

OceanGliders Standard Operating Procedure (SOP)

Oxygen, version 0.3



OceanGliders

Authors

1. Patricia López-García, *Ocean Technology and Engineering Group, National Oceanography Centre, Southampton, UK*
2. Tom Hull, *Centre for Environment Fisheries and Aquaculture Science, Lowestoft, UK*
3. Soeren Thomsen, *LOCEAN, ISPL, Sorbonne University, Paris, France*
4. Johannes Hahn, *Federal Maritime and Hydrographic Agency (BSH), Hamburg, Germany*
5. Bastien Y. Queste, *Department of Marine Science, University of Gothenburg, Gothenburg, Sweden*
6. Gerd Krahnmann, *GEOMAR Helmholtz Centre for Ocean Research Kiel, Germany*
7. Charlotte Williams, *Marine Physics and Ocean Climate Group. National Oceanography Centre, Liverpool, UK*
8. Mun Woo, *IMOS Ocean Gliders, UWA Oceans Institute and Oceans Graduate School, The University of Western Australia, Perth, Australia*
9. Charitha Pattiaratchi, *IMOS Ocean Gliders, UWA Oceans Institute and Oceans Graduate School, The University of Western Australia, Perth, Australia*
10. Laurent Coppola, *Sorbonne Université, CNRS, Laboratoire d'Océanographie de Villefranche (LOV), 06230 Villefranche-sur-Mer, France*
11. Tania Morales, *Plataforma Oceánica de Canarias (PLOCAN), Canary Islands, Spain*
12. Virginie Racapé, *Institut Universitaire Européen de la mer CNRS-UMS 3113, IFREMER-coriolis, Plouzané France*
13. Claire Gourcuff, *Euro-Argo ERIC, Brest, France*
14. John Allen, *SOCIB, Palma de Mallorca, Spain*
15. Eva Alou-Font, *SOCIB, Palma de Mallorca, Spain*
16. Nikolaos D. Zarokanellos,* *SOCIB, Palma de Mallorca, Spain**
17. Victor Turpin, *OceanOps, Brest, France*
18. Catherine Schmechtig, *CNRS, Sorbonne Université, Osu Ecce Terra, Paris, France*
19. Pierre Testor, *CNRS-Sorbonne Universités (UPMC Univ. Pierre et Marie Curie, Paris 06)-CNRS-IRD-MNHN, UMR 7159, Laboratoire d'Océanographie et de Climatologie (LOCEAN), Institut Pierre Simon Laplace (IPSL), Observatoire Ecce Terra, Paris, France*
20. Julius Busecke, *Columbia University/Lamont-Doherty Earth Observatory, New York, USA*

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SOP development process

- 1) Initial SOP was drafted by Patricia López-García, Tom Hull, Soeren Thomsen and Johannes Hahn.
- 2) Two expert sessions during OceanGliders Best Practice Workshop, May 11 - 25 2021. Additional authors joined: Bastien Y. Queste, Gerd Krahmann, Charlotte Williams, Mun Woo, Charitha Pattiaratchi, Laurent Coppola, Tania Morales, Virginie Racape, Claire Gourcuff, John Allen, Eva Alou, Nikolaos D. Zarokanellos
- 3) First community and user feedback was provided during the OceanGliders Best Practice Workshop, May 11 - 25 2021 by attendees.
- 4) SOP moved to this repository by: Patricia López-García, Tom Hull, Soeren Thomsen in September 2021.
- 5) Additional authors joined on GitHub prior to the community review: Victor Turpin, Catherine Schmechtig, Pierre Testor, Julius Busecke
- 6) Next step: 4 months community review on GitHub starting in October 2021.

Introduction

This standard operating procedure (SOP) document for dissolved oxygen (DO) aims to guide the user through the steps necessary for collection of good quality dissolved oxygen using gliders for both real time and post deployment data streams.

Table 1: List of the known sensor/glider combinations. We aim to cover all combinations in this document.

Sensor / Glider	Slocum	Autosub/ ALR (NOC)	Seaglider	Deepglider	SeaExplorer	Spray	Information
Aanderaa 3835, 4330, 4330F, 4831, 4831F and 5013 optodes	X		X	X			Link
RINKO-II	X				X		Link
RINKO- AROD FT					X		Link
SBE 43 and 43F		X	X		X		Link
SBE 63						X	Link
RBRcoda					X		Link
T.ODO							
Contros			X				Link
Hydroflash (1)							

(1)The advanced, optical sensor is based on the principle of fluorescence quenching. Contros are no longer in operation, the sensors cannot be calibrated so they are likely to become obsolete.

Aanderaa Optodes

Aanderaa optodes are the most widely used oxygen sensor on gliders and a large body of work has now been dedicated to their characterisation (e.g. (Bittig et al. 2018)). These sensors are based on the oxygen luminescence quenching of a platinum porphyrin complex (fluorescent indicator) that is immobilized in a sensing foil. These offer low power consumption, good long-term stability, low fouling sensitivity while not being sensitive to H₂S or freezing. Aanderaa optodes have seen several important developments since they were introduced in 2002, with

various hardware and firmware revisions which we outline below (shown in figure 1).

Hardware design: blue or black

While mostly cosmetic, the colour of the optode is a useful short-hand for the two main optode designs. The 3835 and 4835 optodes both feature a black housing with the temperature sensor integrated into the base of the sensor near the connector. This results in a large thermal mass and increases the response time of the temperature sensor significantly. The blue 4330 and 4831 sensors move the thermistor next to the sensing foil which results in much improved performance of the temperature sensor. All optodes other than the 4831 use a 10 pin Lemo connector, these connectors can't be connected when wet and are prone to crevice corrosion. The 4831 is therefore recommended with it's Subconn wet-pluggable connector. Older optode versions (3830) have a titanium housing in the same form factor as the 3835. Some early Slocum gliders were delivered with optodes of type 5013, these are identical to the 3830.

Foil type: F or standard

Most optodes use the PreSens PSt3 foil (PreSens - Precision Sensing GmbH), these have as standard a black opaque protective layer protecting the pink sensing layer. For glider applications the "F" type foils are typically preferred as these remove the opaque layer which results in much faster diffusion across the foil, and therefore faster sensor response (8 s compared to ~ 25 s (Bittig et al. 2014)). However, removal of the protective layer makes the foil more susceptible to UV radiation, and is known to reduce the sensor stability, especially when exposed to strong sunlight. Newer 4330F and 4831F optodes (Since July 8th 2018) use an improved formulation of the Presens fast foil which are less sunlight sensitive and have much lower noise levels. These can be identified by their white appearance. It is recommended that older F-type instruments (with the pink foils) are upgraded with these improved foils. Otherwise foils should typically not be replaced unless mechanically damaged (light intrusion) as older foils perform better, with less drift than new ones.

Calibration equation and firmware versions

The way optode foils are initially calibrated by Aanderaa, and how the measured values are processed by the optode varies between different optode versions. The optode illuminates the sensing foil with both a red and blue LED. Since the red light does not produce fluorescence in the foil the phase measurements are obtained from the difference between the blue (P1) and the red (P2) excitation.

$$P_T = A(T) + (P1 - P2) \cdot B(T)$$

Where P_T is the temperature compensated phase (known as 'TCphase'). A and B are temperature dependent coefficients which allow for temperature compensation of the phase measurement. However for most 4330, 4831 and 4835 optodes these are not used, such that $A(T) = 0$ and $B(T) = 1$. This can be confirmed by communicating with an optode and inspecting the 'PTC0Coef' and 'PTC1Coef' properties. For older optodes (4330 serial numbers < 1000) the temperature compensated phase is then used to calculate 'calphase' (P_c). For newer optodes $P_T = P_c$. Similarly older optodes have their calibration (and recalibration) applied though the modification of the 'PhaseCoef' coefficients. On later optodes the calibration is not applied in phase space, but on the oxygen concentration though the use of the 'ConcCoef0' and 'ConcCoef1' coefficents ('PhaseCoef0' and 'PhaseCoef1' are set to zero and 1 respectively). Consult your optode calibration sheet and confirm which terms are being used. There are three different calibration equations used to convert the measured phase to oxygen equations: The "Mk1" equation used by the older 3835 optodes uses a 5x4 matrix of coefficients. The "Mk2" equation is used by non-multipoint calibrated 4330(F) and 4835 optodes, and uses a 2x14 matrix (FoilCoefA and FoilCoefB) together with a 2x27 matrix for the polynomial degree, this second matrix is the same across all of these type optodes. Newer multipoint calibrated optodes use the Stern-Volmer (SVU) equation proposed by (Uchida et al. 2008) which has 6 terms. Non-multipoint foil calibrations are based on a common characterisation of a production batch. Multipoint calibrations consist of 40 calibration points across a range of concentrations and temperatures and offer improved accuracy and should be preferred when purchasing these sensors. Consult your optode foil calibration document to verify which version your optode is using. Understanding these differences in how the calculations are performed is important when recalculating oxygen from the phase readings, such as when compensating for lag. Regardless of the optode version, oxygen can be recalculated from calphase using the approach of (Uchida et al. 2008). During the initial months of storage/use a Foil maturation process occurs resulting in lower readings by several %. The maximum observed maturation induced drift on more than 1000 sensor has been 8 % for sensors with non-factory

pre-matured WTW foils (model: 4835, 4531 and 5730 Steinsvik) and 6 % for sensors with factory pre-matured PSt3 foils (model: 4330, 4831, 5331 hadal). During/between field deployments there are possibilities for end users to post-adjust the sensors either by a one-point air-saturation adjustment or by taking reference samples (e.g. water samples and Winkler titration) and/or using a well-calibrated sensor in parallel. If done correctly such an adjustment should result in an absolute accuracy of around 1 % for multipoint calibrated sensors (model: 4330, 4831, 5331 and 5730) and 3 % for two-point calibrated (model: 4835, 4531), see below for more information about factory calibrations. The drift will decrease over time so that during the second year it is not likely to be more than 1-2 %. After this it should be less than 0.5 % per year, unless the foil is mechanically damaged (Aanderaa).



