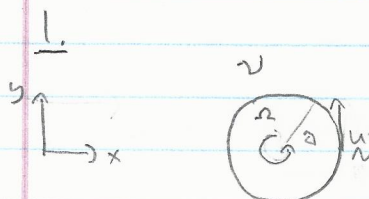


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# PHYS 426

Take Home Final

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1) cylinder rotates as solid body:  $u_r = 0$   
for  $0 \leq r \leq a$   $u_\theta = r\Omega \hat{\theta}$   $u_\theta(a) = a\Omega$

no slip boundary: at  $r=a$   $u_{\text{fluid}} = u_{\text{cyl}} = a\Omega \hat{\theta}$

$$\text{vorticity } \underline{\omega} = \nabla \times \underline{u} = \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \hat{k} = 2\Omega \hat{k} = \omega_0 \hat{k}$$

$$\frac{D(\underline{\omega})}{Dt} = (\underline{\omega} \cdot \nabla) \underline{u} + \nu \nabla^2(\underline{\omega})$$

in steady state  $0 = (\nabla \times \underline{u}) \cdot \nabla \underline{u} + \nu \nabla^2(\nabla \times \underline{u})$   
in polar coordinates:

$$0 = \nu \left( \frac{\partial^2 u_\theta}{\partial r^2} + \frac{1}{r} \frac{\partial u_\theta}{\partial r} - \frac{u_\theta}{r^2} \right)$$

$$\frac{\partial^2 u_\theta}{\partial r^2} + \frac{1}{r} \frac{\partial u_\theta}{\partial r} - \frac{u_\theta}{r^2} = 0 \quad \text{rewrite as ODE:}$$

$$\frac{d^2 u_\theta}{dr^2} + \frac{d}{dr} \left( \frac{u_\theta}{r} \right) = 0 \Rightarrow \frac{du_\theta}{dr} + \frac{u_\theta}{r} = C_1$$

$$\frac{d(r u_\theta)}{dr} = C_1 r$$

$$r u_\theta = \frac{1}{2} C_1 r^2 + C_2$$

$$u_\theta(\infty) = 0 \Rightarrow C_1 = 0$$

$$u_\theta(a) = a\Omega = \frac{C_2}{a} \Rightarrow C_2 = a^2 \Omega$$

$$u_\theta = \frac{1}{2} C_1 r + \frac{C_2}{r}$$

$$u_\theta = \frac{a^2 \Omega}{r}$$

2) Bernoulli:  $\frac{D}{Dt} \left[ \frac{1}{2} |\underline{u}|^2 + gz + \frac{p}{\rho} \right] = \underline{u} \cdot \underline{F} + \frac{1}{\rho} \frac{\partial p}{\partial t}$

in steady state  $\underline{u} \cdot \underline{F} = 0$

$$\underline{u} \cdot \underline{F} = \underbrace{\nabla \cdot (\underline{u} \cdot \underline{\tau})}_{\text{work done by cyl. on fluid}} - \underbrace{\nu (\nabla \underline{u})^2}_{\text{viscous dissipation}} = 0$$

$$\int \nabla \cdot (\underline{u} \cdot \underline{\tau}) = \oint_{\text{cyl}} u_\theta \tau_\theta \cdot d\mathbf{A} \quad \tau_\theta = \nu \cancel{\frac{\partial u_\theta}{\partial \theta}} + \nu \frac{\partial u_\theta}{\partial r} + \nu \cancel{\frac{\partial u_\theta}{\partial z}}$$

$$= \nu \int_{\text{cyl}} u_\theta \frac{\partial u_\theta}{\partial r} d\mathbf{A} = \nu \int_0^{2\pi} \left( \frac{\partial^2 \Omega}{r} \right) \left( -\frac{\partial^2 \Omega}{r^2} \right) d\theta$$

$$= -2\pi \nu \frac{\partial^4 \Omega^2}{r^3} \quad \text{work}$$

$$\nabla u_\theta = \frac{\partial u_\theta}{\partial r} + \frac{1}{r} \cancel{\frac{\partial u_\theta}{\partial \theta}} + \cancel{\frac{\partial u_\theta}{\partial z}}$$

$$\int_{\text{vol}} \nu \left( \frac{\partial u_\theta}{\partial r} \right)^2 dV = \nu \int_0^{2\pi} \int_0^\infty \left( -\frac{\partial^2 \Omega}{r^2} \right)^2 dr d\theta$$

