

$$\bar{\Pi} = \frac{1}{2} \sum_e \{u\}^T \cdot [K] \cdot \{u\} - \{u\}^T \cdot \{F\}$$

FEM SOFTWARE AND SERVICES



# Introduction to Finite Element Simulation

Presented in the Embryo Physics Course <http://www.embryophysics.org>  
September 22, 2010

By

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ANSYS Competence Center FEM

**CADFEM**<sup>®</sup>


$$\bar{\Pi} = \frac{1}{2} \sum_e \{u\}^T \cdot [K] \cdot \{u\} - \{u\}^T \cdot \{F\}$$

FEM SOFTWARE AND SERVICES



# Introduction into FEM

Computer Aided Engineering (CAE)

# Outline

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- PDE, numerical solution
- Discretization
- Meshing
- Numerical errors
- Typical simulation process
- System simulation

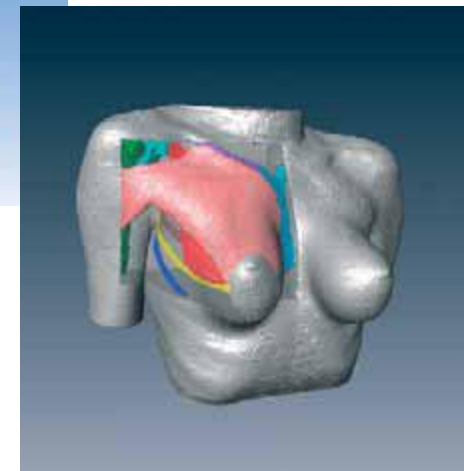
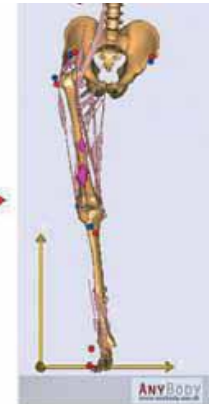
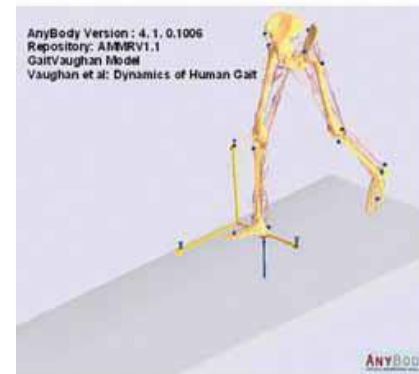
# Infoplaner 2-2010

■ <http://www.cadfem.de/unternehmen/fem-magazin-infoplaner.html>

FEM-Simulation in der Medizintechnik, Biomechanik, Prothetik, Implantologie

## ANSYS im Dienste der Gesundheit

- Optimierung medizinischer Produkte bei Siemens
- Auslegung von Zahnimplantaten: 2 Millionen Mal kraftvoll zubeißen
- CFD-Simulation eines Inhalators: Einfach tief durchatmen



# Partial Differential Equations

## ■ Heat Transfer Equation

$$\rho c_p \frac{\partial T}{\partial t} = \lambda \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \dot{Q}$$

## ■ Goal is to find the temperature field (scalar field)

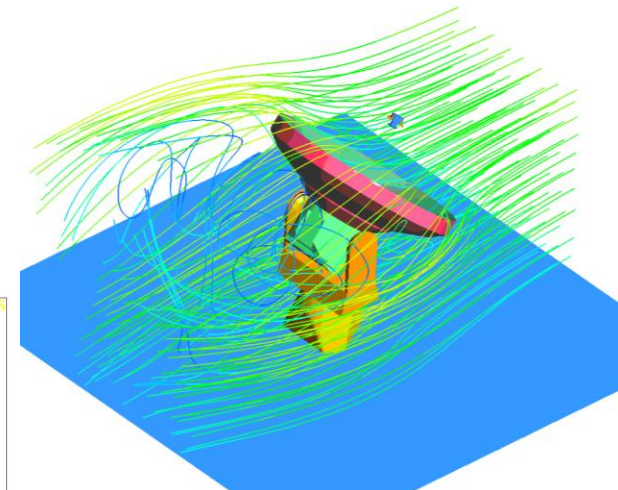
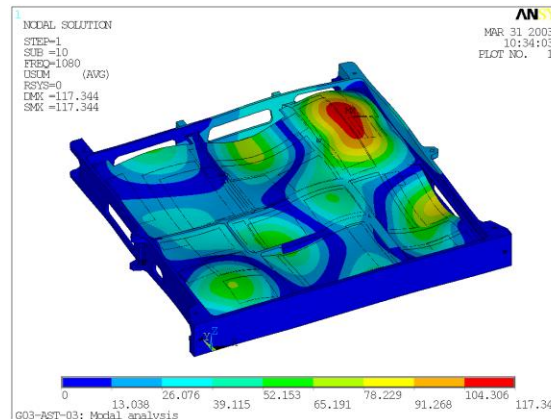
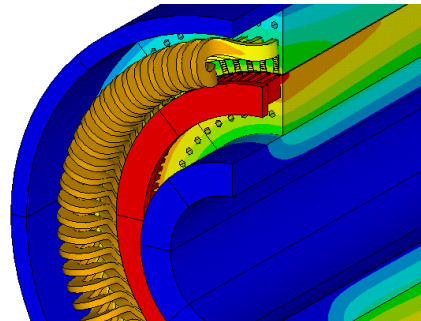
- Stationary  $T(x, y, z)$
- Transient  $T(t, x, y, z)$