Figure 1: Suit of smart optodes sensors. (Image was taken from the manufacturer webpage www.aanderaa.com)

RBR coda T.TODO

The RBRcoda T.TODO uses the same foils and methods as the 4831 and 4831F so everything above specified for the 4831 will also apply to those instruments as well. RBR refers to the standard optode (~30 s tau) foil as “slow” and the fast (~8 s) as the standard. They also use further foil design (~1 s response) which they call fast. The RBR sensor has a smaller form factor than the Aandera optodes, but is overall more similar to a 4831 with the temperature sensor very closely located to the sensing foil. This sensor is still fairly recent on gliders and little is known for now.

JFE Advantech RINKO

AROD-FT sensor (RINKO JFE) is used for the SeaExplorer gliders (Alseamar) and for some Argo floats (small size and low power consumption). This sensor is based on the optical (phosphorescence) principle which is now widely known as a remarkably fast response oxygen sensor (below 1s) with a high accuracy of 2 mumol/kg. This sensor used a multi-points calibration (16 points with 4 temperatures and 4 DO concentrations). In this procedure, the DO reference standards are produced by saturating the primary mixtures with DO concentrations of approximately 4%, 10%, 17% and 25% respectively (certified by the National Metrology Institute of Japan).

The DO concentration is calculated from the (Uchida H. and McTaggart 2010) equation with 9 calibration coefficients. A second equation is used to take into account the pressure effect (linear equation with one calibration coefficient). Finally, the salinity-compensated DO concentration is calculated by multiplying the factor of the effect of salt on the oxygen solubility (Benson and Krause Jr. 1980) and (Garcia and Gordon 1992). This is similar to procedures used on other optodes.

Recent deployments of a SeaExplorer glider equipped with an AROD-FT sensor have shown long-term stability (low drift over time) but with a significant offset observed during sections in the Ligurian Sea (on average 10-15 mumol/kg). Deployments in the Bornholm Basin have shown good agreement across a wide range of oxygen concentrations with a nearby BOOS monitoring station; this sensor was a recent acquisition and had little opportunity to drift in storage.



Figure 2: AROD-FT sensor mounted on a SeaExplorer glider (credit: ALSEAMAR)

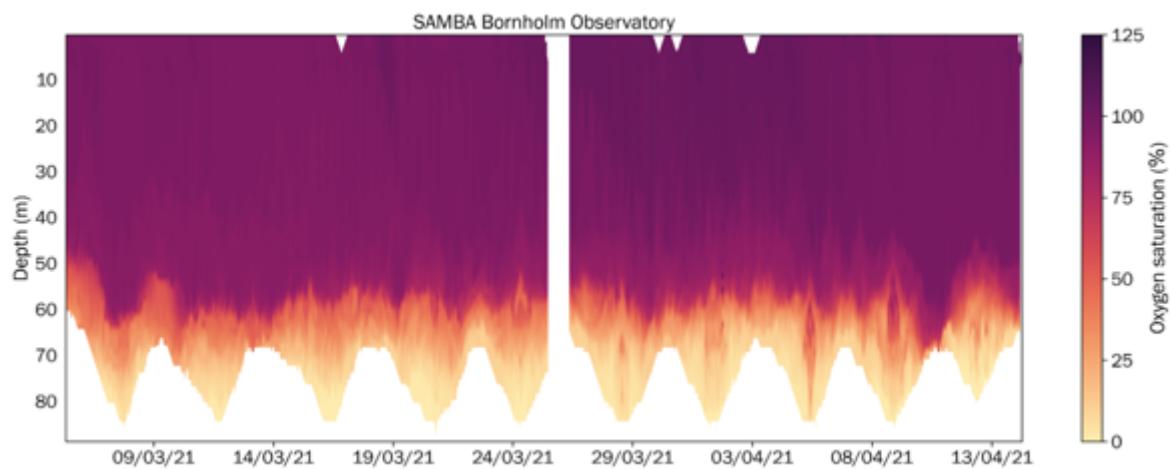


Figure 3: Oxygen saturation from a Rinko AROD-FT on a SeaExplorer glider in the Bornholm Basin (credit: Voice of the Ocean Foundation and University of Gothenburg).

Clark electrode polarographic sensor (SBE43)

- input from expert needed here

Pre-deployment operations and calibrations

Storage and cleaning

Optode foils typically drift more while in storage than while in use, the reasons for this are thought to be due to exposure to UV radiation and dry air (Bittig et al. 2018), (AS 2018). We recommend that all optodes should be stored away from the light (especially fluorescent lights), keep the foil humid and use the plastic caps provided with the sensor. Two-point calibration prior to deployment is always recommended. Sensors should be cleaned before storage and stored with black caps on including some tap water, or with a piece of wet cotton taped against the foil. If sensors are stored dry the foil will dry out which could lead to 1-2 % lower readings. The sensor then needs to be placed in water to hydrate at least 24 h prior to starting field measurements again.



Figure 4: Keeping sensor in small beakers before and during calibration process. Only the membrane will need to be submerged in distilled water.

After recovery the sensor and to remove any biofouling, this is the protocol recommended by the manufacturer: 1. If the sensor has been for too long exposed to the air, leave it overnight in a vinegar solution. 2. Next day, place the sensor in soapy water and use a brush gently if it is necessary to remove all material adhered to the surface. 3. Rinse very well with clean water and dry carefully.

NOTE: Don't change the foil unless it is physically damaged.

Sensor configuration for deployment

Salinity configuration: 0 PSU. For optode sensors: when there is a small variation in salinity (less than 1 g/kg), it can be set to the mid value avoiding the need of salinity compensation. However, even in that case, it is a good practice to set salinity to 0 for two reasons: 1) it is usually difficult to find the salinity value defined for old deployments and 2) in case the equations change, it would be easier to recalculate oxygen values from uncompensated values.

Sensor integration with gliders

Optodes should be configured to record the intermediate parameters (calphase and temperature), not just oxygen. Accurate time-stamps, or offsets relative to CT measurements must be recorded for performing the lag correction.

Mounting location

Spray

- input from expert needed

Seaglider On Seagliders the oxygen sensor is normally mounted externally behind the CT sensor (see figure 5). Given this exposed location it is important to mount the optode with the sensing foil facing away from incident light to avoid unnecessary UV exposure.



Figure 5: UEA OGIVE seaglider with 4330F optode, together with NOC LoC spectrophotometric pH, unpumped SBE CT and Fluidion potentiometric pH sensor.

Slocum On slocum gliders the oxygen optode is typically installed aft close to the fin (figure 6).

However this positioning is not ideal for oxygen measurements due to the optode being within a region of laminar flow (Moat et al. 2016), additionally the optode response time has been observed to be dependent on the sensor orientation relative to the direction of flow (Bittig et al. 2014).

An alternative mounting of the Aanderaa optode in a more prominent location fore of the glider fin has been demonstrated as being much more suitable for measuring oxygen on gliders (Fig. 7) (Nicholson and Feen 2017). This mounting location means that the sensor foil faces the flow directly and therefore the diffusive boundary layer thickness at the optode membrane is minimised, reducing the optode response time. Furthermore, this mounting location also means that in-situ in-air calibrations can be performed during deployment (similar to those done with Argo floats) which are beneficial when processing the DM oxygen data (see ‘in-air calibration’ section).

SeaExplorer On SeaExplorer gliders, all existing oxygen sensor integrations are installed in the forward wet payload section (the nose cone). External mounting is also feasible using external puck mounts on the dry payload, located approximately 1/3 of the way back, but is rare and generally only used for instrument trials. The Rinko AROD-FT is generally installed on the forward starboard connector, with the sensing foil and temperature probe 15 centimeters back from the tip of the nose and lightly sheltered to avoid damage when making contact with the nose. Both the foil and temperature probe are well exposed to flow. The new RBR Coda integration is also planned to present the foil and probe slightly set back from the tip of the nose, while remaining exposed to unmodified flow. The SBE43 is found only when accompanied with a Seabird pumped CT sensor; both of these sensors are placed in the nose where the RBR Legato CT sensor can be seen in the figure below.

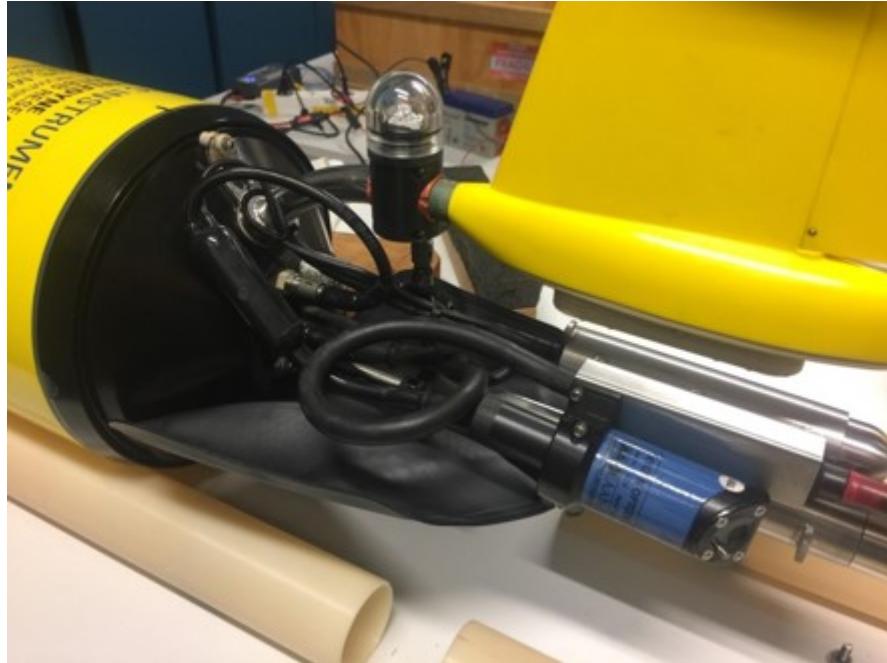


Figure 6: Standard Aanderaa optode 4831 mounting under the fin of the Slocum G2.



