

# 05-Off-Grid Photovoltaic Arrays

*Off-Grid Electrical Systems in Developing Countries, 2<sup>nd</sup> Edition*

Chapter 5

# Preface

- These lectures slides are intended to accompany the textbook *Off-Grid Electrical Systems in Developing Countries, 2<sup>nd</sup> Edition, 2025* written by Dr. Henry Louie and published by [SpringerNature](#)
- Additional content, explanations, derivations, examples, problems, errata, and other materials are found in the book and on [www.drhenrylouie.com](http://www.drhenrylouie.com)
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# Learning Outcomes

At the end of this lecture, you will be able to:

- ✓ Describe the use of solar power in off-grid electrification, emphasizing the key technical, economic, environmental, and social considerations
- ✓ Derive and utilize circuit models of photovoltaic (PV) cells, modules, and arrays to calculate their voltage, current, and power production under different irradiance, temperature, and load conditions
- ✓ Define and describe the relevance of terminology such as Standard Test Conditions and Standard Operating Conditions
- ✓ Explain how shading and other abnormal operating conditions affect PV module performance and identify strategies to mitigate the effects

# Introduction

- Photovoltaic Effect is the mechanism by which solar photovoltaic (PV) works
- DC electricity is directly generated
- Discovered by Edmond Becquerel in 1839
- Established for power generation in 1954 by Chapin, Fuller and Pearson



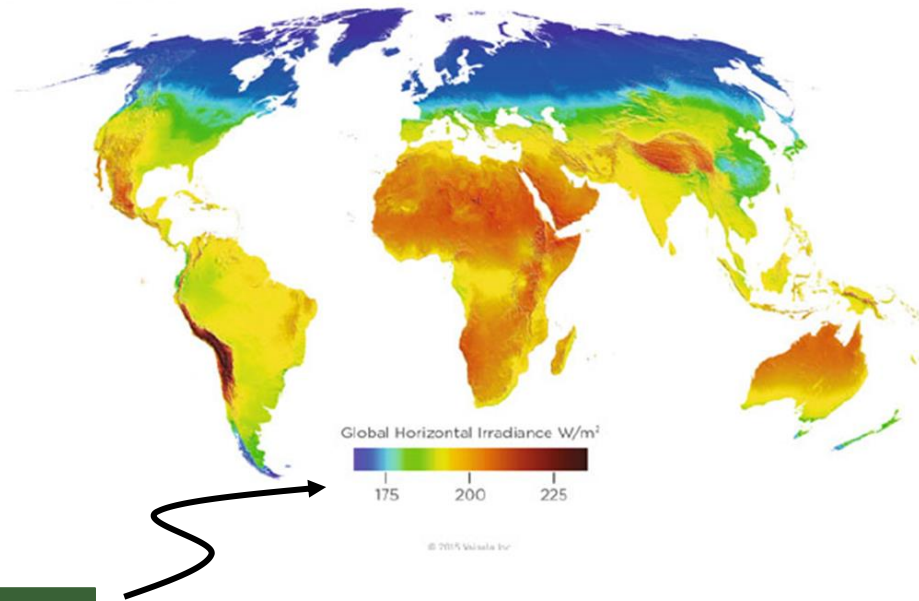
Edmond Becquerel

# Irradiance and Insolation

- Irradiance ( $G$ ): density of the power produced by sunlight ( $\text{W}/\text{m}^2$ )
- Insolation (not “insulation”) ( $I$ ): energy provided by sunlight per square meter of area over a period of time, usually per day ( $\text{kWh}/\text{m}^2/\text{day}$ )

# Solar Resource

VAISALA



units are average irradiance

(courtesy of Viasala, Copyright (c) 2017 Vaisala)



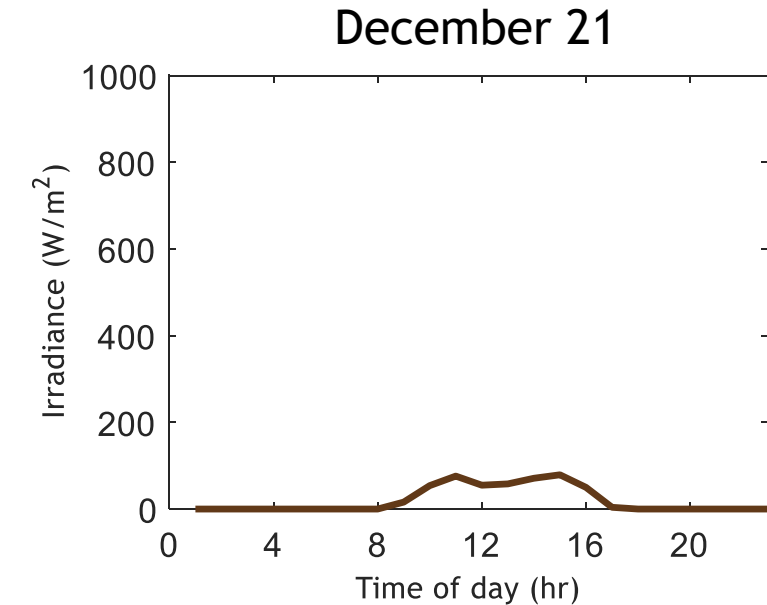
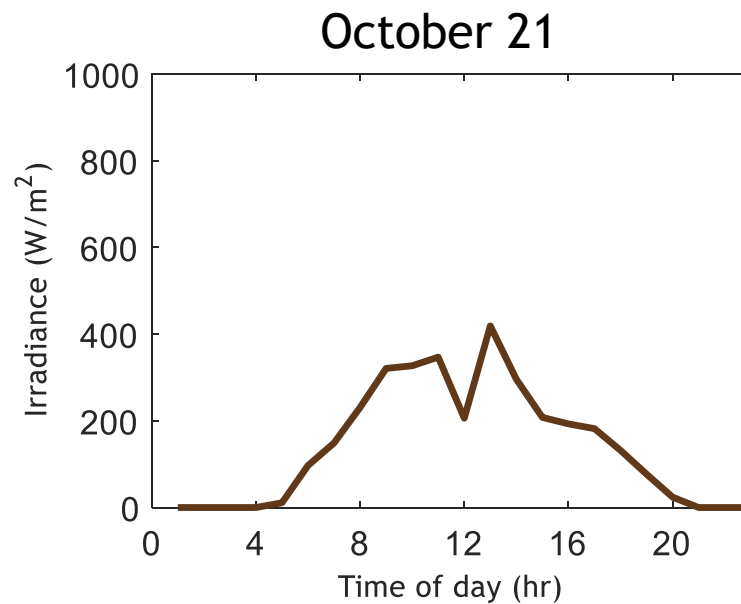
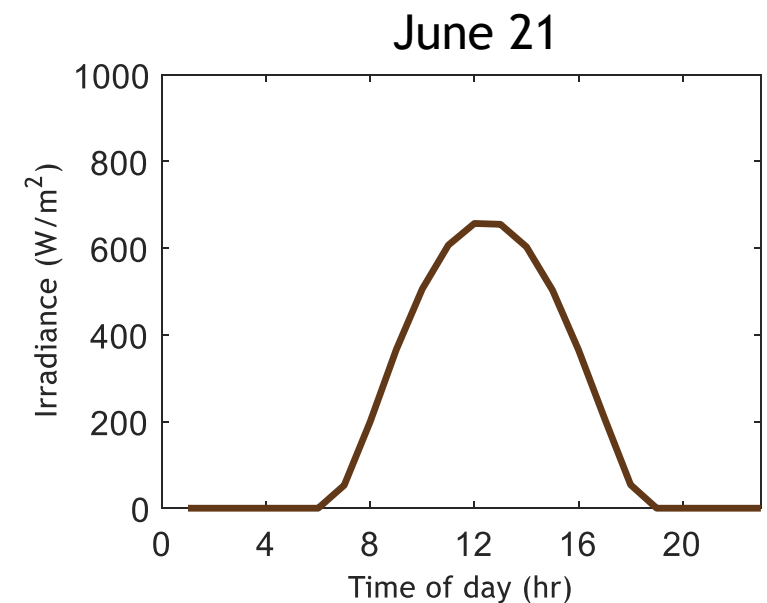
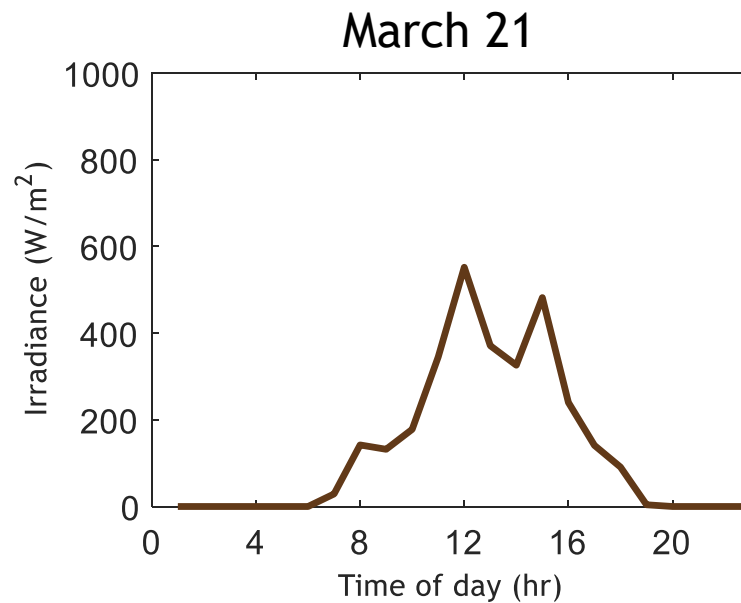
# Typical Values

- Irradiance of  $1000 \text{ W/m}^2$  is approximately the sunlight a horizontal surface receives at 12:00 on a clear sunny day in the mid-continental U.S.
- Typical insolation: 3.5 to 6  $\text{kWh/m}^2/\text{day}$



Irradiance varies  
across the day and  
season

Global Horizontal  
Irradiance (GHI)  
in Seattle



# Physical Description

Silicon cells are most commonly used in off-grid systems

PV cells are connected in series to form PV modules



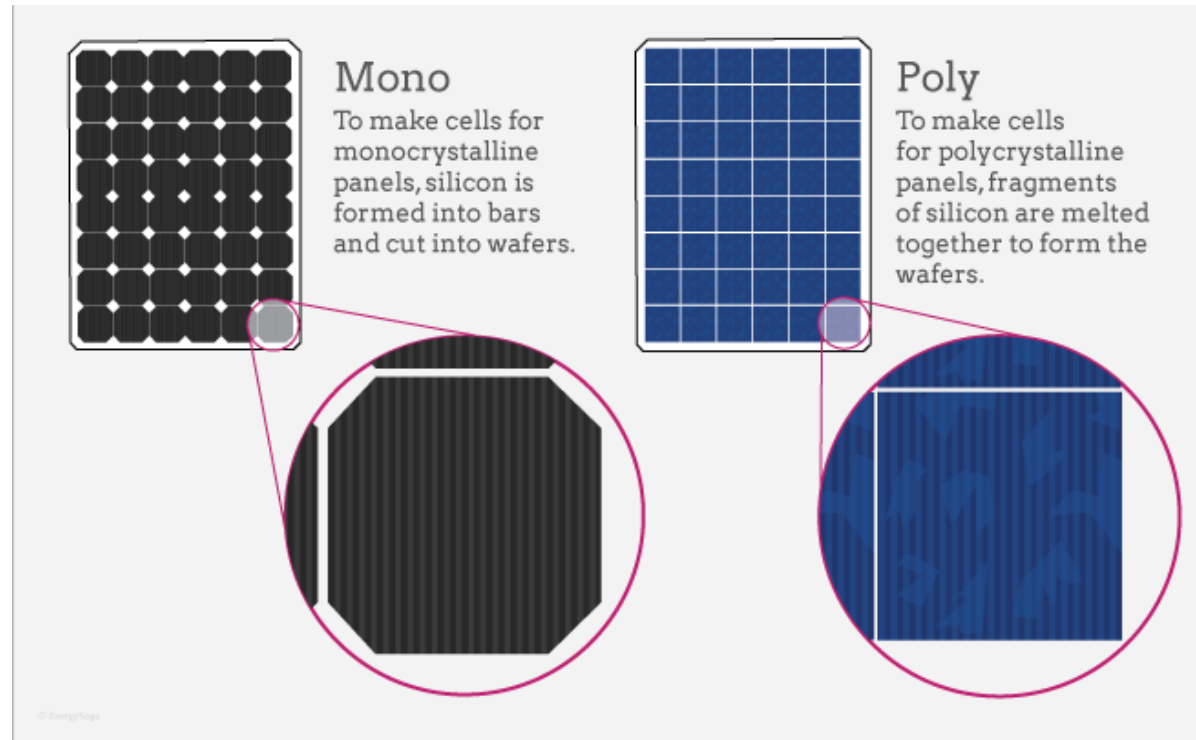
monocrystalline



polycrystalline

PV cell

# Physical Description

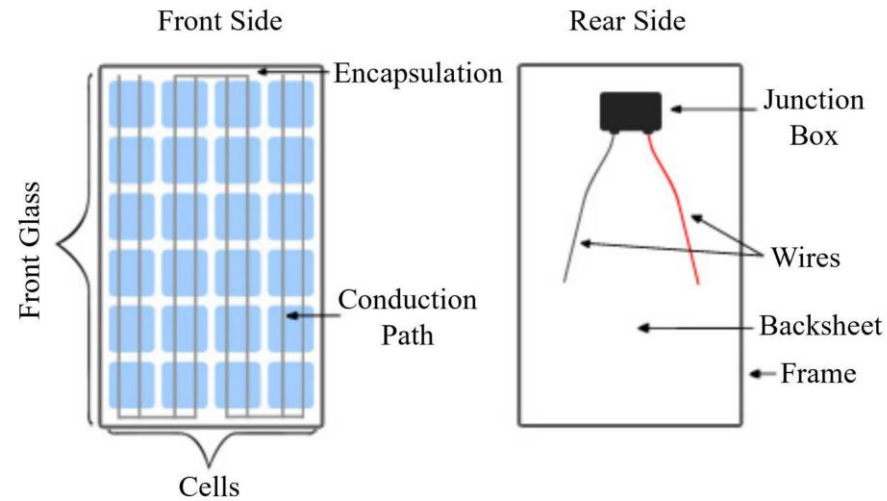


There are two common types of PV cells: mono-crystalline and poly-crystalline

A typical 0.156 m x 0.156 m (6.1 in x 6.1 in) cell produces 2 to 4 W

source <https://www.civicsolar.com/support/installer/articles/monocrystalline-cells-vs-polycrystalline-cells-whats-difference>

# Traditional PV Module



# PV Modules

- PV modules are made from several cells that are connected together (in series)
- Physical size of a 550 W module (shown in picture)
  - 2.4 m x 1.1m x 0.04 m
  - 35 kg

