Detectability.

This is the dual property of stabilizability. Let $A \in \mathbb{C}^{n \times n}$, $C \in \mathbb{C}^{p \times n}$ and consider the system

$$\begin{cases} \dot{x}(t) = Ax(t), & x(t) = \text{state at time } t \ge 0, \\ y(t) = Cx(t), & y(t) = \text{output at time } t \ge 0. \end{cases}$$

This system (or the pair (A,C)) is detectable if y(t) = 0 for all $t \ge 0$ implies that $x(t) \rightarrow 0$ (this is a short way of writing $\lim_{t\to\infty} x(t) = 0$). This property is weaker than (i.e., implied by) observability. Indeed, if (A,C) is observable and y(t) = 0 for all $t \ge 0$, then x(0) = 0 (see WEEK 8) and hence x(t)=0 for all $t \ge 0$.

Theorem (duality). (A,C) is detectable if and only if (A^*,C^*) is stabilizable.

The proof uses the decomposition $\mathbb{C}^n = \mathcal{N} + \mathcal{N}^{\perp}$, Where N is the unobservable space of (A,C), see p. 11 of WEEK 8. Detectability means that the restriction of A to N is stable, and the remaining part of the system is observable. Taking adjoints, we obtain that NI is an invariant subspace under A*, which is controllable via C*, and the remaining part of the system (A*,C*) is stable, which means that (A*,C*) is stabilizable. The argument works also in the converse direction, we omit the details.

$$\frac{\text{Example}}{\text{A} = \begin{bmatrix} 3 & 0 \\ 5 & -2 \end{bmatrix}} \quad C = \begin{bmatrix} 1 & 0 \end{bmatrix}$$

We see that $\operatorname{rank} \begin{bmatrix} A-\lambda I \\ C \end{bmatrix} = 1$ for $\lambda = -2$, but the rank is 2 for any other value of λ . (We have $\sigma(A) = \{-2, 3\}$.) Thus, (A,C) is not observable, but (A,C) is detectable. To check the definition of detectability, we see that y(t) = 0 for all $t \ge 0$ implies $x_1(0) = 0$, while $x_2(0)$ may be any complex number. We have $[x_1(t)] = 0$

 $\times (t) = \begin{bmatrix} \times_{1}(t) \\ \times_{2}(t) \end{bmatrix} = \begin{bmatrix} 0 \\ e^{-2t} \times_{2}(0) \end{bmatrix}$

and indeed we have $\lim_{t\to\infty} x(t) = 0$. For more complicated systems, checking the definition of detectability directly becomes more complicated, while doing the Hautus test remains relatively easy.

Using the duality theorems (from p.2 of WEEK 9 and p.1 of WEEK 10) we conclude that the pair

$$A^* = \begin{bmatrix} 3 & 5 \\ 0 & -2 \end{bmatrix} \qquad C^* = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

is not controllable, but it is stabilizable. [END OF EXAMPLE]

The properties of observability and controllability are generically true. This means the following: if we take the entries of the matrices A and C (of fixed dimensions) as independent random variables with a Gaussian probability density (over IR or over C), then (A,C) is observable with probability 1 ("almost sure"). —2—

Similarly, if we take the elements of A and B randomly (as before), then (A,B) is controllable with probability 1. It follows that stabilizability and detectability are also generically true. Using the duality theorem (from p.1), we can translate the Hautus Test for stabilizability (WEEK 9, p.9) into a Hautus Test for detectability:

Theorem. If $A \in \mathbb{C}^{n \times n}$ and $C \in \mathbb{C}^{p \times n}$, then (A,C) is detectable if and only if $\operatorname{rank} \left[\frac{\lambda \Gamma - A}{C} \right] = n \quad \forall \lambda \in \sigma(A)$ with $\operatorname{Re} \lambda \geq 0$.

Similarly, the definition of stabilizability (WEEK9) can be translated into an equivalent characterization of detectability:

Proposition. Let $A \in \mathbb{C}^{n \times n}$ and $C \in \mathbb{C}^{p \times n}$. Then (A,C) is detectable if and only if there exists $H \in \mathbb{C}^{n \times p}$ such that A + HC is stable.

In control engineering, it is sometimes needed to find a matrix H like in the above proposition. You will see later in this lecture why H is needed. To find H, we use again the translation into an equivalent dual problem, as follows: If (A,C) is given, we compute A^* and C^* (very easy). If (A,C) is detectable, then (A^*,C^*) is stabilizable. Using one of the methods described in WEEK 9 (Ackerman's formula or optimal control) we can find $F \in \mathbb{C}^{P \times n}$ such that $A^* + C^*F$ is stable $\Longrightarrow A + F^*C$ is stable. Thus, we can take $H = F^*$.

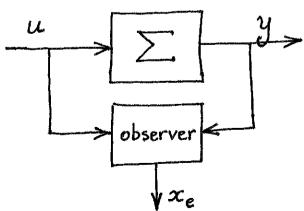


Ubservers and observerbased controllers

An observer is a system whose purpose is to estimate the state (or a function of the state) of another system. Here we discuss only LTI systems and full state observers.

