

# UNIT - IV

## MARKOV MODELING

### Discrete Markov Chains :-

The markov approach can be applied to the random behavior of systems that vary discretely or continuously with respect to time and space. This discrete or continuous random variation is known as a stochastic process.

The markov approach is applicable to those systems whose behavior can be described by a probability distribution i.e. characterized by a constant hazard rate i.e. poisson's and exponential distribution; since only if the hazard rate is constant does the probability of making a transition between two states remain constant at all points of time. If this probability is a function of time & the number of discrete steps, then the process is non-stationary and designated as non-markovian.

In the general case of markov models, both time and space may either be discrete or continuous. In the particular case of system reliability evaluation, space is normally represented only as a discrete function since it represents the discrete and identifiable states in which the system and its components can reside, whereas time may either be discrete or continuous. The discrete case, generally known as Markov chains and the continuous case, generally known as Markov process.

# General Modelling Concept

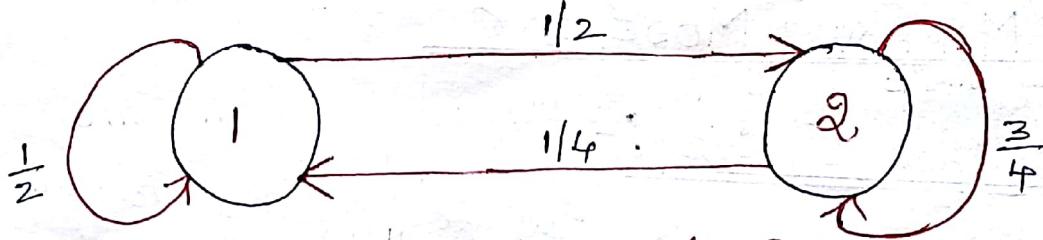


Fig: A two-state system

This is a discrete Markov chain, since the system is stationary and the movement between states occur in discrete steps.

Consider the first time interval and assume that the system is initially in state 1. The system can remain in state 1 with a probability of  $1/2$  (or) it can move into state 2 with a probability of  $1/2$ .

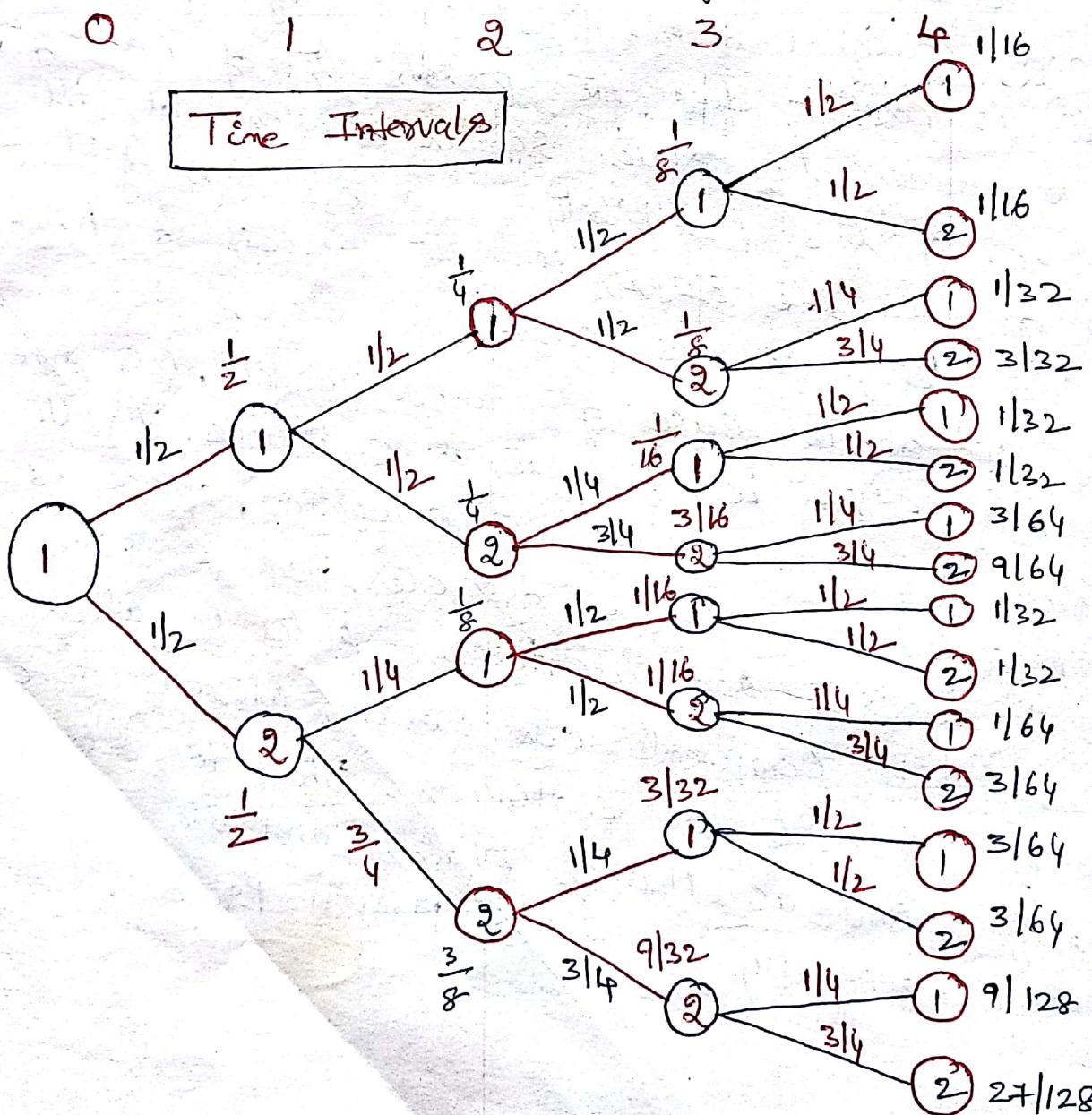


Fig: Tree diagram of the two-state system.

Time Interval	State Probabilities	
Initially in state 1	state 1	state 2
1 <sup>st</sup> time interval	$\frac{1}{2} = 0.5$	$\frac{1}{2} = 0.5$
2 <sup>nd</sup> time interval	$\frac{1}{4} + \frac{1}{8} = \frac{3}{8} = 0.375$	$\frac{1}{4} + \frac{3}{8} = \frac{5}{8} = 0.625$
3 <sup>rd</sup> time interval	$\frac{1}{8} + \frac{1}{16} + \frac{1}{16} + \frac{3}{32}$ $= \frac{11}{32} = 0.344$	$\frac{1}{8} + \frac{3}{16} + \frac{1}{16} + \frac{9}{32}$ $= \frac{21}{32} = 0.656$
4 <sup>th</sup> time interval	$\frac{1}{16} + \frac{1}{32} + \frac{1}{32} + \frac{3}{64} +$ $\frac{1}{32} + \frac{1}{64} + \frac{3}{64} + \frac{9}{128}$ $= \frac{43}{128} = 0.336$	$\frac{1}{16} + \frac{3}{32} + \frac{1}{32} + \frac{9}{64}$ $+ \frac{1}{32} + \frac{3}{64} + \frac{3}{64} + \frac{27}{128}$ $= \frac{85}{128} = 0.664$

The tree diagram method is useful technique for illustrating the concept of Markov chains but it is totally impractical of large systems and a large number of times.

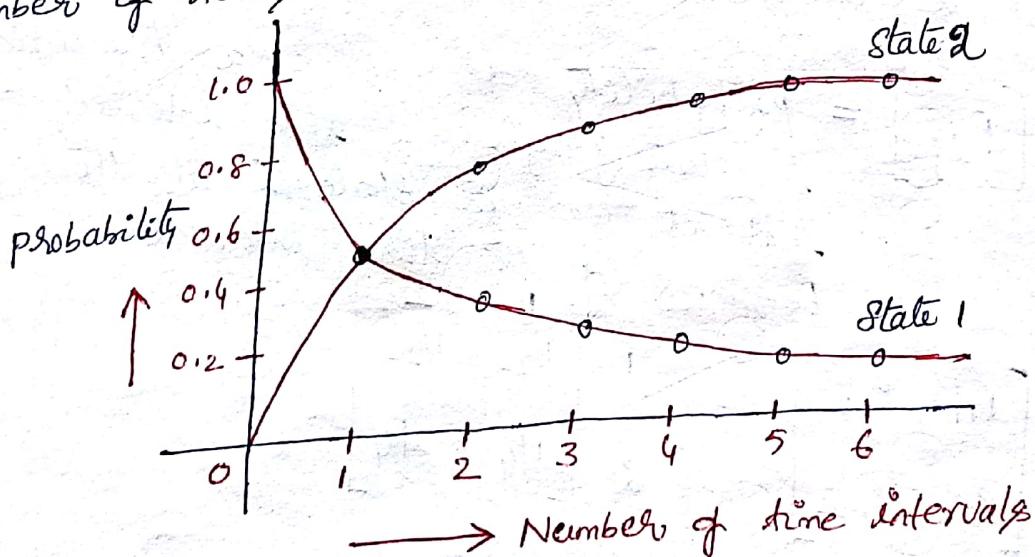


Fig: System Transient Behaviour

# Concept of STPM [Stochastic Transitional Probability Matrix]

An  $n$ -state system, the general form of the matrix, which must be always be square as

$$P = \begin{bmatrix} & 1 & 2 & 3 & \cdots & n \\ 1 & P_{11} & P_{12} & P_{13} & \cdots & P_{1n} \\ 2 & P_{21} & P_{22} & P_{23} & \cdots & P_{2n} \\ 3 & P_{31} & P_{32} & P_{33} & \cdots & \vdots \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ n & P_{n1} & P_{n2} & P_{n3} & \cdots & P_{nn} \end{bmatrix}$$

$\xrightarrow{\text{From state}} \xrightarrow{\text{to state}}$

This matrix is known as the stochastic transitional probability matrix for the system, since it represents in matrix form, the transitional probabilities of the stochastic process. It should be noted that the summation of the probabilities in each row of the matrix must be unity.