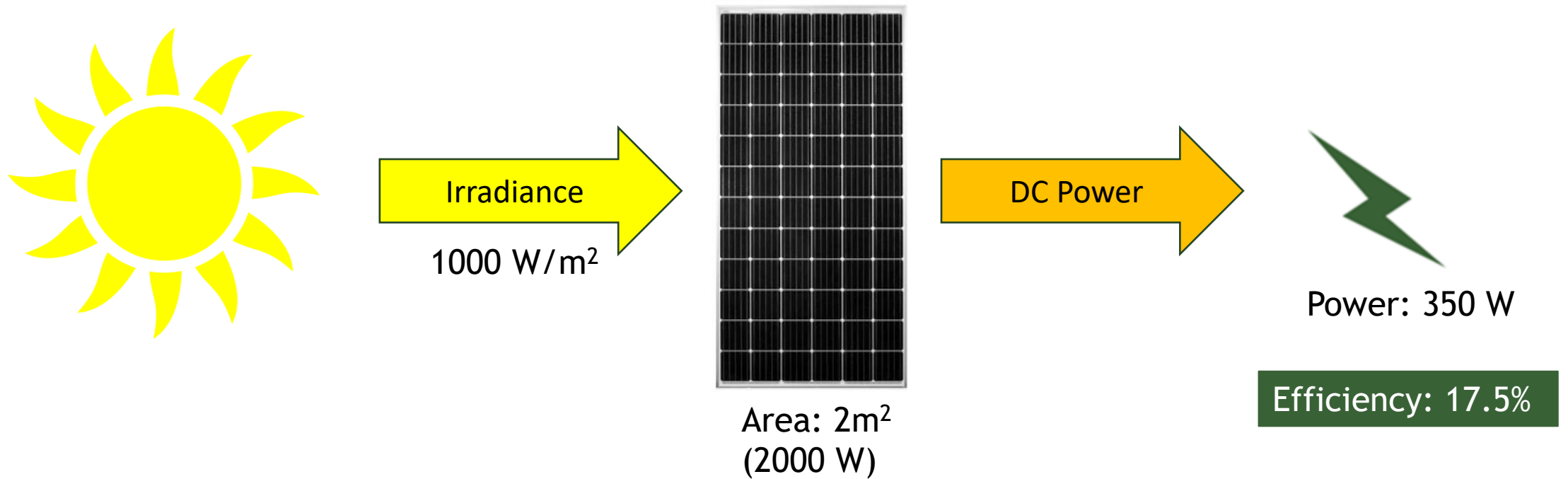


(courtesy P. Dauenhauer)

# Basic Principles

- Electricity is produced via the *photovoltaic* effect
- Power produced by PV module is approximately proportional to incident irradiance
- Power is inherently DC
- Efficiency typically 14-23%

# Example Efficiency





# Basic Principles

- PV cell is a p-n junction (diode)
- Recall p-n junctions are made from doped silicon crystals, which have internal built-in electric fields
- Photons from sunlight excite electrons into the conduction band, built-in field separates charge and voltage appears

# Illuminated p-n Junction

- No net current in un-illuminated p-n junction
  - exception: external battery connected
- What happens when a photon hits the p-n junction?
- Recall:
  - photons can excite electrons into the conduction band

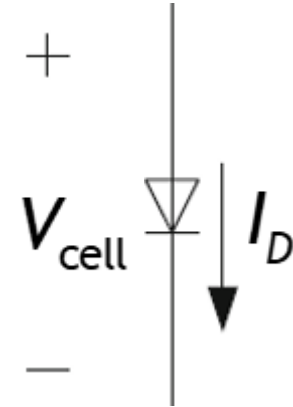
# Unilluminated PV Cell

A PV cell in the dark (unilluminated) operates as a diode

$$I_D = I_0 \left( e^{V_D / nV_T} - 1 \right)$$

$$V_T = \frac{kT}{q}$$

$V_T$ : 25.8 mV at room temperature  
 $I_0$ : usually small (e.g.  $10^{-8}$  A/m<sup>2</sup> of cell area)



$k$ : Boltzmann's constant ( $1.38 \times 10^{-23}$  J/K)  
 $n$ : ideality factor (unitless), is equal to 1 for an ideal diode, but is often  $>1$   
 $T$ : temperature (K)  
 $q$ : charge  $1.602 \times 10^{-19}$  (C)  
 $I_0$ : reverse bias saturation current (A)

# Illuminated PV Cell

Effect of photons exciting electrons is modeled as “illumination current”

- always positive
- approx. proportional to incident irradiance, cell area, and cell efficiency
- typical range: 0.5 to 9 A

$$I_{\text{cell}} = I_G - I_0 \left( e^{V_{\text{cell}}/nV_T} - 1 \right)$$

$$I_{\text{cell}} = I_G - I_D$$

← *characteristic equation of PV cell*

$I_G$ : illumination current (A)  
 $I_{\text{cell}}$ : current out of PV cell (A)  
 $V_{\text{cell}}$ : PV cell voltage (V)

# PV Cell Open-Circuit Voltage

Open-circuit voltage of a PV cell is computed from

$$I_{\text{cell}} = I_G - I_0 \left( e^{V_{\text{cell}}/nV_T} - 1 \right)$$

$$\frac{I_G - I_{\text{cell}}}{I_0} + 1 = e^{V_{\text{cell}}/nV_T}$$

$$nV_T \ln \left( \frac{I_G - I_{\text{cell}}}{I_0} + 1 \right) = V_{\text{cell}}$$

$$V_{\text{cell,OC}} = nV_T \ln \left( \frac{I_G}{I_0} + 1 \right)$$

Typical open-circuit voltage is  
between 0.6 and 0.74 V

# Short-Circuit Current

Under short-circuit conditions  $V_{\text{cell}} = 0 \text{ V}$

$$I_{\text{cell}} = I_G - I_0 \left( e^{V_{\text{cell}}/nV_T} - 1 \right)$$

$$I_{\text{SC}} = I_G - I_0 \left( e^{0/nV_T} - 1 \right)$$

$$I_{\text{SC}} = I_G - I_0 (1 - 1)$$

$$I_{\text{SC}} = I_G$$

The short-circuit current is equal to the illumination current. The illumination current can be determined by shorting the PV cell and measuring the current (assuming the PV cell is ideal)

# Example 5.1

Compute the open-circuit voltage and short-circuit current of a PV cell whose reverse bias saturation current is  $9^{-9}$  A, illumination current is 8.46 A, ideality factor is 1.0, and thermal voltage is 28 mV.



# Example 5.1

Compute the open-circuit voltage and short-circuit current of a PV cell whose reverse bias saturation current is  $9^{-9}$  A, illumination current is 8.46 A, ideality factor is 1.0, and thermal voltage is 28 mV.

The short-circuit current of a PV cell is equal to the illumination current so that the short-circuit current = 8.46 A.

$$V_{\text{cell,OC}} = nV_T \ln \left( \frac{I_G}{I_0} + 1 \right) = 1 \times 0.028 \times \ln \left( \frac{8.46}{9^{-9}} + 1 \right) = 0.613 \text{ V}$$

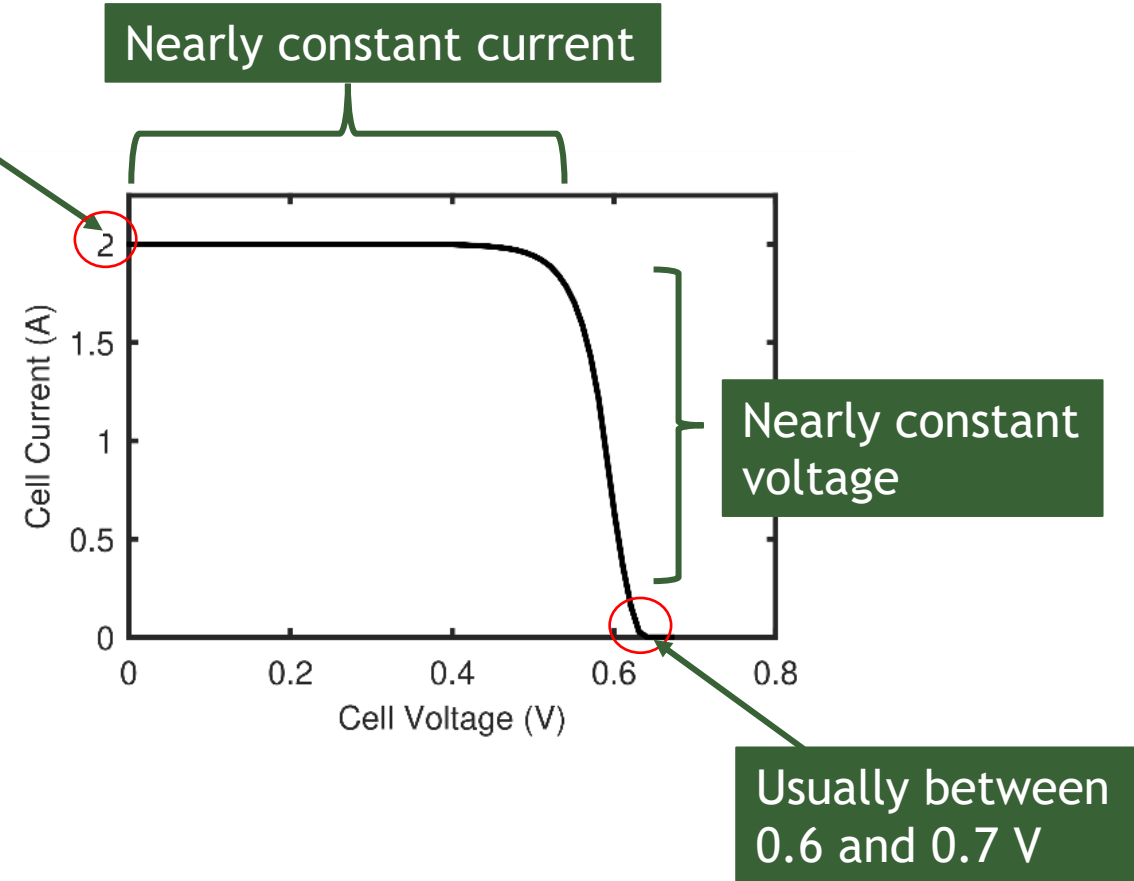
# I-V Curve

Equal to illumination current

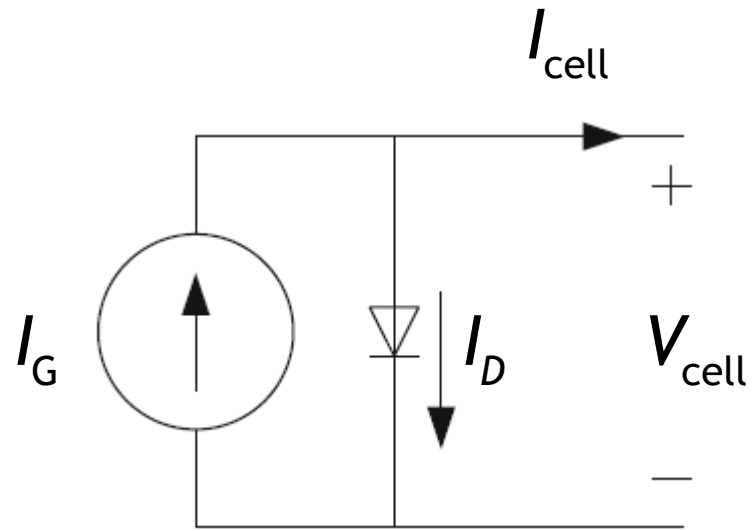
The current–voltage curve of a PV cell can be plotted by solving

$$I_{\text{cell}} = I_G - I_0 \left( e^{V_{\text{cell}}/nV_T} - 1 \right)$$

for different values of  $V_{\text{cell}}$



# Ideal Circuit Model



Assume PV cell is  
ideal unless stated otherwise

# Exercise

Which variable should be set to zero when the PV cell is operated under open-circuit conditions?

- A.  $I_G$
- B.  $I_0$
- C.  $I_{\text{cell}}$
- D.  $V_T$

$$I_{\text{cell}} = I_G - I_0 \left( e^{V_{\text{cell}}/nV_T} - 1 \right)$$

# Exercise

Which variable should be set to zero when the PV cell is operated under open-circuit conditions?

A.  $I_G$

B.  $I_0$

C.  $I_{\text{cell}}$

D.  $V_T$

$$I_{\text{cell}} = I_G - I_0 \left( e^{V_{\text{cell}}/nV_T} - 1 \right)$$

# Exercise

Which of these affects the open-circuit voltage of a PV cell?

- A. Temperature
- B. Ideality factor
- C. Irradiance
- D. Reverse saturation current?

# Exercise

Which of these affects the open-circuit voltage of a PV cell?

- A. Temperature
- B. Ideality factor
- C. Irradiance
- D. Reverse saturation current?

$$V_{\text{cell,OC}} = nV_T \ln \left( \frac{I_G}{I_0} + 1 \right)$$

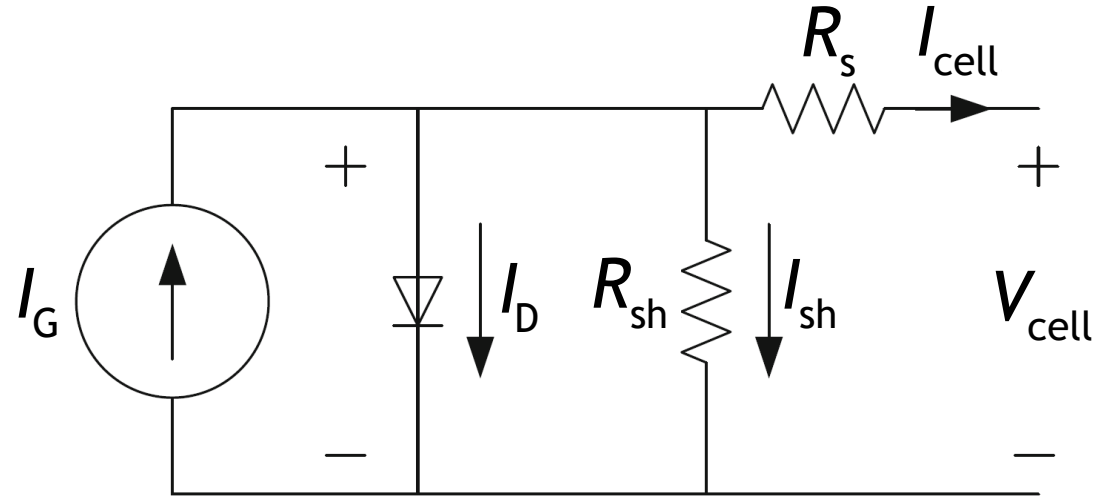


# Circuit Model with Losses (non-ideal)

$$I_{\text{cell}} = I_G - I_D - I_{\text{sh}}$$

$$I_{\text{cell}} = I_G - I_0 \left( e^{(V_{\text{cell}} + I_{\text{cell}} R_s)/V_T} - 1 \right) - \frac{V_{\text{cell}} + I_{\text{cell}} R_s}{R_{\text{sh}}}$$

Implicit equation, must be solved numerically



# Maximum Power Point

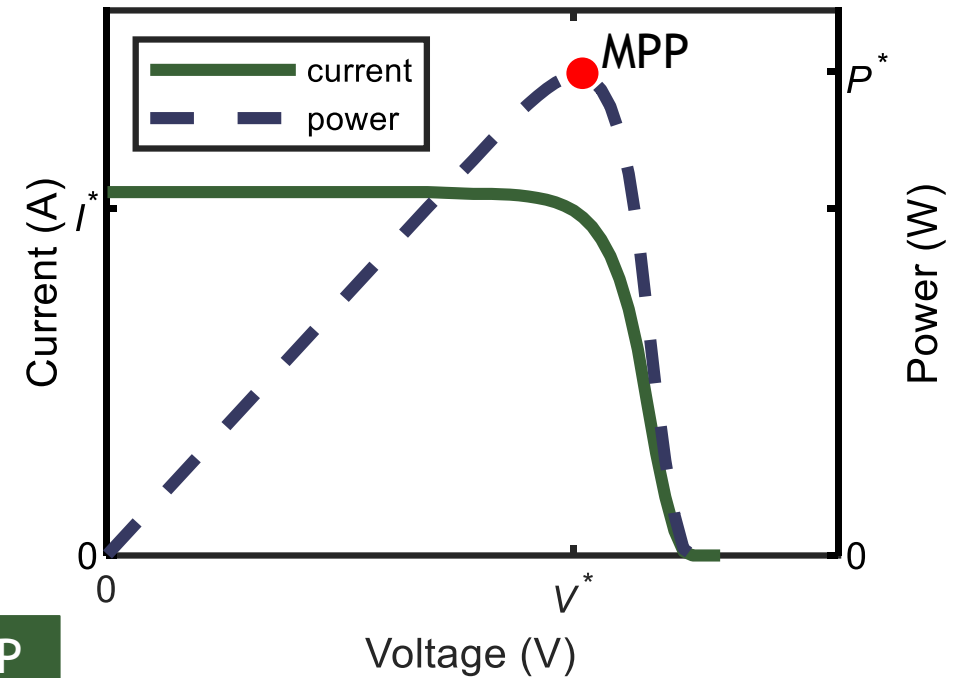
- Power output is found from

$$P_{\text{cell}} = I_{\text{cell}} V_{\text{cell}}$$

- PV arrays have a unique maximum power operating point (maximum power point, MPP)

