

# Midterms Revision Guide

30.102 Electromagnetics & Applications, Term 5 2020

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# 1 W1: Waves and Phasors

## 1.1 Waves

- At high  $f$ , the phase plays an important role.
- Carry energy through vacuum.
  - ✓: EM waves, ✗: mechanical waves
- Types of waves:
  - Transverse waves (displacement  $\perp$  direction of wave travel) e.g. EM waves
  - Longitudinal waves (displacement  $\parallel$  direction of wave travel) e.g. sound waves
  - Surface waves (circular motion) e.g. water, ocean waves

## 1.2 Time-varying Sinusoidal Waves

- General equation:

$$y(x, t) = Ae^{-\alpha x} \cos(\omega t - \beta x + \phi_0)$$

- Parameters:

1. Amplitude,  $A$ : maximum extent of vibration
2. Wavelength,  $\lambda$ : distance between 2 points with same displacement
3. Time period,  $T$ : amount of time for particle to travel back to same position
4. Frequency,  $f$ : number of periods in 1 second

$$f = \frac{1}{T} \quad (\text{Hz})$$

5. Phase,  $\phi$ :

$$\phi = \frac{2\pi t}{T} - \frac{2\pi x}{\lambda} + \phi_0, \text{ where } \phi_0 \text{ is the initial/reference phase}$$

6. Initial/reference phase,  $\phi_0$ :

$$\phi_0 = \arccos\left(\frac{y(0, 0)}{A}\right)$$

- $\phi_0 < 0$ : phase leading
- $\phi_0 > 0$ : phase lagging

7. Phase/propagation velocity,  $u_p$ :

$$u_p = f\lambda = \frac{\omega}{\beta} \quad (\text{m/s})$$

8. Angular frequency/velocity,  $\omega$ :

$$\omega = 2\pi f = \frac{2\pi}{T} \quad (\text{rad/s})$$

9. Wavenumber,  $\beta$ :

$$\beta = \frac{2\pi}{\lambda} \quad (\text{rad/m})$$

10. Direction of propagation:

- Positive x-direction:  $y(x, t) = Ae^{-\alpha x} \cos(\omega t - \beta x + \phi_0)$ 
  - Signs of  $\omega t$  and  $\beta x$  are opposite
- Negative x-direction:  $y(x, t) = Ae^{-\alpha x} \cos(\omega t + \beta x + \phi_0)$ 
  - Signs of  $\omega t$  and  $\beta x$  are the same

11. Attenuation factor,  $e^{-\alpha x}$ : factor that amplitude decreases by

- Attenuation constant of medium,  $\alpha$
- Units: Neper per meter (Np/m)

Solve for  $\alpha$  using  $\frac{Ae^{-\alpha x_1}}{Ae^{-\alpha x_2}} = \frac{y_1}{y_2}$ .

### 1.3 Complex Numbers

- Rectangular form:  $z = x + jy$  (easier to perform addition and subtraction)
  - where  $x = \text{Re}(z)$ ;  $y = \text{Im}(z)$
- Polar form:  $z = |z|e^{j\theta} = |z|\underline{\angle\theta}$  (easier to perform multiplication and division)
  - $|z|$ : magnitude of  $z$ ;  $\theta$ : phase angle;  $\underline{\angle\theta}$ : shorthand for  $e^{j\theta}$
- Euler's identity:  $e^{j\theta} = \cos \theta + j \sin \theta$

$$\text{Similarly, } \cos \theta = \frac{e^{j\theta} + e^{-j\theta}}{2}; \quad \sin \theta = \frac{e^{j\theta} - e^{-j\theta}}{2j}.$$

### 1.4 Phasors

- Any sinusoidally time-varying function  $z(t)$  can be expressed as

$$z(t) = \text{Re} \left[ \tilde{Z} e^{j\omega t} \right], \text{ where } \tilde{Z} \text{ is the phasor of the instantaneous function } z(t).$$