Let I be an LTI system described by the matrices $A \in \mathbb{C}^{n \times n}$, $B \in \mathbb{C}^{n \times m}$, $C \in \mathbb{C}^{p \times n}$, $D \in \mathbb{C}^{p \times m}$ in the usual way. A (full state) observer for I is another system that receives the input u and output y of Σ as inputs, and the output of the observer is an estimate xe of the state x of \sum , such that $\lim \|x_{e}(t) - x(t)\| = 0$,

regardless of the input function u and the initial state x(0), see the figure. Note that I may be unstable, x(0) is unknown to the observer and u may be any signal (for which the state trajectory is defined).



Theorem. There exist observers for Σ if and only if (A,C) is detectable.

We shall prove this theorem. We prove the "only if" part first. If Σ is not detectable, then according to the definition of detectability (on p. 1) there exists $x(0) \in \mathbb{C}^n$ such that, when u=0, then y(t)=0 for all $t \ge 0$, but $\lim_{t\to\infty} x(t) \ne 0$. With this initial state x(0) and this input u=0, both inputs of the observer are zero for all $t \ge 0$, as if x(0)=0. Hence, there is no way for the observer to distinguish between the initial state x(0) and the initial state zero, so it is impossible to achieve $\lim_{t\to\infty} |x_e(t)-x(t)||=0$.

Now we prove the "if" part of the theorem, by constructing an observer (the simplest possible observer, conceptually). Since (A,C) is detectable, we can find $H \in \mathbb{C}^{n \times p}$ such that A + HC is stable. The observer is described by

$$\dot{x}_e = (A + HC)x_e + (B + HD)u - Hy$$

Let us check that this works. If we subtract from this equation (side from side) the equation of the system Σ , $\dot{x} = Ax + Bu$, and we take into account that y = Cx + Du, we obtain

 $\dot{x}_e - \dot{x} = Ax_e - Ax + HCx_e - HCx$.

Denoting $S = x_e - x$ (this is called the estimation error), we obtain $\dot{S} = (A + HC)S$.

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This shows that $S(t) \rightarrow 0$, regardless of the input u and regardless of the initial states. \square

The observer constructed on p.5 is called the Kalman observer, it was invented around 1960.

The Kalman observer has the same order as the plant (n). It is possible to construct (by a more complicated design procedure) observers of lower order (sometimes called Luenberger observers), we do not discuss this. However, we give a very simple example of a lower order observer, which should convey the idea:

Example:

Consider A and C as on p. 2 and $B = \begin{bmatrix} b_1 \\ b_2 \end{bmatrix}$ (the numbers b_1, b_2 do not matter) and D = 0. $y(t) = C \times (t) = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = x_1(t)$. Thus, there is no need to estimate $x_1(t)$, we already know it. We have $\dot{x}_2(t) = 5x_1(t) - 2x_2(t) + b_2 u(t)$

The subsystem with state x_2 { we may regard these } (and inputs u, y) is stable, so that we do not need to search for H, take H = 0. The observer for x_2 : $x_{2e}(t) = -2x_{2e} + b_2u(t) + 5y(t)$.

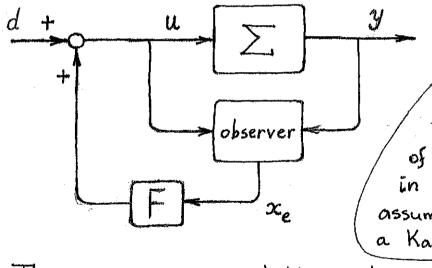
If we denote $S = x_{2e} - x_2$, then $\dot{S} = -2S$, so that $S \rightarrow 0$. Our observer is of order 1. -6—
[END OF EXAMPLE]

How to build a stabilizing controller using an observer:

If I is a plant described by the matrices A, B, C and D and (A,B) is stabilizable, then we can stabilize the system by state feedback:

$$u = Fx + d$$
 ($d = the new input$)

where F is chosen such that A+BF is stable. If x is not available to the controller, but (A,C) is detectable, then the idea is to replace in the above formula x with xe, where xe is an estimate of x, provided by an observer:



This diagram works for any type of observer. However, in the sequel, we assume that we have a Kalman observer.