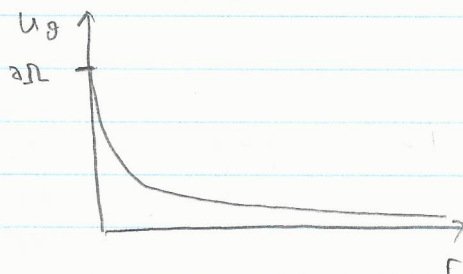
$$= 2\pi \nu \int_0^\infty \left( \frac{\partial^4 \Omega^2}{r^4} \right) dr = 2\pi \nu \left[ -\frac{\partial^4 \Omega^2}{3 r^3} \right]_0^\infty$$

$$= -2\pi \nu \frac{\partial^4 \Omega^2}{r^3} \quad \text{dissipation}$$

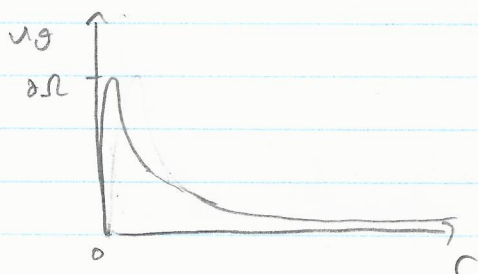
hence rate of work equals viscous dissipation

✓

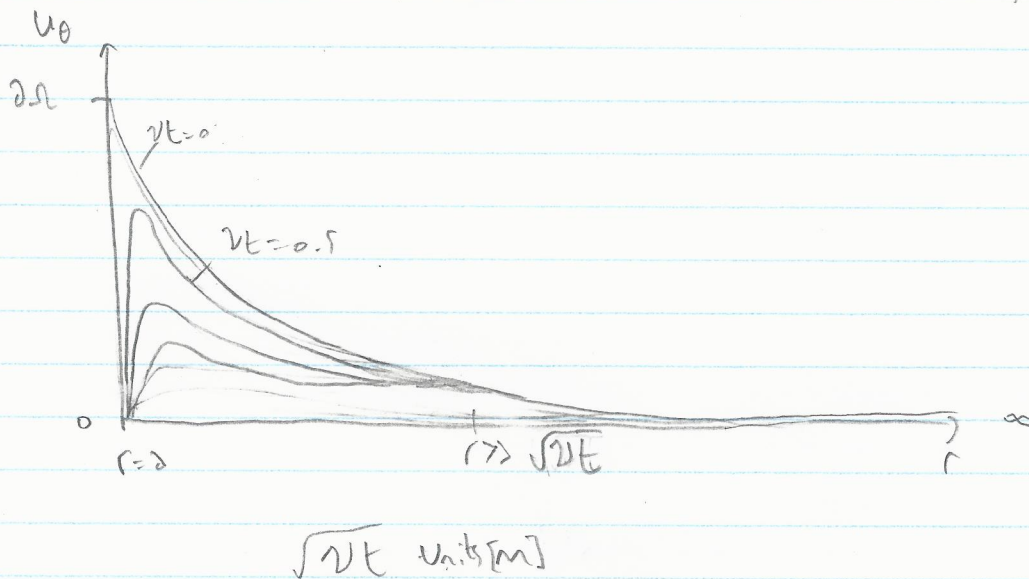
3) when cylinder rotating



when cylinder stops  $t=0$



Sketch of temporal evolution of velocity field



$u_\theta = \frac{\Gamma}{2\pi r}$  - circulation

$\Gamma = 2\pi\Omega a^2$

①  $\frac{\partial u_\theta}{\partial t} = \nu \frac{\partial}{\partial r} \left[ \frac{1}{r} \frac{\partial}{\partial r} (r u_\theta) \right]$

$u_\theta(r, 0) = \frac{\Gamma}{2\pi r}$

$u_\theta(0, t) = 0$

$u_\theta(r \rightarrow \infty, t) = \frac{\Gamma}{2\pi r}$





letting non-dimensional velocity

$$u' \equiv \frac{u_\theta}{\Gamma/2\pi r} = f(r, t, v) = F(\eta)$$

non dimensional grouping  $\frac{r}{\sqrt{2\nu t}}$

$$\eta = \frac{r^2}{4\nu t} \quad \text{sub into ①}$$

$$F'' + F' = 0$$

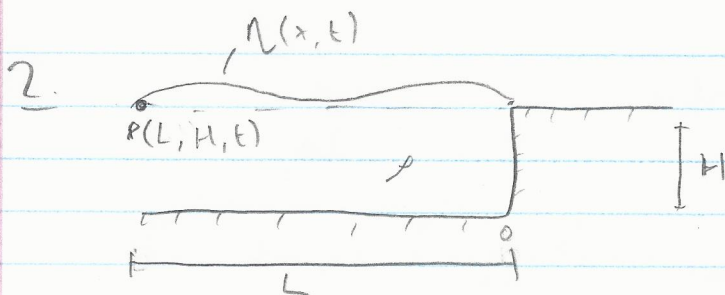
$$F(\infty) = 1$$

$$F(0) = 0$$

$$\Rightarrow F = 1 - e^{-\eta}$$

$$u_\theta = \frac{\Gamma}{2\pi r} [1 - e^{-r^2/4\nu t}] \quad \text{form of sketches}$$





