ME 599/699 Robot Modeling & Control Fall 2021

Robust and Adaptive Inverse Dynamics

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What happens when $\hat{M}(q) \neq M(q)$, $\hat{C}(q, \dot{q}) \neq \hat{C}(q, \dot{q})$, $\hat{G}(q) \neq G(q)$?

Our closed-loop under inverse dynamics control is

$$M(q)\ddot{q} + C(q,\dot{q})\dot{q} + G(q) = \hat{M}(q)a_q(t) + \hat{C}(q,\dot{q})\dot{q} + \hat{G}(q)$$

Rewrite above as

$$M(q)\ddot{q} = \hat{M}(q)a_{q}(t) + \hat{C}(q,\dot{q})\dot{q} - C(q,\dot{q})\dot{q} + \hat{G}(q) - G(q)$$

$$M(q)\ddot{q} = M(q)a_{q}(t) + \left(\hat{M}(q) - M(q)\right)a_{q}(t) + \left(\hat{C}(q,\dot{q}) - C(q,\dot{q})\right)\dot{q} + \left(\hat{G}(q) - G(q)\right)$$

$$= M(q)a_{q}(t) + \tilde{M}a_{q}(t) + \tilde{C}\dot{q} + \tilde{G}$$

 $\Rightarrow \ddot{q} = a_q(t) + M^{-1}(q) \left(\tilde{M} a_q(t) + \tilde{C} \dot{q} + \tilde{G} \right)$

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$$\ddot{q} = a_q(t) + M^{-1}(q) \left(\tilde{M} a_q(t) + \tilde{C} \dot{q} + \tilde{G} \right)$$
 (1)
= $a_q + \eta(q, \dot{q}, \ddot{q}, a_q)$ (2)

If we had perfect knowledge of the model parameters, $\eta(q, \dot{q}, \ddot{q}, a_q) = 0$, because $\tilde{M} = \hat{M}(q) - M(q) = 0$ and so on.

To account for non-zero $\eta(q, \dot{q}, \ddot{q}, a_q)$, we choose a_q as

$$a_q(t) = \ddot{q}_d(t) + K_P\left(q_d(t) - q(t)\right) + K_D\left(\dot{q}_d(t) - \dot{q}(t)\right) + \delta a$$

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Let
$$e(t) = \begin{bmatrix} q(t) - q_d(t) \\ \dot{q}(t) - \dot{q}_d(t) \end{bmatrix}$$
. Our closed-loop is now

$$\dot{e} = \begin{bmatrix} 0 & I \\ -K_P & -K_D \end{bmatrix} e + \begin{bmatrix} 0 \\ I \end{bmatrix} (\delta a + \eta) \tag{3}$$

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We can now easily see why the new term δa is what we use to account for non-zero $\eta(q, \dot{q}, \ddot{q}, a_q)$.

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How do we choose δa ? Lyapunov methods

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Suppose we can bound η as

$$\|\eta\| \leq \rho(e,t),$$

we can then design δa to guarantee ultimate $e(t) \rightarrow 0$.

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Let
$$A = \begin{bmatrix} 0 & I \\ -K_P & -K_D \end{bmatrix}$$
, and $B = \begin{bmatrix} 0 \\ I \end{bmatrix}$. $\dot{e} = Ae + B(\delta a + \eta)$.

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Let $V = e^T P e$ where $A^T P + P A = -Q$. Since A can be made Hurwitz by choosing K_P and K_D , we know that for each Q > 0 there exists P > 0 that satisfies the Lyapunov equation $A^T P + P A = -Q$.