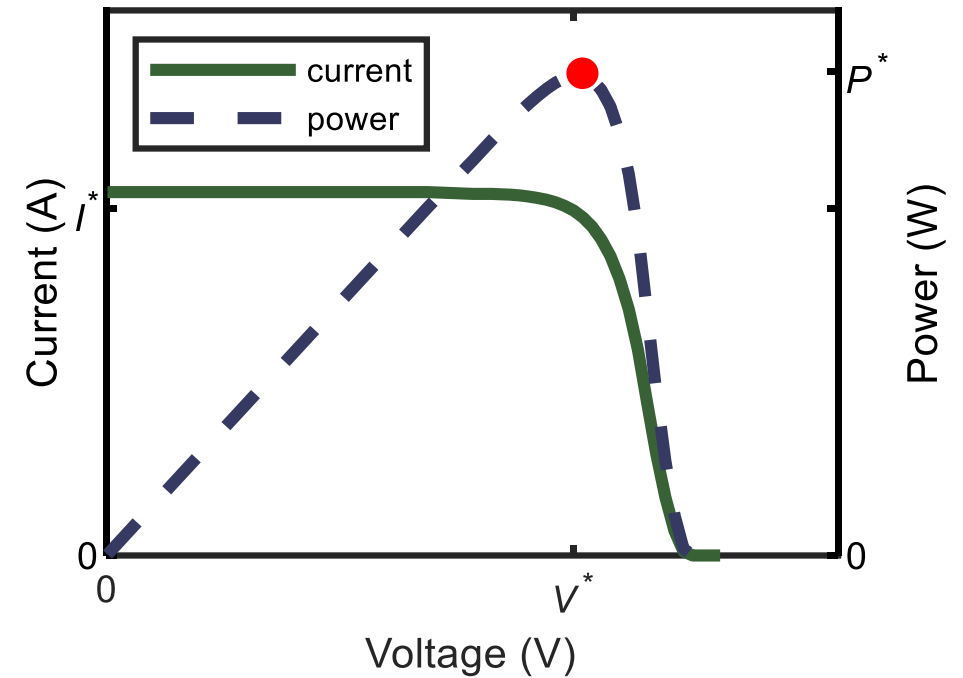
$$P_{\text{cell}}^* = V_{\text{cell}}^* I_{\text{cell}}^*$$

here the \* indicates that the values correspond to the MPP (not complex conjugate)



# Maximum Power Point

- MPP voltage might not correspond to load input impedance or battery voltage
- Use a “maximum power point tracker” to ensure PV cell (module) is operating at the maximum power point (discussed in Chap. 11 and 13)

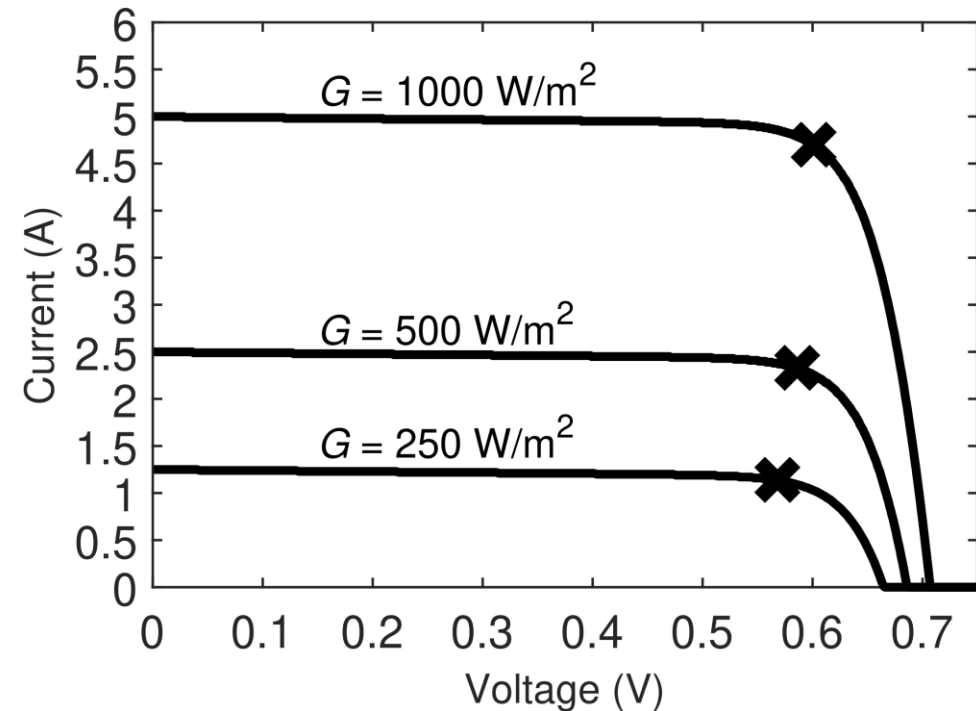


# Maximum Power Point at Different Irradiances

Maximum power point voltage and current depends on the irradiance

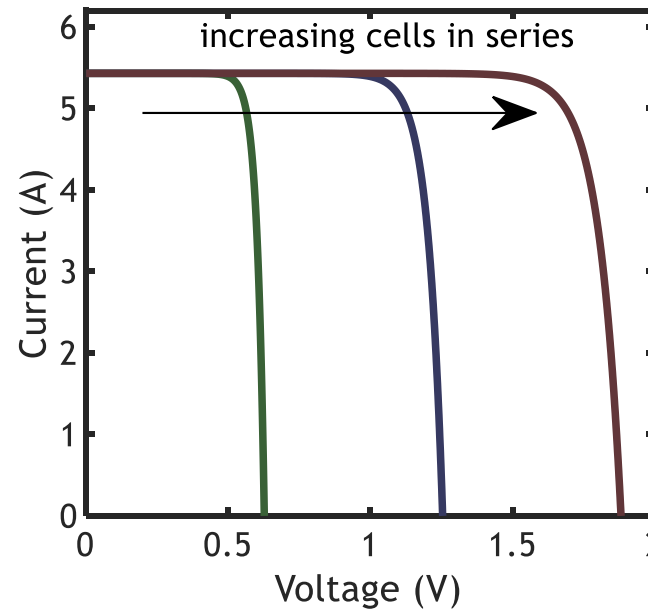
$$P_{\text{cell}}^*(G) = V_{\text{cell}}^*(G) I_{\text{cell}}^*(G)$$

Here we show that the voltage, current, and power at the maximum power point are functions of the irradiance

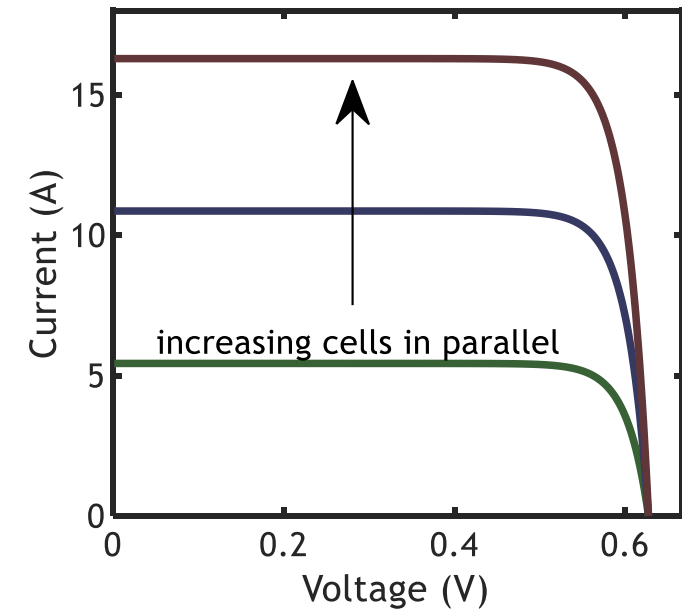


# PV Modules

- PV modules are made by connecting several PV cells
- Increasing number of series or parallel-connected cells affects the I-V curve of the module



Voltage increases



Current increases

# PV Modules

- Most modules are made from connected PV cells in series
- Module voltage is simply the cell voltage multiplied by the number of series-connected cells:

$$V_{\text{module}} = N_{\text{ser}} \times V_{\text{cell}}$$

$$I_{\text{cell}} = I_G - I_0 \left( e^{V_{\text{cell}}/nV_T} - 1 \right)$$

$$\frac{I_{\text{module}}}{N_{\text{par}}} = I_G - I_0 \left( e^{V_{\text{module}}/(nV_T N_{\text{ser}})} - 1 \right)$$

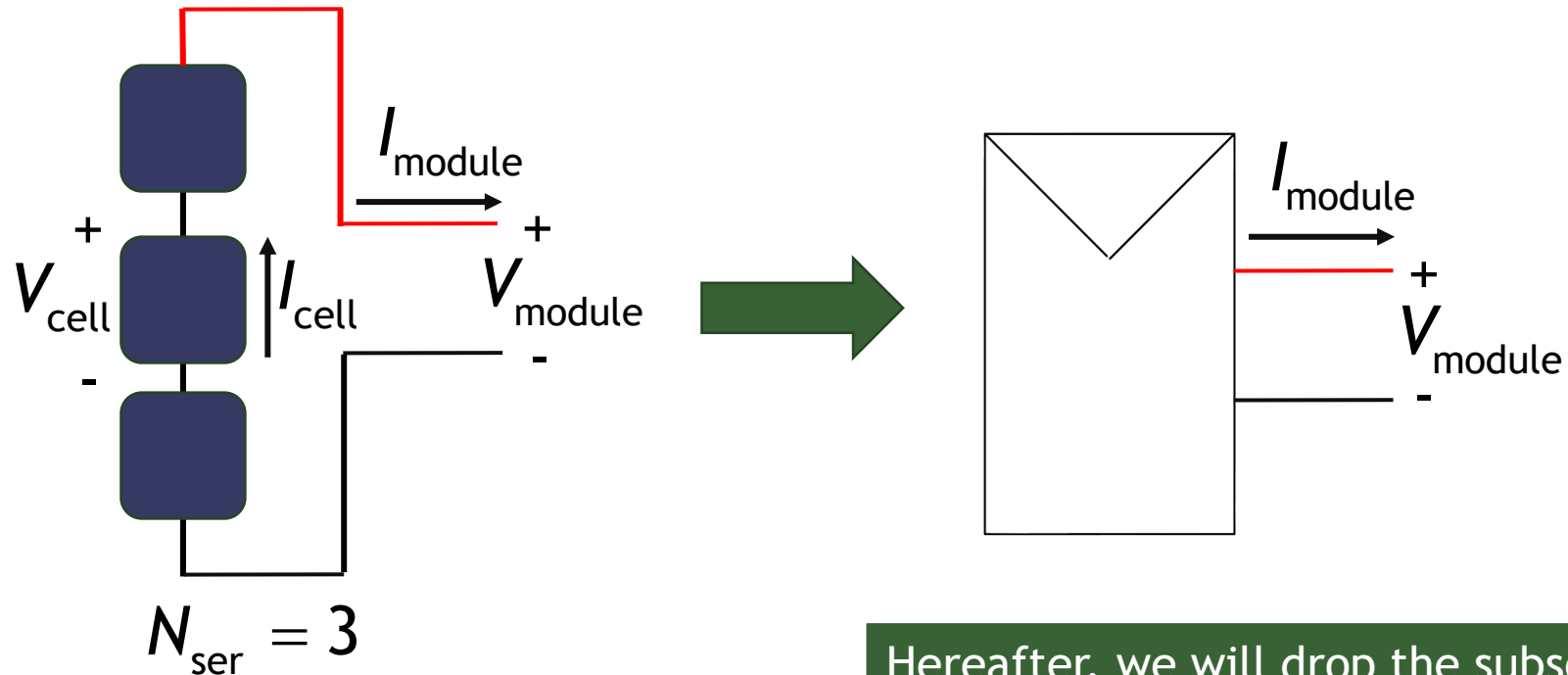
$V_{\text{module}}$  : PV module voltage (V)

$I_{\text{module}}$  : PV module current (A)

$N_{\text{ser}}$  : number of series-connected cells

$N_{\text{par}}$  : number of parallel-connected cells (usually 1)

# PV Modules



Hereafter, we will drop the subscript “module” since we are usually not interested in the characteristics of an individual cell



# PV Module Specifications

- Manufacturer-provided information
- Used to understand and estimate how the module will perform under different conditions

Characteristic at STC	Value
Maximum Power	185.3 W
Optimum Operating Voltage ( $V^*$ )	36.4 V
Optimum Operating Current ( $I^*$ )	5.08 A
Open-Circuit Voltage ( $V_{OC}$ )	45.0 V
Short-Circuit Current ( $I_{SC}$ )	5.43 A
Short-Circuit Current Temp. Coeff. ( $\alpha_i$ )	0.055 %/K
Open-Circuit Temp. Coeff. ( $\alpha_v$ )	-0.37 %/K
Max. Power Temp. Coeff. ( $\alpha_P$ )	-0.48 %/K
NOCT	45 °C
Number of Cells	72 (series)

# What PV Capacity (Power rating) Means

A certain PV module has a maximum power rating of 350 W

- How should that be interpreted?
- Will it produce 350 W on a winter day in Seattle?
- Will it produce 350 W on a summer day in Lusaka?
- Will it ever produce more than 350 W?
- Do the characteristics of the load or battery that it is connected to matter?