$$P(L, t) = P_0 \cos(\omega t)$$

$g = \text{gravitational constant}$

1) hydrostatic approximation:  $\frac{1}{\rho_0} \frac{\partial P}{\partial x} = g \frac{\partial \eta}{\partial x} \Rightarrow \frac{\partial u}{\partial t} = -g \frac{\partial \eta}{\partial x}$

assuming there is no fluid above the basin ( $P \geq (H + \eta) = 0$ )

$$P(L, H, t) = \rho g \eta$$

$$\omega t = \frac{n\pi}{2} \Rightarrow P = 0$$

$$P_0 \cos(\omega t) = \rho g \eta$$

$$(n=1, 3, 5 \dots)$$

let  $\eta_0 = \frac{P_0}{\rho g} \Rightarrow \eta(L, t) = \eta_0 \cos(\omega t)$

$$\eta(x, t) = A e^{i(kx - \omega t)} + B e^{i(-kx - \omega t)} \quad \frac{\omega}{k} = \sqrt{gH}$$

no energy loss  $|A| = |B|$

$$\eta(L, t) = \eta_0 \cos(\omega t) = \text{Re}(\eta_0 e^{-i\omega t})$$

$$\Rightarrow A + B = \eta_0$$

$$u(0, t) = 0 \Rightarrow \frac{\partial \eta(0, t)}{\partial x} = 0 \Rightarrow ik A e^{i(-\omega t)} - ik B e^{i(-\omega t)} = 0$$

$$A = B \Rightarrow B = \frac{\eta_0 e^{ikL}}{e^{ikL} + e^{-ikL}} = \frac{\eta_0 e^{ikL}}{2 \cos kL}$$

$$A = \frac{\eta_0}{2} \frac{e^{-ikL}}{\cos kL}$$

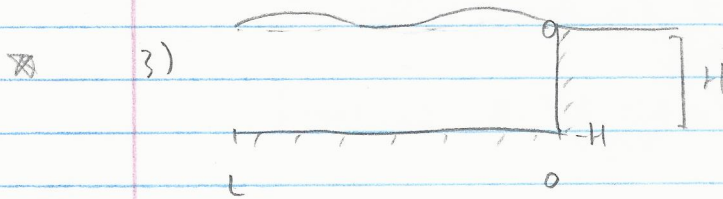
$$\boxed{\eta = \eta_0 \frac{\cos[kx]}{\cos[kL]} \cos[\omega t]}$$

2) from hydrostatic:  $\frac{\partial u}{\partial t} = -g \frac{\partial \eta}{\partial x}$

$$\frac{\partial u}{\partial t} = - \frac{g k \eta_0 \sin(k(x-L))}{\cos(kL)} \cos \omega t$$

$$u(x,t) = - \frac{g k \eta_0}{\omega} \frac{\sin(k(x-L))}{\cos(kL)} \sin \omega t$$

$u(x,t)$  functionally dependent on  $g, \omega, \rho, \rho_0, k, L$  &  $t$



$$u(L,t) = u_0 \sin(\omega t + \phi)$$

No E loss:  $u_{no}(L,t) = - \frac{g k}{\omega} \left( \frac{\rho_0}{\rho g} \right) \frac{\sin(kL)}{\cos(kL)} \sin \omega t = \frac{k \rho_0}{\omega \rho} \tan(kL) \sin(\omega t)$

E loss:  $u(L,t) = u_0 \sin(\omega t + \phi)$

$$\langle KE_{no} \rangle = \int_{-H}^H \frac{1}{2} \rho u_{no}^2 dz = (H+H) \frac{1}{2} \rho u^2$$

$$KE_{no} = \frac{4}{2} \frac{k^2 \rho_0^2}{\omega^2 \rho^2} \tan^2(kL) \sin^2(\omega t)$$

$$\langle KE_{no} \rangle = \frac{H}{2} \frac{k^2 \rho_0^2}{\omega^2 \rho^2} \left( \frac{1}{2} \right)$$

$$APE_{no} = \frac{1}{2} \rho g \eta^2 = \frac{1}{2} \rho g \left( \frac{\rho_0}{\rho g} \right)^2 \cos^2(\omega t)$$

$$\langle APE_{no} \rangle = \frac{\rho_0^2}{4 \rho g}$$

$$\langle E_{no} \rangle = \frac{H}{4} \frac{k^2 \rho_0^2}{\omega^2 \rho^2} + \frac{\rho_0^2}{4 \rho g}$$



$$KE = \int_{-H}^H \frac{1}{2} u^2 dz = \frac{H}{2} u^2 = \frac{H}{2} u_0^2 \sin^2(\omega t + \phi)$$

