tau_I(s).$$

Setting  $u \leftarrow K_m V/R$ , and  $B \leftarrow B_m + K_b K_m/R$ , we obtain the motor equation as

$$J\ddot{\theta}_m + B\dot{\theta}_m = u(t) - \frac{1}{r}\tau_I. \tag{7}$$

## **Combined Link-Actuator Model**

Let's combine the motor *m* with the link *l* 

$$J_m \ddot{\theta}_m + B \dot{\theta}_m = u(t) - \frac{1}{r} \tau_l \tag{8}$$

$$J_l \ddot{\theta}_l + B_l \dot{\theta}_l = \tau_l \tag{9}$$

Due to the gears,  $\dot{\theta}_m = r\dot{\theta}_I$ . We eliminate  $\theta_I$  to obtain

$$(J_m r^2 + J_l) \ddot{\theta}_l + (Br^2 + B_l) \dot{\theta}_l = ru$$
 (10)

Main takeaway: When gear ratio r is large, then link inertia becomes negligible compared to the motor's inertia.

## Full Euler-Lagrangian Model

$$D(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) = \tau + \tau_{friction} + \tau_e,$$

becomes

$$\underbrace{\mathcal{M}(q)}_{+ ext{motor inertia}} \ddot{q} + C(q, \dot{q})\dot{q} + \underbrace{\mathcal{B}\dot{q}}_{+ ext{motor friction}} + G(q) = u + \tau_e,$$

where u denotes the input due to the voltage, whereas  $\tau$  was the torque acting on the link joint.

# **Full Euler-Lagrangian Model**

$$D(q)\ddot{q} + C(q,\dot{q})\dot{q} + G(q) = \tau + \tau_{friction} + \tau_e,$$

becomes

$$\underbrace{\mathcal{M}(q)}_{+ ext{motor inertia}} \ddot{q} + C(q, \dot{q})\dot{q} + \underbrace{\mathcal{B}\dot{q}}_{+ ext{motor friction}} + G(q) = u + \tau_e,$$

where u denotes the input due to the voltage, whereas  $\tau$  was the torque acting on the link joint. In particular,

$$u_k = r_k \frac{K_{m_k}}{R_k} V_k,$$

where  $\theta_{m_k} = r_k q_k$ , and M(q) = D(q) + J, and J is diagonal with  $r_k^2 J_{m_k}$  as  $k^{\text{th}}$  diagonal element.

► The gear ratio is high ( $\approx$ 20 - 200), J dominates D(q) and other terms

- The gear ratio is high ( $\approx$ 20 200), J dominates D(q) and other terms
  - $ightharpoonup M(q) \approx$  diagonal, dynamics of links nearly independent

- The gear ratio is high ( $\approx$ 20 200), J dominates D(q) and other terms
  - $ightharpoonup M(q) \approx$  diagonal, dynamics of links nearly independent
- ► High gear ratios are good for position control

- ► The gear ratio is high ( $\approx$ 20 200), J dominates D(q) and other terms
  - $ightharpoonup M(q) \approx \text{diagonal, dynamics of links nearly independent}$
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction

- ► The gear ratio is high ( $\approx$ 20 200), J dominates D(q) and other terms
  - $ightharpoonup M(q) \approx \text{diagonal, dynamics of links nearly independent}$
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction
  - ▶ the relationship  $\tau = K I = KV/R$  breaks down (cannot set torque without feedback)

- ► The gear ratio is high ( $\approx$ 20 200), J dominates D(q) and other terms
  - $ightharpoonup M(q) \approx \text{diagonal, dynamics of links nearly independent}$
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction
  - ▶ the relationship  $\tau = K I = KV/R$  breaks down (cannot set torque without feedback)
- In dynamic robots, preference for Direct-Drive and Quasi-Direct-Drive motors  $(r \approx 1)$

- ► The gear ratio is high ( $\approx$ 20 200), J dominates D(q) and other terms
  - $ightharpoonup M(q) \approx \text{diagonal, dynamics of links nearly independent}$
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction
  - ▶ the relationship  $\tau = K I = KV/R$  breaks down (cannot set torque without feedback)
- In dynamic robots, preference for Direct-Drive and Quasi-Direct-Drive motors  $(r \approx 1)$ 
  - ▶ Brushless, QDD Motors, instrumental in 4-legged bots

- ► The gear ratio is high ( $\approx$ 20 200), J dominates D(q) and other terms
  - $ightharpoonup M(q) \approx \text{diagonal, dynamics of links nearly independent}$
- ▶ High gear ratios are good for position control
- ▶ They amplify nonlinear motor friction, introduce friction
  - ▶ the relationship  $\tau = K I = KV/R$  breaks down (cannot set torque without feedback)
- In dynamic robots, preference for Direct-Drive and Quasi-Direct-Drive motors  $(r \approx 1)$ 
  - ▶ Brushless, QDD Motors, instrumental in 4-legged bots
- ▶ Boston Dynamics' Atlas robot uses hydraulic actuation