# Main Factors Affecting PV Power Production

Irradiance



Temperature



Load



Spectral distribution of irradiance  
also affects production

# Standard Test Conditions

- We use subscript “STC” to denote a variable referenced to Standard Test Conditions
- Examples:
  - $G_{\text{STC}}$  : irradiance at STC ( $G_{\text{STC}} = 1000 \text{ W/m}^2$ )
  - $P_{\text{STC}}^*$  : maximum power output under STC
  - $V_{\text{STC}}^*$  : voltage at the maximum power point under STC
  - $I_{\text{SC,STC}}$  : short-circuit current under STC

# PV Module Spec Sheets

- Modules rated at Standard Test Conditions (STC)
  - Irradiance: 1000 W/m<sup>2</sup>
  - Cell temperature: 25 °C
  - Spectral distribution: AM 1.5
- PV modules rarely operate under STC

## Itek SE 72-Cell Module

Design & Engineering Data

### GENERAL DATA

<b>Cell Type</b>	• 72 high-efficiency monocrystalline p-type cells • 6 x 12 cell matrix		
<b>Solar Glass</b>	• Ultra-clear anti-reflective treatment • Tempered, with low iron content • Anti-glare prismatic subsurface texture		
<b>Backsheet</b>	• Multi-layered • Engineered adhesion for maximum weather protection		
<b>Frame</b>	• High-strength corrosion-resistant anodized aluminum • Compatible with standard racking, accommodating both top-down clamps and bottom-flange mounting		
<b>Cable</b>	• 90°C 12AWG PV wire		
<b>Junction Box</b>	• 3 bypass diodes	• 1000 VDC MC4 connectors	• Tigo TS4
<b>Grounding</b>	• Certified for Wiley Electronics WEEB™ grounding clips • Eight standard grounding locations per module for reduced ground wire length		

### QUALIFICATIONS

<b>Fire Rating</b>	Type I
<b>PID Free</b>	500+ hours
ARRA, BAA, and TAA Compliant	

### ELECTRICAL DATA\*

	350 SE	355 SE	360 SE	365 SE	370 SE
Maximum Power - P <sub>max</sub> (Wp)	350	355	360	365	370
Maximum Power Voltage - V <sub>mp</sub> (V)	38.55	38.74	38.94	39.12	39.32
Maximum Power Current - I <sub>mp</sub> (A)	9.08	9.16	9.25	9.33	9.41
Maximum Current - I <sub>sc</sub> (A) (O.C.)	12	12	12	12	12
Maximum Voltage (TS4L only) - V <sub>oc</sub> (V)	43.57	43.77	43.99	44.19	44.40
Open Circuit Voltage - V <sub>oc</sub> (V) (D.M.S.O)	47.43	47.64	47.87	48.08	48.31
Short Circuit Current - I <sub>sc</sub> (A) (D.M.S)	9.49	9.55	9.62	9.69	9.76
Module Efficiency	17.54%	17.79%	18.05%	18.30%	18.55%

### MECHANICAL DATA

<b>Dimensions</b>	1001 mm x 1993 mm x 40 mm
<b>Weight</b>	49 lbs/22.2kg

### MAXIMUM RATINGS

<b>Operational Temperature</b>	-40...+90°C
<b>Maximum System Voltage</b>	1000 VDC
<b>Maximum Design Load (UL 1703)</b>	113 psf/[5400pa]
<b>Max Series Fuse Rating</b>	15A
<b>Max Reverse Current</b>	15A

### TEMPERATURE RATINGS

<b>Nominal Operating Cell Temperature (NOCT)</b>	45.01°C
<b>Temperature Coefficient of P<sub>max</sub></b>	-0.39%/°C
<b>Temperature Coefficient of V<sub>oc</sub> (D.M.S.O)</b>	-0.29%/°C
<b>Temperature Coefficient of V<sub>oc</sub> (TS4 - L only)</b>	0.0%/°C
<b>Temperature Coefficient of I<sub>sc</sub></b>	+0.04%/°C
<b>Temperature Coefficient of V<sub>mp</sub></b>	-0.38%/°C

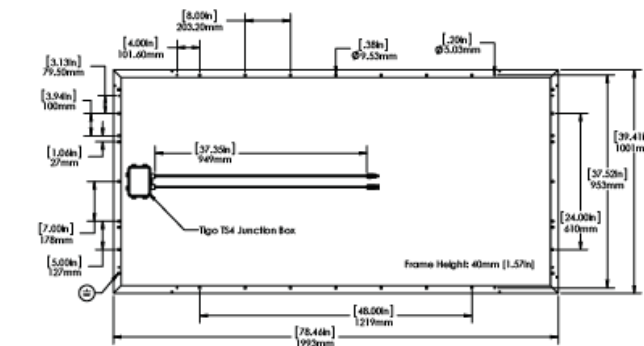
\*Electrical characteristics may vary within ±2% of the indicated values at Standard Test Conditions (STC): Irradiance of 1,000W/m<sup>2</sup>, AM 1.5 spectrum, cell temperature at 25°C.

Note: specifications subject to change without notice.



Choose from **Safety** | **Safety + Optimization** | **Safety + Optimization + Long Strings**  
All of these options include Monitoring

S4 Platform



# Spec Sheet Interpretation

For the 350 SE module, determine:

$P_{STC}^*$  \_\_\_\_\_

$V_{STC}^*$  \_\_\_\_\_

$V_{OC,STC}$  \_\_\_\_\_

$I_{STC}^*$  \_\_\_\_\_

$I_{SC,STC}$  \_\_\_\_\_

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<b>Temperature Coefficient of <math>V_{mp}</math></b>	-0.38%/°C

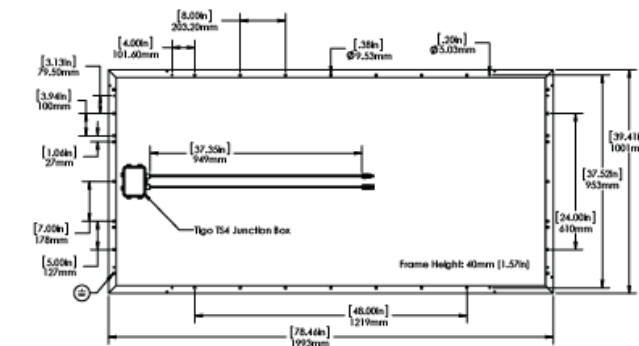
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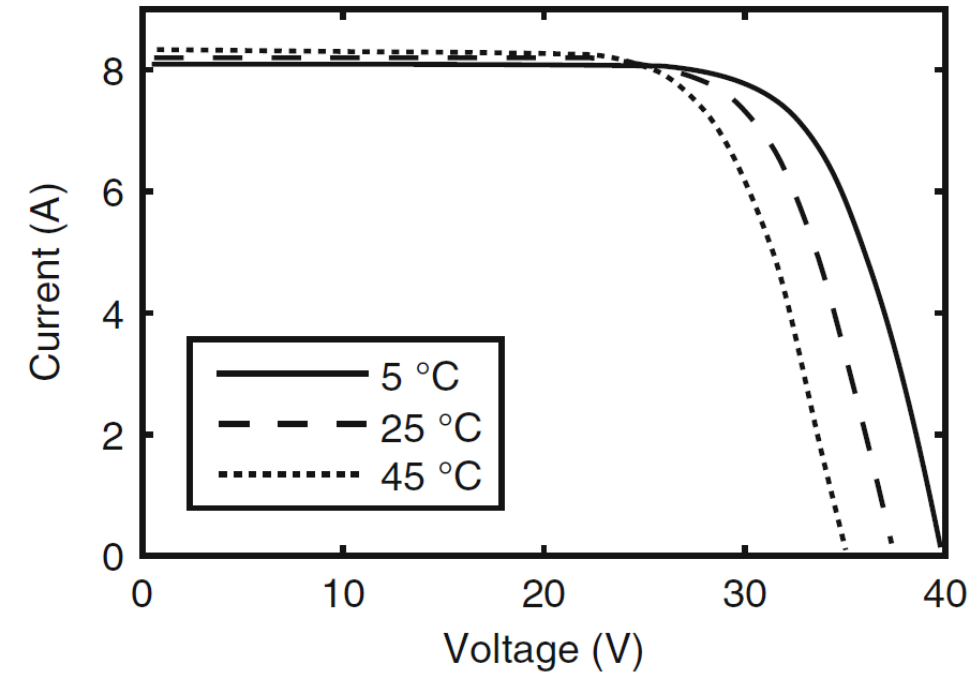
# Rated Power Interpretation

The 350 SE module will produce 350 W when the irradiance incident to it is  $1000 \text{ W/m}^2$ , the cell temperature is  $25^\circ \text{ C}$ , the spectral distribution of the irradiance is AM 1.5, and it is connected to a load that maximizes the power production under these conditions

We will generally assume that the load maximizes power production (i.e. the module operates at the MMP for a given set of conditions)

# Correcting for Temperature

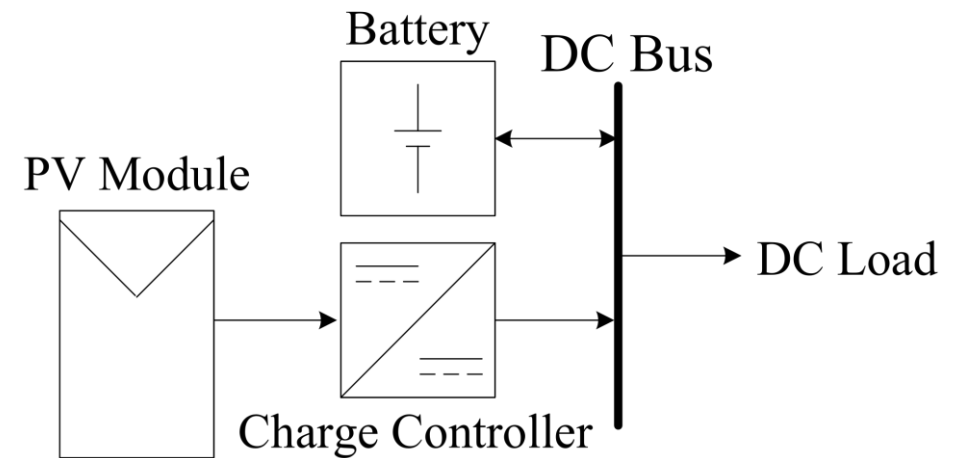
- I-V characteristic of PV module is influenced by the temperature
- Increasing temperature:
  - decreases voltage
  - increases current
- Change in voltage dominates the change in current, so power (voltage x current) decreases





# How does temperature affect the design and operation of off-grid PV systems?

- Charge controllers have a maximum input voltage rating; cold temperatures can increase the PV module voltage, possibly exceeding (and damaging) the charge controller
- Overall energy reduction will be reduced (perhaps significantly) due to temperature-related losses



# Correcting for Temperature

- Sensitivity of voltage, current, and power to temperature is empirically determined and reported by the manufacturer as “temperature coefficients”
- Coefficients are used to determine how open-circuit voltage, short-circuit current, and maximum change as the cell temperature deviates from 25 °C
- Power can be reduced by 10 to 15% because cell temperature is often >20 °C higher than that of STC

# Temperature Coefficients

$\alpha_v$ : open-circuit voltage temperature coefficient (%/K or %/C)

$\alpha_i$ : short-circuit current temperature coefficient (%/K or %/C)

$\alpha_p$ : maximum power temperature coefficient (%/K or %/C)

Temperature coefficients are provided in module spec sheet

# Correcting for Temperature

$$I_{sc}(T_c) = I_{sc}(25^\circ \text{ C}) \left( 1 + \frac{\alpha_i}{100} \times (T_c - 25) \right)$$

$$V_{oc}(T_c) = V_{oc}(25^\circ \text{ C}) \left( 1 + \frac{\alpha_v}{100} \times (T_c - 25) \right)$$

$$P^*(T_c) = P^*(25^\circ \text{ C}) \left( 1 + \frac{\alpha_p}{100} \times (T_c - 25) \right)$$

$V_{oc}$ : open-circuit voltage at 25° C (V)  
 $I_{oc}$ : short-circuit current at 25° C (A)  
 $T_c$ : temperature of the PV cell, (C)

Note that if the cell temperature is 25 °C, then no correction is applied. This makes sense since because 25 °C corresponds to STC

# Example 5.3

The temperature of a PV module with characteristics in the Table is 47 °C. Compute the short-circuit current, open-circuit voltage, and maximum power

Characteristic at STC	Value
Maximum Power	185.3 W
Optimum Operating Voltage ( $V^*$ )	36.4 V
Optimum Operating Current ( $I^*$ )	5.08 A
Open-Circuit Voltage ( $V_{OC}$ )	45.0 V
Short-Circuit Current ( $I_{SC}$ )	5.43 A
Short-Circuit Current Temp. Coeff. ( $\alpha_i$ )	0.055 %/K
Open-Circuit Temp. Coeff. ( $\alpha_v$ )	-0.37 %/K
Max. Power Temp. Coeff. ( $\alpha_P$ )	-0.48 %/K
NOCT	45 °C
Number of Cells	72 (series)

## Example 5.3

We assume that the module is operating at STC with the exception of temperature.

$$I_{sc}(T_c) = 5.43 \left( 1 + 0.00055 \times (47 - 25) \right) = 5.496 \text{ A}$$

$$V_{oc}(T_c) = 45.0 \left( 1 - 0.00370 \times (47 - 25) \right) = 41.337 \text{ V}$$

$$P^*(T_c) = 185.3 \left( 1 - 0.0048 \times (47 - 25) \right) = 165.732 \text{ W}$$

Notice that the magnitude of the percentage change in voltage is greater than that of the current, and the percentage change in power is greater still.

We shouldn't be concerned about the units being in degree Celsius, since the temperature is also expressed in these units (moreover, the difference in one degree Celsius is the same as the difference in one degree Kelvin)

# How do we determine the temperature of the cell?

- Manufacturers report the cell temperature when the PV module is exposed to “Standard Operating Conditions” (SOC)
- The reported temperature is “Nominal Operating Cell Temperature” (NOCT)
  - typically between 45 °C and 50 °C
- When module is not exposed to SOC (often the case), then the cell temperature will likely not be NOCT and the cell temperature must be estimated

# Standard Operating Conditions

## Standard Operating Conditions

- Irradiance:  $800 \text{ W/m}^2$  ( $0.8 G_{\text{STC}}$ )
- Ambient temperature:  $20 \text{ }^{\circ}\text{C}$
- Wind speed:  $1 \text{ m/s}$
- Spectral distribution: AM 1.5
- Power output:  $0 \text{ W}$  (no load)
- see IEC 61215 for test procedure

Do not confuse SOC with STC!



# Nominal Operating Cell Temperature

What happens when the module does not operate under SOC?

Approximate the cell temperature from:

$$T_c = T_a + (NOCT - 20) \frac{G}{800}$$

$T_a$ : ambient temperature (°C)

Other formulations exist for correcting for non-SOC wind speed, but it is not commonly employed

## Example 5.4

Compute the module temperature of a PV module whose reported NOCT is  $45^{\circ}\text{C}$  when exposed to irradiance of  $600\text{ W/m}^2$  and an ambient temperature of  $34^{\circ}\text{C}$ .

## Example 5.4

Compute the module temperature of a PV module whose reported NOCT is 45 °C when exposed to irradiance of 600 W/m<sup>2</sup> and an ambient temperature of 34 °C.

The PV module is not operating under SOC, and so a correction must be applied.

$$T_c = T_a + (NOCT - 20) \frac{G}{800} = 34 + (45 - 20) \frac{600}{800} = 52.75^\circ\text{C}$$

# Short-Circuit Current

- We generally only correct the short-circuit current based on irradiance (not temperature) using:

$$I_{STC}(G) = I_{SC,STC} \times \frac{G}{G_{STC}}$$

- Important when determining conductor ratings and charge controller compatibility

# Open-Circuit Voltage

- We generally only correct the open-circuit current based on temperature (not irradiance) using:

$$V_{oc}(T_c) = V_{oc}(25^\circ \text{C}) \left( 1 + \frac{\alpha_v}{100} \times (T_c - 25) \right)$$

- Important when determining insulation ratings and charge controller compatibility

# Correcting for Irradiance

- Irradiance varies throughout the day
- Whenever the irradiance differs from  $G_{STC}$  (1000 W/m<sup>2</sup>), the maximum power output is affected
  - maximum power is a function of irradiance  $P^*(G)$
- Maximum power is approximately proportional to the irradiance
  - doubling irradiance doubles maximum power

# Correcting for Irradiance

Maximum power accounting for actual irradiance

$$P^*(G) = P_{\text{STC}}^* \times \frac{G}{G_{\text{STC}}}$$

# Correcting for Irradiance

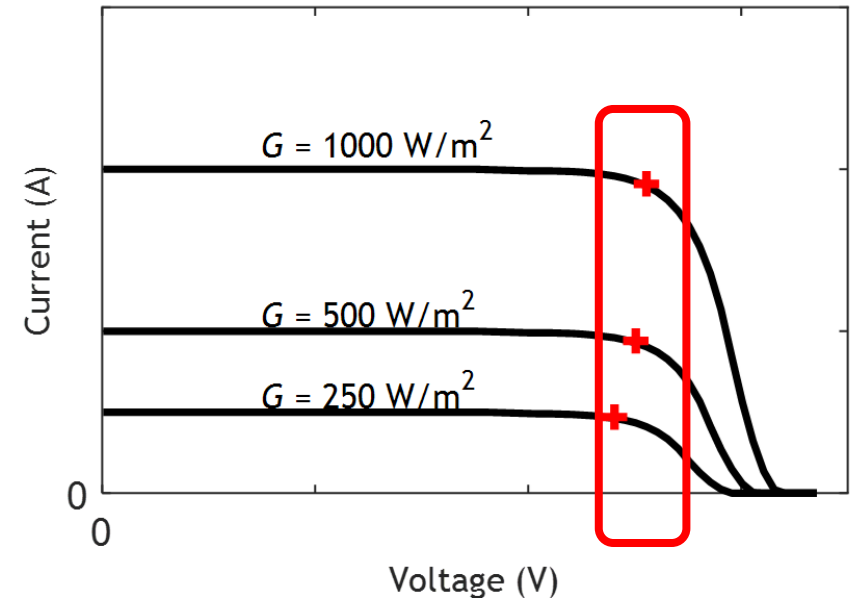
The model assumes (approximates)

$$V^*(G) = V_{\text{STC}}^*$$

Voltage at MPP is not affected by irradiance

$$I^*(G) = I_{\text{STC}}^* \times \frac{G}{G_{\text{STC}}}$$

Current at MPP changes in proportion to irradiance





# Example 5.5

Compute the maximum power of the PV module whose characteristics are described in the Table assuming the irradiance is  $600 \text{ W/m}^2$ .