$P = [P_{ij}]$  = probability of making a transition to state  $j$  after a time interval given that it was in state  $i$  at the beginning of the time interval.

$$P = \begin{bmatrix} P_{11} & P_{12} \\ P_{21} & P_{22} \end{bmatrix} = \begin{bmatrix} 1 & 2 \\ 1 & 2 \end{bmatrix} \begin{bmatrix} 1/2 & 1/2 \\ 1/4 & 3/4 \end{bmatrix}$$

$$\begin{aligned} P^2 &= \begin{bmatrix} 1/2 & 1/2 \\ 1/4 & 3/4 \end{bmatrix} \begin{bmatrix} 1/2 & 1/2 \\ 1/4 & 3/4 \end{bmatrix} \\ &= \begin{bmatrix} 1 & 2 \\ 1 & 2 \end{bmatrix} \begin{bmatrix} 3/8 & 5/8 \\ 5/16 & 11/16 \end{bmatrix} \end{aligned}$$

$$P^3 = P^2 \times P = I \begin{bmatrix} \frac{1}{32} & \frac{21}{32} \\ \frac{21}{64} & \frac{43}{64} \end{bmatrix}$$

## Recursive Relation :-

Consider initially  $P[0] = [1 \ 0]$  is known as initial probability vector.

$$\begin{aligned} P[1] &= P[0]P \\ &= [1 \ 0] \begin{bmatrix} \frac{1}{2} & \frac{1}{2} \\ \frac{1}{4} & \frac{3}{4} \end{bmatrix} \\ &= \left[ \frac{1}{2} \ \frac{1}{2} \right] \end{aligned}$$

$$\begin{aligned} P[2] &= P[1]P \\ &= \left[ \frac{1}{2} \ \frac{1}{2} \right] \begin{bmatrix} \frac{1}{2} & \frac{1}{2} \\ \frac{1}{4} & \frac{3}{4} \end{bmatrix} \\ &= \left[ \frac{3}{8} \ \frac{5}{8} \right] \end{aligned}$$

Similarly  $P[3] = P[2]P$

$$\vdots$$

$$P[N] = P[N-1]P \text{ called Recursive Relation}$$

$$P[1] = P[0]P$$

$$\begin{aligned} P[2] &= P[1]P \\ &= P[0]P^2 \end{aligned}$$

$$P[3] = P[0]P^3$$

$$\therefore P[n] = P[0]P^n$$

The repeated multiplication of S TPM will converge to a definite value and this definite value is known as limiting state probabilities of the states.

### Evaluation of limiting State Probabilities :-

Let  $P_1, P_2$  be the LSP of the state 1 and 2

respectively.

Let  $\alpha$  be the LSP vector

$$\alpha = [P_1 \ P_2]$$

The solution technique

$$\alpha P = \alpha$$

Consider one component repairable model with 2 states

$$[P_1 \ P_2] \begin{bmatrix} P_{11} & P_{12} \\ P_{21} & P_{22} \end{bmatrix} = [P_1 \ P_2]$$

$$P_1 P_{11} + P_2 P_{21} = P_1$$

$$[1 - P_{11}] P_1 - P_2 P_{21} = 0 \rightarrow ①$$

$$P_1 P_{12} + P_2 P_{22} = P_2$$

$$P_1 P_{12} + [P_{22} - 1] P_2 = 0 \rightarrow ②$$

$$P_1 P_{12} + P_2 P_{22} = 1$$

$$P_{11} + P_{12} = 1$$

$$P_{21} + P_{22} = 1$$

$$P_{12} P_1 - P_2 P_{21} = 0 \rightarrow ③$$

$$-P_1 P_{12} + P_{21} P_2 = 0 \rightarrow ④$$

out of eq ③ & ④ only one of them is linearly independent but in order to solve for the LSP another equation is required and is given by

$$P_1 + P_2 = 1 \rightarrow ⑤$$

Writing in matrix form for eq ③ & ⑤

$$\begin{bmatrix} P_{12} & -P_{21} \\ 1 & 1 \end{bmatrix} \begin{bmatrix} P_1 \\ P_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} \frac{1}{2} & -\frac{1}{4} \\ 1 & 1 \end{bmatrix} \begin{bmatrix} P_1 \\ P_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

Using Cramer's rule

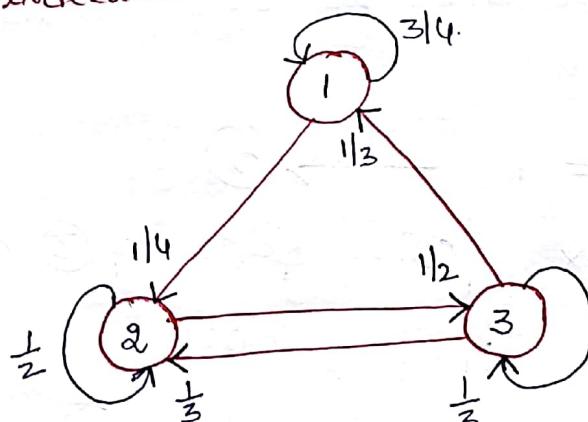
$$P_1 = \frac{\begin{vmatrix} 0 & -1/4 \\ 1 & 1 \end{vmatrix}}{\frac{3}{4}} = \frac{1}{3}$$

$$P_2 = \frac{\begin{vmatrix} \frac{1}{2} & 0 \\ 1 & 1 \end{vmatrix}}{\frac{3}{4}} = \frac{2}{3}$$

- question: Distinguish b/w Markov chain & Markov process with the help of suitable example by writing STPM of each.
1. write short notes on STPM.
  2. write short notes on explain the concept of stochastic
  3. Define Markov chain & explain the concept of transition probability matrix and evaluation of limiting state probabilities.

### Example :-

① Consider a 3 state system shown in fig. with transitional probability indicated. Evaluate the LSPs of each state.



Sol. The steps for solving the problem to be followed are

1. write S TPM of various states.
2. check whether sum of each row elements are equal to 1.
3. To evaluate LSPs of state 1 to n

$\alpha p = \alpha$  from the set of n equations.

4. Take any  $n-1$  equations from  $p_1 + p_2 + \dots + p_n = 1$

5. Take  $n^{th}$  equation as  $p_1 + p_2 + \dots + p_n = 1$

6. Solve for  $p_1$  to  $p_n$  using cramer's rule.

$$\text{STPM} = P = \begin{matrix} & 1 & 2 & 3 \\ 1 & \left[ \begin{matrix} 3/4 & 1/4 & 0 \end{matrix} \right] \\ 2 & \left[ \begin{matrix} 0 & 1/2 & 1/2 \end{matrix} \right] \\ 3 & \left[ \begin{matrix} 1/3 & 1/3 & 1/3 \end{matrix} \right] \end{matrix}$$

$$\alpha = [p_1 \ p_2 \ p_3]$$

The solution technique is

$$\alpha p = \alpha$$

$$[p_1 \ p_2 \ p_3] \begin{bmatrix} 3/4 & 1/4 & 0 \\ 0 & 1/2 & 1/2 \\ 1/3 & 1/3 & 1/3 \end{bmatrix} = [p_1 \ p_2 \ p_3].$$

$$p_1 \frac{3}{4} + p_3 \frac{1}{3} = p_1$$

$$-\frac{1}{4} p_1 + \frac{p_3}{3} = 0 \rightarrow ①$$

$$P_2|_2 + P_3|_3 = P_3$$

$$\frac{P_2}{2} - \frac{2}{3} P_3 = 0 \rightarrow (2)$$

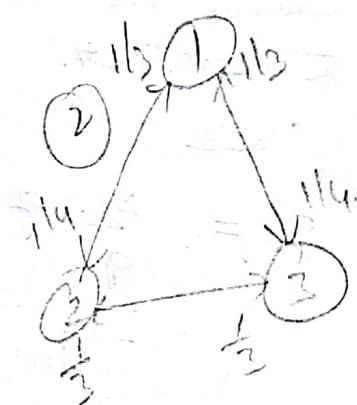
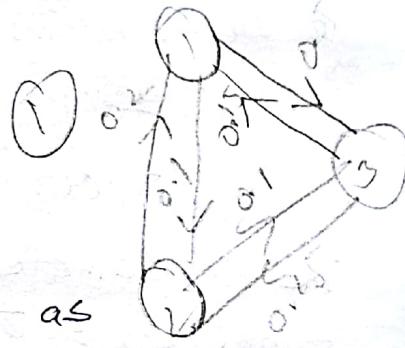
~~out of eq 1~~

$$P_1 + P_2 + P_3 = 1 \rightarrow (3)$$

Writing eq (1), (2) and (3) in matrix form as

$$\begin{bmatrix} -1/4 & 0 & 1/3 \\ 0 & 1/2 & -2/3 \\ 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} P_1 \\ P_2 \\ P_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