- Time domain voltage across resistors, inductors and capacitors
  - Resistors:  $v_R(t) = Ri(t) \Leftrightarrow v_R(t) = R \cdot \text{Re} \left[ \tilde{I} e^{j\omega t} \right]$
  - Inductors:  $v_L(t) = L \frac{di(t)}{dt} \Leftrightarrow v_L(t) = L \cdot \text{Re} \left[ j\omega \tilde{I} e^{j\omega t} \right]$
  - Capacitors:  $v_C(t) = \frac{1}{C} \int i(t) dt \Leftrightarrow v_C(t) = \frac{1}{C} \cdot \text{Re} \left[ \frac{\tilde{I}}{j\omega} e^{j\omega t} \right]$

## 1.5 Phasor Analysis

1. Adopt a cosine reference.

- e.g.  $v_S(t) = V_0 \sin(\omega t + \phi_0) = V_0 \cos\left(\frac{\pi}{2} - \omega t + \phi_0\right) = V_0 \cos\left(\omega t + \phi_0 - \frac{\pi}{2}\right)$

2. Express time-dependent variables as phasors.
3. Write equation in phasor form.
4. Solve phasor domain equation.
5. Find instantaneous value.

$$i(t) = \operatorname{Re} \left[ \widetilde{I} e^{j\omega t} \right]$$

## 1.6 Impedance

- Ratio of phasor voltage across element to phasor current through element,  $Z = \frac{\widetilde{V}}{\widetilde{I}}$
- Impedance of resistors, inductors and capacitors
  - Resistor:  $Z_R = R$
  - Inductor:  $Z_L = j\omega L$
  - Capacitor:  $Z_C = \frac{1}{j\omega C}$

## 2 W2: Antennas I

Definition of antenna: a transducer that converts guided wave on TL  $\leftrightarrow$  EM wave in free space

### 2.1 Properties

1. Reciprocity: Same radiation pattern for reception and transmission on 3 conditions:

- (a) Materials used for the antennas are linear.
- (b) Wave propagation medium is linear.
- (c) Transmit and receive modes of antenna are polarization matched.

2. Transmission Line Equivalent Circuit

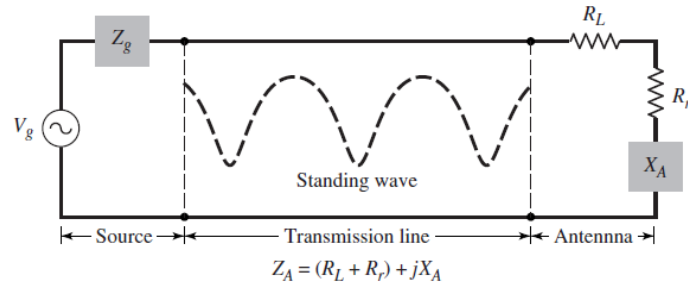


Figure 1: Transmission-line equivalent circuit of antenna from Balanis' *Antenna Theory* (2016)

3. Radiation efficiency,  $\xi$

$$\xi = \frac{P_{\text{rad}}}{P_t}$$

- where  $P_{\text{rad}}$  is the radiated power,
- and  $P_t$  is the transmitter power.

### 2.2 Antenna Field Regions

Letting  $D$  be the largest dimension of the antenna and  $\lambda$  be the wavelength, they are:

1. Reactive near-field region: at a distance  $R$ , where  $0 < R < 0.62 \sqrt{\frac{D^3}{\lambda}}$
2. Radiating near-field (Fresnel) region: at distance  $R$ , where  $0.63 \sqrt{\frac{D^3}{\lambda}} < R < \frac{2D^2}{\lambda}$
3. Far-field (Fraunhofer) region: at a distance  $R$ , where  $R > \frac{2D^2}{\lambda}$

### 2.3 Far Field Approximation

- Near radiation source: spherical wavefronts
- Far field: approximated as plane waves

## 2.4 Radiation Mechanism

- To create radiation, there must be:
  - either a time-varying current,
  - or an acceleration/deceleration of charge.
- Electric charges needed to excite fields but not sustain them.