## ■ Vector field

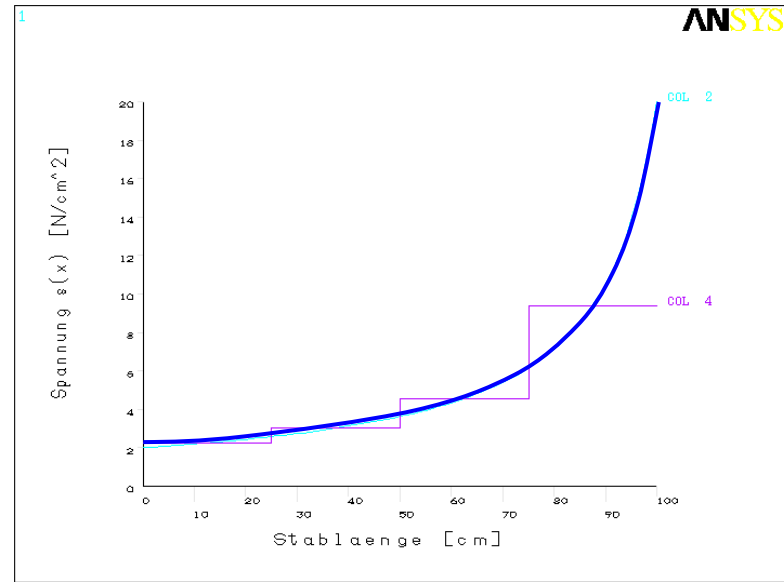
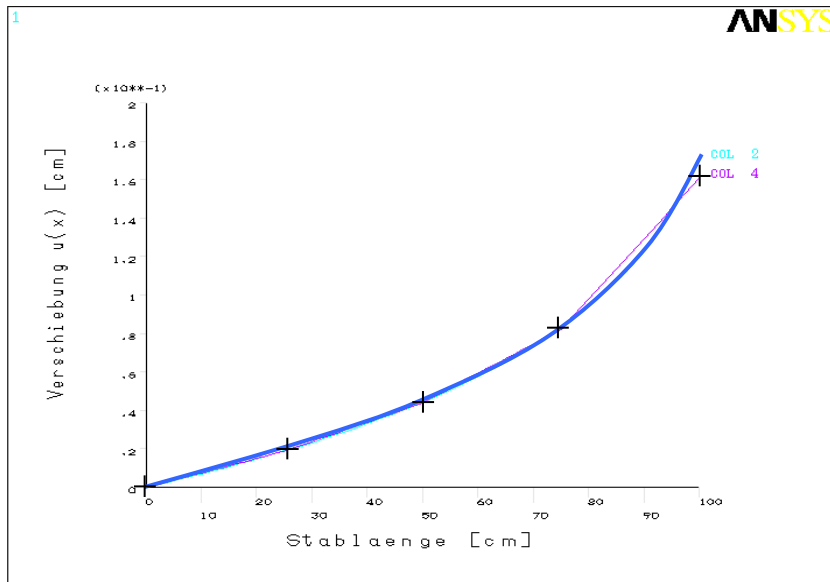
## ■ Structural Mechanics