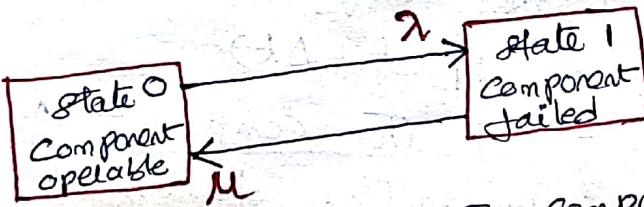
Solving these equations we get  
 $P_1 = 4/11, P_2 = 2/11, P_3 = 3/11.$



## Continuous Markov Process:-

### Transition Rate Concept :-

Consider the case of a single repairable component den which are characterized by its exponential distribution.



def  $P_0(t)$  = probability that the component is operable at time  $t$

$P_1(t)$  = probability that the component is failed at time  $t$

$\lambda$  = failure rate

$\mu$  = repair rate

The failure density function for a component with a constant hazard rate of  $\lambda$  is given by

$$f(t) = \lambda e^{-\lambda t}$$

The density functions of the operating and failed states of the system shown in fig. are

$$f_0(t) = \gamma e^{-\gamma t}$$

$$f_1(t) = \mu e^{-\mu t}$$

The parameters  $\gamma$  and  $\mu$  are referred to as state transition rates since they represent the rate at which the system transits from one state of the system to another.

Whole

$$\gamma = \frac{\text{No. of failures of a component in a given period of time}}{\text{Total period of the time the component was operating.}}$$

$$\mu = \frac{\text{No. of repairs of a component in a given period of time}}{\text{Total period of the time the component is repaired}}$$

Evaluating Time dependent probabilities :-

The probability of the component functioning during the time  $(t + \Delta t)$  is  $P_1(t + \Delta t)$

= The probability of the component functioning at time  $t$  and not failing during  $t$  to  $t + \Delta t$  + probability of component failed at time  $t$  and functioning goes into operable state during  $\Delta t$ .

Let  $P_1(t)$  be the probability of the component being in operable state at time 't'

$P_2(t)$  be the probability of the component being in failed state at time 't'

$$P_1(t + \Delta t) = P_1(t)(1 - \gamma \Delta t) + P_2(t)\mu \Delta t$$

$$P_1(t + \Delta t) - P_1(t) = -\gamma P_1(t) \Delta t + \mu P_2(t) \Delta t \quad (\text{or})$$

$$\lim_{\Delta t \rightarrow 0} \frac{P_1(t + \Delta t) - P_1(t)}{\Delta t} = -\gamma P_1(t) + \mu P_2(t)$$

$$P_1'(t) = -\gamma P_1(t) + \mu P_2(t) \rightarrow ①$$

Let the probability of the component failing during the time  $t + \Delta t$  is defined as  $P_2(t + \Delta t)$

= The probability of the component functioning at time 't' and failed during  $t$  to  $t + \Delta t$   
The probability of the component failed at time 't'  
and not transitioning to other state

$$P_2(t + \Delta t) = P_1(t) \gamma \Delta t + P_2(t) (1 - \mu \Delta t)$$

$$P_2(t + \Delta t) = P_2(t) = P_1(t) \gamma \Delta t - P_2(t) \mu \Delta t$$

$$\lim_{\Delta t \rightarrow 0} \frac{P_2(t + \Delta t) - P_2(t)}{\Delta t} = \gamma P_1(t) - \mu P_2(t)$$

$$P_2'(t) = \gamma P_1(t) - \mu P_2(t) \rightarrow ②$$

1. Evaluation of the expression for  $P_1(t), P_2(t)$   
(time dependent prob. of each state) using LT  
approach as

$$t \rightarrow \infty \quad \left. \begin{array}{l} P_1(t) = P_1 \\ P_2(t) = P_2 \end{array} \right\} \text{ are LSP of the states}$$

$$t \rightarrow \infty \quad \left. \begin{array}{l} P_1(t) = P_1 \\ P_2(t) = P_2 \end{array} \right\} \text{ 1 and 2 respectively.}$$

2. To evaluate LSP using

(a) Differential Equation Approach

(b) STPM Approach ( $\alpha p = \alpha$ )

From eq. (1) taking LT

$$SP_1(s) - P_1(0) = -\gamma P_1(s) + \mu P_2(s)$$

$$(s+\gamma)P_1(s) - \mu P_2(s) = P_1(0) \rightarrow (3)$$

From eq (2) taking LT

$$SP_2(s) - P_2(0) = \gamma P_1(s) - \mu P_2(s)$$

$$P_2(s)[s+\mu] - \gamma P_1(s) = P_2(0) \rightarrow (4)$$

Writing eqs. (3) and (4) in matrix form

$$\begin{bmatrix} s+\gamma & -\mu \\ -\gamma & s+\mu \end{bmatrix} \begin{bmatrix} P_1(s) \\ P_2(s) \end{bmatrix} = \begin{bmatrix} P_1(0) \\ P_2(0) \end{bmatrix}$$

Applying Cramer's rule.

$$P_1(s) = \frac{\begin{bmatrix} P_1(0) & -\mu \\ P_2(0) & s+\mu \end{bmatrix}}{\Delta} = \frac{(s+\mu)P_1(0) + \mu P_2(0)}{\Delta}$$

$$\text{where } \Delta = (s+\gamma)(s+\mu) - \gamma\mu$$

$\circlearrowleft$

$$= s^2 + s\mu + s\gamma + \gamma\mu - \gamma\mu$$
$$= s^2 + (\mu + \gamma)s$$
$$= s[s + (\gamma + \mu)]$$

$$P_1(s) = \frac{SP_1(0) + \mu[P_1(0) + P_2(0)]}{s[s + (\gamma + \mu)]}$$

$$\text{Assuming } P_1(0) = 1 \text{ and } P_2(0) = 0$$

$$P_1(s) = \frac{s}{s + (\gamma + \mu)} + \frac{\mu}{s[s + (\gamma + \mu)]}$$

Using Heavyside partial fraction expansion theorem

$$\frac{\mu}{s[s + (\gamma + \mu)]} = \frac{A}{s} + \frac{B}{s + (\gamma + \mu)}$$

$$A = \frac{\mu}{s + (\gamma + \mu)} \Big|_{s=0} = \frac{\mu}{\gamma + \mu}$$

$$B = \mu |s| / s = -(\gamma + \mu) = \frac{\mu}{-(\gamma + \mu)}$$

Using inverse laplace transformation

$$= \frac{\mu}{\gamma + \mu} - \frac{\mu}{\gamma + \mu} e^{-(\gamma + \mu)t}$$

$$P_1(t) = \cancel{B e^{-\gamma t}} + \frac{\mu}{\gamma + \mu} [1 - e^{-(\gamma + \mu)t}]$$

$$= e^{-(\gamma + \mu)t} \left[ 1 - \frac{\mu}{\gamma + \mu} \right] + \frac{\mu}{\gamma + \mu}$$

$$P_1(t) = \frac{\gamma}{\gamma + \mu} e^{-(\gamma + \mu)t} + \frac{\mu}{\gamma + \mu} \rightarrow ⑤$$

$$P_2(s) = \frac{(s + \gamma - P_1(0))}{(-\gamma - P_2(0))} = \frac{(s + \gamma)P_2(0) + P_1(0)}{s(s + \gamma + \mu)}$$

$$= \frac{sP_2(0) + \gamma [P_1(0) + P_2(0)]}{s(s + \gamma + \mu)}$$

$$= \frac{P_2(0)}{s + (\gamma + \mu)} + \frac{\gamma [P_1(0) + P_2(0)]}{s(s + \gamma + \mu)}$$

Taking inverse L.T.

$$P_2(t) = P_2(0) e^{-(\gamma + \mu)t} + \frac{\gamma}{\gamma + \mu} - \frac{\gamma}{\gamma + \mu} e^{-(\gamma + \mu)t}$$

Assuming  $P_1(0) = 0$  and  $P_2(0) = 0$

$$\therefore P_2(t) = \frac{\gamma}{\gamma + \mu} - \frac{\gamma}{\gamma + \mu} e^{-(\gamma + \mu)t} \rightarrow ⑥$$

Let LSP of states ① and ② be  $P_1$  and  $P_2$

$$\text{At } t \rightarrow \infty, P_1(t) = P_1 \quad \times \quad \text{At } t \rightarrow \infty, P_2(t) = P_2$$

Substituting the above in eq ⑤ and ⑥, we get

$$P_1 = \frac{\mu}{\lambda + \mu}, \quad P_2 = \frac{\lambda}{\lambda + \mu}$$

Equation Approach :-

## 2. Differential

We know

$$P_1'(t) = -\lambda P_1(t) + \mu P_2(t)$$

$$P_2'(t) = \lambda P_1(t) - \mu P_2(t)$$

$$\text{As } t \rightarrow \infty, P_1'(t) = 0 \quad \times \quad P_2'(t) = 0$$

$$0 = -\lambda P_1(t) + \mu P_2(t) \rightarrow ⑦$$

$$0 = \lambda P_1(t) - \mu P_2(t) \rightarrow ⑧$$

The above equations are not linearly independent.

