

Chapter 3 – Robot Trajectory Planning

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- Trajectory: Time history of position, velocity, and acceleration for each dof
- User simply specifies desired goal position and orientation of the end-effector; system decides the trajectory
- Desired to have smooth path: one that is continuous and has a continuous first derivation, or even a continuous second derivative.

Note: Rough or jerky motions increase wear on mechanism

Joint space schemes

Path shapes described in terms of "functions of joint angles"

Identify path points[1]



Desired position and orientation of tool frame {T} relative to the station frame {S}

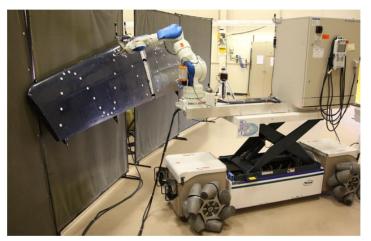
Using inverse kinematics



A set of desired joint angles



A smooth function is used for each joint



Source:http://www.swri.org/3pubs/ird2010/synopses/108019.htm

All joints reach the via points at the same time

Path points includes all the via points plus the initial and final points; via point is a point located midway between the starting and stopping positions of a robot tool tip, through which the tool tip passes without stopping.



Joint space schemes

Remark:

- Joint space schemes
 - achieve desired position and orientation only at via points.
 - Discrete correspondence between joint space and Cartesian space => No problem with singularities



- Say we wish to move the tool from its initial position to a goal position in a certain amount of time:
 - Inverse kinematics to calculate the set of joint angles corresponding to the initial and goal positions and orientations.
 - Adopt a smooth function to interpolate each joint value from initial value to goal value.

4 constraints for each of the joints' motion:

Initial & Final Positions

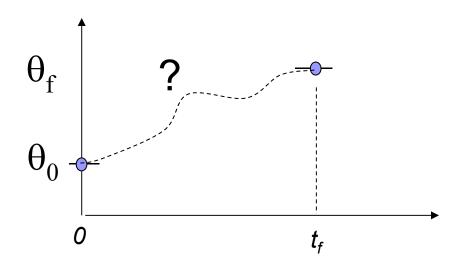
$$\theta(0) = \theta_0$$

$$\theta(0) = \theta_0 \qquad \theta(t_f) = \theta_f$$

Initial & Final Velocities

$$\dot{\theta}(0) = 0 \qquad \dot{\theta}(t_f) = 0$$

$$\dot{\theta}(t_f) = 0$$





The constraints can be satisfied by a third degree polynomial:

$$\theta(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$
 (2-1)

Joint velocity and acceleration along this path:

$$\dot{\theta}(t) = a_1 + 2a_2t + 3a_3t^2 \tag{2-2}$$

$$\ddot{\theta}(t) = 2a_2 + 6a_3t \tag{2-3}$$



Four equations (constraints) in four unknowns

$$(a_0, ..., a_3) =>$$

$$a_0 = \theta_0$$

$$a_1 = 0$$

$$a_2 = \frac{3}{t_f^2} (\theta_f - \theta_0)$$

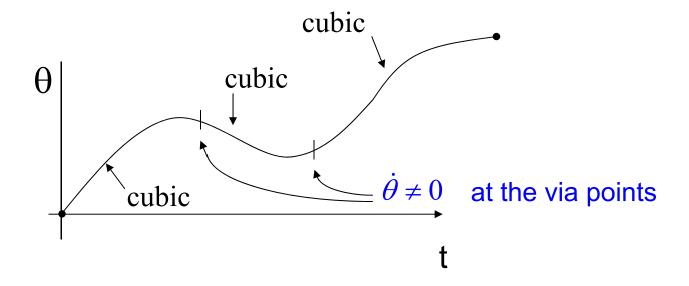
$$a_3 = \frac{-2}{t_f^3} (\theta_f - \theta_0)$$

Remark:

This solution is for the case when the joint starts and finishes at zero velocity



- In general, path specification may include intermediate via points.
- Desired velocities of the joints at the via points may not be zero.

