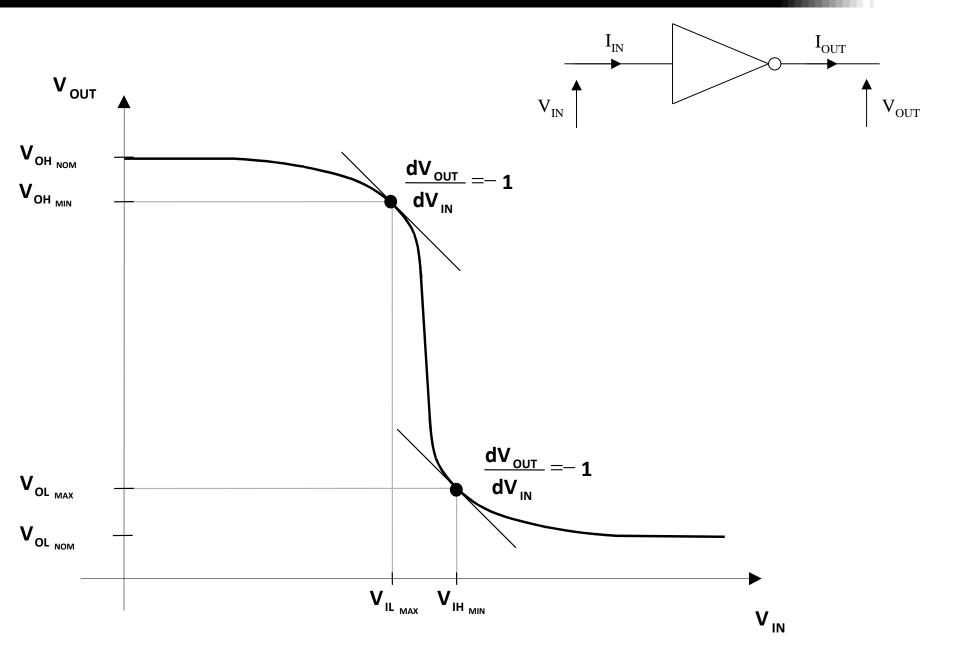
A.A. 2021-2022

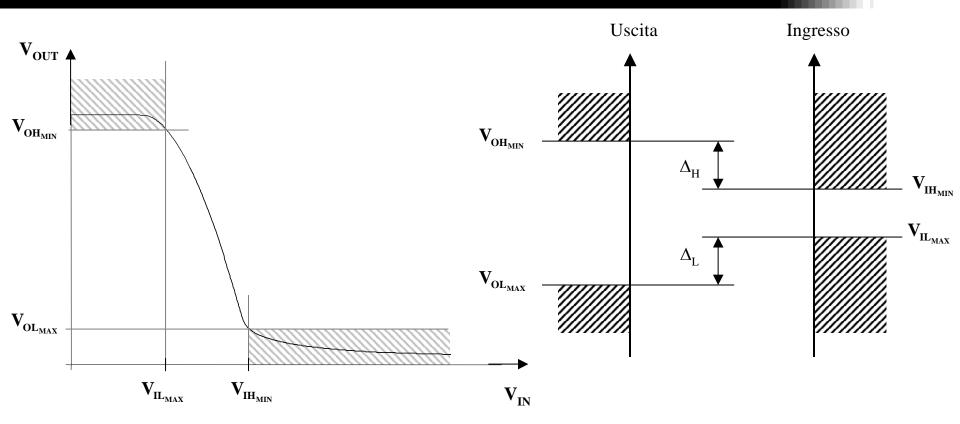
Elementi di Elettronica (INF) Prof. Paolo Crippa