$$\therefore P_1 + P_2 = 1 \rightarrow ⑨$$

$$-\lambda P_1(t) + \mu P_2(t) = 0$$

$$P_1 + P_2 = 1$$

$$\begin{bmatrix} -\lambda & \mu \\ 1 & 1 \end{bmatrix} \begin{bmatrix} P_1(t) \\ P_2(t) \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$P_1(t) = \frac{\begin{bmatrix} 0 & \mu \\ 1 & 1 \end{bmatrix}}{-(\lambda + \mu)} = \frac{\mu}{\lambda + \mu}$$

$$P_2(t) = \frac{\begin{bmatrix} -\lambda & 0 \\ 1 & 1 \end{bmatrix}}{-(\lambda + \mu)} = \frac{\lambda}{\lambda + \mu}$$

### 3. Stochastic Transitional Probability Matrix (STPM)

To evaluate limiting state probabilities using STPM approach

$$\alpha = [P_1 \ P_2]$$

$$P = \begin{bmatrix} 1 - \gamma \Delta t & \gamma \Delta t \\ \mu \Delta t & 1 - \mu \Delta t \end{bmatrix}$$

$$\alpha' P = \alpha$$

$$[P_1 \ P_2] \begin{bmatrix} 1 - \gamma \Delta t & \gamma \Delta t \\ \mu \Delta t & 1 - \mu \Delta t \end{bmatrix} = [P_1 \ P_2]$$

$$P_1 [1 - \gamma \Delta t] + \mu \Delta t P_2 = P_1$$

$$-\gamma \Delta t P_1 + \mu \Delta t P_2 = 0$$

$$-\gamma P_1 + \mu P_2 = 0 \rightarrow ①$$

$$\gamma \Delta t P_1 + P_2 (1 - \mu \Delta t) = P_2$$

$$\gamma \Delta t P_1 - \mu \Delta t P_2 = 0$$

$$\gamma P_1 - \mu P_2 = 0 \rightarrow ②$$

The above equations are not linearly independent

$$\therefore P_1 + P_2 = 1 \rightarrow ③$$

Solving eqns. ① and ③, we get

$$\begin{bmatrix} -\gamma & \mu \\ 1 & 1 \end{bmatrix} \begin{bmatrix} P_1 \\ P_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$P_1 = \frac{\begin{bmatrix} 0 & \mu \\ 1 & 1 \end{bmatrix}}{-(\gamma + \mu)} = \frac{\mu}{\gamma + \mu} \quad P_2 = \frac{\begin{bmatrix} -\gamma & 0 \\ 1 & 1 \end{bmatrix}}{-(\gamma + \mu)} = \frac{\gamma}{\gamma + \mu}$$

## Two - Component Repairable System :-

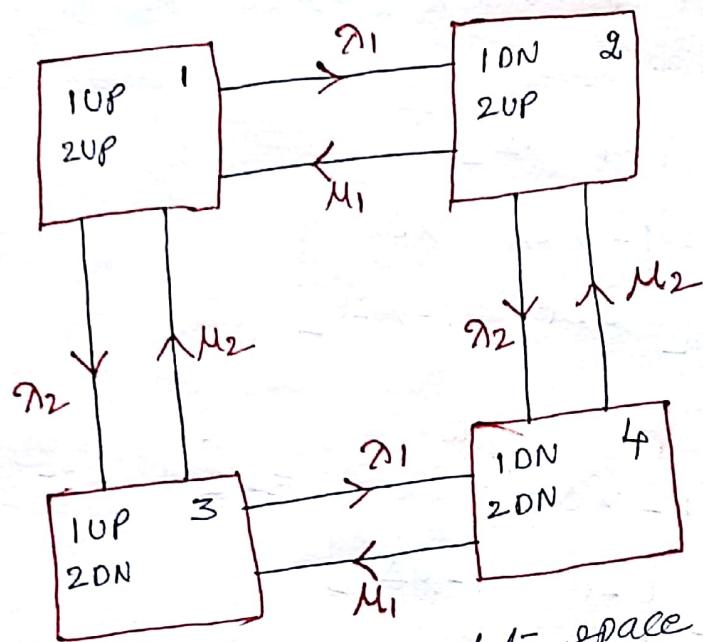


Fig. (1) : Complete state space diagram

Evaluation of LSP's :-

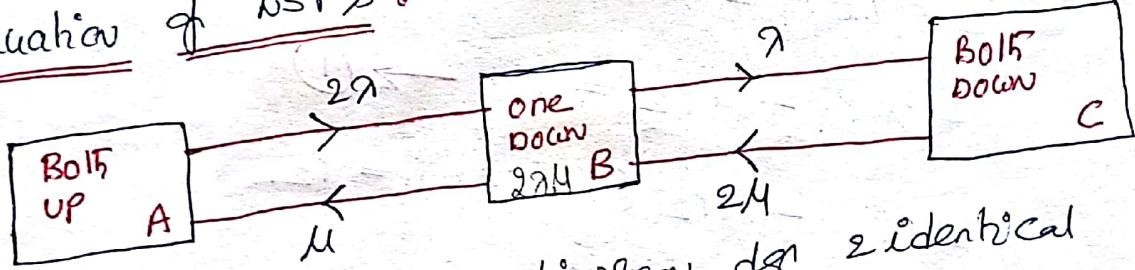


Fig. (2) : State space diagram for 2 identical Components

Minimum No. of states for  $n$ -identical Components

is  $(n+1)$  states.

$2^n$  maximum number of states for non-identical  $n$  components.

$$\gamma_1 = \gamma_2 = \gamma \quad [\text{Assume Identical Components}]$$

$$\mu_1 = \mu_2 = \mu$$

To evaluate LSP's of states ABC :-

$$STPM =$$

$$\begin{bmatrix} A & B & C \\ \hline 1-\gamma & \gamma & 0 \\ \gamma & 1-(\gamma+\mu) & \mu \\ 0 & \mu & 1-\mu \end{bmatrix}$$

The solution is  $\alpha P = \alpha$   
where  $\alpha$  is LSP vector

$$\alpha = [P_A \ P_B \ P_C]$$

$$[P_A \ P_B \ P_C] \begin{bmatrix} 1-2\gamma & 2\gamma & 0 \\ \mu & 1-(\gamma+\mu) & \gamma \\ 0 & 2\mu & 1-2\mu \end{bmatrix} = [P_A \ P_B \ P_C]$$

$$(1-2\gamma)P_A + P_B\mu = P_A$$

$$-2\gamma P_A + P_B\mu = 0 \rightarrow \textcircled{1}$$

$$2\gamma P_A + [1-(\gamma+\mu)]P_B + 2\mu P_C = P_B$$

$$2\gamma P_A - (\gamma+\mu)P_B + 2\mu P_C = 0 \rightarrow \textcircled{2}$$

$$\gamma P_B + (1-2\mu)P_C = P_C$$

$$\gamma P_B - 2\mu P_C = 0 \rightarrow \textcircled{3}$$

Writing eq \textcircled{1}, \textcircled{2} and \textcircled{3} in matrix form

$$\begin{bmatrix} -2\gamma & \mu & 0 \\ 2\gamma & -(\gamma+\mu) & 2\mu \\ 0 & \gamma & -2\mu \end{bmatrix} \begin{bmatrix} P_A \\ P_B \\ P_C \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

out of which only two of them linearly independent.  
The linear equation is

$$P_A + P_B + P_C = 1.$$

$$\begin{bmatrix} -2\gamma & \mu & 0 \\ 0 & \gamma & -2\mu \\ 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} P_A \\ P_B \\ P_C \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

Solving using Cramer's rule

$$P_A = \frac{1}{\Delta} \begin{bmatrix} 0 & \mu & 0 \\ 0 & \gamma & -2\mu \\ 1 & 1 & 1 \end{bmatrix} = -2\mu^2$$

$$\Delta = -2\gamma(\gamma + 2\mu) - \mu(2\mu)$$

$$= -2(\gamma + \mu)^2$$

$$P_A = \frac{\mu^2}{(\gamma + \mu)^2}$$

$$P_B = \frac{1}{\Delta} \begin{bmatrix} -2\gamma & 0 & 0 \\ 0 & 0 & -2\mu \\ 1 & 1 & 1 \end{bmatrix} = 4\gamma\mu$$

$$P_B = \frac{-4\gamma\mu}{2(\gamma + \mu)^2} = \frac{2\gamma\mu}{(\gamma + \mu)^2}$$

$$P_C = \frac{1}{\Delta} \begin{bmatrix} -2\gamma & \mu & 0 \\ 0 & \gamma & 0 \\ 1 & 1 & 1 \end{bmatrix} = -2\gamma^2$$

$$P_C = \frac{\gamma^2}{(\gamma + \mu)^2}$$

(1) Now, consider fig ① i.e., a 2-component separable model with non-identical components.