## 2.5 Hertzian Dipole

- A thin, linear conductor with a length  $\ell$ , where  $\ell < \frac{\lambda}{50}$
- Current  $i(t)$  is constant along the wire
- Current  $i(t) = 0$  at the ends of the wire

### 3 W3: Transmission Lines

#### 3.1 Unbounded & Guided Waves

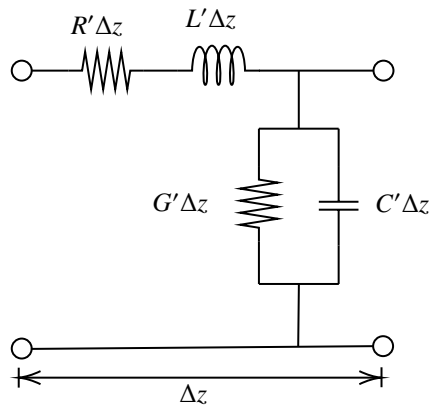
- Unbounded waves
  - Propagate in a homogeneous medium
  - No obstacles
  - No material interface
- Guided waves
  - Propagate along a material surface/structure
  - e.g. coax cable <30 GHz, waveguide 5-100 GHz

#### 3.2 Transmission Lines

- Can be classified into 2 types:
  1. Transverse electromagnetic (TEM) transmission lines
    - Electric and magnetic fields transverse to direction of propagation
    - Non-transverse fields negligible
    - Common feature: 2 || conducting surfaces
    - e.g. coaxial line, two-wire line, parallel-plate line, strip line, microstrip line, coplanar waveguide, etc.
  2. Higher-order transmission lines
    - $\geq 1$  significant field component in direction of propagation
    - e.g. rectangular waveguide, optical fibre, etc.



### 3.3 Distributed Transmission Line Model



- 4 transmission line parameters:
  1.  $R'$ : Resistance per unit length in  $\Omega/\text{m}$
  2.  $L'$ : Inductance per unit length in  $\text{H}/\text{m}$
  3.  $G'$ : Conductance per unit length in  $\text{S}/\text{m}$
  4.  $C'$ : Capacitance per unit length in  $\text{F}/\text{m}$
- Geometric parameters
  - Coaxial line
    - $a$ : Outer radius of inner conductor in m
    - $b$ : Inner radius of outer conductor in m
  - Two-wire line
    - $d$ : Diameter of each line in m
    - $D$ : Spacing between the centers of the wires in m
  - Parallel-plate line
    - $w$ : Width of each plate in m
    - $h$ : Thickness of insulation between plates in m
- Constitutive parameters
  - Conductors
    - $\mu_c$ : Magnetic permeability of conductors
    - $\sigma_c$ : Electrical conductivity of conductors
  - Insulators
    - $\epsilon$ : Electrical permittivity of insulating material
    - $\mu$ : Magnetic permeability of insulating material
    - $\sigma$ : Electrical conductivity of insulating material

### 3.3.1 Surface Resistance and Other Useful Relations

- Surface Resistance,  $R_s = \sqrt{\frac{\pi f \mu_c}{\sigma_c}}$
- Perfect conductor:  $\sigma_c = \infty, \Rightarrow R_s \text{ and } R' = 0$ .
- Perfect dielectric:  $\sigma = 0, \Rightarrow G' = 0$ .
- Air line:  $\epsilon = \epsilon_0, \mu = \mu_0, \sigma = 0, G' = 0$ .
- All TEM transmission lines have the following relationships:

$$L' C' = \mu \epsilon$$

$$\frac{G'}{C'} = \frac{\sigma}{\epsilon}$$

### 3.3.2 Summary for Distributed Transmission Line Model

Parameter	Coaxial	Two-Wire	Parallel-Plate	Unit
$R'$	$\frac{R_s}{2\pi} \left( \frac{1}{a} + \frac{1}{b} \right)$	$\frac{2R_s}{\pi d}$	$\frac{2R_s}{w}$	$\Omega/\text{m}$
$L'$	$\frac{\mu}{2\pi} \ln \frac{b}{a}$	$\frac{\mu}{\pi} \ln \left[ \frac{D}{d} + \sqrt{\left( \frac{D}{d} \right)^2 - 1} \right]$	$\frac{\mu h}{w}$	$\text{H}/\text{m}$
$G'$	$\frac{2\pi\sigma}{\ln \left( \frac{b}{a} \right)}$	$\frac{\pi\sigma}{\ln \left[ \frac{D}{d} + \sqrt{\left( \frac{D}{d} \right)^2 - 1} \right]}$	$\frac{\sigma w}{h}$	$\text{S}/\text{m}$
$C'$	$\frac{2\pi\epsilon}{\ln \left( \frac{b}{a} \right)}$	$\frac{\pi\epsilon}{\ln \left[ \frac{D}{d} + \sqrt{\left( \frac{D}{d} \right)^2 - 1} \right]}$	$\frac{\epsilon w}{h}$	$\text{F}/\text{m}$

## 3.4 Transmission Line Equations

$$\begin{aligned} -\frac{\partial v(z, t)}{\partial z} &= R' i(z, t) + L' \frac{\partial i(z, t)}{\partial t} \Leftrightarrow -\frac{\partial \tilde{V}(z)}{\partial z} = (R' + j\omega L') \tilde{I}(z) \\ -\frac{\partial i(z, t)}{\partial z} &= G' v(z, t) + C' \frac{\partial v(z, t)}{\partial t} \Leftrightarrow -\frac{\partial \tilde{I}(z)}{\partial z} = (G' + j\omega C') \tilde{V}(z) \end{aligned}$$

## 3.5 Characteristic Parameters

### 3.5.1 Propagation Constant

$$\gamma = \sqrt{(R' + j\omega L')(G' + j\omega C')} = \alpha + j\beta$$

- $\gamma$ : complex propagation constant
- $\alpha$ : attenuation constant in Np/m
- $\beta$ : phase constant in rad/m

### 3.5.2 Characteristic Impedance

$$Z_0 = \frac{V_0^+}{I_0^+} = \frac{-V_0^-}{I_0^-} = \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}} \text{ in units of } \Omega$$

### 3.5.3 Summary for Characteristic Parameters

	Propagation constant $\gamma = \alpha + j\beta$	Phase velocity $u_p$	Characteristic impedance $Z_0$
<b>General case</b>	$\sqrt{(R' + j\omega L')(G' + j\omega C')}$	$\frac{\omega}{\beta}$	$\sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}}$
<b>Lossless (R' = G' = 0)</b>	$\alpha = 0, \beta = \frac{\omega \sqrt{\epsilon_r}}{c}$	$\frac{c}{\sqrt{\epsilon_r}}$	$\sqrt{\frac{L'}{C'}}$
<b>Lossless coaxial</b>			$\frac{60}{\sqrt{\epsilon_r}} \ln \frac{b}{a}$
<b>Lossless two wire</b>			$\frac{120}{\sqrt{\epsilon_r}} \ln \left[ \frac{D}{d} + \sqrt{\frac{D^2}{d^2} - 1} \right]$ If $D \gg d$ , $\approx \frac{120}{\sqrt{\epsilon_r}} \ln \frac{2D}{d}$
<b>Lossless    plate</b>			$\frac{120\pi}{\sqrt{\epsilon_r}} \frac{h}{w}$

## 3.6 Dispersion & Guided Wavelength

- Dispersion: phase velocity of wave depends on its frequency
  - ✓: Dispersive media, ✗: non-dispersive media
  - Degree of distortion  $\propto$  length of dispersive line
- Guided wavelength,  $\lambda_g$ : distance between two equal phase planes along the transmission line

$$\lambda_g = \frac{c}{f \sqrt{\epsilon_r}} = \frac{\lambda_0}{\sqrt{\epsilon_r}}$$

### 3.7 Standing Waves & Standing Wave Pattern

- Standing wave: formed when two waves on transmission line propagating in opposite directions
- Standing wave patterns: sinusoidal patterns caused by interference of two travelling waves

$$\widetilde{V}(z) = \widetilde{V}^+(z) + \widetilde{V}^-(z) = V_0^+ e^{-\gamma z} + V_0^- e^{\gamma z}$$

$$\widetilde{I}(z) = \widetilde{I}^+(z) + \widetilde{I}^-(z) = I_0^+ e^{-\gamma z} + I_0^- e^{\gamma z}$$