Figure 7: Slocum glider showing alternative mounting of an Aanderaa optode perpendicular to the fin.

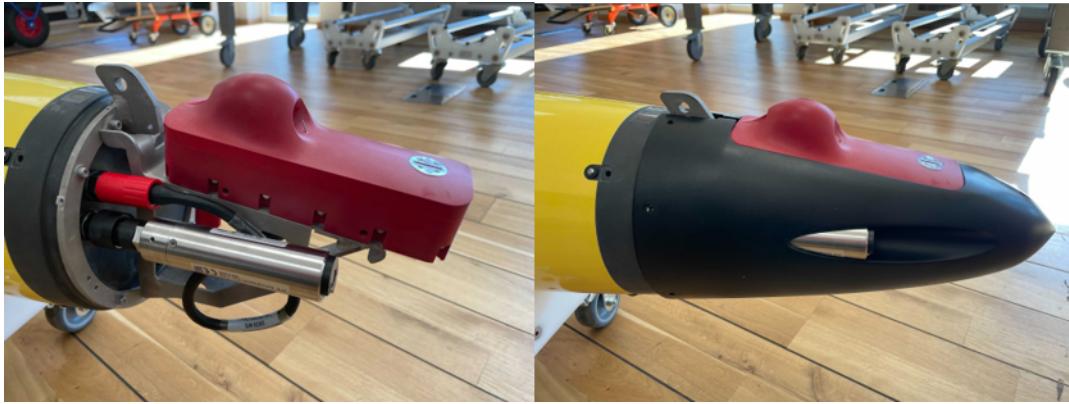


Figure 8: Rinko AROD-FT in the flooded nose cone payload bay of a SeaExplorer next to an RBR Legato sensor.

Antifouling

Materials immersed in water experience a series of biological and chemical processes, resulting in the formation of complex layers with attached organisms. This biofouling can be divided into microfouling and macrofouling (Delgado, Briciu-Burghina, and Regan 2021).

In optodes sensors, biofouling can be severe enough to block oxygen molecules from entering the sensing foil. Aanderaa has different solutions that have been successfully applied, some includes:

- 1) Copper tape (e.g. 3M 1181) or Copper/Nickel (last much longer) are easy antifouling solutions. When applying the tape, be sure that it is not in contact with any other metal parts otherwise, the tape will lose its antifouling properties.
- 2) Paints / coatings - optical sensors, so these can only reduce growth nearby but not on the actual sensing foil.
- 3) Ongoing trials: Aanderaa is focusing on non-toxic methods like fiber/hair cloth and “shark skin” film.

Mechanical wipers or UV radiation based approaches are generally unsuitable for gliders due to their increased power requirements and drag.

Regardless of whether efforts to prevent fouling are made, it is vital that post-recovery photographs are taken of the optode so that the impact of biofouling can be assessed during DMQC.

Air saturation quality check

Based on in-air calibrations on Argo floats and gliders (Bittig and Körtzinger 2015), (Johnson et al. 2015), (Nicholson and Feen 2017) and (Bittig et al. 2018) a simpler method has been recommended by the manufacturer to do it before and after deployments (Aanderaa Best Practices for Maintaining High Data Quality). This could be used during campaigns. This won't be useful if sensor foil is not wet or the temperature of the foil is different from that measured with the temperature sensor. You will need to leave the sensor logging outside in the free air for several hours before and after deployment. Remember to save the air pressure.

NOTE: At sea level at standard air pressure (101.3 kPa = 1 Atm = 14.69 psi) the sensors should show 100 % if wet and 102 % if completely dry; at air pressure 100 kPa it should show $(1.3/101.3)100 = 1.3\%$ lower.

NOTE: It is highly recommended to do this protocol at night when humidity is higher and the temperature is lower and more stable.

Pre-deployment calibration

Optodes and similar instruments generally drift more while in storage than they do in-situ. It is therefore essential that these instruments are recalibrated prior to each deployment. This is generally true even if in-situ reference (Winkler) samples are going to be taken as reference samples often won't cover the full range of oxygen concentrations seen during the mission. As the instrument drift manifests as an increasing offset from zero in addition to a reducing sensitivity, a two point calibration is required to rescale the optodes measuring range.

Two point calibration procedure, optode example

This protocol is recommended to do for at least two different temperatures, which cover the expected in-situ temperature range. There are several possibilities in order to achieve this, some examples: 1. Doing the experiments in labs with different temperatures. You need to leave all materials, reagents and sensors in the lab/workshop/room at least 8 hours (e.g. overnight) before starting the calibration. 2. Doing the experiment in the lab and changing the temperature. This is possible if the lab has an AC that we can turn on/off or change the temperature easily. You need to leave all materials, reagents and sensors in the lab at least 8 hours (e.g. overnight) before starting the calibration. 3. Doing the experiment using a thermostatic bath. You need to leave the 0 and 100% solutions in the bath at least overnight before starting the calibration. In this case, because we won't be able to use a magnetic stirrer, we need to be sure we place the end of the bubble tube in the bottom of the bottle/beaker.

In situ intercomparisons will be required to find the outset of the sensor in different seawater conditions. Therefore, samples should be taken in the tank during the ballasting (if this is 1-2 days before deployment, no more) and at the deployment/recovery site (ideally at different depths).

NOTE: A multipoint DO calibration is necessary to obtain new foil coefficients and that can be done at the manufacturer laboratories or in any fully equipped calibration lab. These values shouldn't be changed otherwise.

The Winkler method is used to determine the concentration of dissolved oxygen in discrete water samples which is a highly accurate method for determination of dissolved oxygen ($\pm 0.15 \text{ } \mu\text{mol kg}^{-1}$). We recommend to follow the GO-SHIP protocol described by (Langdon 2010) and a well trained technician to do the sampling and analysis.

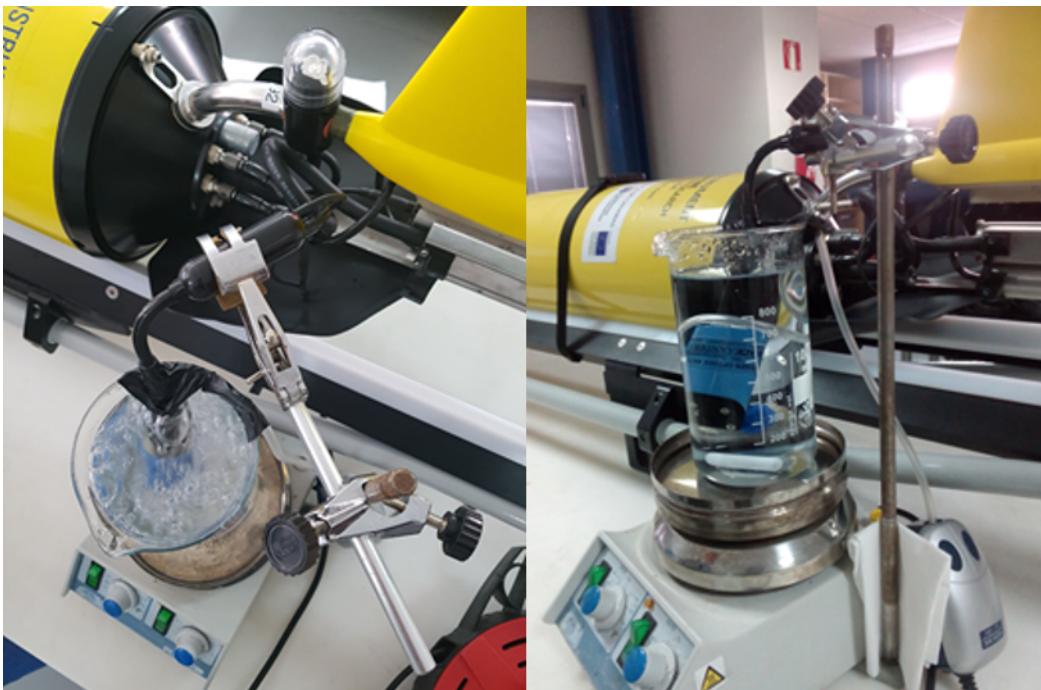


Figure 9: During 100% and 0% calibration.

Issues with Winkler method at low oxygen concentrations (below 1 μM , some researchers consider that values below 20 μM shouldn't be used for the sensor calibration): - There are various issues with Winkler at low oxygen concentrations as Winkler always biases towards too high oxygen: the detection limit of the method is around 1 μM (Langdon 2010), the oxygen absorbed in the plastic of the Niskin bottles might be transferred to the water sampled (reference needed). - Within the core of the Peruvian oxygen minimum zones oxygen concentrations at nmol levels are present other approaches for 0 % in-situ calibration (Revsbech et al. 2009) and (Thomsen et al. 2016). - STOX sensor, new lox-oxygen sensing foils (0-10% saturation) from Aanderaa.