(2) Now, consider fig ② i.e., the LSP states 1 to 4

Let  $P_1, P_2, P_3, P_4$  be the

$$P_1 = \frac{\mu_1}{(\gamma_1 + \mu_1)} \cdot \frac{\mu_2}{(\gamma_2 + \mu_2)}$$

$$P_2 = \frac{\gamma_1}{(\gamma_1 + \mu_1)} \cdot \frac{\mu_2}{(\gamma_2 + \mu_2)}$$

$$P_3 = \frac{\gamma_2}{(\gamma_1 + \mu_1)} \cdot \frac{\mu_1}{(\gamma_2 + \mu_2)}$$

$$P_4 = \frac{\pi_1}{(\pi_1 + \mu_1)} \cdot \frac{\pi_2}{(\pi_2 + \mu_2)}$$

① 2 - Component identical model

series system :-

$$R_S = P_A$$

$$Q_S = P_B + P_C = 1 - P_A$$

parallel system :-

$R_P = P_A + P_B$  - fully redundant system.

$Q_P = P_C \rightarrow$  unavailability of the system.

② 2 - Component unidentical model :-

series system :-

$$R_S = P_1$$

$$Q_S = 1 - P_1$$

parallel system :-

$$R_P = P_1 + P_2 + P_3$$

$$Q_P = P_4$$

### 3 - Component Repairable Model :-

Let  $P_1$  to  $P_8$  be the limiting state probabilities of states 1 to 8.

10, 11, 28.

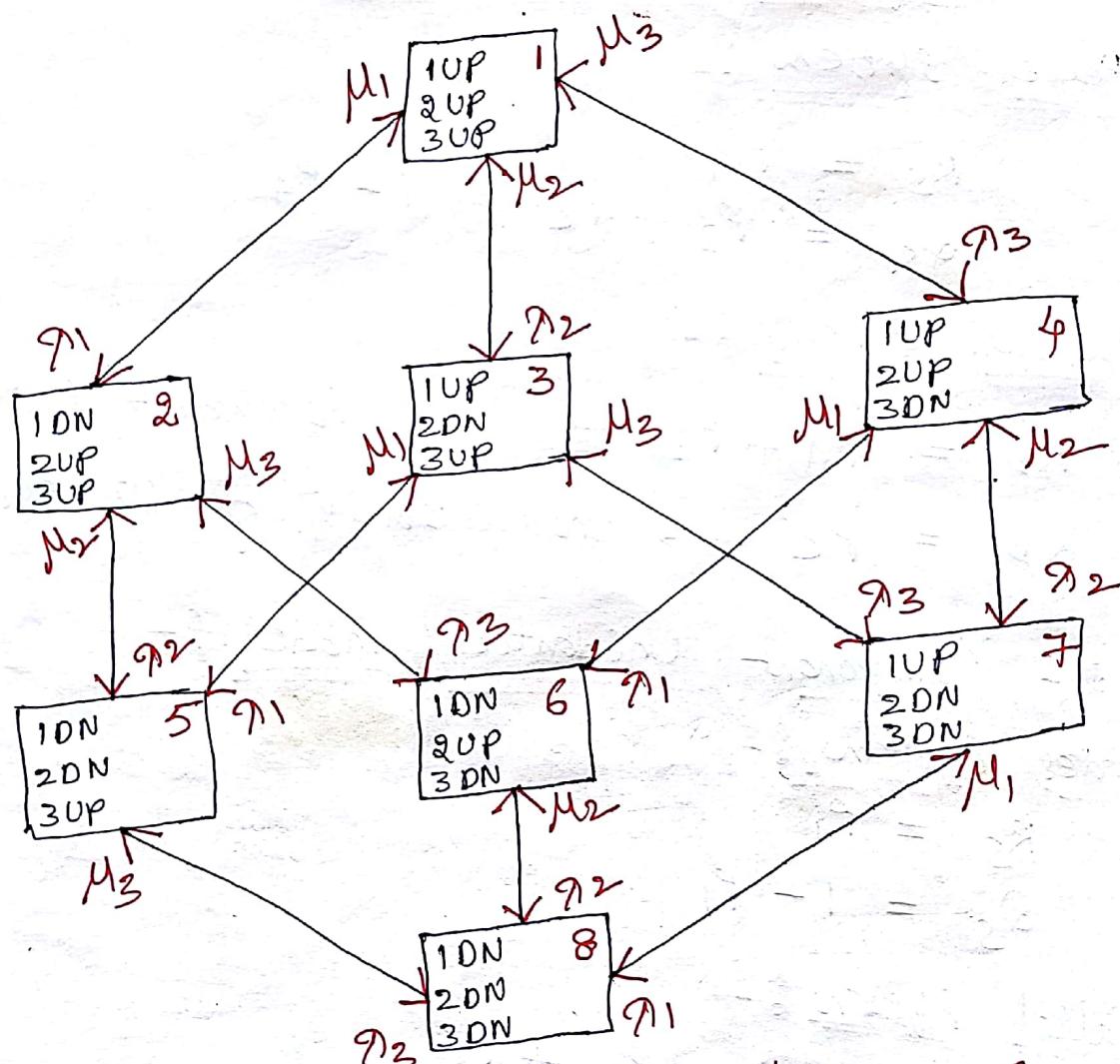


Fig. : state space diagram for 3 - Component repairable model.

#### Series System :-

$$R_S = P_1$$

$$Q_S = 1 - P_1 \\ = P_2 + P_3 + P_4 + P_5 + P_6 + P_7 + P_8$$

#### Parallel System :-

$$Q_P = P_8$$

$$R_P = P_1 + P_2 + P_3 + P_4 + P_5 + P_6 + P_7 = 1 - P_8$$

## Partially Redundant System :-

Atleast 2 out of 3 must function

$$R_S = P_1 + P_2 + P_3 + P_4$$

$$Q_S = P_5 + P_6 + P_7 + P_8.$$

1. (a) Explain the methods of calculating the steady state probabilities for a single component with repair by two state Markov process.
2. (b) Develop the expression for time dependent probability of a one component separable model in terms of failure and repair rates of the component.
3. Develop the state space model of two component separable system and hence obtain the expressions for lifetimes probabilities of the states of the states have identical transition rates and the components have identical capacities.
4. How the reliability calculator is done for two-component separable models with an example.
5. For the markov process of a two state system determine the availability of each state as a function of time

## UNIT - IV

(iv)

1. Explain how cumulative probability and cumulative frequency is evaluated for merged states.
2. (i) Write short notes on frequency and elevation concept.
3. Explain one, two component separable models reliability evaluations using the concept of frequency of occurring states.
4. Define cumulative probability and explain the cumulative frequency of failure evaluation in generation of system reliability analysis.
5. Develop the expression for elevation of cumulative probability and cumulative frequencies of an n-component model.

V-IV

6.

The S-T-PM of a discrete state system is given below.

$$P = \begin{bmatrix} 0.5 & 0.2 & 0.3 \\ 0.3 & 0.4 & 0.3 \\ 0.2 & 0.2 & 0.6 \end{bmatrix}$$

$$P_1 = 0.3214$$

$$P_2 = 0.28$$

$$P_3 = 0.4285$$

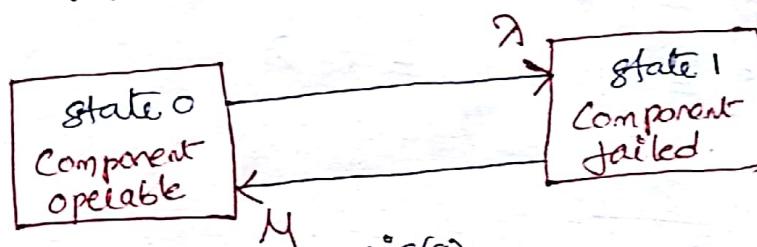
- (1) Draw state space diagram
- (2) Compute the LPS of each state

# UNIT - IV

## FREQUENCY X DURATION TECHNIQUE

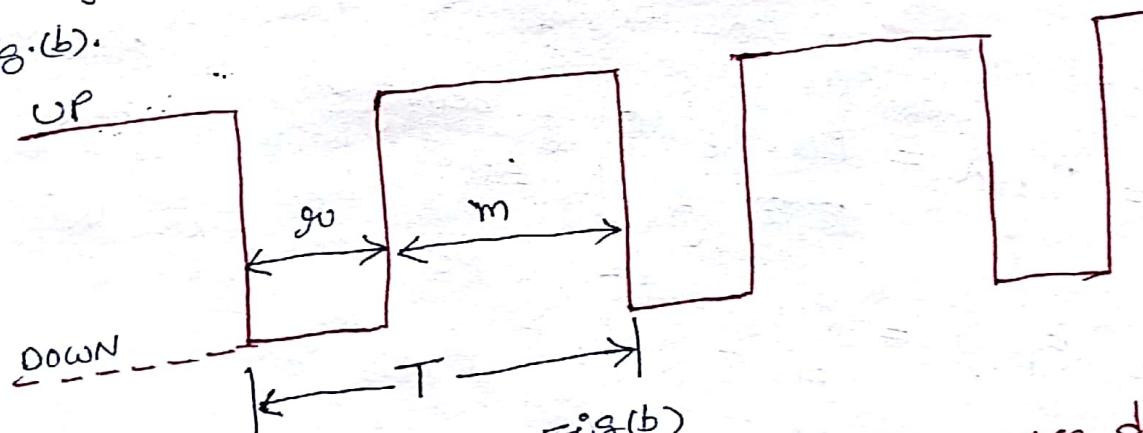
### Frequency X Duration Concept :-

The basic concept associated with the frequency and duration technique are best in terms of the single repairable component used to describe the continuous Markov process. The state space diagram of this system is shown in fig(a).