Characteristic at STC	Value
Maximum Power	185.3 W
Optimum Operating Voltage ( $V^*$ )	36.4 V
Optimum Operating Current ( $I^*$ )	5.08 A
Open-Circuit Voltage ( $V_{OC}$ )	45.0 V
Short-Circuit Current ( $I_{SC}$ )	5.43 A
Short-Circuit Current Temp. Coeff. ( $\alpha_i$ )	0.055 %/K
Open-Circuit Temp. Coeff. ( $\alpha_v$ )	-0.37 %/K
Max. Power Temp. Coeff. ( $\alpha_P$ )	-0.48 %/K
NOCT	45 °C
Number of Cells	72 (series)

# Example 5.5

Compute the maximum power of the PV module whose characteristics are described in the Table assuming the irradiance is 600 W/m<sup>2</sup>.

$$P^*(G) = P_{\text{STC}}^* \times \frac{G}{G_{\text{STC}}} = 185.3 \times \frac{600}{1000} = 111.18 \text{ W}$$

Notice that power has been reduced

Characteristic at STC	Value
Maximum Power	185.3 W
Optimum Operating Voltage ( $V^*$ )	36.4 V
Optimum Operating Current ( $I^*$ )	5.08 A
Open-Circuit Voltage ( $V_{\text{OC}}$ )	45.0 V
Short-Circuit Current ( $I_{\text{SC}}$ )	5.43 A
Short-Circuit Current Temp. Coeff. ( $\alpha_i$ )	0.055 %/K
Open-Circuit Temp. Coeff. ( $\alpha_v$ )	-0.37 %/K
Max. Power Temp. Coeff. ( $\alpha_p$ )	-0.48 %/K
NOCT	45 °C
Number of Cells	72 (series)

# Correcting for Temperature & Irradiance

- Last example conveniently had an irradiance of  $1000 \text{ W/m}^2$  (STC)
- What about when the cell temperature AND irradiance deviate from STC?
  - mostly concerned about maximum power, not open-circuit voltage or short-circuit current

# PV Power Production

- Several different methods possible
- Osterwald's method:

$$P = P_{\text{STC}}^* \times \frac{G}{1000} \times \left( 1 + \frac{\alpha_P}{100} \times (T_c - 25) \right)$$

$P$ : power produced by PV module (W)  
 $P_{\text{STC}}^*$ : rated power under Standard Test Conditions (W)  
 $G$ : irradiance ( $\text{W}/\text{m}^2$ )  
 $\alpha_P$ : power coefficient (% /K)  
 $T_c$ : PV cell temperature (C)

# Osterwald's Method

$$P = P_{\text{STC}}^* \times \frac{G}{1000} \times \left( 1 + \frac{\alpha_p}{100} \times (T_c - 25) \right)$$

Corrects for irradiance

Corrects for temperature

## Example 5.6

Compute the maximum power of the PV module whose characteristics are described in the Table assuming the irradiance is  $600 \text{ W/m}^2$ , and the ambient temperature is  $34^\circ \text{C}$ , using Osterwald's method.

## Example 5.6

Compute the maximum power of the PV module whose characteristics are described in the Table assuming the irradiance is  $600 \text{ W/m}^2$ , and the ambient temperature is  $34^\circ \text{C}$ , using Osterwald's method.

$$\begin{aligned} P &= P_{\text{STC}}^* \times \frac{G}{1000} \times \left( 1 + \frac{\alpha_p}{100} \times (T_c - 25) \right) \\ &= 185.3 \times \frac{600}{1000} \times \left( 1 + \frac{-0.48}{100} \times (52.75 - 25) \right) = 96.37 \text{ W} \end{aligned}$$

# PV Power Production

PV power production is increased when:

- irradiance is high
- temperature is low
- load corresponds to the maximum power point (or maximum power point tracker is used)



# Soiling and Snow Coverage

- Complete or partial shading of PV module or array can severely reduce power production
- Energy output reduced 10-20% or more
- Partial shading reduces power production and can damage cells due to overheating
- Avoid locations where shading occurs



(courtesy: D. Nausner)



source: Global Himalayan Expedition

# Soiling

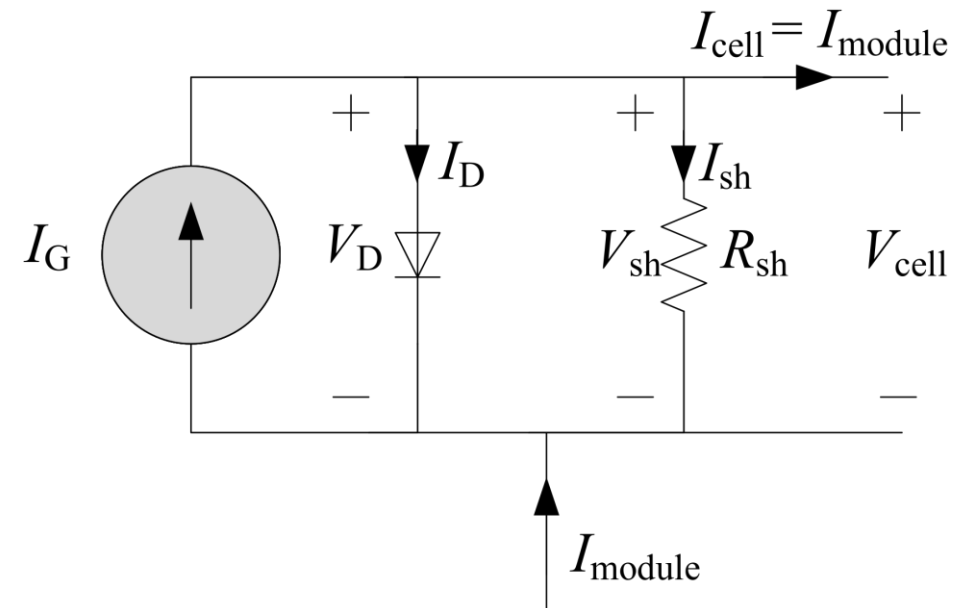
- Increased tilt reduces dust accumulation
- Dusty PV modules can be wiped clean



*(courtesy: H. Louie)*

# Shaded Cell

- Consider a PV module with one partially shaded cell
- Assume PV module's operating point is such that  $I_{\text{module}} > I_G$
- All cells are series-connected so that:  $I_{\text{cell}} = I_{\text{module}}$



# Shaded Cell

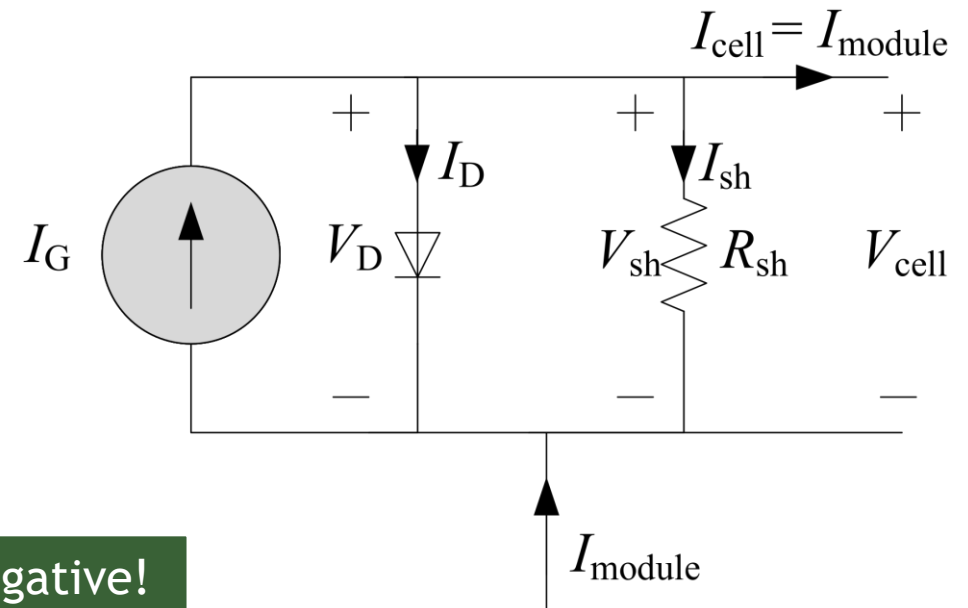
- KCL at the bottom node

$$I_{\text{module}} - I_G = -I_D - I_{\text{sh}}$$

With  $I_{\text{module}} > I_G$ , the diode and shunt currents and voltages must be negative

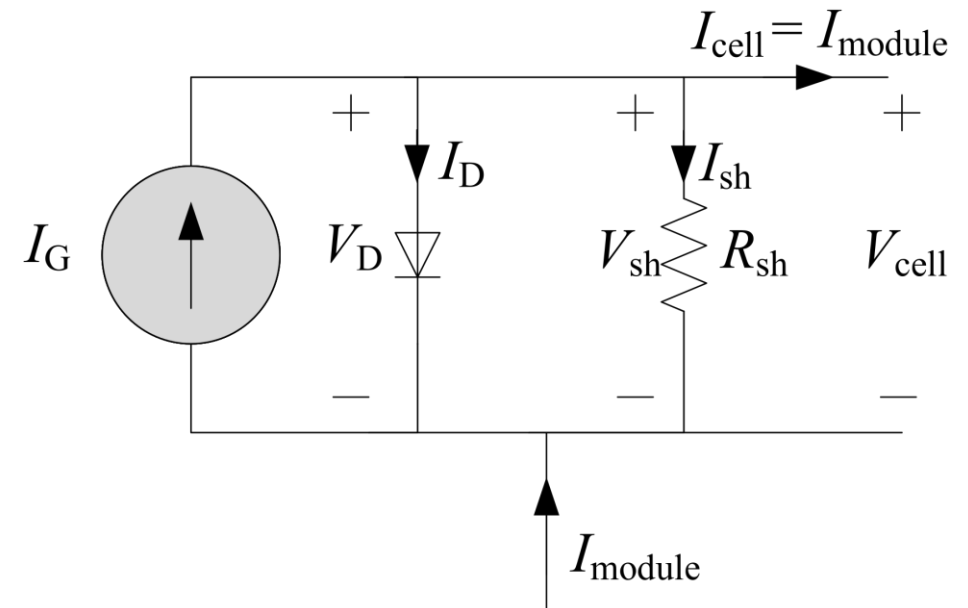
- Diode is reverse biased so  $I_D = 0$

and  $V_{\text{cell}} = -(I_{\text{module}} - I_G)R_{\text{sh}}$  the cell voltage is negative!