100 / 0 % saturation protocol This method is necessary to check drift over time as the foil wears out. It's recommended to do it before the deployment and after recovery. NOTE: Sensor foil must be wet during all processes. Some information to read before we proceed with the calibration: 1. For a 100 % bubbled bath, connect an aquarium

pump to a tube which has been fitted with a porous stone (bubble dispenser) at the end. This will create small air bubbles that are sufficient to equilibrate the water rapidly. NOTE: It is important that the aquarium pump takes in air from an open atmosphere outside, not from inside the room/laboratory where O₂ levels will be affected by the on-going activities and/or the ventilation. To verify that optodes are in saturated water you can take them up from the water and hold them just above the surface for a few minutes. There should then be no change in the saturation readings (Aanderaa Best Practices). 2. For 0 % saturation solution, add 20 g sodium sulphite to approx. 1 L. Sodium sulphite rapidly removes the oxygen and, as long as crystals of the compound can be seen, the oxygen level in the water will stay at 0. Sodium sulphite also has the advantage of being inexpensive and the level of toxicity is low. This solution is considered irritating and wearing appropriate PPE (gloves, goggles and lab coat) is recommended. There is also an option of removing the oxygen from the water bubbling nitrogen all time. In this case you have to be sure all oxygen is removed from the solution, this will happen after 3-5 minutes bubbling (maximum volume of 100 mL approx., for bigger volume you will have to increase the time). You have to keep injecting N₂ during all time of the zero calibration. 3. If any residue of the sodium sulphite solution remains on the sensing surface, the 100 % measurement will be inaccurate. Therefore, 100 % DO saturation calibration should be performed first. To avoid contamination, always rinse well with distilled water. 4. Immerse the sensor in the 100 % bath overnight. If this is not possible, having the sensor submerged in distilled water will be enough to keep the foil wet for the calibration. 5. Always check saturation values: an outset of ± 5 % is adequate, so a value between 95 to 105 % is correct. 6. While calibrating, measure air pressure and water temperature to calculate the DO saturation estimated at current pressure. When we are on board of a ship and would like to use the data from the ship weather station, we need to check where the calibration is taking place: lab air pressure will be influenced by air conditioning systems, location of the lab (at sea level or in decks below), size and occupancy of the lab, among others. These considerations should be taken into account when working in onshore labs also. Therefore, having a portable weather station is highly recommended. For measuring temperature, a sonde with the same or better precision as the glider sensors must be used.

Communicating with the sensor using a terminal program and a cable When the DO sensor is disconnected from the glider: 1. Connect the sensor to a PC by using a Sensor Cable (Cable #3855 for 4330/4835 optodes, Cable #5335 for 4831). 2. Start a terminal program with the following set-up: 9600 Baud 8 Data bits 1 Stop bit No Parity Xon/Xoff Flow Control 3. If using Tera Terminal Pro, after setting up the com port according to settings above please select “Terminal” in the “Set up” menu and click “Local echo” also select “CR+LF” for both “Receive” and “Transmit” under “New line”. To stop, type ‘Do Stop’. 4. Once the sensor is measuring, continue with the procedure (see section Calibration Procedure).

There is also a possibility of using a Data Logger while we are working with the sensors.

image file missing

Figure X: Recording data using a terminal program (left image) and using a data logger (right image).

Calibration procedure Materials: Distilled water, aquarium pump, 1L and small volume beakers, stirrer and magnetic stirrer, BOD bottles, Winkler reagents, sodium sulfite solution, pipettes and tips, barometer, termometer.

Type *Get All* command for saving the initial sensor configuration to be able to restore old values in case something goes wrong.

1. With the sensor submerged in the 100 % water, connect to it and start measuring. Set the Interval property to 30 seconds. (This interval is recommended during the calibration to reduce the risk of self heating in the small container).

Set Passkey(1000)

Set Interval(30)

Save

2. Wait until both the temperature and the phase measurements are stabilized.
3. Store calibration values by typing:

```
Set Passkey(1000)
```

```
Do CollectCalDataSat
```

The Save command is automatically performed.

4. Set the CalDataAPress property to the actual air pressure in hPa at the site:

```
Set Passkey(1000)
```

```
Set CalDataAPress (...)
```

```
Save
```

5. Take 2 samples for Winkler measurement.
6. Dry the sensor carefully (make sure that the sensing foil is free from air bubbles) and immerse it in 0 % bath (0 % almost always reads correctly and is part of the calibration process). Wait until both the temperature and the phase measurements have stabilized (approx. 3 min).
7. To store calibration values for 0 %:

```
Set Passkey(1000)
```

```
Do CollectCalDataZero
```

The Save command is automatically performed.

8. To accept the new calibration and store the new coefficients in the sensor:

```
Set Passkey(1000)
```

```
Do Calibrate
```

The Save command is automatically performed.

9. Rinse well with distilled water and dry the sensor foil carefully and check how it works at air. Save the data to check the sensor performance through time (a barometer is needed). Value of oxygen saturation should be 100 % or higher.
10. Put the sensor back into the 0 % water, the reading should drop to zero.
11. Set back the Interval property to 1 second (or the desired sampling frequency).

```
Set Passkey(1000)
```

```
Set Interval(1)
```

```
Save
```

12. Type Get All command for saving the final sensor configuration for reference.

In situ intercomparison in the tank during ballasting

This is an extra in situ intercomparison to carry out if access to the tank while ballasting the glider is possible and the ballasting is close in time to the deployment (no more than 1-2 days before) (reference PLOCAN).

Materials: Silicon tube for sampling, multiparameter sonde, BOD bottles, Winkler reagents, pipettes and tips (or a bottle-top dispenser for reagent bottles), titration material (buretes or titrator).

1. The sensor should stay overnight submerged in water to make the membrane wet. If the sensor is already mounted in the glider, use a wet sponge. *NOTE: Keep the sensor in the dark all time.*
2. Once the glider is in the ballasting tanks, place the silicon tube for sampling near the sensor.
3. Once the sensor measurements are stable (variations in the measurements are not higher than the precision/resolution of the sensor), start sampling water for Winkler analysis. Take samples every 5-10 minutes, in total 4-6 samples will be required. *NOTE: Record the time we collect a sample for Winkler titration.*

4. A multiparameter sonde with a DO sensor whose precision is less than 0.1 % can be measured in the tank near the glider's sensors (record at least values for Temperature, Conductivity and DO). *NOTE: Some DO sensors consume oxygen so, in this case, it's recommended to move the sonde often to renew the water so the DO value does not decrease.*
5. Check the outset of the sensor by comparing values measured by the Optode sensor with Winkler values after measuring the bottle samples in the lab.



Figure 10: Taking samples for Winkler analysis during ballasting in the glider tank at PLOCAN facilities

Missions execution

This section covers the activities of those deploying and recovering the gliders in the field in addition to best practices for glider pilots.

Deployment

While keeping the oxygen sensor protected from sunlight and kept moist any lens cover must be removed prior to deployment, use of highly visible material, such as a red flag, can aid in ensuring its removal in addition to the pre-deployment checklist.

In-air measurements prior to deployment can and should be carried out together with the in-situ air pressure and relative humidity measurements to provide an additional reference for calibration. Details of this procedure can be found in section in-air-calibration.

In-situ reference samples

Even with good ballasting it can require several dives for a glider to fly correctly with an ideal dive profile. In warm and dry conditions the optode foil can still partially dry out even if good care is taken. Reference data should therefore only be performed after the glider is flying well, and ideally as close to the glider's last known position as possible. Ideally multiple sets of samples should be taken unless the horizontal variability of the deployment region is very well characterised. This requires coordination between the deployment team and the glider pilot and should be part of the mission planning.

In situ intercomparison during deployment/recovery from a small boat.

Materials: Silicon tube for sampling, Niskin bottles, multiparameter sonde, BOD bottles, Winkler reagents, pipettes and tips, cooling box. It is very important that the sensor has been kept wet before the deployment and after recovery. This can be done by placing a wet sponge in the sensor membrane at least 8 hours before the deployment (ensure that it doesn't get dry).

NOTE: Remember to remove the sponge and any other material used to keep the sensor wet.

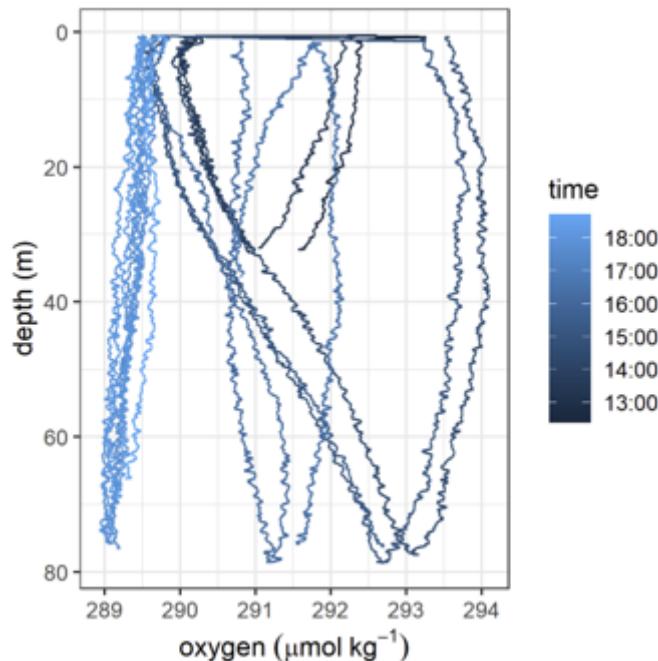


Figure 11: Effect of dry foil, first dives show elevated oxygen concentrations and slow foil response times. taken from AlterEco AE2 Slocum “Stella” using a 4330 optode (standard foil).