Fig(a)

The two system states and their associated transitions can be shown chronologically on a time graph. The mean values of up and down times can be used to give the average performance of this two state system shown in fig.(b).



Fig(b)

Fig.: Single Component System (a) state space diagram  
(b) Mean time state diagram

Where  $\lambda$  = failure rate of the component

$\mu$  = repair rate of the component

$m$  = mean operating time of the component

$\vartheta$  = mean repair time of the component.

The probability of residing in the operate state (availability) and the probability of residing in the failed state (unavailability) given as

$$P_0 = \frac{\mu}{\lambda + \mu}$$

$$= \frac{\frac{1}{g_U}}{\frac{1}{m} + \frac{1}{g_U}} = \frac{m}{m + g_U} = \frac{m}{T} = m\tau$$

$$\therefore P_0 = m\tau$$

$$\tau = P_0 \times \frac{1}{m} = P_0 \lambda$$

$$P_1 = \frac{\lambda}{\lambda + \mu}$$

$$= \frac{1/m}{\frac{1}{m} + \frac{1}{g_U}} = \frac{g_U}{m + g_U} = \frac{g_U}{T} = g\tau.$$

$$\therefore P_1 = g\tau \Rightarrow \tau = P_1 \times \frac{1}{g_U} = P_1 \mu.$$

$\therefore$  Frequency of encountering the up state

$P_0 \cdot \lambda$  = Probability of being in the state  $\times$  Rate of departure from the state

$P_1 \mu$  = Probability of NOT being in the state  $\times$  Rate of entry into the state.

## 2. Two- Component Repairable Model :-

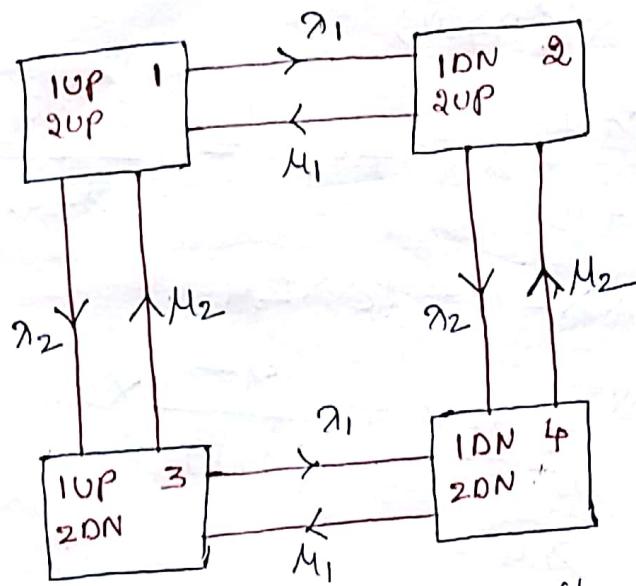
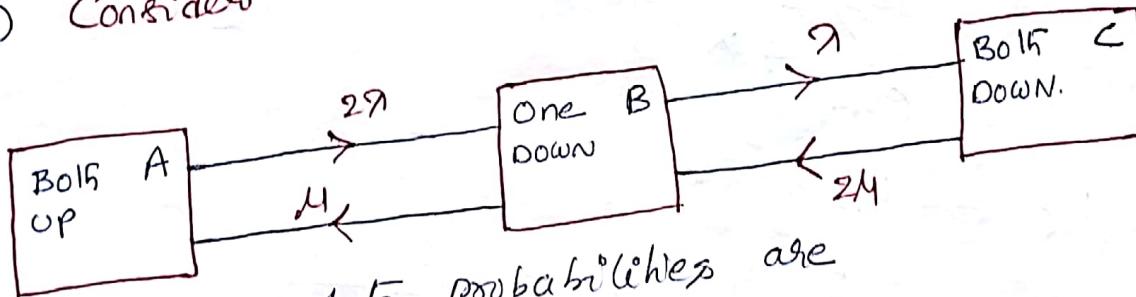


Fig.: Two Component Repairable Model.  
state space diagram  
Identical Components.

(a) Consider



The limiting state probabilities are

$$P_A = \mu^2 / (\gamma + \mu)^2$$

$$P_B = 2\gamma\mu / (\gamma + \mu)^2$$

$$P_C = \gamma^2 / (\gamma + \mu)^2$$

Let  $\gamma_A$ ,  $\gamma_B$  and  $\gamma_C$  be the frequency of encountering states A, B and C respectively.

states A, B and C respectively.

rate of departure

$$\gamma_A = P_A \times \text{rate of entry} = \frac{\mu^2}{(\gamma + \mu)^2} \cdot 2\gamma \quad (\text{eqn})$$

$$\gamma_A = P_B \times \text{rate of entry} = P_B \times \mu$$

$$= \frac{2\gamma\mu}{(\gamma + \mu)^2} \times \mu = \frac{2\gamma\mu^2}{(\gamma + \mu)^2}$$

$$\begin{aligned}
 g_B &= P_B \times \text{rate of departure} \\
 &= P_B \times (\lambda + \mu) \\
 &= \frac{2\lambda\mu}{(\lambda + \mu)^2} \times (\lambda + \mu) = \frac{2\lambda\mu}{(\lambda + \mu)}
 \end{aligned}$$

$$\begin{aligned}
 g_B &= P_A \times 2\lambda + P_C \times 2\mu \\
 &= \frac{\mu^2}{(\lambda + \mu)^2} \times 2\lambda + \frac{\lambda^2}{(\lambda + \mu)^2} \times 2\mu \\
 &= \frac{2\lambda\mu}{(\lambda + \mu)}
 \end{aligned}$$

$$g_C = P_C \times \text{rate of departure}$$

$$\begin{aligned}
 &= \frac{\lambda^2}{(\lambda + \mu)^2} \times 2\mu
 \end{aligned}$$

$$g_C = P_B \times \text{rate of entry} = P_B \times \lambda$$

$$\begin{aligned}
 &= \frac{2\lambda\mu}{(\lambda + \mu)^2} \times \lambda = \frac{2\lambda^2\mu}{(\lambda + \mu)^2}.
 \end{aligned}$$

$$T_A = \frac{1}{g_A} = \frac{(\lambda + \mu)^2}{2\lambda\mu^2}, \quad T_B = \frac{1}{g_B} = \frac{(\lambda + \mu)}{2\lambda\mu}$$

$$T_C = \frac{1}{g_C} = \frac{(\lambda + \mu)^2}{2\lambda^2\mu}$$

State No.

A

B

C

Rate of Departure:

$2\lambda$

$\lambda + \mu$

$2\mu$

Rate of Entry:

$\lambda$

$2(\lambda + \mu)$

Let  $\gamma_1, \gamma_2, \gamma_3$  and  $\gamma_4$  be the frequency of encountering states 1 to 4 respectively.

The LSPs of the states 1 to 4 i.e.,  $P_1$  to  $P_4$  can be expressed as

$$P_1 = \frac{\mu_1 \mu_2}{(\gamma_1 + \mu_1)(\gamma_2 + \mu_2)}$$

$$P_2 = \frac{\gamma_1 \mu_2}{(\gamma_1 + \mu_1)(\gamma_2 + \mu_2)}$$

$$P_3 = \frac{\mu_1 \gamma_2}{(\gamma_1 + \mu_1)(\gamma_2 + \mu_2)}$$

$$P_4 = \frac{\gamma_1 \gamma_2}{(\gamma_1 + \mu_1)(\gamma_2 + \mu_2)}.$$

$$\begin{aligned}\gamma_1 &= P_1 \times \text{rate of departure} \\ &= \frac{\mu_1 \mu_2}{(\gamma_1 + \mu_1)(\gamma_2 + \mu_2)} \times (\gamma_1 + \gamma_2)\end{aligned}$$

$$\begin{aligned}\gamma_1 &\approx P_2 \mu_1 + P_3 \mu_2 \\ &= \frac{\gamma_1 \mu_1 \mu_2}{(\gamma_1 + \mu_1)} + \frac{\gamma_2 \mu_1 \mu_2}{(\gamma_2 + \mu_2)}.\end{aligned}$$

$$\begin{aligned}\text{Similarly, } \gamma_2 &= P_2 \times \text{rate of departure} \\ &= P_2 [\gamma_2 + \mu_1] \\ &= \frac{\gamma_1 \mu_2}{(\gamma_1 + \mu_1)(\gamma_2 + \mu_2)} \times (\gamma_2 + \mu_1)\end{aligned}$$

$$\gamma_2 = P_1 \gamma_1 + P_4 \mu_2$$

$$\begin{aligned}
 f_3 &= p_3 \times \text{rate of departure} \\
 &= p_3 \times (\gamma_1 + \mu_2) \\
 &= \frac{\mu_1 \gamma_2}{(\gamma_1 + \mu_1)(\gamma_2 + \mu_2)} \times (\gamma_1 + \mu_2)
 \end{aligned}$$

$$\begin{aligned}
 f_3 &= p_1 \gamma_2 + p_4 \mu_1 \\
 f_4 &= p_4 \times [\mu_1 + \mu_2] = p_4 \times \text{rate of departure} \\
 &= \frac{\gamma_1 \gamma_2}{(\gamma_1 + \mu_1)(\gamma_2 + \mu_2)} \times [\mu_1 + \mu_2]
 \end{aligned}$$