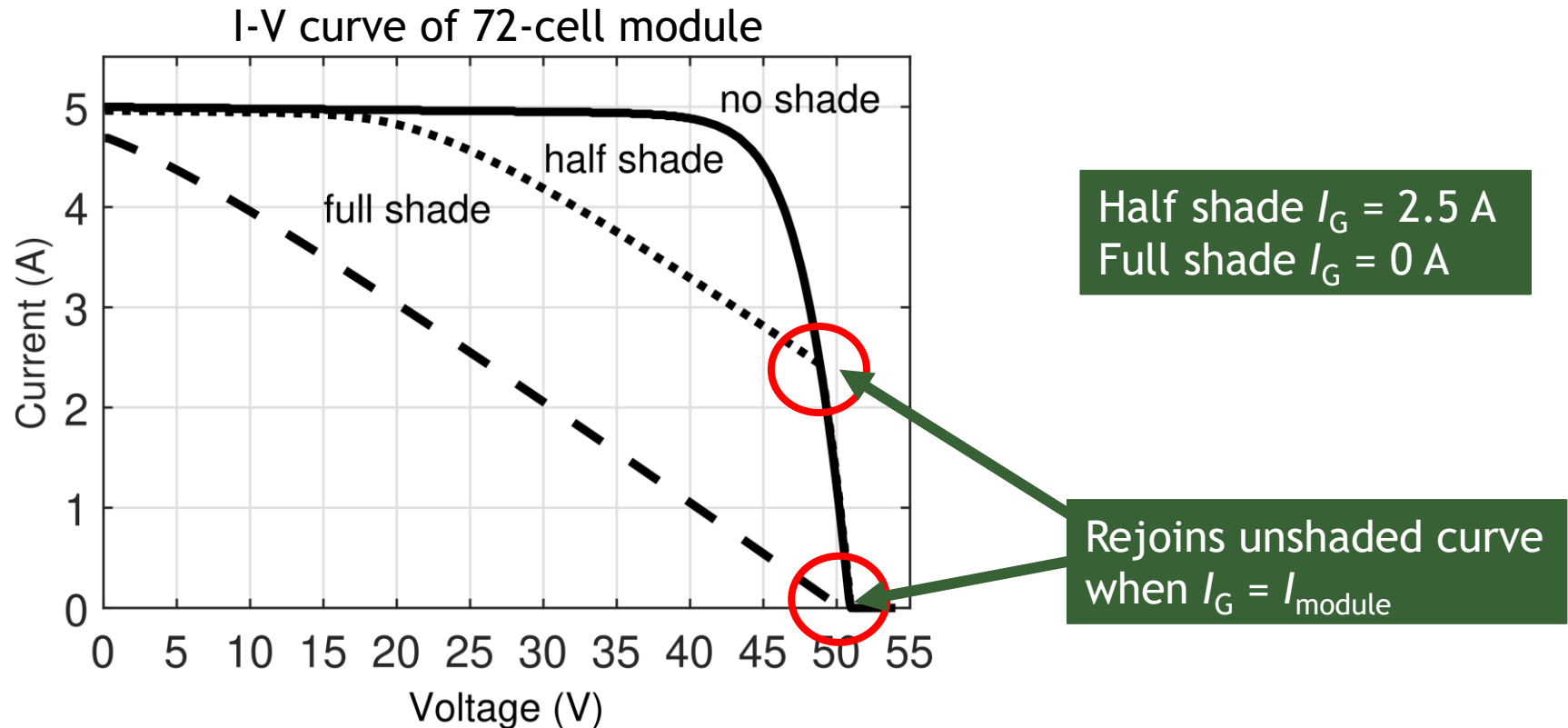


# Shaded Cell

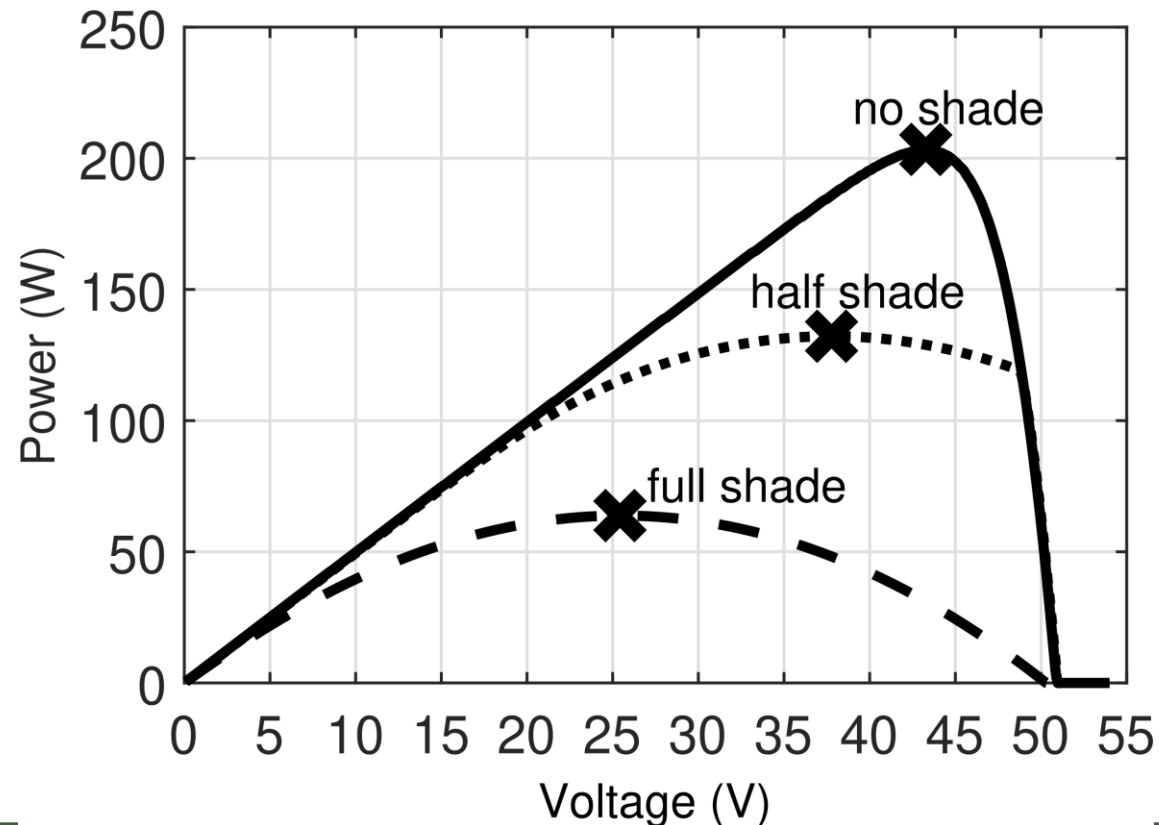
- Cell voltage is negative and its magnitude can exceed tens of volts
- Shunt resistance dissipates power
  - may cause damage or fire due to overheating
  - reduces power output by the PV module



# I-V Curve of Shaded Module with One Shaded Cell



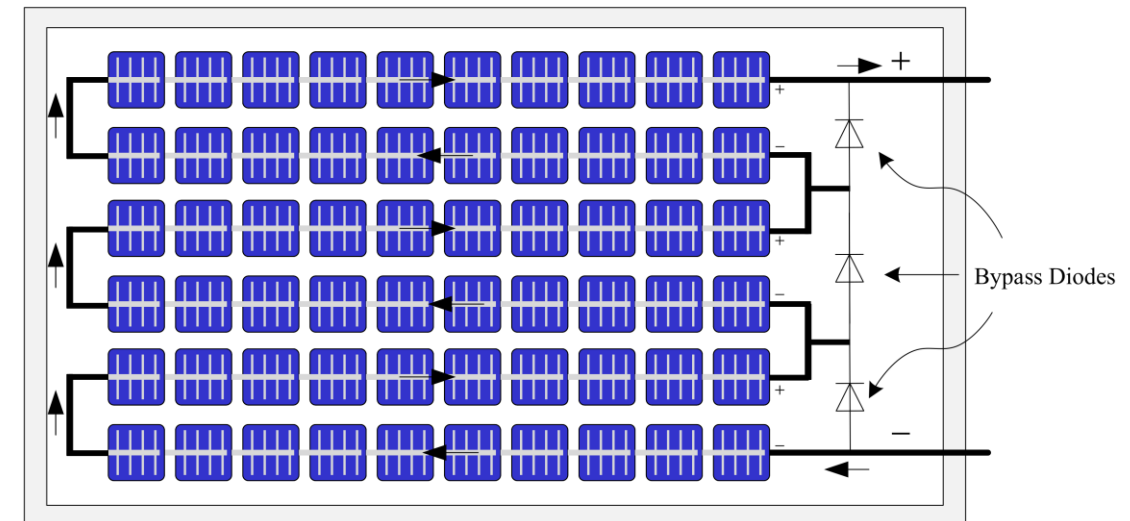
# P-V Curve of Shaded Module with One Shaded Cell



maximum power reduced due to shading AND voltage at which the MPP occurs changes

# Bypass Diodes

- Solution to partial shading is to use bypass diodes
- Provide a parallel path for a portion of the module current around shaded cell(s)
- Bypass diodes are integrated into most PV modules





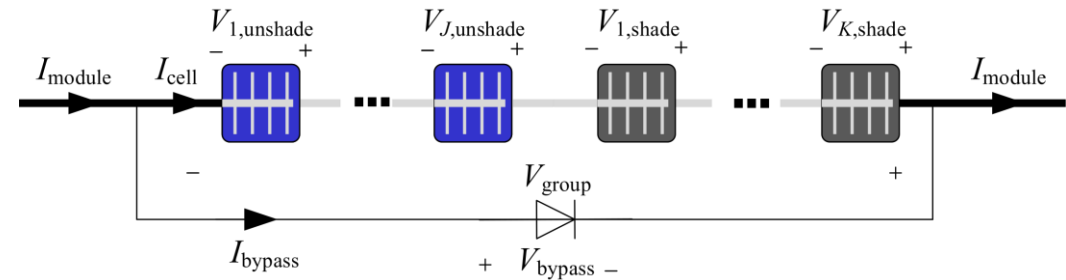
# Bypass Diodes

- Cells connected in parallel to a bypass diode are a “group”

$$V_{\text{group}} = \sum_{j=1}^J V_{j,\text{unshade}} + \sum_{k=1}^K V_{k,\text{shade}}$$

$$V_{\text{bypass}} = -V_{\text{group}}$$

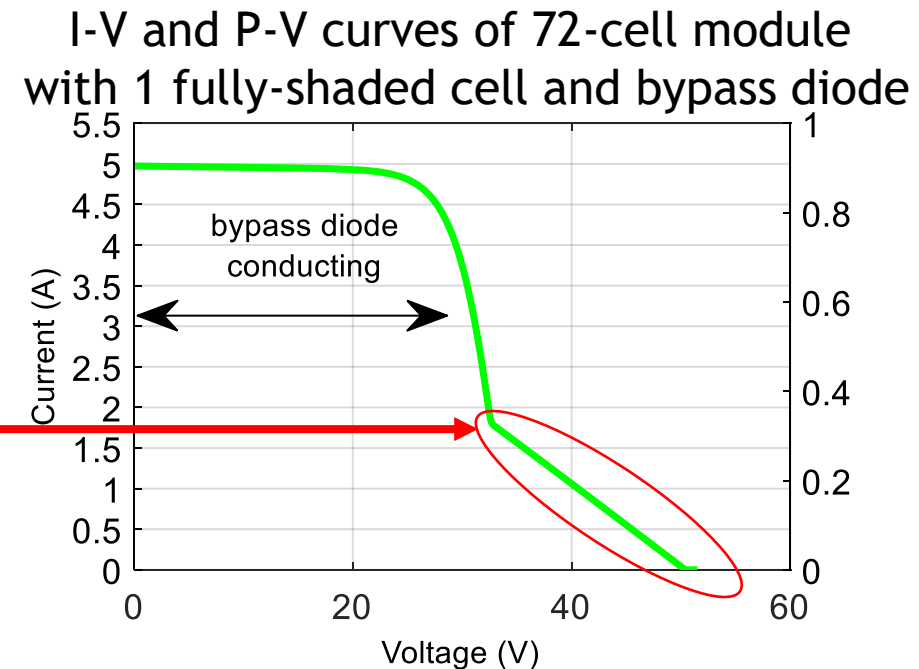
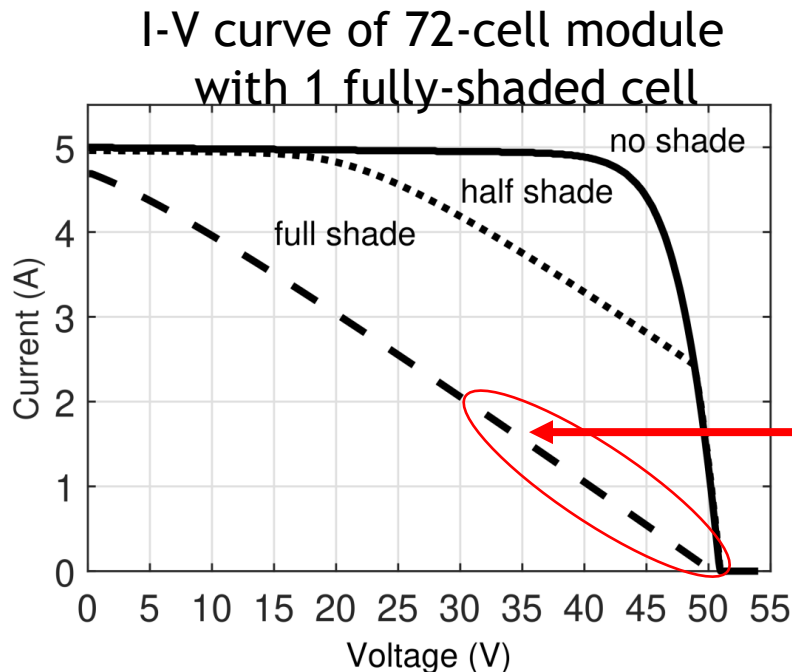
$$I_{\text{module}} = I_{\text{cell}} + I_{\text{bypass}}$$



When shaded cell(s) voltage is negative, the group voltage can be negative and a portion of the diode current conducts through the bypass diode

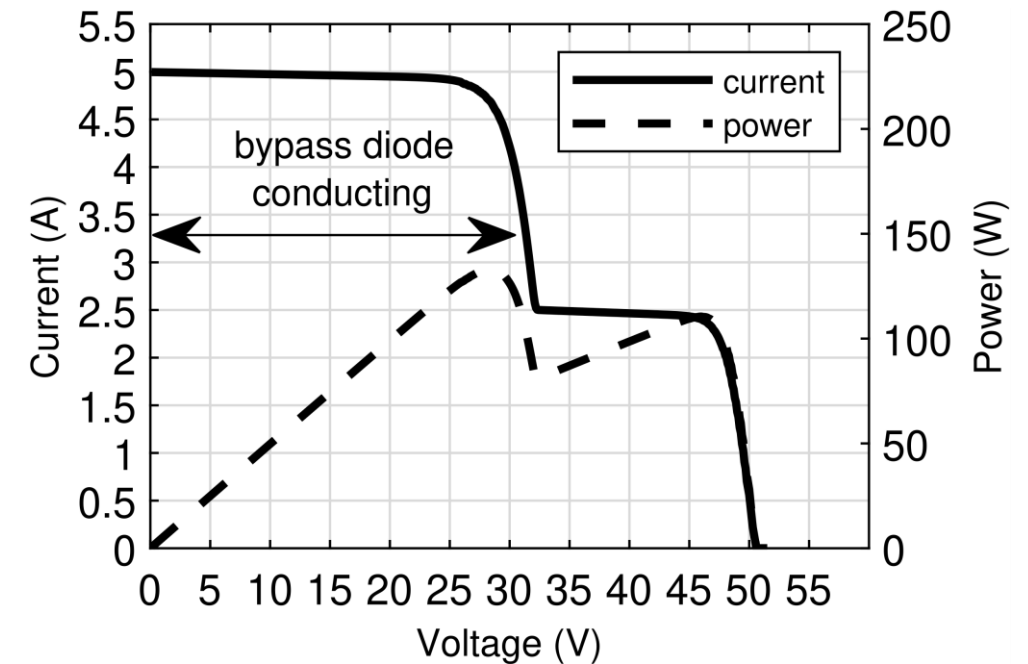
# I-V Curve with Bypass Diode

When bypass diode is not forward biased ( $V_{\text{bypass}} > 0$ ), the I-V curve resembles that of a PV module without a bypass diode



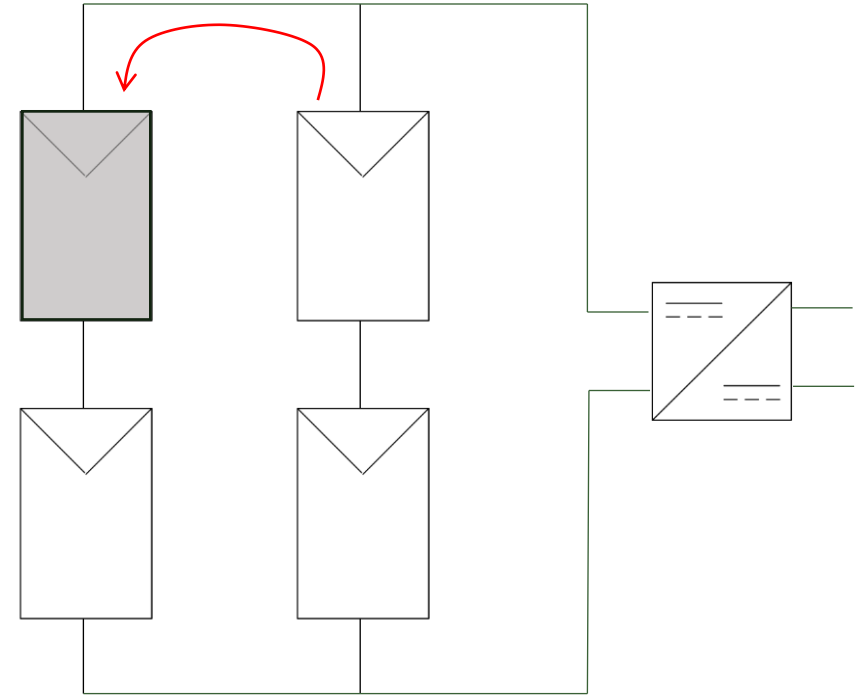
# Bypass Diodes

- Partial shaded conditions with bypass diodes can lead to strange P-V curves
- Two unequal “peaks”
- Can confuse MPPT algorithms, resulting in sub-maximal operation at the lower peak



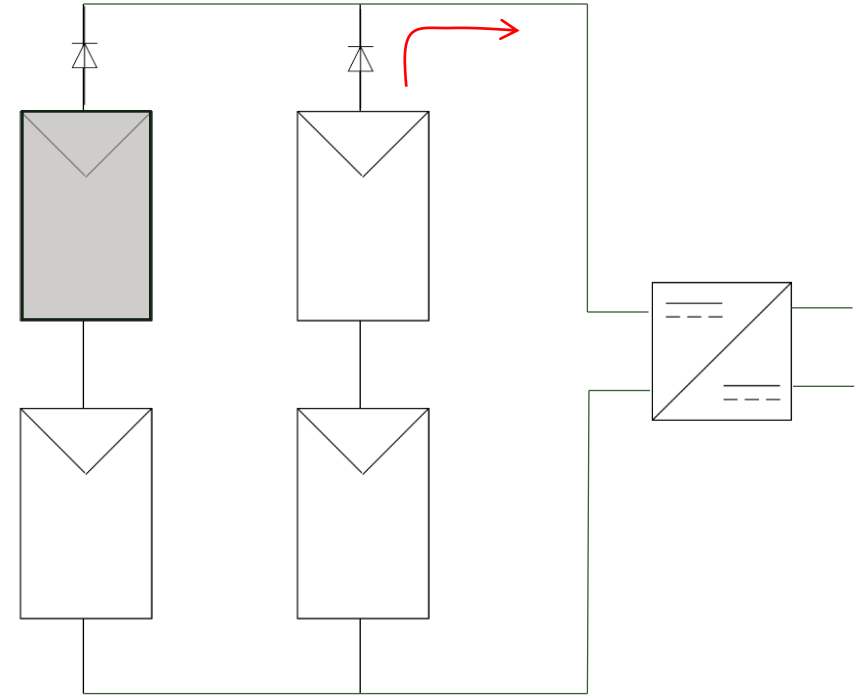
# Blocking Diodes

- Shading or other abnormal conditions can result in current of the opposite polarity in a PV module or array
- Any strings in parallel may have current flow through the shaded string