Inverter

Caratteristiche dell'Inverter



Margini di Immunità ai Disturbi



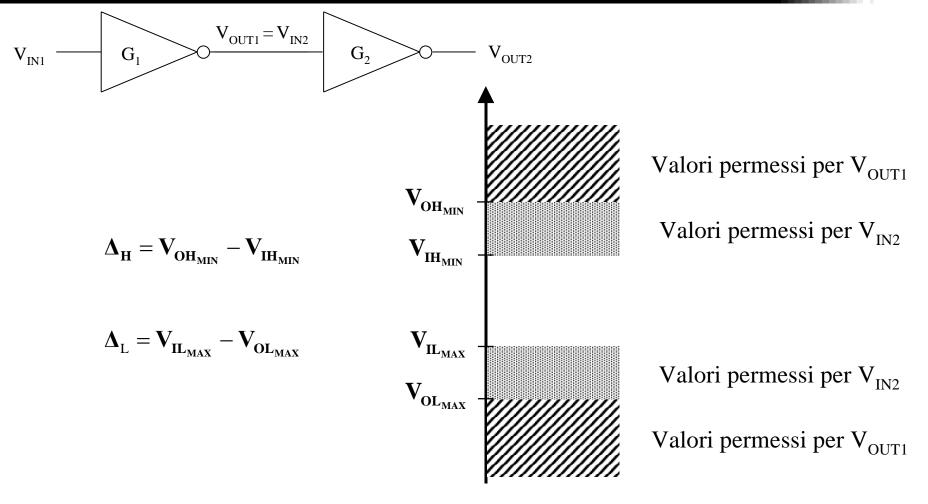
In condizioni statiche la porta deve lavorare in una delle regioni con

$$|\mathbf{A}_{\mathbf{v}}| < 1$$

deve essere:

$$V_{IL_{MAX}} > V_{OL_{MAX}}$$
 $V_{OH_{MIN}} > V_{IH_{MIN}}$

Margini di Immunità ai Disturbi



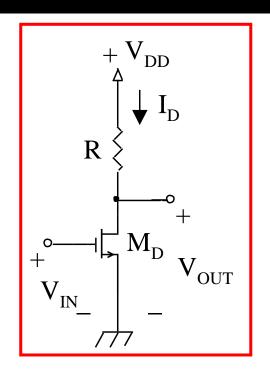
 $\Delta_{\rm H}$ = margine di immunità ai disturbi sui valori alti

 Δ_{L} = margine di immunità ai disturbi sui valori bassi

margine di immunità della porta = min (Δ_{H}, Δ_{L})

(caso peggiore)

Inverter NMOS con Carico Resistivo



$$I_{D} = \frac{V_{DD} - V_{OUT}}{R} =$$

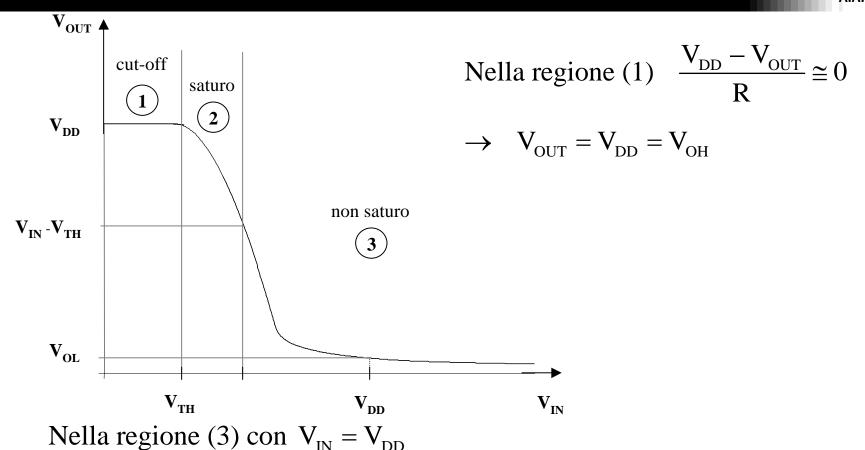
$$I_{\text{sub}}$$
, per $V_{\text{IN}} \leq V_{\text{TH}}$ Cut - off (1)

$$\begin{cases}
\frac{\beta}{2} \cdot \left(V_{IN} - V_{TH}\right)^2 & \text{per } V_{IN} \ge V_{TH}, \text{ per } V_{OUT} \ge V_{IN} - V_{TH} \\
& \text{Saturazione}
\end{cases}$$
(2)

$$\beta \cdot \left[\left(V_{IN} - V_{TH} \right) \cdot V_{OUT} - \frac{V_{OUT}^{2}}{2} \right] \quad \text{per } V_{IN} \ge V_{TH} ,$$

$$\text{per } V_{OUT} \le V_{IN} - V_{TH} \quad \textbf{Triodo} \quad (3)$$

Inverter NMOS con Carico Resistivo



$$\frac{V_{DD} - V_{OL}}{R} = \beta \cdot \left[\left(V_{DD} - V_{TH} \right) \cdot V_{OL} - \frac{1}{2} \cdot V_{OL}^{2} \right]$$

$$V_{OL} \cong \frac{V_{DD}}{1 + \beta \cdot R \cdot (V_{DD} - V_{TH})} \rightarrow 0V$$