- Using either one of the two axes:
  - $z$ -axis: load at  $z = 0$ , generator at  $z = -l$
  - $d$ -axis: load at  $d = 0$ , generator at  $d = l$
- Affected by:
  - Relation of  $\widetilde{V}^-(z)$  and  $\widetilde{V}^+(z)$  at  $z = 0$
  - Relation of  $V_0^+$  and  $V_0^-$
- Magnitude of voltage,  $|\widetilde{V}(d)| = |V_0^+| \left[ 1 + |\Gamma|^2 + 2|\Gamma| \cos(2\beta d - \theta_r) \right]^{1/2}$
- Magnitude of current,  $|\widetilde{I}(d)| = \frac{|V_0^+|}{Z_0} \left[ 1 + |\Gamma|^2 + 2|\Gamma| \cos(2\beta d - \theta_r) \right]^{1/2}$
- Voltage maximum,  $d_{max}$ : distance from load where  $|\widetilde{V}(d)|$  is a maximum

$$d_{max} = \frac{\theta_r}{4\pi} + \frac{n\lambda}{2}, \begin{cases} n = 1, 2, \dots & \text{if } \theta_r < 0 \\ n = 0, 1, 2, \dots & \text{if } \theta_r \geq 0 \end{cases}$$

- Voltage minimum,  $d_{min}$ : distance from load where  $|\widetilde{V}(d)|$  is a minimum

$$d_{min} = \begin{cases} d_{max} + \frac{\lambda}{4}, & \text{if } d_{max} < \frac{\lambda}{4} \\ d_{max} - \frac{\lambda}{4}, & \text{if } d_{max} \geq \frac{\lambda}{4} \end{cases}$$

- Voltage standing wave ratio (VSWR),  $S = \frac{|\widetilde{V}|_{max}}{|\widetilde{V}|_{min}} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$  (dimensionless)

### 3.8 Reflection Coefficient

- Ratio of reflected and incident voltages at the load.  $\frac{I_0^-}{I_0^+} = -\frac{V_0^-}{V_0^+} = -\Gamma_L$
- A complex quantity.  $\Gamma_L = |\Gamma_L|e^{j\theta_r} = \frac{V_0^-}{V_0^+} = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{z_L - 1}{z_L + 1}$  (dimensionless)
- Normalized load impedance,  $z_L = \frac{Z_L}{Z_0}$  (dimensionless)

Load	$ \Gamma $	$\theta_r$
$Z_L = (r + jx)Z_0$	$\sqrt{\frac{(r-1)^2 + x^2}{(r+1)^2 + x^2}}$	$\tan^{-1}\left(\frac{x}{r-1}\right) - \tan^{-1}\left(\frac{x}{r+1}\right)$
$Z_L = Z_0$	0	NA
$Z_L = \text{short-circuit}$	1	$\pm 180^\circ$
$Z_L = \text{open-circuit}$	1	0
$Z_L = jX = j\omega L$ (capacitor)	1	$\pm 180^\circ - 2 \tan^{-1}(X)$
$Z_L = jX = -\frac{j}{\omega C}$	1	$\pm 180^\circ + 2 \tan^{-1}(X)$

### 3.9 Wave Impedance

$$Z(d) = \frac{\tilde{V}(d)}{\tilde{I}(d)} = Z_0 \left( \frac{1 + \Gamma_d}{1 - \Gamma_d} \right)$$

- Phase-shifted voltage reflection coefficient  $\Gamma_d = |\Gamma|e^{j(\theta_r - 2\beta d)}$