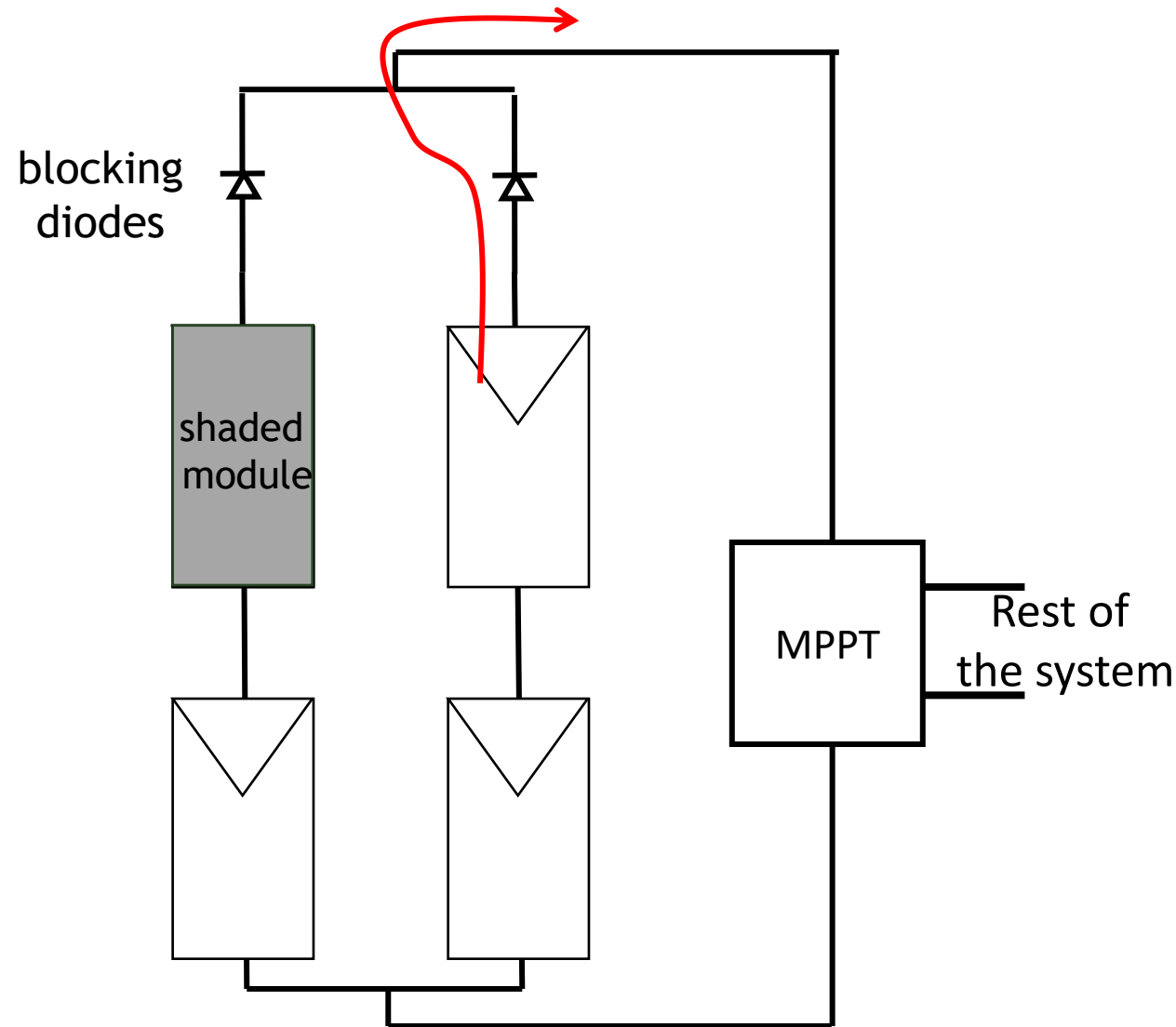
# Blocking Diodes

- Blocking diodes installed when strings are in parallel to prevent one string from sending current through the other
- Under unshaded operation, there is loss associated with the blocking diodes



# Blocking Diodes

- Blocking diodes installed when strings are in parallel to prevent one string from sending current through the other
- Under unshaded operation, there is loss associated with the blocking diodes



# Bifacial Modules

- New variant to traditional PV module
- Can convert reflected irradiance from the rear of the PV module
- Improves power production
- Highly dependent on orientation of module and albedo (reflection) of surface underneath



*(courtesy H. Louie)*

# Bifacial Modules

- Power produced by bifacial module is sum of front (f) and rear (r) -side power production, accounting for differing irradiance received

$$P = P_f(G_f) + P_r(G_r)$$

- Bifaciality coefficient relates rear-side power under STC to front-side power

$$\psi = \frac{P_{\text{STC},r}^*}{P_{\text{STC},f}^*}$$

usually 0.70 to 0.90



# Bifacial Modules

- Power is estimated as

$$P = P_f(G_f) + (\psi \times P_f(G_r))$$

- Osterwald's method can be adapted as:

$$P = P_{STC}^* \times \frac{G_f + \psi G_r}{1000} \times \left( 1 + \frac{\alpha_p}{100} \times (T_c - 25) \right)$$

# Bifacial Name Plate Irradiance (BNPI)

- Similar concept to STC
- Assumes irradiance of 1000 W/m<sup>2</sup> on front and 135 W/m<sup>2</sup> on rear
- In practice, irradiance on rear side varies widely

Notice:  $570 + (0.80 \times 0.135 \times 570) = 632 \text{ W}$

Characteristic at STC	Value
Maximum Power	570 W
Optimum Operating Voltage ( $V^*$ )	39.2 V
Optimum Operating Current ( $I^*$ )	14.56 A
Open-Circuit Voltage ( $V_{OC}$ )	46.4 V
Short-Circuit Current ( $I_{SC}$ )	15.49 A
Short-Circuit Current Temp. Coeff. ( $\alpha_i$ )	0.05 %/K
Open-Circuit Temp. Coeff. ( $\alpha_v$ )	-0.25 %/K
Max. Power Temp. Coeff. ( $\alpha_P$ )	-0.29 %/K
NOCT	41 °C
Number of Cells	132
Bifaciality Coeff.	0.80
Characteristic at BNPI	Value
Maximum Power	632 W
Open-Circuit Voltage ( $V_{OC}$ )	46.7 V
Short-Circuit Current ( $I_{SC}$ )	17.16 A

# Example 5.10

Consider the bifacial PV module described in the Table. The PV module is exposed to a front side irradiance of  $900 \text{ W/m}^2$  and rear side irradiance of  $100 \text{ W/m}^2$ . The cell temperature is  $44 \text{ }^\circ\text{C}$ . Determine the power output of the module.

Characteristic at STC	Value
Maximum Power	570 W
Optimum Operating Voltage ( $V^*$ )	39.2 V
Optimum Operating Current ( $I^*$ )	14.56 A
Open-Circuit Voltage ( $V_{OC}$ )	46.4 V
Short-Circuit Current ( $I_{SC}$ )	15.49 A
Short-Circuit Current Temp. Coeff. ( $\alpha_i$ )	0.05 %/K
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## Example 5.10

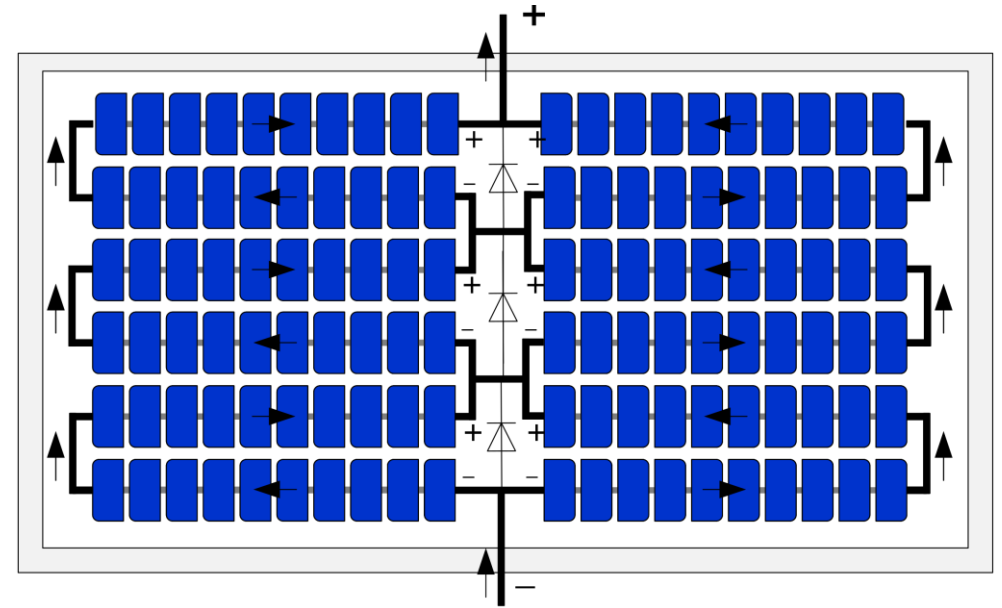
Consider the bifacial PV module described in the Table. The PV module is exposed to a front side irradiance of 900 W/m<sup>2</sup> and rear side irradiance of 100 W/m<sup>2</sup>. The cell temperature is 44 °C. Determine the power output of the module.

$$\begin{aligned} P &= P_{\text{STC}}^* \times \frac{G_f + \psi G_r}{1000} \times \left( 1 + \frac{\alpha_p}{100} \times (T_c - 25) \right) \\ &= 570 \times \frac{900 + (0.80 \times 100)}{1000} \times \left( 1 + \frac{-0.29}{100} \times (44 - 25) \right) = 527.8 \text{ W} \end{aligned}$$

Characteristic at STC	Value
Maximum Power	570 W
Optimum Operating Voltage ( $V^*$ )	39.2 V
Optimum Operating Current ( $I^*$ )	14.56 A
Open-Circuit Voltage ( $V_{\text{OC}}$ )	46.4 V
Short-Circuit Current ( $I_{\text{SC}}$ )	15.49 A
Short-Circuit Current Temp. Coeff. ( $\alpha_i$ )	0.05 %/K
Open-Circuit Temp. Coeff. ( $\alpha_v$ )	-0.25 %/K
Max. Power Temp. Coeff. ( $\alpha_p$ )	-0.29 %/K
NOCT	41 °C
Number of Cells	132
Bifaciality Coeff.	0.80
Characteristic at BNPI	Value
Maximum Power	632 W
Open-Circuit Voltage ( $V_{\text{OC}}$ )	46.7 V
Short-Circuit Current ( $I_{\text{SC}}$ )	17.16 A

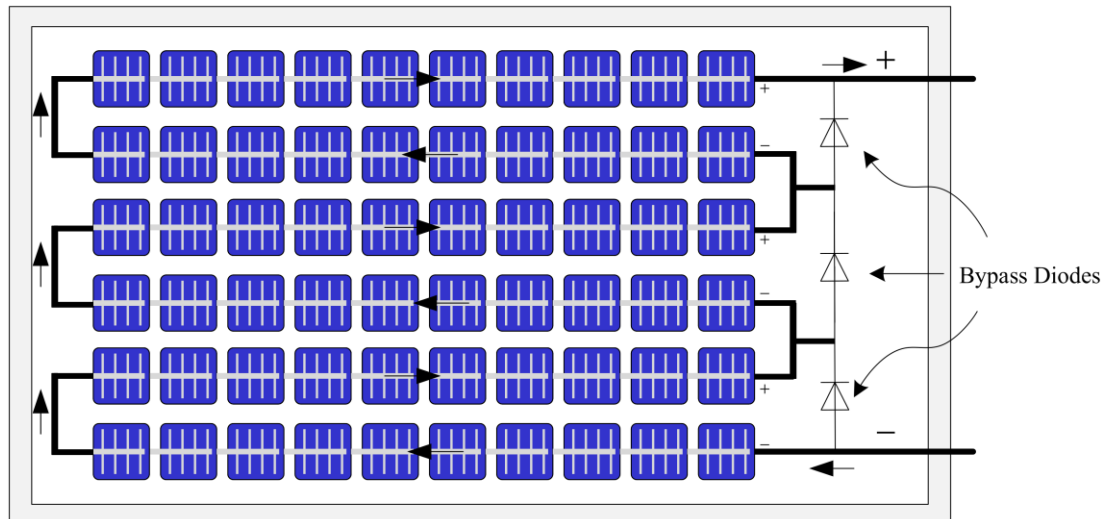
# Half-Cut Cell Modules

- Larger panels often use half-cut cells
- Regular cell is cut in half
- Arrangement in PV module is changed to make two sub-modules in parallel
- Reduces  $I^2R$  losses and effects of shading

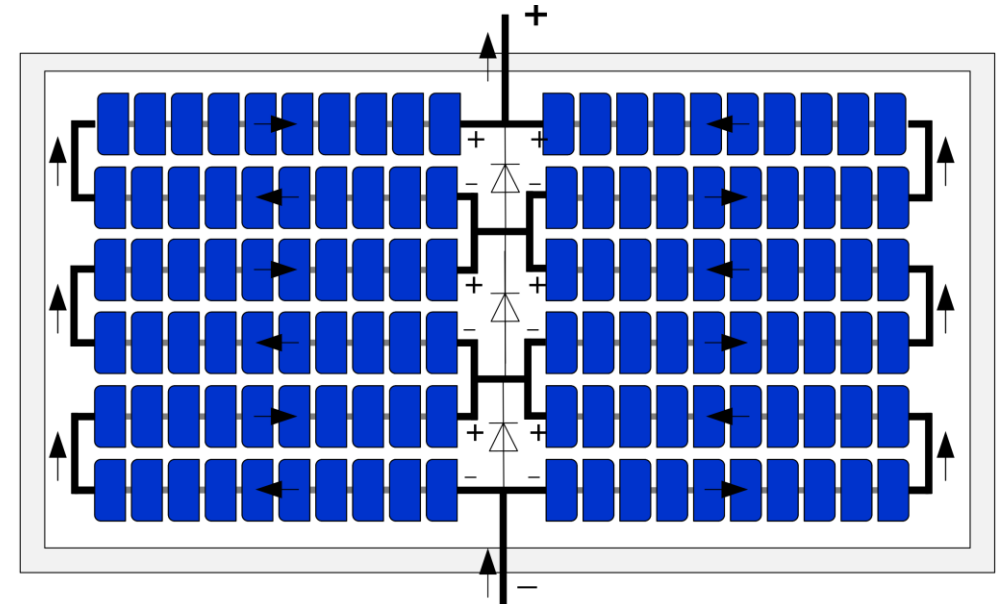


# Half-Cut Cell Modules

Traditional module with 60 cells



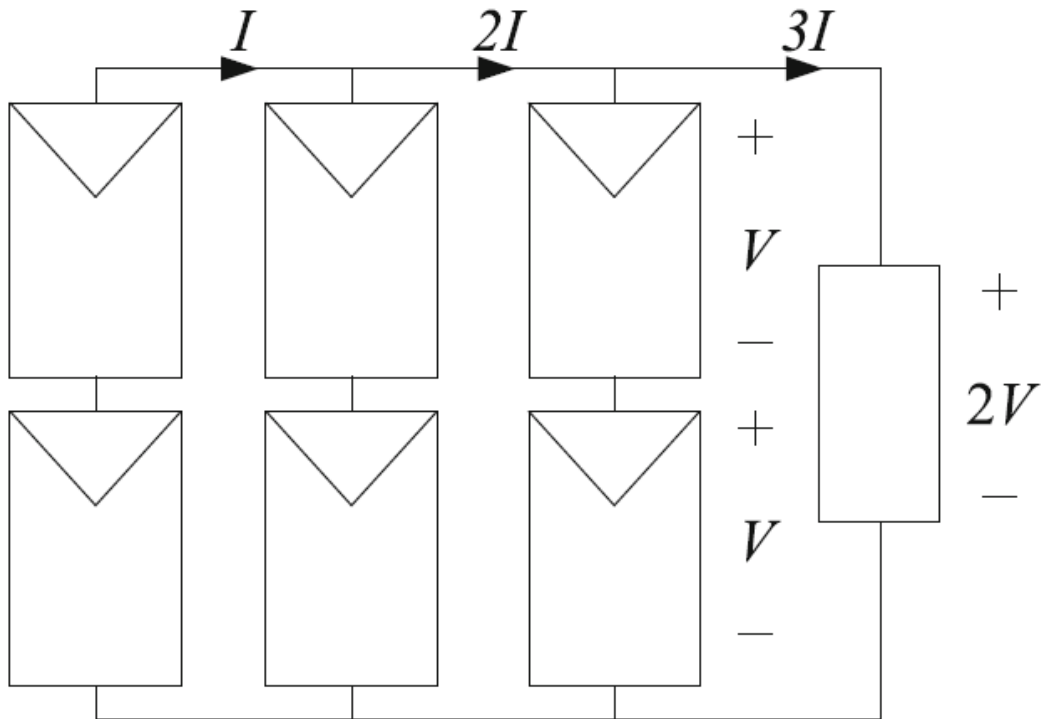
Module with 60 half-cut cells (120 halves)