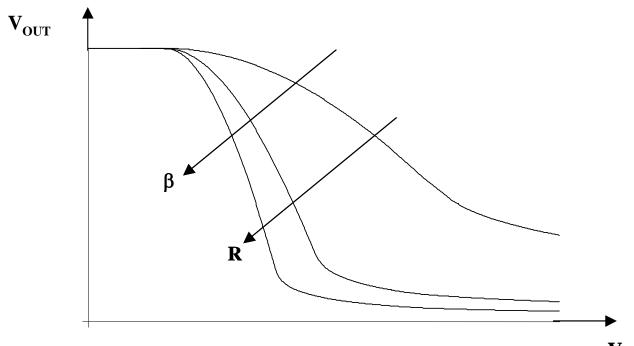
Inverter NMOS con Carico Resistivo

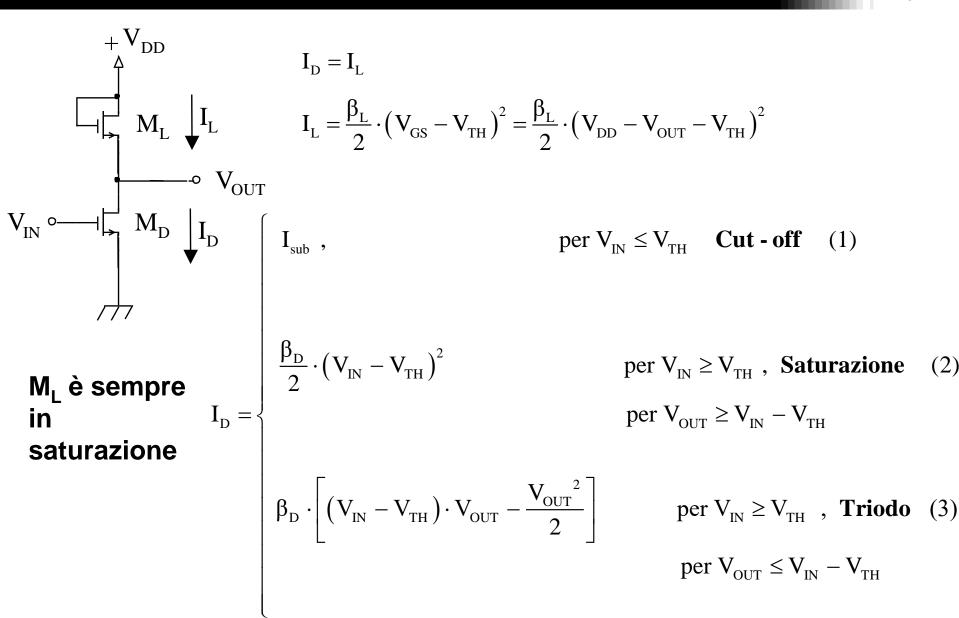
La pendenza nella regione (2) è

$$\frac{dV_{\text{OUT}}}{dV_{\text{IN}}} = A_{\text{v}} \rightarrow -\frac{1}{R} \cdot \frac{dV_{\text{OUT}}}{dV_{\text{IN}}} = \beta \cdot (V_{\text{IN}} - V_{\text{TH}})$$

$$A_{v} = \frac{dV_{OUT}}{dV_{IN}} = -\beta \cdot (V_{IN} - V_{TH}) \cdot R$$

 A_v aumenta in modulo all'aumentare di R e β .





$$I_D = I_L$$

$$I_{L} = \frac{\beta_{L}}{2} \cdot \left(V_{GS} - V_{TH}\right)^{2} = \frac{\beta_{L}}{2} \cdot \left(V_{DD} - V_{OUT} - V_{TH}\right)^{2}$$

$$I_{\text{sub}}$$
,

per
$$V_{IN} \leq V_{TH}$$
 Cut - off (1)

$$M_L$$
 è sempre in $I_D =$ saturazione

$$\frac{\beta_{\rm D}}{2} \cdot \left(V_{\rm IN} - V_{\rm TH}\right)^2$$

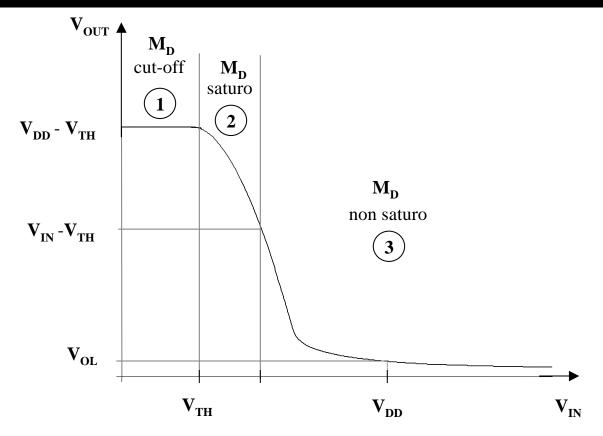
per
$$V_{IN} \ge V_{TH}$$
, Saturazione (2