Samples should be collected with the Niskin bottle(s) for Winkler analysis during the deployment (following (Langdon 2010) protocol). It's recommended to take between 4-6 samples on the surface (approx. 5m) (ideally samples will be taken at different depths). After adding the Winkler reagents, samples should be kept in the dark and try to avoid high temperatures. It's also recommended to use a calibrated multiparameter sonde to do DO profiles at the deployment site while taking samples with the Niskin bottles. This will also help to record the sampling depths. When taking samples for the Winkler is not possible, values from the multiparameter sonde might be useful for in situ intercomparisons. The sonde must be calibrated before and after the deployment/recovery (some sondes require to be calibrated the same day, please follow manufacturer recommendations).

Calibration during deployment/recovery from a ship with a CTD rosette equipped with a calibrated oxygen sensor

If the glider is deployed/recovered from a research vessel equipped with a CTD and a calibrated O₂ sensor, the glider optode can either be connected directly to the CTD profiler if able to receive the digital (RS232) output from the Optode (Uchida H. and McTaggart 2010), or attached via a data logger. Record down- and upcast data to allow hysteresis correction. The Optode data obtained during the bottle-firing stop for collection of water samples can be used for in situ calibration, since the difference between the downcast and upcast oxygen profiles is relatively small (1 uM approx., (Uchida et al. 2008)). The error in the Optode can be reduced by allowing sufficient time for the sensor equilibration after the stop (minimum 2 min as recommended by (Hahn et al. 2014)). *NOTE: For Oxygen Minimum Zone regions follow recommendations in the section below.*

To summarize, the steps we recommend to follow to calibrate oxygen sensors during regular CTD/O₂ casts before deployment and after recovery, are:



Figure 12: Coastal deployment of a Slocum glider from a small boat (photo taken during the Glider School at PLOCAN).



Figure 13: Using a multiparameter sonde for in-situ intercomparison during deployments from small boats.

- 1) Attach the glider's O₂ sensors (optodes) to the CTD rosette at the same depths where the CTD oxygen sensor pumps in the water.
- 2) Record down- and upcast data. Timestamps of oxygen measurements are required. In case a logger is used, ensure before the calibration cast that the internal logger time is correct (i.e. in line with the CTD time).
- 3) Collect calibration points against measurements with the CTD rosette oxygen sensor, which itself is calibrated against Winkler titrated water samples (Langdon 2010).
- 4) Reference points for calibration are the same as the calibration stops. As for salinity, samples for Winkler titration will be collected during the upcast. When reached the selected depth, wait at least 2 min to ensure an equilibrated oxygen sensor (Hahn et al. 2014). Fire the bottles after this time.
- 5) Do 0 % and 100 % calibration after recovering the sensor at two different temperatures (warm and cold lab). If 100 % is not possible, 0 % should be done to ensure that the central temperature range at zero oxygen is covered within the calibration (Hahn et al. 2014).

The combined data collected following these (CTD and lab calibration) steps will be used to evaluate the calibration coefficients and it's called hypercast calibration.

NOTE: This calibration should be done before the deployment and after the recovery. It's important that the membrane is kept wet.

NOTE: Save all data from the profiles and calibrations before deploying the glider. Always record Dphase (Coppola 2013).

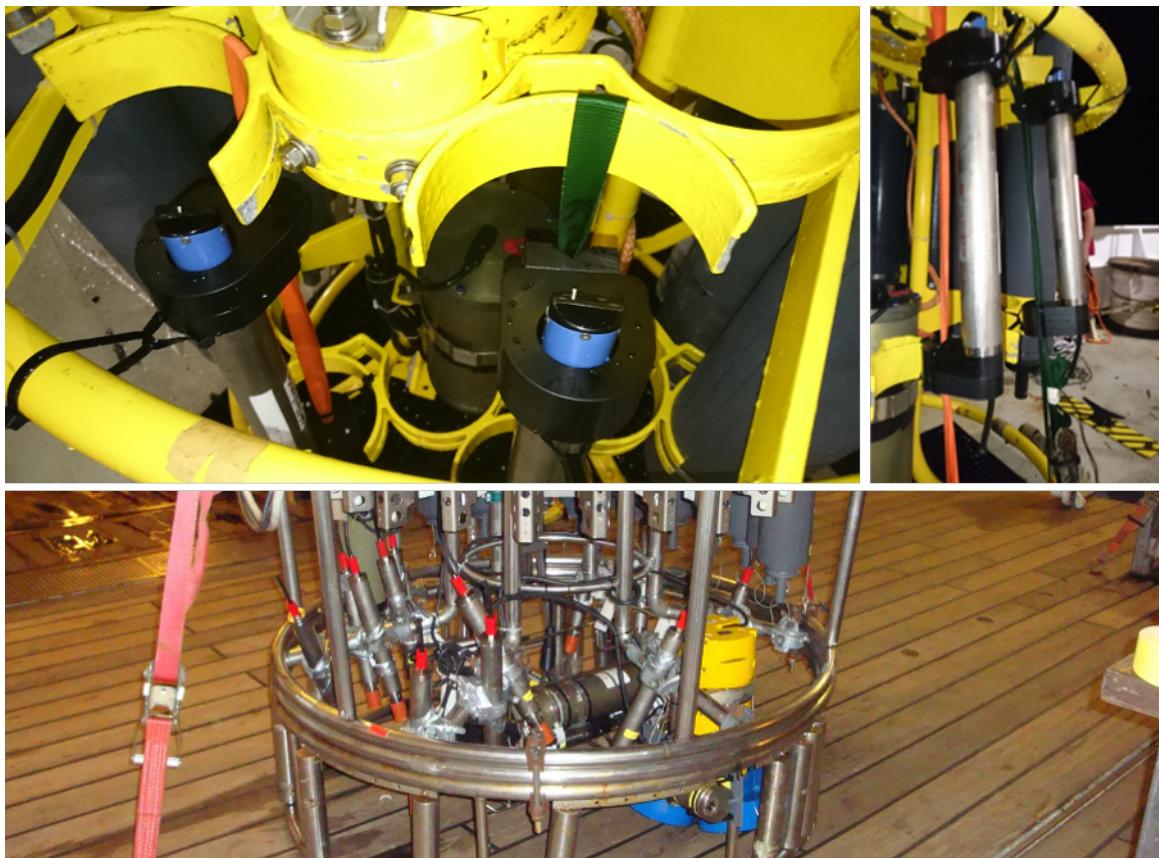


Figure 14: GEOMAR oxygen data loggers (Aanderaa Optode mounted on data logger) attached to a CTD frame and prepared for in-situ calibration during a CTD cast. Panels in the upper row show fixation with straps and zip ties. Panel in the lower row shows fixation with scaffolding clamps and tape in the interior lower part of the CTD frame.

Deploying gliders in Oxygen Minimum Zones (OMZ)

Note that the classical Winkler titration method is not reliable at oxygen concentrations in OMZ core (Thomsen et al. 2016) since the method has a detection limit of around 1 uM (Langdon 2010).

Steps recommended in these regions: 1) Do a 0/100 % calibration before and after deployment in the lab.

- 2) Measure Winkler in samples with concentration higher than 20 uM, typically in the mixed layer during the deployment and/or recovery. The Winkler method is also a problem when there is a strong vertical gradient, typically found in OMZ regions. Thus calibration points below the mixed layer are often not suitable. Look for regions with weak vertical gradients.
- 3) Park the glider for a few hours in the OMZ core at different temperatures to get an in-situ zero calibration points.

Piloting

In this section specific piloting requirements during the mission execution are mentioned which are needed to allow quality control. Towards the end of the mission power constraints often require the reduction in sampling frequency or even turning the oxygen sensor off. It is however essential that at least one good quality up and down cast to the maximum deployment depth is performed immediately prior to the pre-recovery samples being taken. Coordination between the recovery group and the pilots is essential.

Gather data to help correct for sensor response time

Regular up- and downcasts are needed to estimate and correct for the sensor response time. Combined up- and downcasts should be carried out at least every week and particularly at the beginning and at the end of the deployment. One to two days per week appear to be a reasonable compromise between energy saving and calibration quality. If bio-fouling is expected during the deployment it is better to collect up-down pairs earlier rather than later.

A sufficient high frequency sampling is required for a good lag correction. In particular in areas with a strong oxycline, we recommend to always sample at 5 s period. If battery lifetime is an issue period up- and down dives with high frequency sampling are more useful than continuous measurement at a lower frequency.

Gather data to correct for sensor drift

Deep water masses or known anoxic waters In regions with known oxygen concentrations i.e. within the core of the Peruvian Oxygen Minimum Zone (OMZ) oxygen concentrations of close to zero or few nmol are typical (Revsbech et al. 2009), (Kalvelage et al. 2013), (Thomsen et al. 2016) in-situ calibration points can be recorded. For this glider can be parked at this depth to get a 0 calibration at the beginning and at the end of the deployment. This can also be done by adding different depth/temperature levels if the anoxic layer is thick enough to cover different temperatures. i.e. further offshore where the OMZ is several 100 m thick.

In-air calibration In-air calibration can be carried out if optodes are attached in a way that they reach out of the water when the glider is surfacing (Nicholson and Feen 2017) as done also for long float deployments (Bittig et al. 2018) This can be valuable in particular if no 0 / 100 % lab calibration or CTD intercomparison is available as well as for long deployments. Contamination from splashing water and/or residual seawater on the sensor face have to be considered and corrected (Nisholson and Feen, 2017). Few gliders currently have this capability.

Gather data for in-situ inter-comparisons

Other oxygen monitoring platforms, such as moorings can be used as an inter-comparison reference if the quality of these data is better than those of the glider. The mission plan should aim to pass close to these platforms, ideally multiple times across the length of the mission.