*mean duration*

$$f_4 = p_2 \gamma_2 + p_3 \gamma_1$$

$$m_1 = \frac{1}{\gamma_1 + \gamma_2} \quad m_2 = \frac{1}{\mu_1 + \gamma_2} \quad m_3 = \frac{1}{\gamma_1 + \mu_2}$$

$$m_4 = \frac{1}{\mu_1 + \mu_2}$$

<u>state</u>	<u>Rate of Departure</u>	<u>Rate of Entry</u>
1	$\gamma_1 + \gamma_2$	$\mu_1 + \mu_2$
2	$\gamma_2 + \mu_1$	$\gamma_2 + \mu_1$
3	$\gamma_1 + \mu_2$	$\gamma_1 + \gamma_2$
4	$\mu_1 + \mu_2$	

## Evaluation of Cumulative Probability, Cumulative Frequency & Equivalent Transition Rates :-

1. First obtain the individual state probabilities of each of state  $p_i$  &  $i = 1$  to  $2^n$ . where  $n$  is number of generating units. and obtain the capacity outage probability table.
2. Let  $f_i$  = frequency of encountering a state 'i'  
 $= p_i \times \text{rate of transition}$  &  $i = 1$  to  $2^n$
3. Let the identical capacity states be 'K' in number of the available states ( $K^{th}$  combined state). In each of the  $K^{th}$  combined state, the capacity of  $K^{th}$  combined state will be identical. Let 'g<sub>u</sub>' such capacity states are present in  $K^{th}$  combined state.

$c_1 = c_2 = \dots = c_u$  for  $K^{th}$  combined state.

The Combined probability of state 'K' is

$$P_K = \sum_{i=1}^{g_u} p_i$$

The frequency of  $K^{th}$  combined state K is

$$f_K = \sum_{i=1}^{g_u} f_i$$

$$= \sum_{i=1}^{g_u} p_i \times \text{rate of transition}$$

4. Equivalent Transitional Rates :- Equivalent failure rate :-

$$\gamma_{K-L} = \frac{\sum_{i=1}^{g_u} p_i \gamma_{Lij}}{P_K}$$

$$\lambda_{K-L} = \frac{\sum_{i=1}^{g_L} p_i \sum_{j \in L} \lambda_{ij}}{P_K}$$

$$P_K = \sum_{i=1}^{g_L} p_i$$

where  $\lambda_{K-L}$  is  $K^{th}$  combined state to its lower state ( $L$ ).

Equivalent Repair Rate :-

$$\mu_{K-H} = \frac{\sum_{i=1}^{g_L} p_i \sum_{j \in H} \mu_{ij}}{P_K}$$

$P_K = \sum_{i=1}^{g_L} p_i$  where  $\mu_{K-H}$  is  $K^{th}$  combined state to its higher margin state ( $H$ )

5. Cumulative Probabilities :-

Let there be 'N' combined states in the combined state model [lies b/w  $(n+1)$  to  $2^n$ ].

where  $n$  is the number of components.

Let  $p_A, p_B, \dots, p_N$  be the cumulative probabilities

of the combined states  $A, B, \dots, N$  respectively.

Where  $A$  is highest available capacity state

$N$  is lowest available capacity state

$p_{N-1}$  = Cumulative probability upto  $(N-1)^{th}$  state  
starting from  $N^{th}$  state

$$\therefore p_{N-1} = p_N + p_K$$

6. Cumulative Frequency :-

$$F_{N-1} = F_N + P_K [\mu_{K-H} - \lambda_{K-L}]$$

$$= F_N + P_K [(r_{n+K}) - (r_{-K})]$$

32. The prob density function

$$f(x) = \frac{2000}{x^3}, x > 100 \\ = 0 \quad \text{elsewhere}$$

Expected life  $E(x) = \int_{-\infty}^{\infty} x f(x) dx$

$$= \int_{-\infty}^{\infty} x f(x) dx$$

$$= \int_{100}^{\infty} x \cdot \frac{2000}{x^3} dx$$

$$= \int_{100}^{\infty} \frac{2000}{x^2} dx$$

$$= 2000 \left[ \frac{x^{-2+1}}{-2+1} \right]_{100}^{\infty} = -\frac{2000}{2} \left[ 0 - \frac{1}{100} \right]$$

Expected life = 20 years

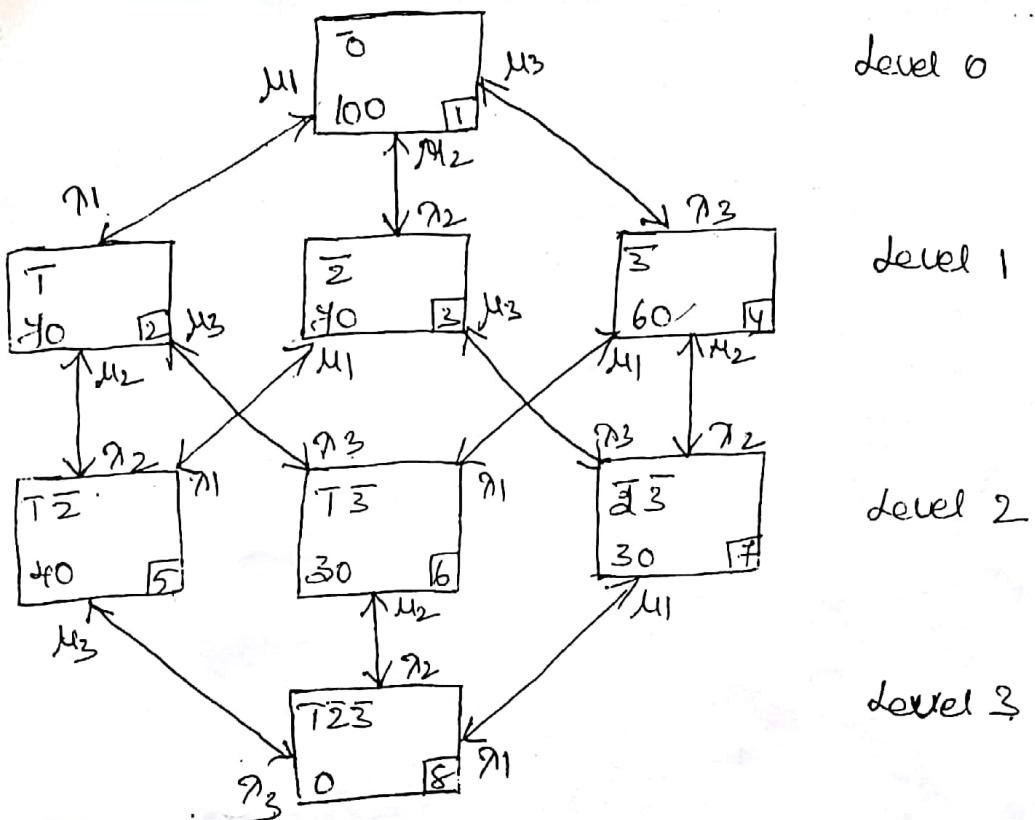
1A A generating station has 3 generators, two rated for 30 MW and the third of 40 MW. The failure and repairs rate of each unit are 0.5 /year and 9.5 /year respectively. Obtain the state space diagram and mark various transition rates. Hence evaluate the calculation probability and cumulative frequency of various merged states.