per
$$V_{OUT} \ge V_{IN} - V_{TH}$$

$$\beta_{D} \cdot \left[\left(V_{IN} - V_{TH} \right) \cdot V_{OUT} - \frac{{V_{OUT}}^{2}}{2} \right]$$

per
$$V_{IN} \ge V_{TH}$$
, **Triodo** (3)

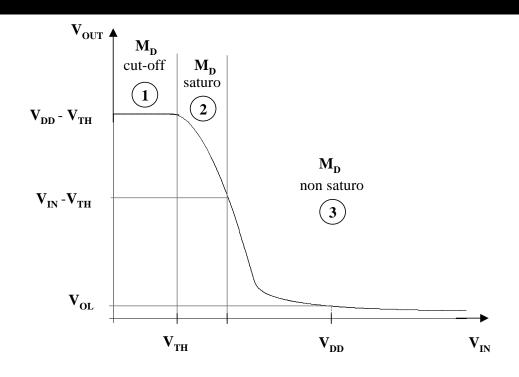
$$per V_{OUT} \le V_{IN} - V_{TH}$$



Nella regione (1)
$$V_{IN} \le V_{TH}$$
, $I_D = I_{sub} \cong 0$

ma
$$I_D = I_L = \frac{\beta_L}{2} \cdot (V_{GS} - V_{TH})^2 = 0 \implies (V_{GS})_L = V_{TH}$$

$$(V_{GS})_{I} = V_{DD} - V_{OUT} = V_{TH} \rightarrow V_{OUT} = V_{OH} = V_{DD} - V_{TH}$$
 (max valore di V_{OUT})



Nella regione (3)

$$\frac{\beta_{L}}{2} \cdot \left[\left(V_{DD} - V_{OL} \right) - V_{TH} \right]^{2} = \beta_{D} \cdot \left[\left(V_{DD} - V_{TH} \right) \cdot V_{OL} - \frac{V_{OL}}{2} \right]$$

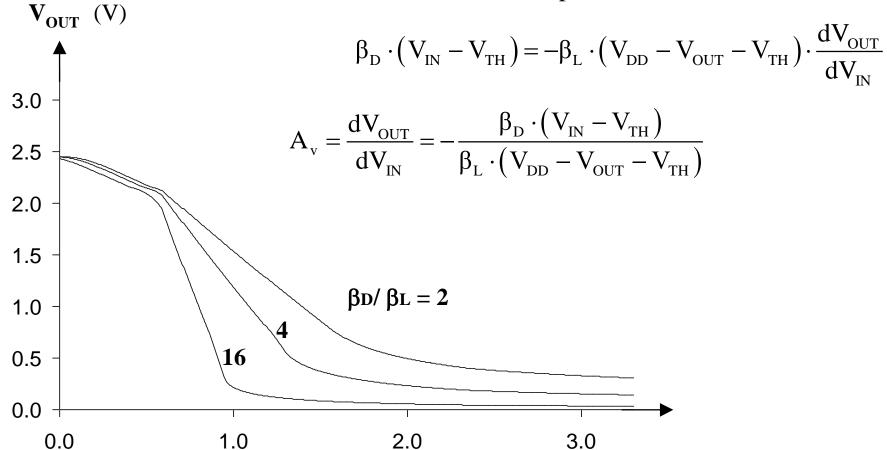
$$\frac{\beta_{L}}{2} \cdot \left(V_{DD} - V_{TH}\right)^{2} \cong \beta_{D} \cdot \left(V_{DD} - V_{TH}\right) \cdot V_{OL}$$

$$\mathbf{V_{OL}} \cong \frac{\beta_L}{2 \cdot \beta_D} \cdot \mathbf{V_{OH}}$$
 deve essere $\frac{\beta_L}{\beta_D} \ll 1$

Nella regione (2)