### 3.10 Input Impedance

$$\begin{aligned}
 Z_{\text{in}} &= Z_0 \left( \frac{z_L \cos \beta l + j \sin \beta l}{\cos \beta l + j z_L \sin \beta l} \right) \\
 &= Z_0 \left( \frac{z_L + j \tan \beta l}{1 + j z_L \tan \beta l} \right) \\
 V_0^+ &= \left( \frac{\tilde{V}_g Z_{\text{in}}}{Z_g + Z_{\text{in}}} \right) \left( \frac{1}{e^{j\beta l} + \Gamma e^{-j\beta l}} \right)
 \end{aligned}$$

### 3.11 Short-Circuited Line

- $\Gamma = -1, S = \infty$
- $\widetilde{V}_{sc}(d) = V_0^+ (e^{j\beta d} - e^{-j\beta d}) = 2jV_0^+ \sin \beta d$
- $\widetilde{I}_{sc}(d) = \frac{V_0^+}{Z_0} (e^{j\beta d} + e^{-j\beta d}) = \frac{2V_0^+}{Z_0} \cos \beta d$
- $Z_{sc}(d) = \frac{\widetilde{V}_{sc}(d)}{\widetilde{I}_{sc}(d)} = jZ_0 \tan \beta d$
- By choosing  $\ell$ , can make  $L$  and  $C$  of any reactance.
  - If  $\tan \beta l \geq 0$ ,  $jZ_0 \tan \beta l = j\omega L_{eq}$ .
  - If  $\tan \beta l \leq 0$ ,  $jZ_0 \tan \beta l = \frac{1}{j\omega C_{eq}}$ .

### 3.12 Open-Circuited Line

- $\Gamma = 1, S = \infty$
- $\widetilde{V}_{oc}(d) = V_0^+ (e^{j\beta d} + e^{-j\beta d}) = 2V_0^+ \cos \beta d$
- $\widetilde{I}_{oc}(d) = \frac{V_0^+}{Z_0} (e^{j\beta d} - e^{-j\beta d}) = \frac{2jV_0^+}{Z_0} \sin \beta d$
- $Z_{oc}(d) = \frac{\widetilde{V}_{oc}(d)}{\widetilde{I}_{oc}(d)} = -jZ_0 \cot \beta d$
- By choosing  $\ell$ , can make  $L$  and  $C$  of any reactance.
  - If  $Z_{in}^{oc} \geq 0$ ,  $-jZ_0 \cot \beta l = j\omega L_{eq}$ .
  - If  $Z_{in}^{oc} \leq 0$ ,  $-jZ_0 \cot \beta l = \frac{1}{j\omega C_{eq}}$ .

### 3.13 Measuring Characteristic Impedance and Phase Constant

$$Z_0 = \sqrt{Z_{in}^{sc} Z_{in}^{oc}}$$

$$\tan \beta l = \sqrt{\frac{-Z_{in}^{sc}}{Z_{in}^{oc}}} \quad \text{can be used to find } \beta$$

### 3.14 Quarter and Half Wavelength TLs

- For a half wavelength TL, where  $l = \frac{n\lambda}{2}$ ,  $\boxed{Z_{in} = Z_L}$ .
- For a quarter wavelength TL, where  $l = \frac{\lambda}{4} + \frac{n\lambda}{2}$ ,  $\boxed{Z_{in} = \frac{Z_0^2}{Z_L}}$ .

### 3.15 Instantaneous Power of a Lossless TL

- $v(d, t) = |V_0^+| [\cos(\omega t + \beta d + \phi^+) + |\Gamma| \cos(\omega t - \beta d + \phi^+ + \theta_r)]$
- $i(d, t) = \frac{|V_0^+|}{Z_0} [\cos(\omega t + \beta d + \phi^+) - |\Gamma| \cos(\omega t - \beta d + \phi^+ + \theta_r)]$
- $P(d, t) = \frac{|V_0^+|^2}{Z_0} [\cos^2(\omega t + \beta d + \phi^+) - |\Gamma|^2 \cos^2(\omega t - \beta d + \phi^+ + \theta_r)]$ 
  - The instantaneous power oscillates at twice the rate of the voltage or current.
- Incident power  $P^i(d, t) = \frac{|V_0^+|^2}{2Z_0} [1 + \cos(2\omega t + 2\beta d + 2\phi^+)]$
- Reflected power  $P^r(d, t) = -|\Gamma|^2 \frac{|V_0^+|^2}{2Z_0} [1 + \cos(2\omega t - 2\beta d + 2\phi^+ + 2\theta_r)]$