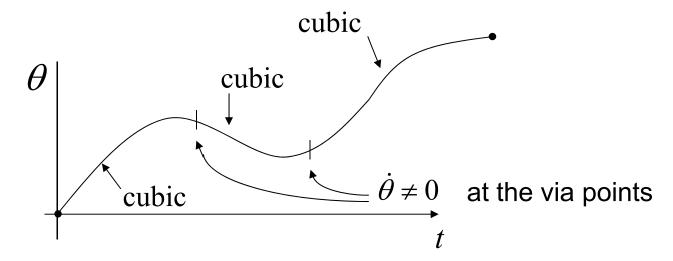




Using a cubic polynomial for each segment Velocity constraints at each end: $\dot{\theta}(0) = \dot{\theta}_0$

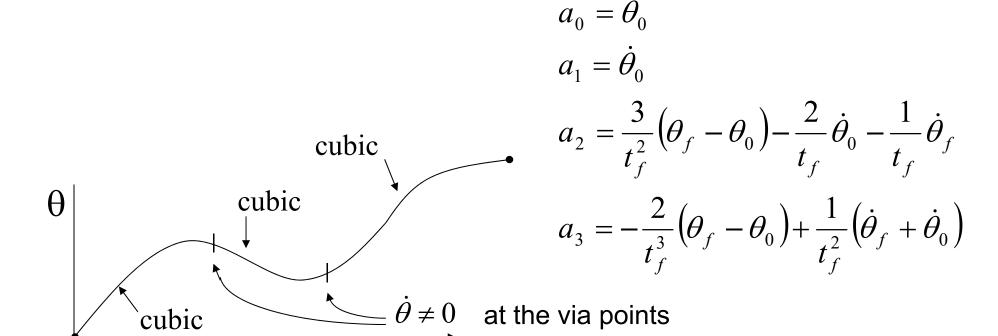
$$\dot{\theta}(t_f) = \dot{\theta}_f$$

(here, velocity constraints need not be zero)



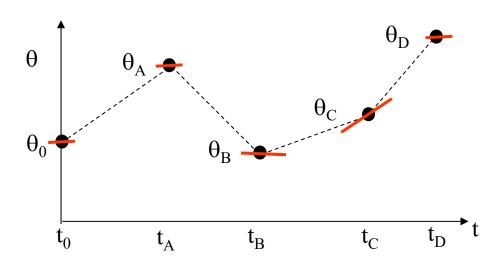


Applying the position and velocity constraints at each end to Eqs (2-1) and (2-2), we obtain:





- How to specify the joint velocities at via points?
 - □ User specifies desired velocity at each via point in terms of a Cartesian linear and angular velocity of the tool frame at that instant. Then, apply inverse Jacobian (singularity issue).
 - System automatically chooses the velocities at the via points by suitable heuristic:





Higher order polynomials

To specify the position, velocity, and acceleration at the beginning and end of a path segment, a quintic polynomial is required:

$$\theta(t) = a_0 + a_1t + a_2t^2 + a_3t^3 + a_4t^4 + a_5t^5$$

Remark:

- Cubic trajectory has discontinuities in acceleration => Leads to impulsive jerk (derivative of acceleration) => May excite vibrational modes => Reduce tracking accuracy
- With fifth order polynomial, can specify constraints (say zero) for acceleration at the start and end

NA.

Higher order polynomials

6 Equations in 6 unknowns:

$$a_{0} = \theta_{0}$$

$$a_{1} = \dot{\theta}_{0}$$

$$a_{2} = \frac{\ddot{\theta}_{0}}{2}$$

$$a_{3} = \frac{20 \theta_{f} - 20 \theta_{0} - (8 \dot{\theta}_{f} + 12 \dot{\theta}_{0}) t_{f} - (3 \ddot{\theta}_{0} - \ddot{\theta}_{f}) t_{f}^{2}}{2 t_{f}^{3}}$$