We have that

$$\dot{V} = e^{T} P A e + e^{T} A^{T} P e + 2 e^{T} P B (\delta a + \eta)$$

$$= -e^{T} Q e + 2 e^{T} P B (\delta a + \eta)$$
(4)

We choose

$$\delta a = \begin{cases} -\rho(e, t) \frac{B^T P e}{\|B^T P e\|} & , & \text{if } \|B^T P e\| \neq 0 \\ 0 & , & \text{if } \|B^T P e\| = 0 \end{cases}$$
 (5)

Let $w = B^T Pe$. Then the second term in (4) is then

$$w^{T} \left(-\rho \frac{w}{\|w\|} + \eta \right) \leq -\rho \|w\| + \|w\| \|\eta\| \quad (w^{T} \eta \leq \|w\| \|\eta\|)$$

$$\leq \|w\| (-\rho + \|\eta\|)$$

$$\leq 0, \qquad (\|\eta\| \leq \rho(e, t))$$

when $e \neq 0$.

So,

$$\dot{V} = -e^T Q e + 2 w^T (\delta a + \eta)$$
 $\leq -e^T Q e + 0$ (from previous slide)
 < 0 ($Q > 0$)

In summary, if we can bound η (see notes Section 5.5),

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Issues:

- ▶ If the bound ρ is large (due to large errors η), then the demanded control u becomes larger than motor capacity
- ▶ The control is discontinuous at w = 0, which is tricky to implement; overheats electric motors.

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- ▶ Ideally, we want smaller model errors to achieve lower error.
- Luckily, we can learn models on-the-fly using adaptive control theory.

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We don't know true parameters Θ .

We have a guess $\hat{\Theta}$ (which we may convert into $\hat{M}(q)$, $\hat{C}(q, \dot{q})$, $\hat{G}(q)$).

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KEY ADAPTIVE CONTROL BEHAVIOR:

This update rule WILL NOT ensure that $\hat{\Theta}(t) \to \Theta$, but it ensures that

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This update rule relies on the linearity in parameters property.

Let $\tilde{q}=q-q_d$, $\tilde{\dot{q}}=\dot{q}-\dot{q}_d$ Choosing $u=Y(q,\dot{q},a_q)\hat{\Theta}$, where $a_q=\ddot{q}_d(t)-K_P\tilde{q}-K_D\tilde{\dot{q}}$ we get

$$\ddot{\ddot{q}} + K_1 \dot{\ddot{q}} + K_0 \dot{\ddot{q}} = M^{-1} Y(q, \dot{q}, \ddot{q}) \tilde{\Theta} = \Phi \tilde{\Theta}, \tag{6}$$

where $\tilde{\Theta} = \hat{\Theta} - \Theta$.

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where $\tilde{\Theta} = \hat{\Theta} - \Theta$.

Let
$$e = \begin{bmatrix} \tilde{q} \\ \tilde{a} \end{bmatrix}$$
. We get the ODE

$$\dot{e} = Ae + B\Phi\tilde{\theta} \tag{7}$$

which is effectively the same ODE as in the robust case, but without δa .

Consider a function of $e, \tilde{\Theta}$ given by

$$V(e, \tilde{\Theta}) = e^{T} P e + \tilde{\Theta}^{T} \Gamma \tilde{\Theta}.$$
 (8)

For P>0 and $\Gamma>0$, $V(e,\tilde{\Theta})=0$ when e=0 and $\Theta=\hat{\Theta}$.

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We have

$$\dot{V}(e,\tilde{\Theta}) = -e^{T}Qe + 2\tilde{\Theta}^{T}\left(\Phi^{T}B^{T}Pe + \Gamma\dot{\hat{\Theta}}\right)$$
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If we knew Θ the second term is made zero by choosing $\hat{\Theta} = \Theta$. Since we don't, we instead choose

$$\dot{\hat{\Theta}} = -\Gamma^{-1} \Phi^T B^T P e \tag{10}$$

$$(\implies \dot{V} \le 0, \text{ and } \dot{V} < 0 \text{ when } e \ne 0) \tag{11}$$

It's like a nonlinear integral control!

Summary:

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 - ▶ PoE: says when $\hat{\Theta}(t) \to \Theta$ as opposed to $\|\hat{\Theta}(t)\| \to \infty$
 - ▶ PoE rule is important. Bad updates caused the NASA X-15 to crash in 1967.
 - (Mathematical analysis is sometimes not optional).