$$\langle KE \rangle_T = \frac{H u_0^2}{4} = \langle APE \rangle$$

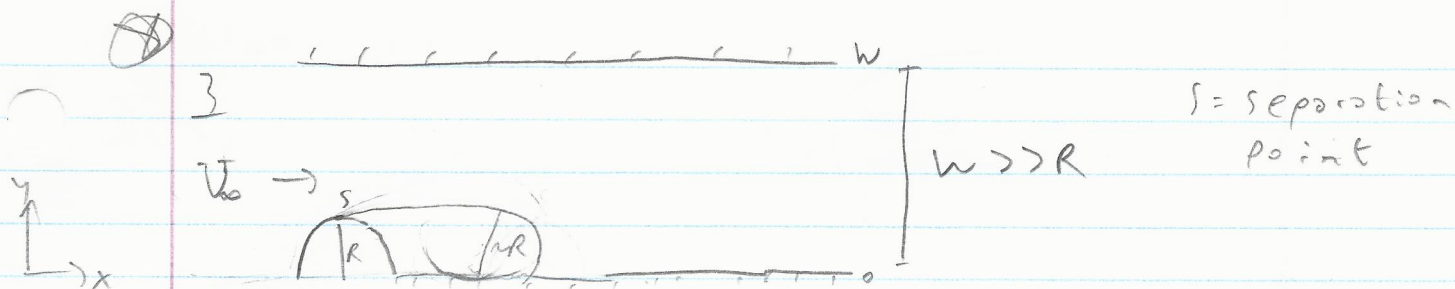
$$\left\langle \frac{dE}{dt} \right\rangle_T = \langle E_{N_0} \rangle_T - \langle E \rangle_T$$

$$= \frac{P_0^2}{4} \left[ \underbrace{\frac{H \kappa^2}{\omega^2 \rho^2} + \frac{1}{\rho g}}_{A} \right] - \frac{H u_0^2}{2}$$

$$= \frac{P_0^2 - H u_0^2}{4} \left[ A \right]$$



$$\star 4) \quad \phi \ll 1 \quad \rho_0 \ll \rho g H \quad L \ll \frac{2\pi \sqrt{gH}}{\omega}$$



$$\left. \begin{aligned} u_r &= 0 \\ u_\theta &= 0 \end{aligned} \right\} \text{at surface} \Rightarrow \psi(R, \theta) = 0$$

$$\frac{\partial \psi}{\partial r}(R, \theta) = 0$$

Outside of boundary layer

(assuming viscous flow)

$$\psi = U_\infty \left( r - \frac{R^2}{r} \right) \sin \theta \quad \text{at } x=2R \text{ to } w$$

$$\psi = 0$$

$$\phi = U_\infty \left( r - \frac{R^2}{r} \right) \cos \theta$$

$$u_\theta = -U_\infty \left( 1 + \frac{R^2}{r^2} \right) \sin \theta = -2U_\infty \sin \theta \text{ at } r=R$$

$$|u_\theta|_{\max} = 2U_\infty$$

2)  $P_{\text{bubble}} = P_s$        $P_\infty + \frac{1}{2} \rho U_\infty^2 = P_s + \frac{1}{2} \rho u_{\theta s}^2$

$$P_s = P_\infty - \frac{1}{2} \rho U_\infty^2 (1 - 4 \sin^2 \theta)$$

$$D = - \int_0^{\pi/2} R \cos \theta P_s d\theta \quad \text{since } P = \text{const } \theta \geq \pi/2$$

$$D = - \frac{1}{2} \rho U_\infty^2 R$$

defining drag & pressure coefficients

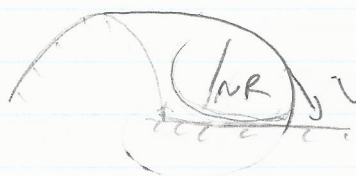
$$C_D \equiv \frac{D}{\frac{1}{2} \rho U_\infty^2 R}$$

$$C_D = - \frac{1}{2} \int_0^{\pi/2} C_p \cos \theta d\theta$$

$$C_p \equiv \frac{P - P_\infty}{\frac{1}{2} \rho U_\infty^2}$$



3)



$$u_g = \begin{cases} \Gamma r / (2\pi R^2) & r \leq R \\ \Gamma / (2\pi r) & r > R \end{cases}$$

Surface of water in vortex ( $r \sim R$ )

rough and turbulent  
outside vortex smoother, with  
no flow along surface of headland  
& channel edge (looks like an eddy)

4) At the moment the flow  
turns off, the vortex will  
travel back towards the headland  
with initial speed  $-U_0$  because  
of negative  $\zeta_p$  where  
vortex is.



5)  $h < H \rightarrow U_0$  decreases  $\frac{\omega_0}{H} = \frac{\omega_f}{h}$

Surface height will

be parabolic with  $\eta = h - \frac{R^2}{r^2}$