### 3.16 Time-Average Power of a Lossless TL

- Time-average incident power,  $P_{av}^i = \frac{|V_0^+|^2}{2Z_0}$  is measured in W.
- Time-average reflected power,  $P_{av}^r = -|\Gamma|^2 \frac{|V_0^+|^2}{2Z_0} = -|\Gamma|^2 P_{av}^i$  is measured in W.
  - Average reflected power is average incident power diminished by  $|\Gamma|^2$ .

## 4 W5: Matching Networks

### 4.1 Concept of Matching Networks

- Eliminate reflections for waves incident from source
- All power goes to load
- May consist of lumped elements i.e. capacitors and inductors, or sections of TLs

### 4.2 Matching Networks in Series

1. In-series  $\lambda/4$  transformer inserted in front of  $Z_L$  (if  $Z_L$  is real)
2. In-series  $\lambda/4$  transformer inserted at  $d = d_{\max}$  or  $d = d_{\min}$  (if  $Z_L$  is complex)

### 4.3 Matching Networks in Parallel

1. In-parallel insertion of capacitor at distance  $d_1$
2. In-parallel insertion of inductor at distance  $d_2$
3. In-parallel insertion of a short-circuited stub

### 4.4 Lumped Element Matching

- To achieve matched condition,  $y_{\text{in}} = y_d + y_s + g_d + j(b_d + b_s) = 1 + j0$ . As such,

$g_d = 1$	(real condition)
$b_d = -b_s$	(imaginary condition)



## 5 W5: Smith Chart

1. Complex unit circle
2. Concentric  $r_L$  circles
3.  $x_L$  curves
4. Wavelengths toward generator (WTG) scale (clockwise)
5. Wavelengths toward load (WTL) scale (counterclockwise)

### 5.1 How to Use the Smith Chart

- Read off  $\Gamma_L$  from  $z_L$ :  $\Gamma_L = |\Gamma_L|e^{j\theta_r}$
- Constant  $\Gamma_L$ /SWR circle, move towards WTG/WTL directions
- Read off to find distance  $d$
- Find  $Y$  from  $Z$ 
  - $y$  opposite from  $z$  in SWR circle
  - $\Rightarrow Y_L = y_L \cdot Y_0$  in units of S

## 6 W6: Vector Algebra

### 6.1 Basic Vector Operations

- Unit vector  $\hat{a} = \frac{\vec{A}}{|\vec{A}|} = \frac{\hat{x}A_x + \hat{y}A_y + \hat{z}A_z}{\sqrt{A_x^2 + A_y^2 + A_z^2}}$
- Position vector:  $\vec{R}_1 = \overrightarrow{OP_1}$
- Distance vector:  $\vec{R}_{12} = \overrightarrow{P_1P_2} = \vec{R}_2 - \vec{R}_1$ 
  - Distance  $d = |\vec{R}_{12}|$
- Vector addition
  - Done graphically using parallelogram or head-to-tail method.
  - Commutative:  $\vec{A} + \vec{B} = \vec{B} + \vec{A}$

### 6.2 Dot Product

$$\vec{A} \cdot \vec{B} = AB \cos \theta_{AB}, \quad \theta_{AB} = \cos^{-1} \left( \frac{\vec{A} \cdot \vec{B}}{\sqrt{\vec{A} \cdot \vec{A}} \cdot \sqrt{\vec{B} \cdot \vec{B}}} \right)$$

- Commutative and distributive.

$$\begin{aligned} \vec{A} \cdot \vec{B} &= \vec{B} \cdot \vec{A} \text{ (commutative)} \\ \vec{A} \cdot (\vec{B} + \vec{C}) &= \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C} \text{ (distributive)} \end{aligned}$$

- Can be used to find magnitude of vector.