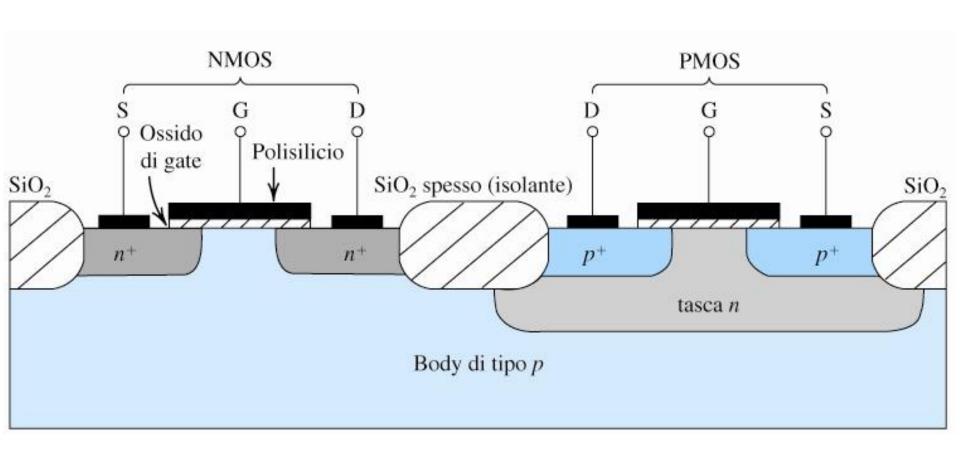
$$\frac{\beta_{D}}{2} \cdot \left(V_{IN} - V_{TH}\right)^{2} = \frac{\beta_{L}}{2} \cdot \left(V_{DD} - V_{OUT} - V_{TH}\right)^{2}$$

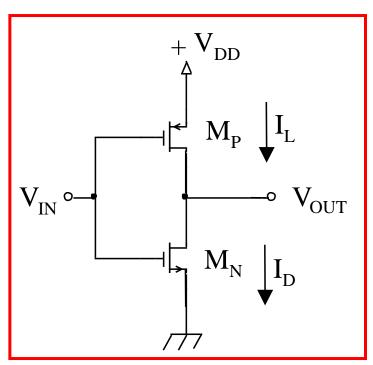
Calcoliamo la derivata rispetto a V_{IN}

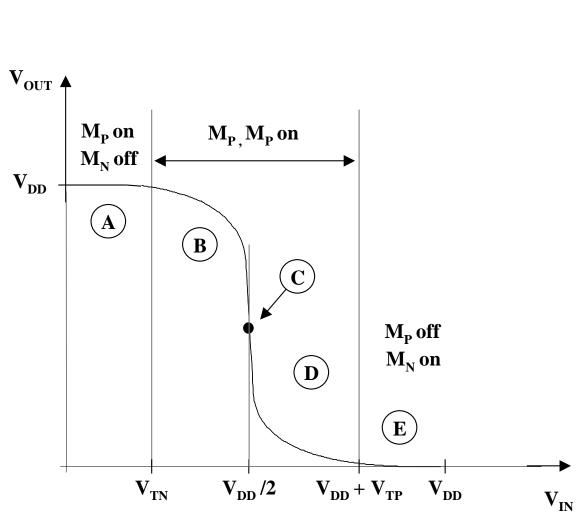


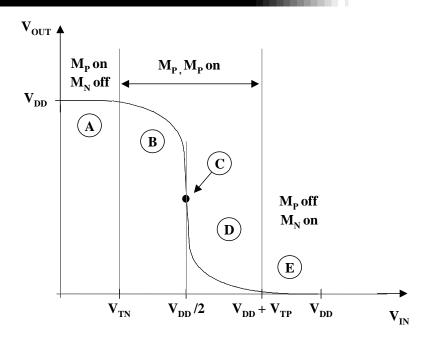
Tecnologia CMOS

Realizzazione in tecnologia planare CMOS di un nMOSFET e di un pMOSFET









A)
$$0 \le V_{IN} \le V_{TN}$$

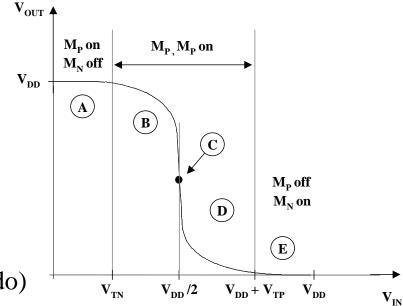
$$\Rightarrow$$
 $M_N = OFF \Rightarrow I_N = 0 \Rightarrow I_P = 0$