This system is stable, because

$$\dot{x} = Ax + Bu = Ax + B(Fx_e + d)$$

$$= Ax + BF(x + \delta) + Bd$$

$$= (A + BF)x + BF\delta + Bd.$$

Choosing the state variables of the closed-loop system to be x and δ , we obtain

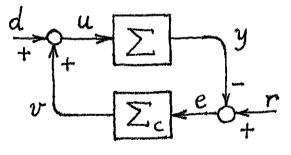
$$\frac{d}{dt} \begin{bmatrix} x \\ S \end{bmatrix} = \begin{bmatrix} A + BF & BF \\ O & A + HC \end{bmatrix} \begin{bmatrix} x \\ S \end{bmatrix} + \begin{bmatrix} B \\ O \end{bmatrix} d.$$

From the block-triangular structure of the large square matrix above it follows that

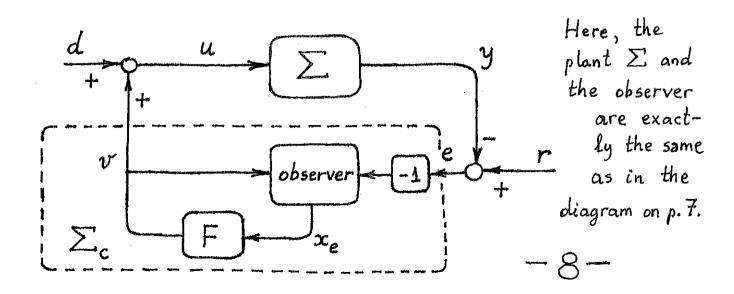
$$\sigma\left(\begin{bmatrix} A+BF & BF \\ O & A+HC \end{bmatrix}\right) = \sigma(A+BF) \cup \sigma(A+HC) \subset \mathbb{C}_{-}$$

So that the system is indeed stable. The above decomposition of the closed-loop eigenvalues into the sets $\sigma(A+BF)$ and $\sigma(A+HC)$ is called the separation principle.

We want to derive a stabilizing controller Σ_c for the plant Σ , which receives r-y as input, connected to the plant as shown in the standard



block diagram shown here (as studied from WEEK 2 onwards). For this, we modify the block diagram on p.7 as follows:



This diagram is not equivalent to the one on p.7, for two reasons: (1) we have the new signal r, (2) the input from the left of the observer is Fx_e , instead of Fx_e+d . However, the two diagrams (from p.7 and from the bottom of p.8) are equivalent if d=0 and r=0. Since the closed-loop system shown on p.7 is stable, it follows that also the one on p.8 is stable (since stability does not depend on the external signals). Thus, the system shown in the big dotted frame on the bottom of p.8 is a stabilizing controller Σ_c for the plant Σ . Its equations are

$$\begin{cases} \dot{x}_e = (A + HC)x_e + (B + HD)Fx_e + He \\ v = Fx_e \end{cases}$$

Thus, it is described by the matrices Ac, Bc, Cc and Dc defined by

$$A_c = A + BF + HC + HDF$$
, $B_c = H$, $C_c = F$, $D_c = O$.

The controller Σ_c may be unstable (but the closed-loop system is stable). Note that in this closed-loop system it is not true that $x_e-x\to 0$.

The above controller is stabilizing, but there is no guarantee that it will have good tracking properties (i.e., e may not be small).

Theorem. If Σ is a plant described by the matrices A,B,C,D then a stabilizing controller Σ_c exists for Σ if and only if (A,B) is stabilizable and (A,C) is detectable.

We prove this theorem: If (A,B) is slabilizable and (A,C) is detectable, then a stabilizing controller Ic can be found as described on p. 8-9. Conversely, if a stabilizing controller Σ_c exists, then we connect Σ and Σ_c in feedback (see the figure on p.8), obtaining a stable system. For any initial state x_0 of Σ , we obtain (assuming d=0, r=0) an input function u such that $\lim_{t\to\infty} u(t) = 0$ (because uis an output of the closed-loop system) and $\lim_{t\to\infty} x(t) = 0$. According to the proposition on p.7 of WEEK 9, it follows that (A,B) is stabilizable. It remains to show that (A,C) is detectable. Suppose that $x_0 \in \mathbb{C}^n$ is an initial state of Σ with the following property: if u=0then y=0 (for all $t\geq 0$). In the closed-loop system, consider the initial state of Ic to be O. Then (with d=0 and r=0) we have u=0 and y=0 (for all $t\geq 0$). Because the closed-loop system is stable, we have $\lim_{t\to\infty} x(t)=0$. By definition, it follows that (A,C) is detectable. \square

Suppose that an unstable (possibly MIMO) transfer Sunction P is given, and we want to find a controller transfer function C such that their standard feedback connection (as in the figure) is stable d pup y

+

C e o r (in the sense discussed in WEEK 2). How can we find such a C?

According to the material on p. 7-8 here, we may construct a minimal realization for P, denoted (A,B,C,D), then (A,B) is controllable and (A,C) is observable (see the last theorem on p. 5 of WEEK9). Then we may construct a stabilizing controller for (A,B,C,D) (as on p.7-8) and C may be taken to be the transfer function of this controller. & Po(0) is onto }

An application: suppose that a (possibly unstable, possibly MIMO) transfer function P is given and we want that its output w should track any constant reference signal r. Then we connect a PI controller $C_{p_1}(s) = K(1 + \frac{1}{75})$ such that its error &=w-r, and + Po + & Cps y
we search for a sta-C -3-0-0 bilizing controller for the plant $P = C_{P_1}P_0$ (think about why).

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