# PV Arrays

- PV modules connected together are known as a *PV Array*
- Series-connected modules are known as “strings”
- Strings with the same number of series-connected modules can be connected in parallel
- Assume that all modules in the array are operating under the same conditions

# PV Arrays



This array has three strings of two modules

$$V_{\text{array}} = N_{\text{ser, str}} \times V$$

$$I_{\text{array}} = N_{\text{par}} \times I$$

$N_{\text{ser, str}}$ : number of modules connected in series per string  
 $N_{\text{par}}$ : number of strings connected in parallel



# PV Array Power

- Power produced by the array:

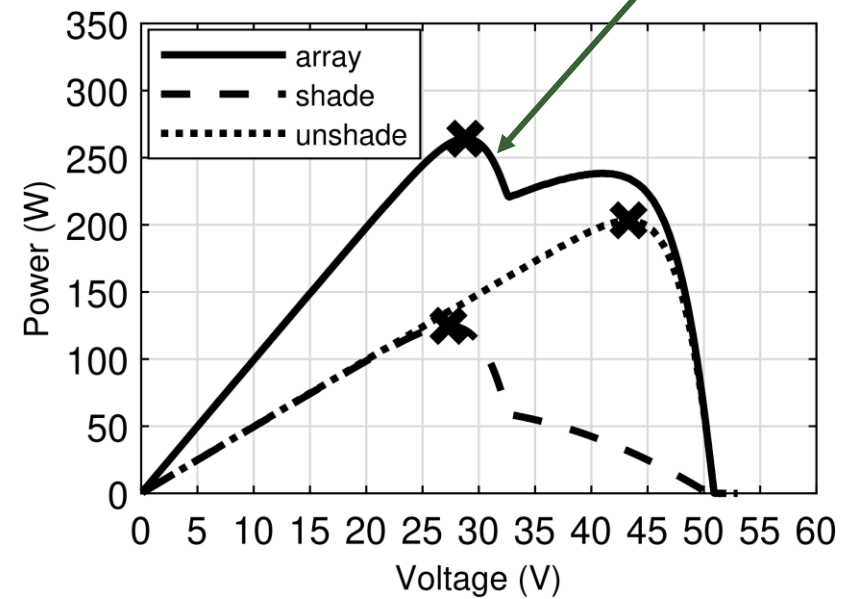
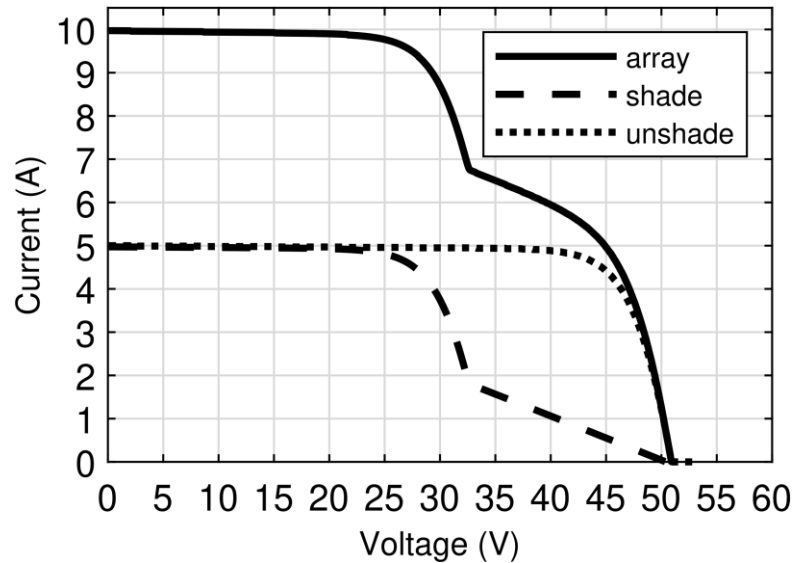
$$\begin{aligned}P_{\text{array}} &= V_{\text{array}} \times I_{\text{array}} = N_{\text{ser,str}} \times V \times N_{\text{par}} \times I \\&= N_{\text{ser,str}} \times N_{\text{par}} \times P \\&= \text{Number of modules} \times P\end{aligned}$$

- In other words, the power produced is independent of how the modules are connected (as long as each string has the same number of modules connected in series)

# Module Mismatch

- PV modules in an array have some variation in their irradiance and temperature
  - I-V and P-V curves do not exactly match
- Each module has a different maximum power point
- Modules in parallel operate at same voltage, modules in series operate at same current
- Modules with different P-V curves connected together cannot each operate at their own maximum power point
- Lost power production is known as “mismatch loss”

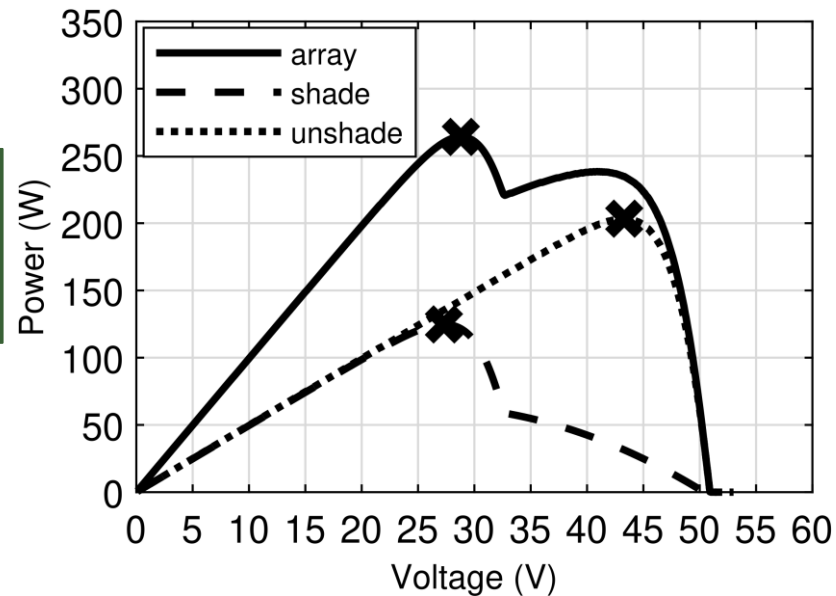
# Module Mismatch of Parallel Modules



# Module Mismatch of Parallel Modules

MPP shaded: 203 W at 43V  
MPP unshaded: 125 W at 27 V  
MPP array: 265 W at 28 V

Array MPP of 265 W is less than  
 $203 + 125 = 328$  W. Difference  
is the mismatch loss (63 W)



Parallel modules must operate at the same voltage.

MPP for array is different than MPP of each module individually

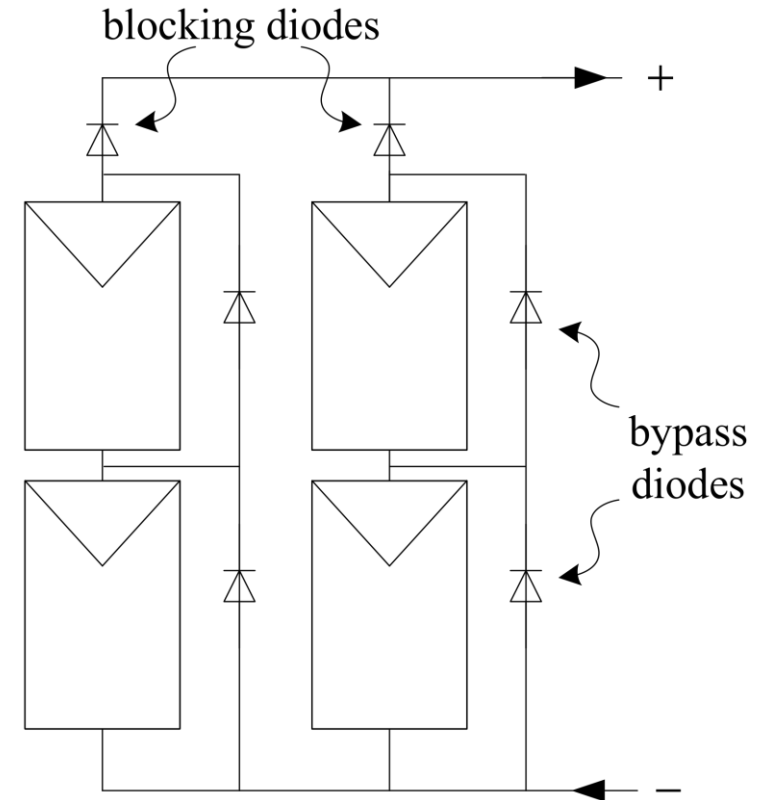
# Module Mismatch Mitigation

## Ways to minimize mismatch losses

- use identical PV modules in array
- avoid shading
- locate modules in an array near each other (with same orientation)
- connect fewer PV modules to each charge controller

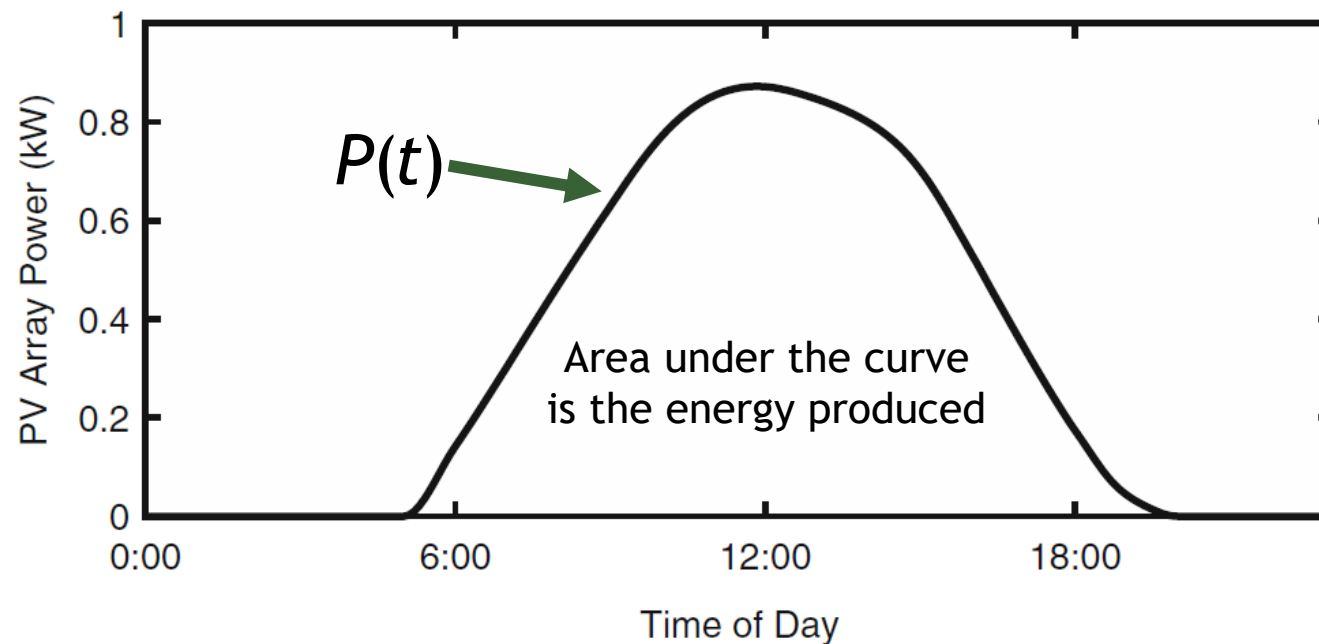
# External Diodes

- Large PV arrays may use external bypass diodes in case an entire module is shaded while others are not
- Similar concept as when bypass diodes are used inside an individual PV module



# Energy Production from PV Arrays

The energy produced by a PV array over the course of a day is found by integrating its power production



# Energy Production from PV Arrays

Integrate power between sunrise and sunset times (be careful of the units)

$$P(t) = P_{\text{STC}}^* \times \frac{G(t)}{1000} \times \left(1 + \alpha_p \times (T_c(t) - 25)\right)$$

We expect both the irradiance and cell temperature to vary with time ( $t$ )

$$E = \int_{t_{\text{rise}}}^{t_{\text{set}}} P(t) dt$$

$t_{\text{set}}$ : time the sun sets  
 $t_{\text{rise}}$ : time the sun rises



# Economic Considerations

- PV module costs have rapidly decreased (US\$250-US\$1000/kW)
  - require balance of systems components such as charge controllers and inverters
- No fuel cost, low operation and maintenance cost
- Energy cost US\$0.35-US\$0.60/kWh for mini-grids
- Potential to earn renewable energy credits

# Environmental Considerations

- Solar resource is sufficient in most areas with low electricity access
- Zero emissions, low water use, no noise pollution
- Large amount of land can be needed
- Minimal impact to wildlife
- Manufacturing PV modules is energy intensive, and mining of silicon, aluminum, and other metals can cause environmental harm

# Social Considerations

- PV modules can benefit most people in community, from small solar lanterns to large metro-grids
- Little health and safety concerns
- Can be a target for theft and vandalism
- External design expertise is likely needed for larger-capacity systems

# Other Considerations

- PV modules and their associated components are now widely available with mature supply chains
- PV system design can be challenging due to the variable and uncertain nature of irradiance

# Summary

- PV cells are p-n junctions
- PV modules produce maximum power at a single operating point
- Power produce depends on irradiance, temperature, and load
  - Osterwald's method and temperature coefficients are used to estimate power production
- Shading can dramatically reduce the power from a PV module (mismatch losses) and cause damage but is managed by bypass diodes
- New PV module technology
  - Bifacial: makes use of irradiance on front and rear of module
  - Half-cut cells: reduce losses and impact of shading
- PV arrays can increase the voltage and current from several PV modules connected together