## ■ Fluid Dynamics

## ■ Electromagnetics



# Numerical Solution – Discretization



## ■ From PDE to:

- Stationary problem: a system of algebraic equations
- Transient problem: ODEs

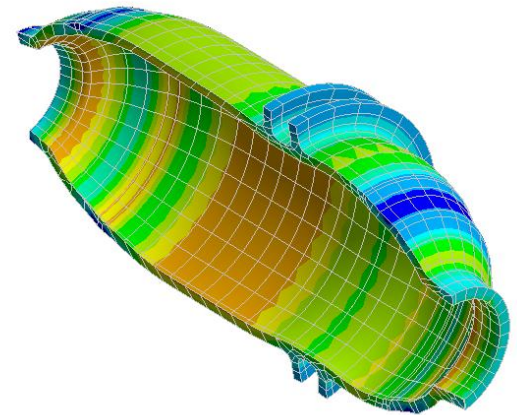
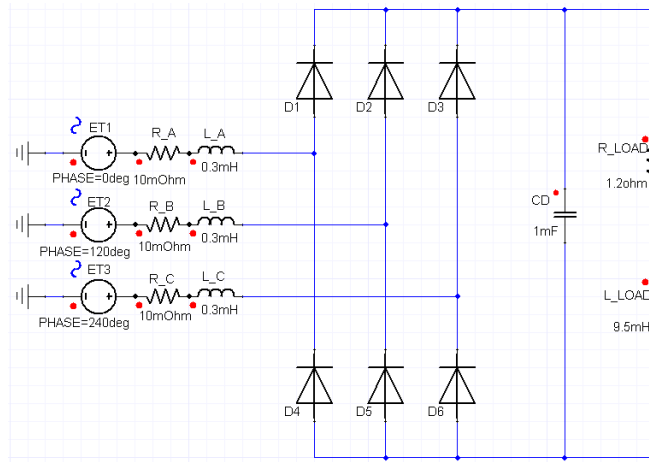
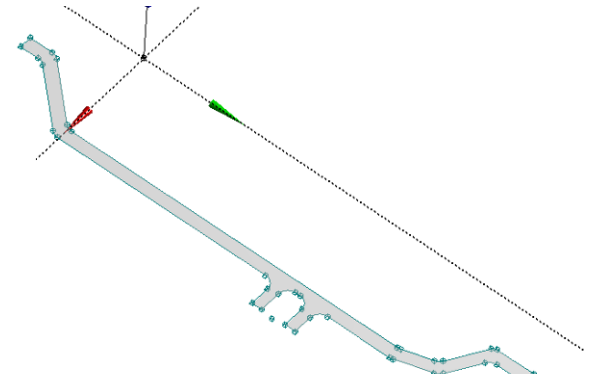
$$\rho c_p \frac{\partial T}{\partial t} = \lambda \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + \dot{Q}$$

$$E \frac{\partial T}{\partial t} + KT = F$$

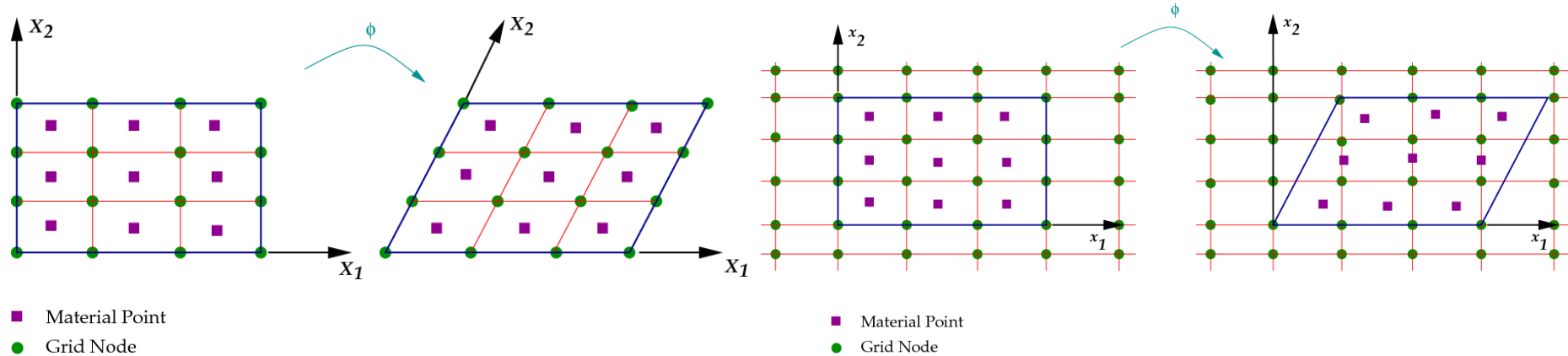


# Space Simplifications

- 3D simulation: Mesh  $10 \times 10 \times 10 = 1000$ 
  - How to reduce complexity?
- 2D simulation  $T(z) = \text{const} \Rightarrow T(x, y)$
- 2D-axisymmetrical simulation
- 1D simulation
- 0D: a lumped model