Observe data for evidence of biofouling

- to add text and figure to allow user separating real and “biofouling” diurnal cycling

Real time data processing & Quality Control

Real Time data processing

Prior to deployment, oxygen sensor metadata (i.e. sensor model, sensor serial number and calibration coefficients) should be sent ahead of the mission to the Data Assembly Center. It is important that the glider is well configured, intermediate parameters (phase measurements) should be sent in real time (RT) as well. This will allow first to check if dissolved oxygen values computed inside the glider are appropriate and then this adds the possibility to recompute the dissolved oxygen concentration using the up to date method associated with the sensor model, intermediate parameters and calibration coefficients.

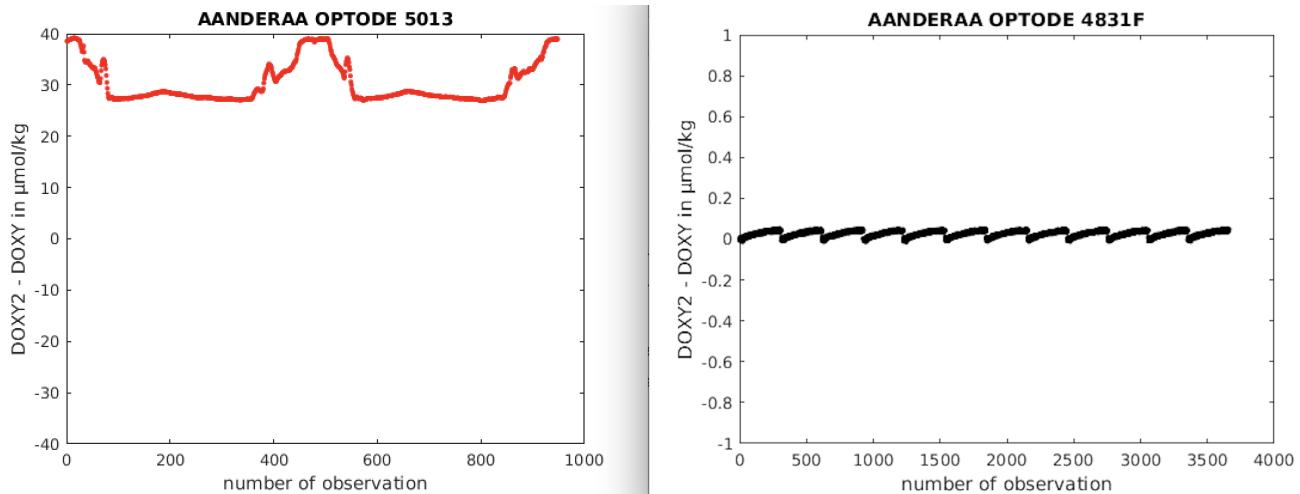


Figure 15: Difference between oxygen concentration computed by the glider (DOXY) and those computed by the Data Assembly Center (DAC) from intermediate parameters and associated calibration coefficient (DOXY2).

Configurations for the calculation of DOXY are in fact function of the sensor model and intermediate parameters. The recommended configurations (e.g. salinity compensation of MOLAR_DOXY, pressure correction for pressure effect on quenching, temperature compensation) are available in the Processing Argo oxygen data at the DAC level. For some optode models, it may be appropriate to apply a time lag correction in RT, taking into account the sensor time response, using either the manufacturer value or any value defined from previous deployments with the specific sensor. A real time lag correction might improve the useability of the real time data significantly. The method is described in (Bittig et al. 2014).

There is no unique procedure for Real time data and metadata sending. Protocols, format and file naming convention should be discussed with DACs before deployment. OceanOPS and DACs requirements on data and metadata are described in the OceanGliders Best Practices document in the data and metadata management section, paragraph 6 (link to be added when overview paper is in review).

Real Time quality control (RTQC)

Real time quality control tests applied on EGO oxygen data are extracted from the Argo quality control manual for dissolved oxygen. Details are summarized below. These tests are applied in supplement to trajectory tests. RTQC applied on the temperature measured by the oxygen sensor should follow the RTQC procedure defined for the CTD temperature.

Doxy QC initialisation

Several oxygen sensors suffer from predeployment storage drift that can reduce accuracy by up to 20% or more (Bittig et al. 2019). As a consequence and because this bias can be corrected, dissolved oxygen concentration measured in real time should be set to 3 “bad data that are potentially correctable”. To retrieve usable oxygen data, an adjustment in real time should be quickly performed.

Global range check

This test applies a gross filter on EGO oxygen data. If one observation is out of the global range [-5 600] /mumol/kg, its QC flag is set up to 4 “bad data”.

Outlier and spike check

Outliers and spikes are difficult to detect as optodes typically smooth out spikes due to their slow response time. A simple test checking the differences between sequential measurements is nevertheless possible if i) it is applied on a specific phase (ascending or descending for example) and ii) assuming a sampling adequately reproduces changes in dissolved oxygen concentrations. In this context, if one measurement is significantly different from adjacent ones, it is a spike in both size and gradient.

$$\text{Test value} = | V_2 - (V_3 + V_1)/2 | - | (V_3 - V_1) / 2 |$$

Where V_2 is the measurement being tested as a spike, V_1 and V_3 are the values above and below.

V_2 value should be flagged as 4 “bad data”, when: Test value > 50 $\mu\text{mol}/\text{kg}$ for pressure < 500 dbar Test value > 25 $\mu\text{mol}/\text{kg}$ for pressure ≥ 500 dbar

Stuck value test

This test looks for EGO oxygen data in the same phase (ascending or descending for example) being identical. Stuck values should be flagged as 4 “bad data”.

Bad P/T/S QC spreading

The test checks that the dissolved oxygen concentration in $\mu\text{mol}/\text{kg}$ is computed from a valid pressure, temperature and salinity. Considering the pressure or temperature impact on the oxygen conversion, when pressure or temperature is marked as bad ($qc = 4$), oxygen concentration should be set to 4. Conversely, and as the salinity impact on the oxygen conversion is less than previous parameters, when salinity is marked as bad, oxygen concentration should be set to 3.

Post-recovery operations and calibrations

At first users should report that their mission is over to support(at)oceanobs.org

Biofouling assessment

Fotos should be taken for biofuiling assessment. - to add: examples of typical biofouling

Sensor storage

Foil must be kept wet and protected from light after recovery until validation in the lab.

Lab calibration

When the glider is recovered, a 0% and 100% calibration is recommended as outlined above at two different temperatures levels.

Field calibration

Follow protocol described in section ‘Calibration during deployment/recovery from a ship with a CTD rosette equipped with a calibrated oxygen sensor’.

Delayed Mode Quality Control (DMQC)

Calculation of oxygen variables

Following Bittig et al. (2018).

Sensor drift correction

Aanderaa describe the in-situ drift characteristics of the 4330 and 4831 series optodes as being < 0.5 % per year and they make no distinction between the standard or fast (“F”-type) foils (Tengberg and Hovdenes 2014). Optodes made after 2016 undergo a “burning-in period” during manufacture and therefore have substantially less drift (Tengberg and Hovdenes 2014). Drift is a function of UV exposure and sampling frequency. The foil becomes less sensitive and therefore drift is always towards lower oxygen concentrations. The drift is believed to be due to bleaching of the luminophore foil via ambient light; it is particularly sensitive to fluorescent lights. The bleaching effect is partly counteracted by a destabilising effect on the luminophore. Together this manifests as a positive factor on the oxygen concentration (slope > 1) and a positive offset at zero oxygen.

(Queste et al. 2018) recorded drifts of 0.0176 and 0.0109 /mumol/kg/day for two Seagliders using inflections in the oxygen profiles as the glider penetrated to Arabian Sea Oxygen Minimum Zone and the sodium sulphite method, but no Winklers. (Bittig and Körtzinger 2015) report a 10 % drift over 3 years, but this is a combination of in-situ and ex-situ drift. (Bittig et al. 2018) determined the drift to be typically 0.1-0.2 % per year in-situ. A drift of 0.0004 % d-1 has been calculated based on UEA seagliders against Baltic deep water oxygen climatology (Possenti et al., 2020). Tom Hull found values between 0.0004 and 0.0035 % d-1 across 16 vehicles in-situ (slocums and seagliders with 4330F (old foil formulation), 4835 and 4831 optodes (unpublished?).

The drift correction should be applied to the oxygen concentration, not the measured phase (Bittig et al. 2018).

Sensor time response correction

In all but the most homogeneous waters it is essential to correct for the slow time response of optodes (Bittig et al. 2014, @Bittig2017) (see figure ??). This is particularly critical for optodes using the “standard” black foils, and as previously mentioned Slocum gliders with the optode in the standard location near the tail of the glider(Moat et al. 2016).