1	2	3	Total
30 MW	30 MW	40 MW	100

$$\lambda_1 = \lambda_2 = \lambda_3 = 0.5 \text{ /year}$$

$$\mu_1 = \mu_2 = \mu_3 = 9.5 \text{ /year}$$

$$\mu = \lambda/\lambda + \mu = 0.095 \quad U = 1 - A = 0.05^2$$



The probabilities are

$$P_1 = A^3 = (0.95)^3 = 0.85 + 345 -$$

$$P_2 = P_3 = P_4 = A^2 U = (0.95)^2 \times 0.05 -$$

$$= 0.047125$$

$$P_5 = P_6 = P_7 = U^2 A = (0.05)^2 \times 0.95 -$$

$$= 0.002375$$

$$P_8 = U^3 = (0.05)^3 = 0.000125$$

Frequency of transitioning to each state

$$f_1 = P_1 \times \text{rate of transition}$$

$$= P_1 [\gamma_1 + \gamma_2 + \gamma_3] = 1.2860625$$

$$f_2 = P_2 [\gamma_2 + \gamma_3 + \gamma_4]$$

$$= 0.4738125$$

$$f_3 = P_3 [\gamma_1 + \gamma_3 + \gamma_2] = 0.4738125$$

$$f_4 = P_4 [\gamma_1 + \gamma_2 + \gamma_3] = 0.4738125$$

$$f_5 = P_5 [\gamma_3 + \gamma_1 + \gamma_2] = 0.00063125$$

76

78

level 0

level 1

level 2

level 3

$$P_2 + P_3 + P_4 = 0.2860625 + 0.047125 + 0.002375 = 0.3355625$$

Eqn

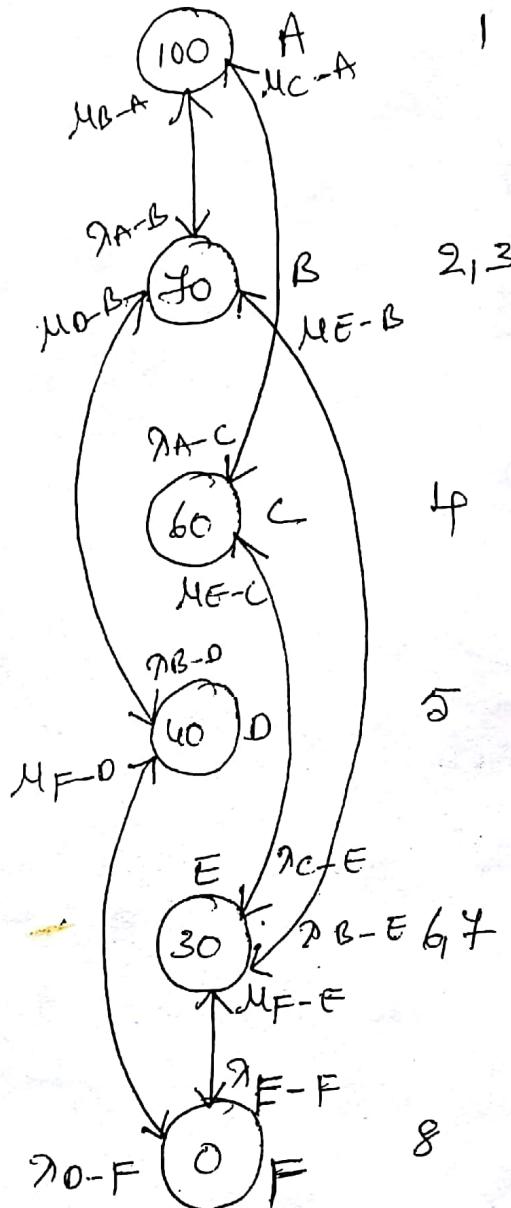
7

8

7B  
213

$$\gamma_6 = P_6 [\gamma_2 + \mu_1 + \mu_3] = 0.0463125$$

$$\gamma_8 = P_8 [\mu_1 + \mu_2 + \mu_3] = 0.0035625$$



Equivalent functioning rates :-

$$\gamma_{A-B} = \frac{P_1 [\gamma_1 + \gamma_2]}{P_1} = 1.0$$

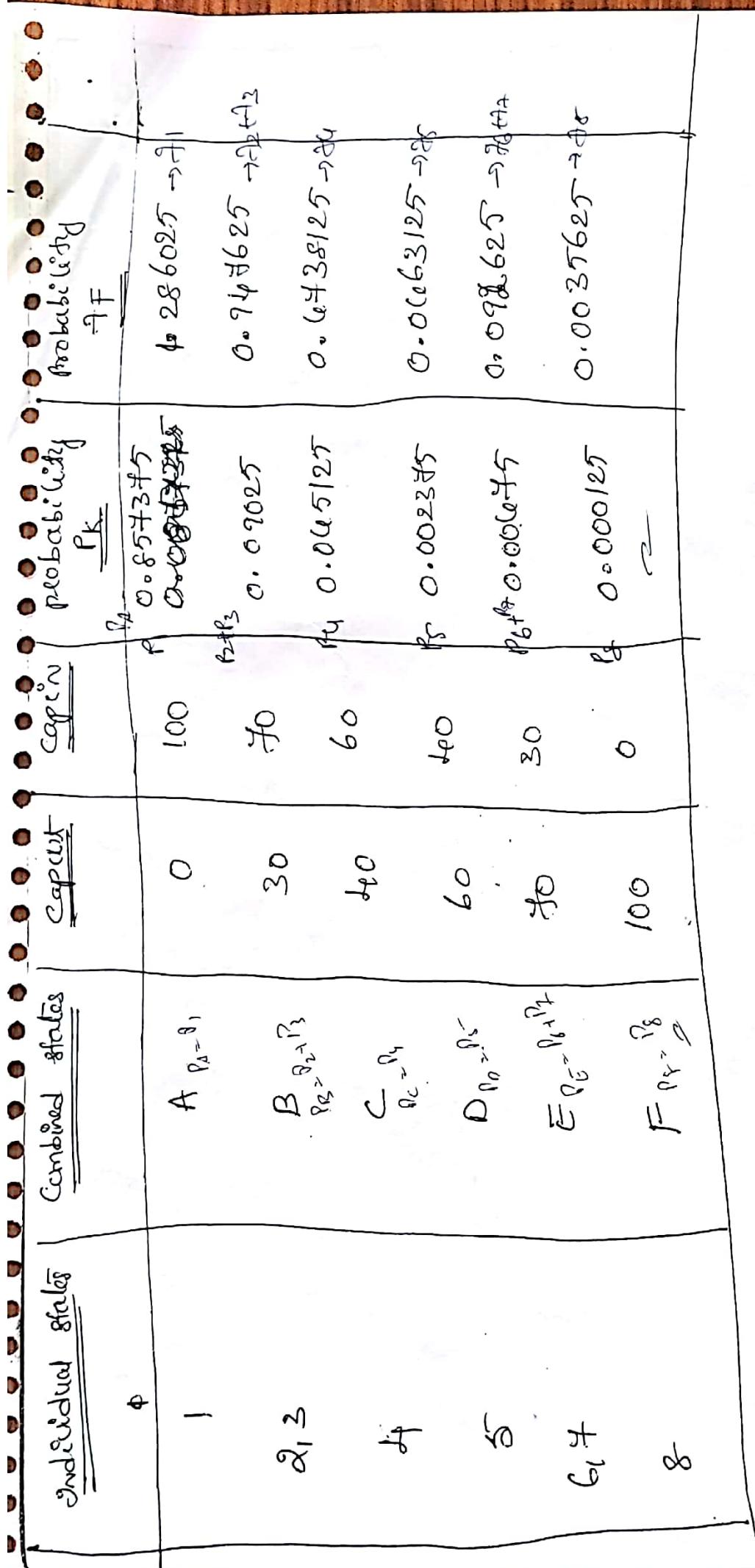
1 - 2, 3

$$\gamma_{A-C} = \frac{P_1 [\gamma_1 + \gamma_2 + \gamma_3]}{P_1} = 0.5$$

1 - 4, 5

$$\gamma_{B-D} = \frac{P_2 [\gamma_2 + \gamma_3 + \gamma_4]}{P_2 + P_3} = 0.5$$

2, 3 - 5



$$\lambda_{C-E} = \frac{P_4 [\lambda_1 + \lambda_2]}{P_4} = 1.0$$

$\lambda_F - 6.4$

$$\lambda_{D-F} = \frac{P_5 [\lambda_3]}{P_5} = 0.5$$

$5-8$

$$\lambda_{B-E} = \frac{P_2 [\lambda_3 + 0] + P_3 [\lambda_3]}{P_2 + P_3}$$

$2.3 - 6.4$

$$= 0.5$$

$$\lambda_{E-F} = \frac{P_6 (\lambda_2) + P_7 (\lambda_1)}{P_6 + P_7}$$

$6.4 - 8$

$$= 0.5.$$

Equivalent Repair Rates :

$$\mu_{F-E} = \frac{P_8 [\mu_2 + \mu_1]}{P_8} = 19$$

$8 - 6.4$

$$\mu_{F-D} = \frac{P_8 [\mu_3]}{P_8} = 9.5$$

$8 - 5$

$$\mu_{E-C} = \frac{P_6 [\mu_1] + P_7 [\mu_2]}{P_6 + P_7}$$

$6.4 - 4$

$$= 9.5$$

$$\mu_{C-A} = \frac{P_4 [\mu_3]}{P_4} = 9.5$$

$4 - 1$

$$\mu_{E-B} = \frac{P_6 [\mu_3] + P_7 [\mu_3]}{P_6 + P_7} = 9.5$$

$1 - 0.2$

$$\mu_{B-A} = \frac{P_2[\mu_1] + P_3[\mu_2]}{P_2 + P_3} = 9.5$$

P<sub>B</sub>

$$\mu_{D-B} = \frac{P_5[\mu_2 + \mu_1]}{P_5} = 19$$

P<sub>A</sub>

Cumulative frequencies and probabilities:

F<sub>A</sub>

$$P_{N-1} = P_K + P_N$$

$$F_{N-1} = F_N + P_K [\mu_{K-H} - \gamma_{K-L}]$$

1 pb

$$P_F = 0.000125$$

$$F_F = 0.0035625$$

$$P_E = P_F + P_E = 0.004875$$

$$F_E = F_F + P_E [\mu_{E-C} - \gamma_{E-F}] + \mu_{E-B}$$

1.

$$= 0.0914375$$

$$P_D = P_E + P_D = 0.00425$$

$$F_D = F_E + P_D [\mu_{D-B} - \gamma_{D-F}]$$

The

$$= 0.135375$$

$$P_C = P_D + P_C = 0.052375$$

$$F_C = F_D + P_C [\mu_{C-A} - \gamma_{C-E}]$$

2. !

$$= 0.5189375$$

The

$$\rho_B = \rho_c + \rho_B = 0.162625$$

$$F_{Bz} = F_c + \rho_B [ \gamma_{B-A} - (\gamma_{B-D} + \gamma_{B-E}) ]$$

$$= 1.2860625$$

$$\begin{aligned}\rho_A &= \rho_B + \rho_A = 1.0 \\ F_A &= F_B + \rho_A [ \gamma_{A-D} - [ \gamma_{A-B} + \gamma_{A-C} ] ]\end{aligned}$$

$$= 0$$