# Lagrangian and Eulerian Formulations

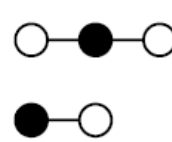


- [http://en.wikiversity.org/wiki/Nonlinear\\_finite\\_elements/Lagrangian\\_and\\_Eulerian\\_descriptions](http://en.wikiversity.org/wiki/Nonlinear_finite_elements/Lagrangian_and_Eulerian_descriptions)

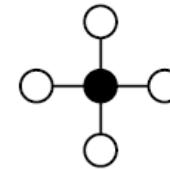
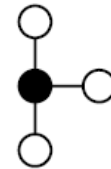


# Finite Differences

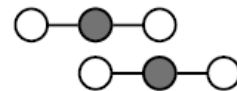
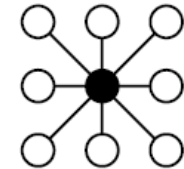
- Derivative is approximated through finite differences;
- Difficult to use on not Cartesian mesh;
- Difficult to apply boundary conditions.



1D stencils

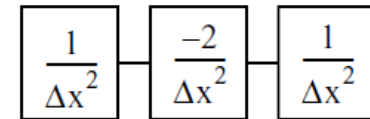


2D stencils



Staggered 1D “leap-frog” stencil

$$\nabla^2 \phi \approx \frac{\phi_{i-1} - 2\phi_i + \phi_{i+1}}{\Delta x^2}$$



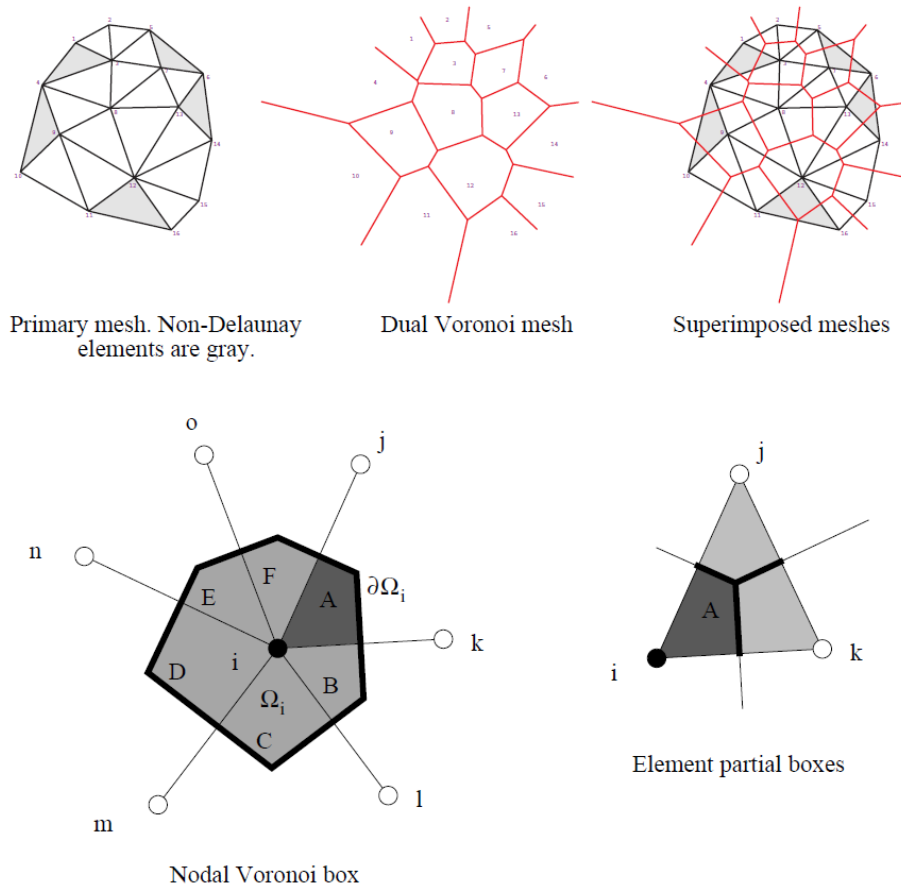
1D stencil with matrix entries for the Laplace operator

**Figure 22. Finite difference nodal equation structure, showing typical stencil diagrams. Special stencils are required at the mesh boundaries, and multiple stencils are needed for some coupled PDEs (e.g. leap-frog schemes such as the 1D Yee stencil.) For a particular operator, a stencil may be drawn with its matrix entry values.**

