Estimation and Control of Dynamical Systems

Fall 2023

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Homework 4

Due: Jan. 2nd, 2024, Submit to TA

Exercise 1. Observability

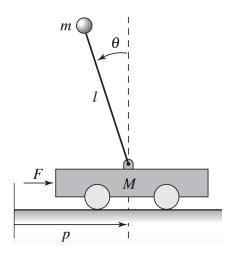


Figure 1: Cart-pendulum system

The dynamics of the cart-pendulum system shown in Figure 1 can be computed using Newtonian mechanics and have the form

$$\begin{bmatrix} (M+m) & -ml\cos\theta \\ -ml\cos\theta & (J+ml^2) \end{bmatrix} \begin{bmatrix} \ddot{p} \\ \ddot{\theta} \end{bmatrix} + \begin{bmatrix} c\dot{p} + ml\sin\theta\dot{\theta}^2 \\ \gamma\dot{\theta} - mgl\sin\theta \end{bmatrix} = \begin{bmatrix} F \\ 0 \end{bmatrix}$$
(1)

where p, \dot{p} represent the position and velocity of the base of the system, $\theta, \dot{\theta}$ are the angle and angular rate of the structure above the base, F represents the force applied at the base of the system, assumed to be in the horizontal direction (aligned with p), M is the mass of the base, m and J are the mass and moment of inertia of the system to be balanced, l is the distance from the base to the center of mass of the balanced body, c and γ are coefficients of viscous friction, and g is the acceleration due to gravity.

- 1. Define the state vector as $x = (p, \theta, \dot{p}, \dot{\theta})^T$, the input as u = F, and the output vector as $y = (p, \theta)^T$. Also, let $M_t = M + m$ and $J_t = J + ml^2$. Write down the system model in the form $\dot{x} = f(x, u), y = g(x, u)$.
- 2. In many cases, the angle θ will be very close to 0, and hence we can use the approximations $\sin \theta \approx \theta$ and $\cos \theta \approx 1$. Furthermore, if $\dot{\theta}$ is small, we can ignore quadratic and higher terms in $\dot{\theta}$. Under these approximations, write down a linear state space equation of the model obtained in 1.
- 3. Let us further simplify the linear state space model obtained in 2., by setting $c = \gamma = 0$. For this simplified system, can we determine the state x from measuring y? How about the cases when we can only measure the position p, or the angle θ ?

SO(USION:

1.
$$\int M d\tilde{p} - (m(\cos\theta)\tilde{p} + c\tilde{p} + (m(\sin\theta)\tilde{p}^2 - \tilde{p} - 2)) d\tilde{p} = (m(\cos\theta)\tilde{p} + J_{\perp}\tilde{p} + r_{\theta} - mg(\sin\theta)\tilde{p}^2 + 2) d\tilde{p} = m(\cos\theta)\tilde{p} - c\tilde{p} - (m(\sin\theta)\tilde{p}^2 + 2) d\tilde{p} = m(\cos\theta)\tilde{p} - mg(\sin\theta)\tilde{p}^2 + 2) d\tilde{p} = m(\cos\theta)\tilde{p} - mg(\sin\theta)\tilde{p} - m(\cos\theta)\tilde{p} - m(\cos\theta)\tilde{p} - m(\cos\theta)\tilde{p} - m(\cos\theta)\tilde{p}^2 + 2) d\tilde{p} = [m(\cos\theta)\tilde{p} - (m(\sin\theta)\tilde{p} - m(\cos\theta)\tilde{p} - m(\cos\theta$$