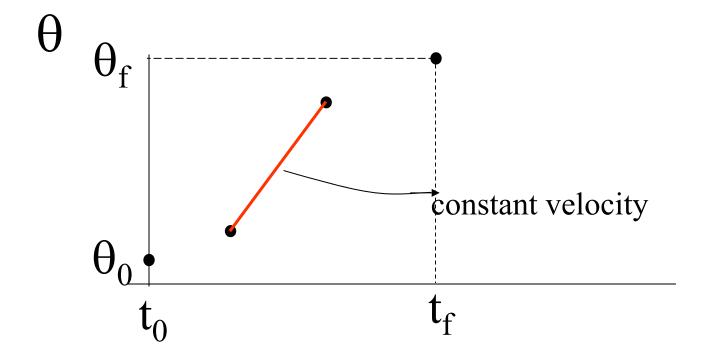
$$a_{4} = \frac{30 \theta_{0} - 30 \theta_{f} + (14 \dot{\theta}_{f} + 16 \dot{\theta}_{0}) t_{f} + (3 \ddot{\theta}_{0} - 2 \ddot{\theta}_{f}) t_{f}^{2}}{2 t_{f}^{4}}$$

$$a_{5} = \frac{12 \theta_{f} - 12 \theta_{0} - (6 \dot{\theta}_{f} + 6 \dot{\theta}_{0}) t_{f} - (\ddot{\theta}_{0} - \ddot{\theta}_{f}) t_{f}^{2}}{2 t_{f}^{5}}$$



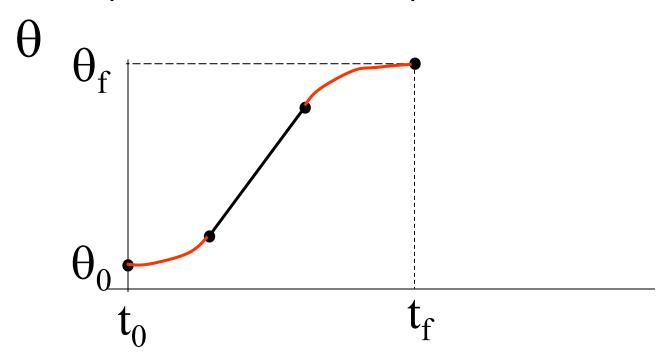
Another choice of path shape is linear

Let's assume $\dot{\theta}(t_o) = \dot{\theta}(t_f) = 0$



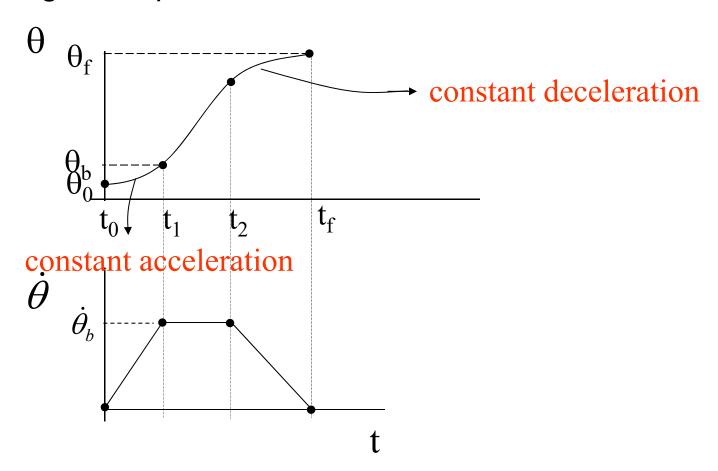


 Add parabolic blend region at each path point to ensure smooth path with continuous position and velocity