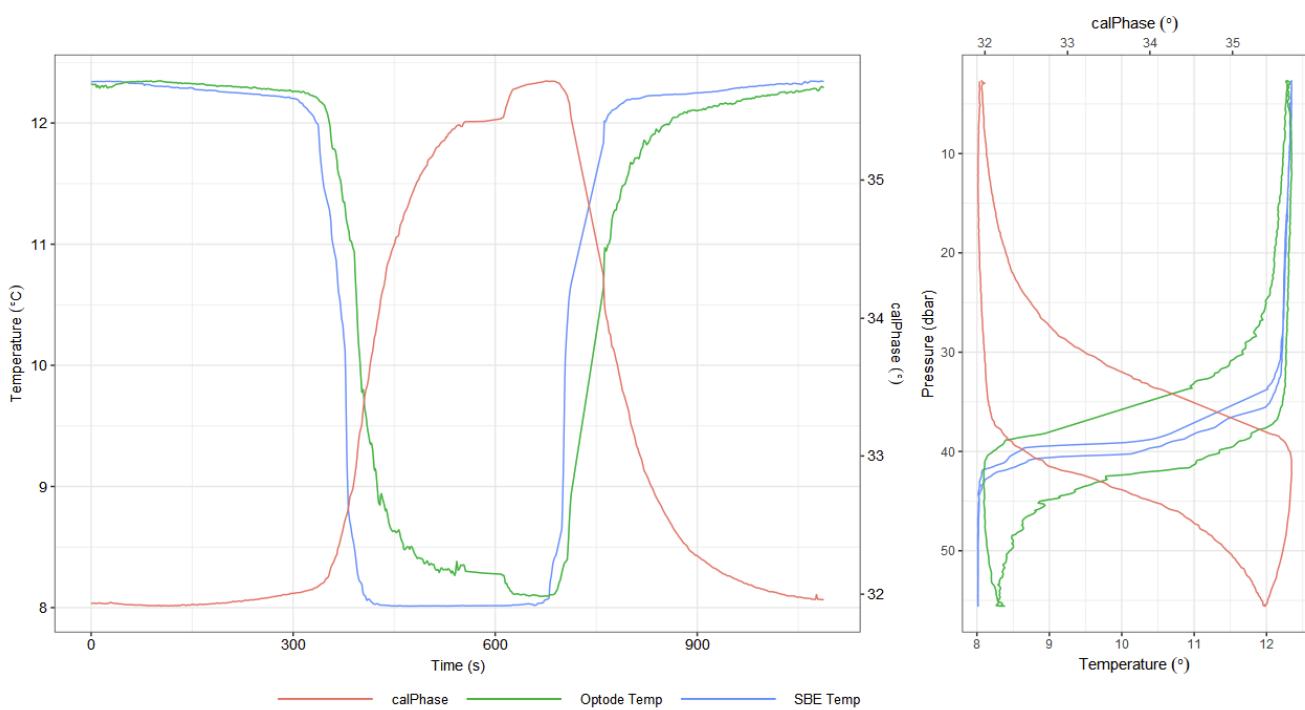


Figure 16: Example uncorrected profiles from AlterEco AE5 “Kelvin” Slocum with a 4831 optode with standard foil demonstrating significant lag in both optode temperature and phase.

Correction requires the collection of optode phase, temperature and time. Therefore the instruments and gliders should be configured to collect these variables and not just oxygen concentration or saturation. If only optode temperature and concentration are recorded, routines exist to recalculate phase, but this can introduce some inaccuracy and is best avoided. Accurate time-stamps for these data are required to be able to perform this

correction. Many data processing routines may remove these timestamps, such as to place the oxygen data on the same time-axis as the CTD, but for best results the oxygen sensor time should be used for the time response correction before interpolating to match the CTD. Users should be aware that many gliders have independent guidance-control computers and sensor computers and timestamps may differ between them. An important note is which temperature, be it optode or CTD, is used for the correction. The optode temperature typically has a lower accuracy and a slower response.

The lag is caused by a combination of factors, the relevance of these changes depending on the environment, optode type and glider platform. The rate of diffusion across the membrane (foil) is controlled by the water temperature and the thickness of the foil. Diffusion across the boundary layer above the membrane is also temperature dependent, but also influenced by the flow of water, which is determined by the position of the sensor and the glider speed and/or angle of attack. Lastly geometric lag is caused by a delay in water reaching the sensor due to glider geometry and the flow path of the surrounding water.

The boundary layer diffusion lag and the geometric lag will also affect the optode temperature response, which itself may have a time response due to the type of PRT used. As noted above, the type 3835 optodes have particularly slow responding temperature sensors and it is typical for users to use the CTD temperature in these instances.

The ideal correction method is still a point of discussion. We suggest users try each of these procedures and assess how well they work for their own use case.

Time response correction 1 - GEOMAR

Optode calibration and processing methods were developed by Johannes Hahn in collaboration with Henry Bittig for use on moored and glider-attached Aanderaa optodes. A set of routines were adapted to the particularities of optodes on gliders and to the typical conditions of GEOMAR glider deployments. This processing has now been used on nearly 100 glider deployments mostly in the Tropical Atlantic and Pacific Oceans [XXX reference]. The processing determines two delay time constants. One τ_{CTD} describes the time constant of an exponential filter which, when applied to the glider's CTD temperature, gives an estimate of the temperature of the optode foil. And the other describes the optode response time to changing oxygen concentrations. The processing so far makes no explicit correction for the “geometric” lag, that is any lag introduced by the CTD and optode being some distance from each other. This “geometric” lag should be of the order of a few seconds and thus is significantly smaller than the other two delay time constants. Implementing and correcting such a lag should however be fairly simple.

To determine the two time constants a number of steps are performed:

1. Linearly interpolate optode phase, optode temp, CTD temp, pressure and salinity variables onto 1 sec grid to avoid issues from different measurement times.
2. A set of foil temperatures is estimated by applying an exponential filter to the CTD temperature with time scales from 10 to 50 seconds (in steps of 5 sec), thereby creating different ‘virtual’ foil temperatures.
3. With this set of virtual foil temperatures oxygen concentrations are calculated using either the Aanderaa supplied or the own-calibration derived set of optode coefficients.
4. For each of the resulting oxygen concentrations a reverse exponential filter with time scales of 0 to 200 seconds (in steps of 20 sec) is applied to create sets of oxygen concentration profiles.
5. These sets of concentration profiles are then filtered with a forward-backward filter (`MATLAB filtfilt`) to remove the noise introduced by the reverse filtering. Currently a fixed time constant of 40 seconds is used for this filter. Depending on whether fast or slow foils are used, other values might deliver better results.
6. All concentrations are gridded to a 1 dbar grid (first binned and then linearly interpolated to the full dbar).
7. Differences between all up-down pairs are calculated and summed up for each of the concentration sets.
8. The one delay pair (CTD-temp delay for virtual foil temperature & Optode response delay) with the smallest difference sum is chosen and applied to the whole deployment.
9. Typically the ‘best’ delays are CTD-temp: 30-100 seconds, optode response : 20-50 seconds.
10. Included into the optimization are only up-down pairs that were not influenced by obvious bio-fouling.

Time response correction 2 - IMOS

The routine developed by Mun Woo for the IMOS glider toolbox also compares up and down casts in pressure space, but applies a time-shift rather than an exponential filter. These time-shift values are determined per dive, but a rolling median is calculated to exclude dives with very high or low lag values. **TODO - is this done with phase**

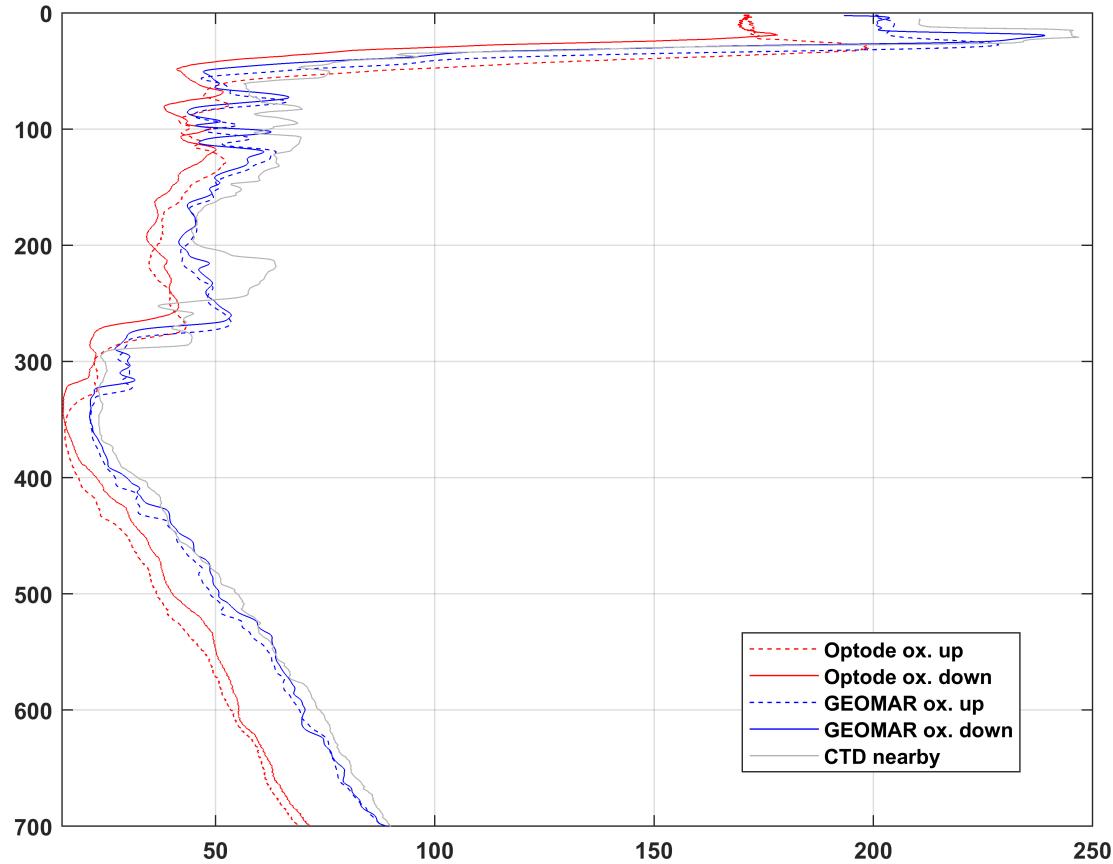


Figure 17: Example of original Optode oxygen concentrations (red) and GEOMAR processed and calibrated (blue) oxygen concentrations. Shown is an up-down pair from a deployment off Angola. Solid lines are the up and dashed lines the down data. Also shown are calibrated oxygen concentrations from a nearby and contemporaneous CTD cast.

or oxygen? - TH advantage of this method is it does not amplify noise which the filter will tend to do. However, simply shifting the optode data relative to time will not remove some of the second order effects.