$$\beta_{P} \cdot \left[\left(V_{SG} + V_{TP} \right) \cdot \left(V_{DD} - V_{OUT} \right) - \frac{\left(V_{DD} - V_{OUT} \right)^{2}}{2} \right] = 0$$

$$\Rightarrow$$
 $V_{OUT} = V_{DD} = V_{OH}$

Elementi di **Elettronica** (INF) A.A. 2021-22

Inverter CMOS



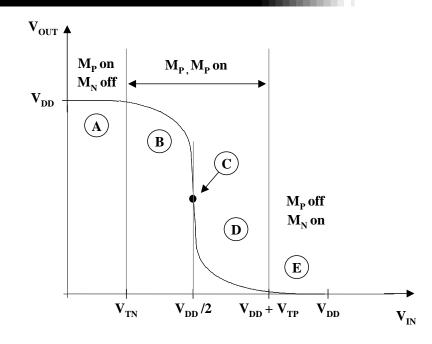
B)
$$V_{TN} < V_{IN} < V_{DD}/2$$

 M_N saturazione M_P non saturazione (triodo)

$$I_{N} = \beta_{N} \cdot \frac{\left(V_{IN} - V_{TN}\right)^{2}}{2}$$

$$\begin{cases} I_{N} = \beta_{N} \cdot \frac{\left(V_{IN} - V_{TN}\right)^{2}}{2} \\ \\ I_{P} = \beta_{P} \cdot \left[\left(V_{DD} - V_{IN} + V_{TP}\right) \cdot \left(V_{DD} - V_{OUT}\right) - \frac{\left(V_{DD} - V_{OUT}\right)^{2}}{2} \right] \end{cases}$$

$$I_{N} = I_{P}$$

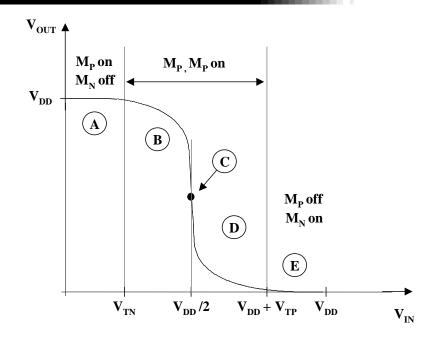


C) M_N saturazione M_P saturazione

$$I_{N} = I_{P} \quad \Rightarrow \quad \frac{\beta_{N}}{2} \cdot \left(V_{IN} - V_{TN}\right)^{2} = \frac{\beta_{P}}{2} \cdot \left(V_{DD} - V_{IN} + V_{TP}\right)^{2}$$

• Se
$$\beta_N = \beta_P$$
, $V_{TP} = -V_{TN} = -V_{TH}$

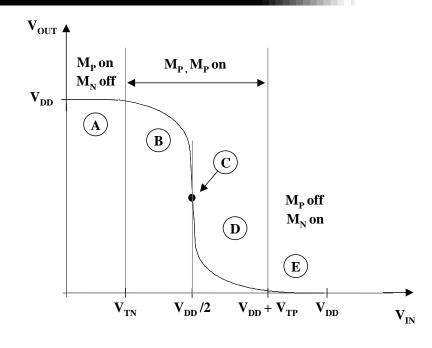
$$(V_{IN} - V_{TH})^2 = (V_{DD} - V_{IN} - V_{TH})^2 \implies V_{IN} = \frac{V_{DD}}{2}$$



D)
$$V_{DD}/2 < V_{IN} < V_{DD} + V_{TP}$$

 M_N non saturazione M_P saturazione

$$\begin{cases} I_{N} = \beta_{N} \cdot \left[\left(V_{IN} - V_{TN} \right) \cdot V_{OUT} - \frac{V_{OUT}^{2}}{2} \right] \\ I_{P} = \frac{\beta_{P}}{2} \cdot \left(V_{DD} - V_{IN} + V_{TP} \right)^{2} \end{cases}$$



E)
$$V_{IN} \ge V_{DD} + V_{TP} \implies V_{SG} \le -V_{TP} \implies M_P = OFF \implies I_P = 0$$

$$I_{P} = I_{N} = \beta_{N} \cdot \left[\left(V_{IN} - V_{TN} \right) \cdot V_{OUT} - \frac{V_{OUT}^{2}}{2} \right] = 0 \quad deve \ essere \quad V_{OUT} = V_{OL} = 0$$