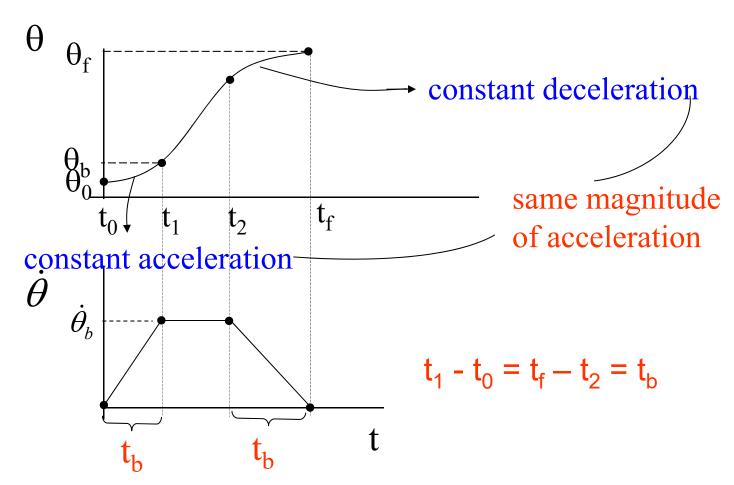




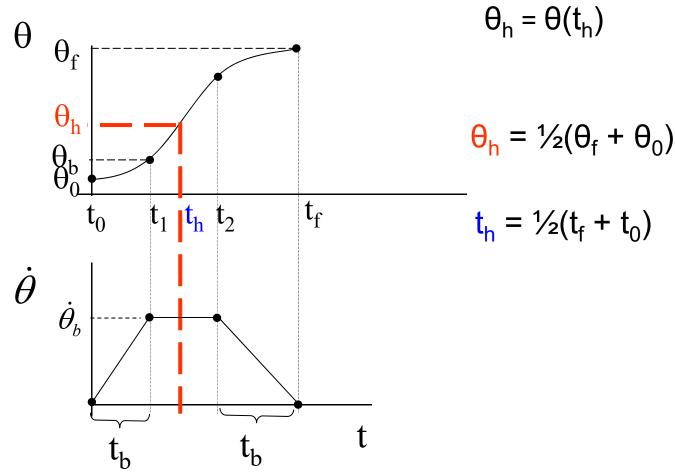
• During blend portion, constant acceleration is used



Assume both parabolic blends have same duration (=> same magnitude for the acceleration)



• Halfway point position θ_h occurs at halfway point in time t_h (some form of symmetry)





There are many possible solutions, given

$$\theta(0) = \theta_0$$
 $\dot{\theta}(0) = 0$ (assume $t_0 = 0$)

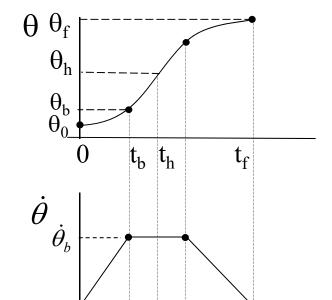
$$\theta(t_f) = \theta_f \qquad \dot{\theta}(t_f) = 0$$

Assume blend acceleration $\ddot{ heta}$ is given, find t_{b}

Velocity at end of first = velocity of linear blend region section

$$\dot{\theta}_b = \dot{\theta}_0 + \ddot{\theta} t_b = \frac{\theta_h - \theta_b}{t_h - t_b}$$
 (2-4)

where $\theta_h = \left(\frac{\theta_f + \theta_0}{2}\right)$, $t_h = t_f/2$, θ_b is value of θ at the end of blend region, t_b is the duration of the parabolic blends



 t_b t_h

 t_f



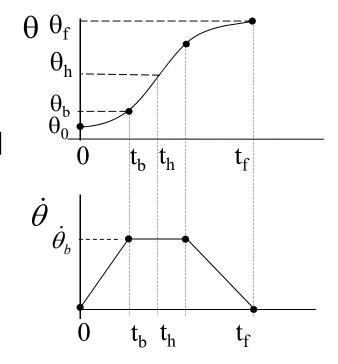
• θ_b is given by:

$$\theta_{\rm b} = \theta_{\rm 0} + \frac{1}{2} \ddot{\theta} t_{\rm b}^2$$
 (2-5)

where $\ddot{\theta}$ is the constant acceleration at the blends

Given θ_0 , θ_f and t_f (total move time), and substitute Eq (2-5) into (2-4), we get:

$$\ddot{\theta}t_b^2 - \ddot{\theta}t_f t_b + (\theta_f - \theta_0) = 0$$





Hence,

$$t_{b} = \frac{t_{f}}{2} - \frac{\sqrt{\ddot{\theta}^{2} t_{f}^{2} - 4\ddot{\theta}(\theta_{f} - \theta_{0})}}{2\ddot{\theta}}$$

For
$$t_b$$
 to exists, $\ddot{\theta} \ge \frac{4 (\theta_f - \theta_0)}{{t_f}^2}$