$$A = |\vec{A}| = \sqrt{\vec{A} \cdot \vec{A}}$$

### 6.3 Cross Product

$$\vec{A} \times \vec{B} = \hat{n} AB \sin \theta_{AB}, \quad \hat{n} \text{ in direction of right hand rule}$$

- Anti-commutative and distributive.

$$\begin{aligned} \vec{A} \times \vec{B} &= -\vec{B} \times \vec{A} \text{ (anti-commutative)} \\ \vec{A} \times (\vec{B} + \vec{C}) &= \vec{A} \times \vec{B} + \vec{A} \times \vec{C} \text{ (distributive)} \end{aligned}$$

- Can be re-expressed as a determinant.

$$\vec{A} \times \vec{B} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

## 6.4 Scalar Triple Product

$$\vec{A} \cdot (\vec{B} \times \vec{C}) = \vec{B} \cdot (\vec{C} \times \vec{A}) = \vec{C} \cdot (\vec{A} \times \vec{B}) = \begin{vmatrix} A_x & A_y & A_z \\ B_x & B_y & B_z \\ C_x & C_y & C_z \end{vmatrix}$$

## 6.5 Vector Triple Product

$$\vec{A} \times (\vec{B} \times \vec{C})$$

- Not associative.

$$\vec{A} \times (\vec{B} \times \vec{C}) \neq (\vec{A} \times \vec{B}) \times \vec{C}$$

- Follows the "bac-cab" rule.

$$\vec{A} \times (\vec{B} \times \vec{C}) = \vec{B}(\vec{A} \cdot \vec{C}) - \vec{C}(\vec{A} \cdot \vec{B})$$

## A Appendix

### A.1 Derivatives

$$\frac{d}{dt}$$

$$\sin \rightarrow \cos, \quad \cos \rightarrow -\sin, \quad \tan \rightarrow \sec^2, \quad x^n \rightarrow nx^{n-1}, \quad e^{ax} \rightarrow ae^{ax}, \quad \ln x \rightarrow \frac{1}{x}$$

### A.2 Integrals

$$\int$$

$$\sin \rightarrow -\cos, \quad \cos \rightarrow \sin, \quad \sec^2 \rightarrow \tan, \quad x^n \rightarrow \frac{1}{n}x^{n+1}, \quad e^{ax} \rightarrow \frac{1}{a}e^{ax}, \quad \frac{1}{x} \rightarrow \ln|x|$$

### A.3 Integration by Parts

$$\int u \, dv = uv - \int v \, du$$

Priority of choosing  $u$ :

1. Logarithmic terms
2. Inverse trigonometric terms
3. Algebraic terms
4. Trigonometric terms
5. Exponential terms

### A.4 Phasors

- Identities:  $\sin x = \cos\left(\frac{\pi}{2} - x\right)$ ;  $\cos(-x) = \cos x$
- Voltage across capacitor,  $v_C(t)$ :

$$\begin{aligned} \int i(t) &= \operatorname{Re} \left[ \frac{\tilde{I} e^{j\omega t}}{j\omega} \right] = \operatorname{Re} \left[ \frac{-j\tilde{I} e^{j\omega t}}{\omega} \right] = \operatorname{Re} \left[ \frac{-\tilde{I} j \cos \omega t + \tilde{I} \sin \omega t}{\omega} \right] \\ &= \frac{\tilde{I} \sin \omega t}{\omega} \\ \Rightarrow v_C(t) &= \frac{\int i(t)}{C} = \frac{\tilde{I} \sin \omega t}{\omega C} \end{aligned}$$

- Voltage across inductor,  $v_L(t)$ :

$$\begin{aligned} \frac{di(t)}{dt} &= \operatorname{Re} \left[ j\omega \tilde{I} e^{j\omega t} \right] = \operatorname{Re} \left[ j\omega \tilde{I} \cos \omega t - \tilde{I} \omega \sin \omega t \right] = -\tilde{I} \omega \sin \omega t \\ \Rightarrow v_L(t) &= L \frac{di(t)}{dt} = -L\omega \tilde{I} \sin \omega t \end{aligned}$$