TODO example image of IMOS correction

Time response correction 3 - UEA

The routine developed by Bastien Queste for the UEA Seaglider toolbox works as follows:

1. The CTD temperature is aligned based on flight speed to the optode phase using a 1-D interpolation and a flight speed dependent time-shift. (the optode and seabird temperature are close together on a Seaglider so the time-shift is small).
2. Oxygen partial pressure is calculated using the optode phase and time shifted optode temperature.
3. Up and down profiles are compared (in pressure or density space depending on environmental conditions) and either:
 1. A shoelace algorithm is used to minimise the area between the curves or
 2. The RMSD from vertically binned data is calculated
4. A minimisation algorithm (`fminsearch` from MATLAB) is used to fit two lag coefficients: $\tau = \tau_0 + \tau_1(T - 20)$ as per Hahn et al. (2014).
5. This τ is then used with an exponential inverse-filter, typically against optode phase (and oxygen recalculated) but partial pressure or concentration as per Bittig et al. (2018) has also been tested. The correction is applied on a per-dive basis.

Time response correction 4 - AlterEco

For AlterEco many gliders were not collecting data on both up and down casts which precludes the use of the above routines. 1. A τ was calculated for the geometric and boundary layer diffusive lag by minimising the difference between the CTD and optode temperatures. 1. This τ was used to then inverse-filter the optode phase and temperature. 1. A secondary lag correction based on the temperature as per the UEA toolbox and Hahn et al. (2014).

Light intrusion

Optodes can be sensitive to light intrusion if the foil is damaged. These instruments will typically still provide good data in the absence of light. A check should be made for increased sensor noise near the surface during daylight hours and contrast this with night-time observations.

Data delivery to public open access archives

- list archives and best practices how to store data
- get input of data management

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References

- AS, Aanderaa Data Instruments. 2018. "Aanderaa Oxygen Optodes: Best Practices for Maintaining High Data Quality." *Aanderaa Data Instruments AS, Bergen, Norway*, 28pp. <https://doi.org/http://dx.doi.org/10.25607/OBP-868>.
- Benson, Bruce B., and Daniel Krause Jr. 1980. "The Concentration and Isotopic Fractionation of Gases Dissolved in Freshwater in Equilibrium with the Atmosphere. 1. Oxygen." *Limnology and Oceanography* 25 (4): 662–71. <https://doi.org/https://doi.org/10.4319/lo.1980.25.4.00662>.
- Bittig, Henry C., Björn Fiedler, Roland Scholz, Gerd Krahmann, and Arne Körtzinger. 2014. "Time Response of Oxygen Optodes on Profiling Platforms and Its Dependence on Flow Speed and Temperature." *Limnology and Oceanography: Methods* 12 (8): 617–36. <https://doi.org/https://doi.org/10.4319/lom.2014.12.617>.

- Bittig, Henry C., and Arne Körtzinger. 2015. "Tackling Oxygen Optode Drift: Near-Surface and in-Air Oxygen Optode Measurements on a Float Provide an Accurate in Situ Reference." *Journal of Atmospheric and Oceanic Technology* 32 (8): 1536–43. <https://doi.org/10.1175/JTECH-D-14-00162.1>.
- Bittig, Henry C., and Arne Körtzinger. 2017. "Technical Note: Update on Response Times, in-Air Measurements, and in Situ Drift for Oxygen Optodes on Profiling Platforms." *Ocean Science* 13 (1): 1–11. <https://doi.org/10.5194/os-13-1-2017>.
- Bittig, Henry C., Arne Körtzinger, Craig Neill, Eikbert van Ooijen, Joshua N. Plant, Johannes Hahn, Kenneth S. Johnson, Bo Yang, and Steven R. Emerson. 2018. "Oxygen Optode Sensors: Principle, Characterization, Calibration, and Application in the Ocean." *Frontiers in Marine Science* 4 (January): 1–25. <https://doi.org/10.3389/fmars.2017.00429>.
- Bittig, Henry C., Tanya L. Maurer, Joshua N. Plant, Catherine Schmechtig, Annie P. S. Wong, Hervé Claustre, Thomas W. Trull, et al. 2019. "A Bgc-Argo Guide: Planning, Deployment, Data Handling and Usage." *Frontiers in Marine Science* 6: 502. <https://doi.org/10.3389/fmars.2019.00502>.
- Coppola, F.; Delauney, L.; Salvatet. 2013. "White Paper on Dissolved Oxygen Measurements: Scientific Needs and Sensors Accuracy." *Jerico Project*. <https://www.jerico-ri.eu/previous-project/publications/white-paper-on-dissolved-oxygen-measurements-scientific-needs-and-sensors-accuracy/>.
- Delgado, Adrián, Ciprian Briciu-Burghina, and Fiona Regan. 2021. "Antifouling Strategies for Sensors Used in Water Monitoring: Review and Future Perspectives." *Sensors* 21 (2). <https://doi.org/10.3390/s21020389>.
- Garcia, Herncin E., and Louis I. Gordon. 1992. "Oxygen Solubility in Seawater: Better Fitting Equations." *Limnology and Oceanography* 37 (6): 1307–12. <https://doi.org/10.4319/lo.1992.37.6.1307>.
- Hahn, J., P. Brandt, R. J. Greatbatch, G. Krahmann, and A Körtzinger. 2014. "Oxygen Variance and Meridional Oxygen Supply in the Tropical North East Atlantic Oxygen Minimum Zone." *Clim. Dyn.* 43 (11): 2999–3024.
- Johnson, Kenneth S., Joshua N. Plant, Stephen C. Riser, and Denis Gilbert. 2015. "Air Oxygen Calibration of Oxygen Optodes on a Profiling Float Array." *Journal of Atmospheric and Oceanic Technology* 32 (11): 2160–72. <https://doi.org/10.1175/JTECH-D-15-0101.1>.
- Kalvelage, Tim, Gaute Lavik, Phyllis Lam, Sergio Contreras, Lionel Arteaga, Carolin R. Löscher, Andreas Oschlies, Aurélien Paulmier, Lothar Stramma, and Marcel M. M. Kuyper. 2013. "Nitrogen cycling driven by organic matter export in the South Pacific oxygen minimum zone." *Nature Geoscience* 6 (3): 228–34. <https://doi.org/10.1038/ngeo1739>.
- Langdon, C. 2010. "Determination of Dissolved Oxygen in Seawater by Winkler Titration Using Amperometric Technique." In, the GO-SHIP Repeat Hydrography Manual: A Collection of Expert Reports and Guidelines. 134 (1): 1–17. <https://doi.org/10.25607/OPB-1350>.
- Moat, B., D. Smeed, C. Marcinko, S. Popinet, and S Turnock. 2016. "Flow Dis-Tortion Around Underwater Gliders and Impacts on Sensor Measurements:A Pilot Study Using Large-Eddy Simulations." *National OceanographyCentre Research and Consultancy Report, National Oceanography Centre, Southampton, UK* 58. <http://nora.nerc.ac.uk/id/eprint/514980/>.
- Nicholson, David P., and Melanie L. Feen. 2017. "Air Calibration of an Oxygen Optode on an Underwater Glider." *Limnology and Oceanography: Methods* 15 (5): 495–502. <https://doi.org/10.1002/lom3.10177>.
- Queste, Bastien Y., Clément Vic, Karen J. Heywood, and Sergey A. Piontkovski. 2018. "Physical Controls on Oxygen Distribution and Denitrification Potential in the North West Arabian Sea." *Geophysical Research Letters* 45 (9): 4143–52. <https://doi.org/10.1029/2017GL076666>.
- Revsbech, Niels Peter, Lars Hauer Larsen, Jens Gundersen, Tage Dalsgaard, Osvaldo Ulloa, and Bo Thamdrup. 2009. "Determination of Ultra-Low Oxygen Concentrations in Oxygen Minimum Zones by the Stox Sensor." *Limnology and Oceanography: Methods* 7 (5): 371–81. <https://doi.org/10.4319/lom.2009.7.371>.
- Tengberg, A., and J. Hovdenes. 2014. "Information on Long-Term Stability and Accuracy of Aanderaa Oxygen Optodes and Information About Multipoint Calibration System and Sensor Option Overview." *Aanderaa Data Instruments AS*. <https://www.aanderaa.com/media/pdfs/2014-04-O2-optode-and-calibration.pdf>.

- Thomsen, Soeren, Torsten Kanzow, Gerd Krahmann, Richard J. Greatbatch, Marcus Dengler, and Gaute Lavik. 2016. "The Formation of a Subsurface Anticyclonic Eddy in the Peru-Chile Undercurrent and Its Impact on the Near-Coastal Salinity, Oxygen, and Nutrient Distributions." *Journal of Geophysical Research: Oceans* 121 (1): 476–501. [https://doi.org/https://doi.org/10.1002/2015JC010878](https://doi.org/10.1002/2015JC010878).
- Uchida, Hiroshi, Takeshi Kawano, Ikuo Kaneko, and Masao Fukasawa. 2008. "In Situ Calibration of Optode-Based Oxygen Sensors." *Journal of Atmospheric and Oceanic Technology* 25 (12): 2271–81. <https://doi.org/10.1175/2008JTECHO549.1>.
- Uchida H., G. C. Johnson, and K. E. McTaggart. 2010. "CTD Oxygen Sensor Calibration Procedures." In, *the GO-SHIP Repeat Hydrography Manual: A Collection of Expert Reports and Guidelines. IOCCP Report N°14* 134 (1): 1–17. [https://doi.org/https://doi.org/10.25607/OPB-1344](https://doi.org/10.25607/OPB-1344).