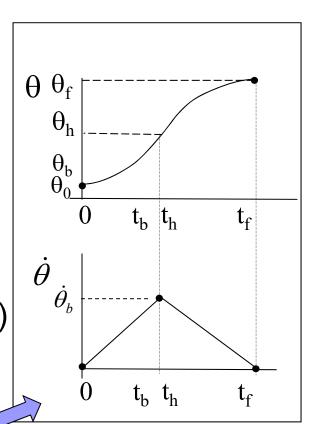


(acceleration must be sufficiently high)

When equality holds:

$$t_b = \frac{t_f}{2} = t_h$$

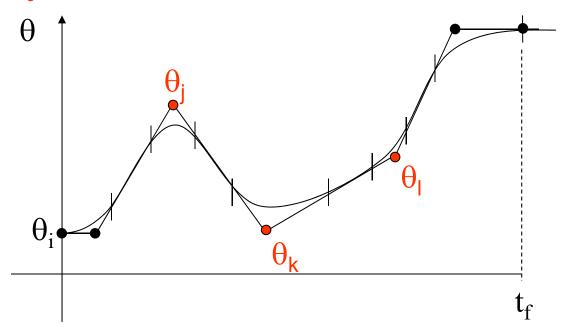
no constant $t_b = \frac{t_f}{2} = t_h$ velocity or linear segment





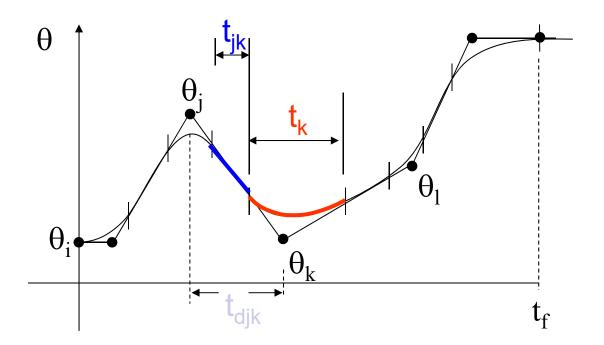
 Linear functions connect via points and parabolic blend regions added around each via point (or pseudo via point)

Considering three neighbouring path points which we call points j, k and l



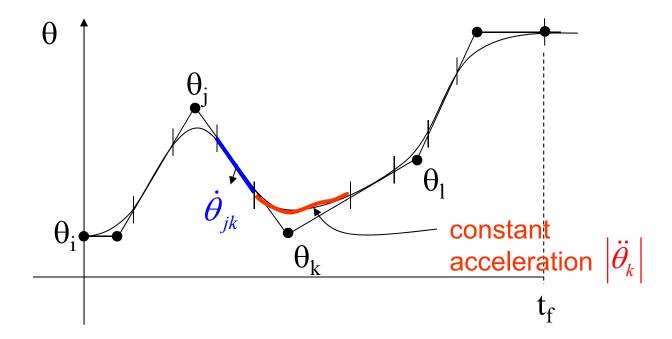


Given: t_{djk} – overall duration of the segment connecting points j and k Find: t_k – duration of blend region at path point k and t_{ik} – duration of the linear portion between points j and k





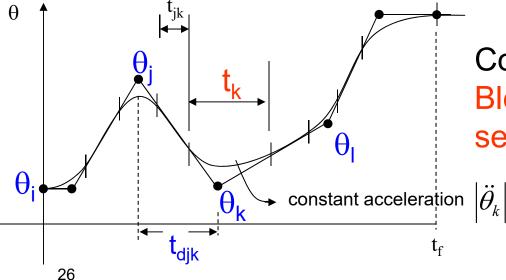
- $\dot{\theta}_{ik}$ velocity during the linear portion
- $\ddot{\theta}_{\nu}$ acceleration during the blend at point k





Given:

- all path points θ_k
- all durations t_{dik}
- magnitude of acceleration at each path point $\ddot{\theta}_{k}$



Compute:

Blend times t_k and linear segment times t_{jk}

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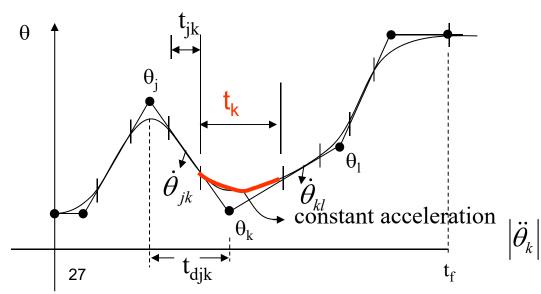
Linear Segments with Parabolic Blends & with Via Points

For interior path points (say between j & k):

$$\dot{\theta}_{jk} = \frac{\theta_k - \theta_j}{t_{d_{jk}}} \qquad \dot{\theta}_{kl} = \frac{\theta_l - \theta_k}{t_{d_{kl}}}$$

$$\dot{t}_k = \frac{\dot{\theta}_{kl} - \dot{\theta}_{jk}}{\ddot{\theta}_k}$$

$$\ddot{\theta}_k = \operatorname{sgn}(\dot{\theta}_{kl} - \dot{\theta}_{jk}) |\ddot{\theta}_k|$$



Similarly, t_i can be obtained.

Then, duration of linear segment,

$$t_{jk} = t_{djk} - \frac{1}{2} t_j - \frac{1}{2} t_k$$

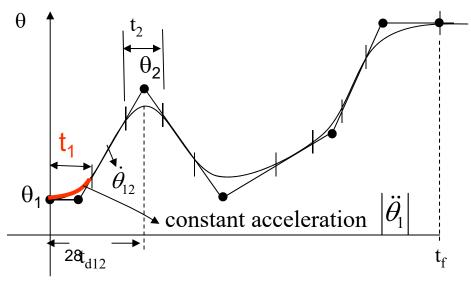
Assuming parabolic blend is symmetric around the path points

First Segment

To find the blend time t₁ at the initial point :

$$\frac{\theta_2 - \theta_1}{t_{d12} - \frac{1}{2}t_1} = \ddot{\theta}_1 t_1 = \text{velocity at 1st line segment } (\dot{\theta}_{12})$$

$$t_{d12} - \frac{1}{2}t_1 \qquad \text{where} \quad \ddot{\theta}_1 = \text{sgn}(\theta_2 - \theta_1) \left| \ddot{\theta}_1 \right|$$



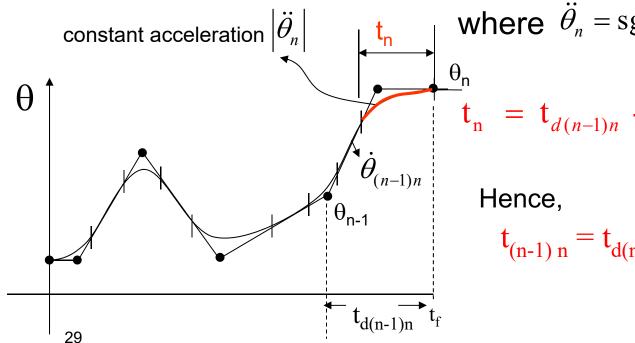
$$\therefore t_1 = t_{d_{12}} - \sqrt{t_{d_{12}}^2 - \frac{2(\theta_2 - \theta_1)}{\ddot{\theta}_1}}$$

Hence,

$$t_{12} = t_{d12} - t_1 - \frac{1}{2} t_2$$

■ Last segment connecting $\theta_{n-1} \& \theta_n$

$$\dot{\theta}_{(n-1)n} = \frac{\theta_{n} - \theta_{n-1}}{t_{d(n-1)n} - \frac{1}{2}t_{n}} = -\ddot{\theta}_{n}t_{n}$$



where $\ddot{\theta}_n = \operatorname{sgn}(\theta_{n-1} - \theta_n) \left| \ddot{\theta}_n \right|$

$$\frac{\theta_{n}}{t_{n}} = t_{d(n-1)n} - \sqrt{t_{d(n-1)n}^{2} + \frac{2(\theta_{n} - \theta_{n-1})}{\ddot{\theta}_{n}}}$$

$$t_{(n-1)n} = t_{d(n-1)n} - t_n - \frac{1}{2} t_{n-1}$$



Summary

- Plan point-to-point trajectories in joint space
- Plan trajectories with via points
- Plan trajectories with velocity and acceleration constraints