*Figure from “MEMS and NEMS Simulation”. In MEMS: A Practical Guide to Design, Analysis, and Applications, William Andrew Publishing, 2005.*

# Finite Volumes

- CFD world
- Finite volume schemes are conservative
- Needs dual meshes



**Figure 19. Finite volume mesh concepts. Above: general mesh constructions. Below: nodal and element view of the mesh. Adapted from [3].**

*Figure from “MEMS and NEMS Simulation”. In MEMS: A Practical Guide to Design, Analysis, and Applications, William Andrew Publishing, 2005.*

# Finite Elements

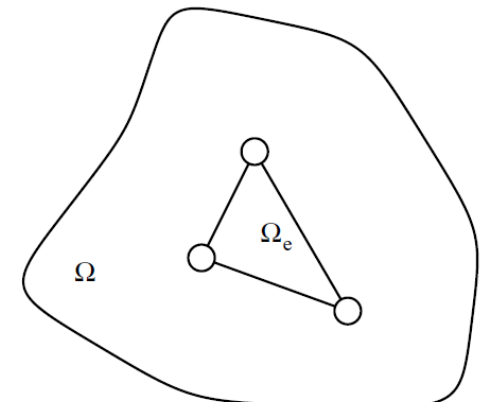
- Variational formulation
- Virtual work principle
- Very general

$$a(u, v) \Rightarrow \int_{\Omega} g(u, v) d\Omega \Rightarrow [A]\{u\}$$
$$a(u, v) + b(v) = 0$$

$$b(v) \Rightarrow \int_{\Omega} h(v) d\Omega \Rightarrow \{F\}$$

Typical form of the finite element equations

$$\int_{\Omega} \dots d\Omega = \sum_{e=1}^{ne} \int_{\Omega_e} \dots d\Omega_e$$



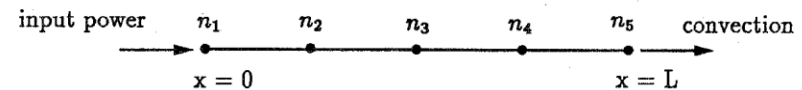
Decomposing domain integrals into a sum of element integrals

**Figure 17. Finite element matrix equations typically arise from a bilinear and a linear form that are domain integrals (top). Here  $u$  is the unknown field (i.e., the temperature) and  $v$  is a known test function. Since the integrals are linear over their domain, we can perform all integrations element-by-element (bottom). Once the integrals are evaluated by the finite element software, we obtain a simultaneous equation system  $[A]\{u\} = \{F\}$  that is solved for the nodal unknowns (the values of field  $u$  at the finite element nodes).**

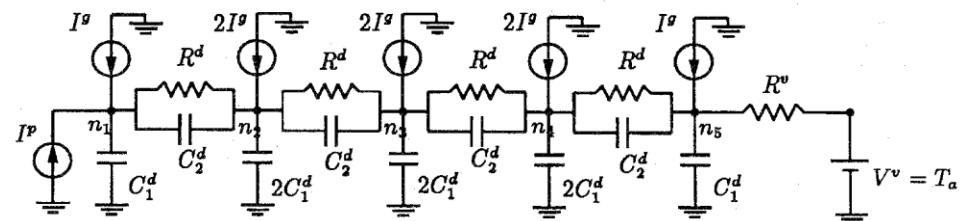
# Thermal Networks in Finite Elements

- J. T. Hsu, L. Vu-Quoc, "A Rational Formulation of Thermal Circuit Models for Electrothermal Simulation - Part I: Finite element Method", *IEEE Transactions on Circuits and Systems*, 43(9), pp. 721-732, (1996).

$$E \frac{\partial T}{\partial t} + KT = F$$



(a)



(b)

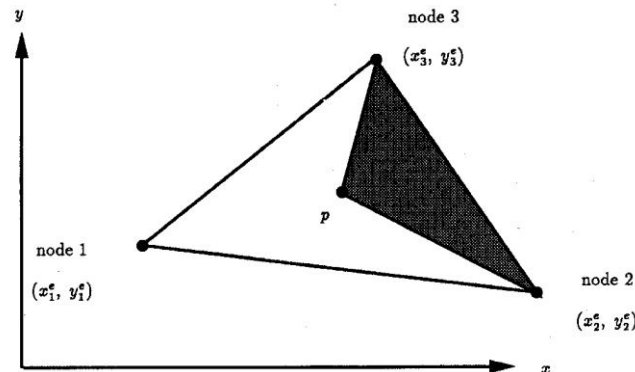
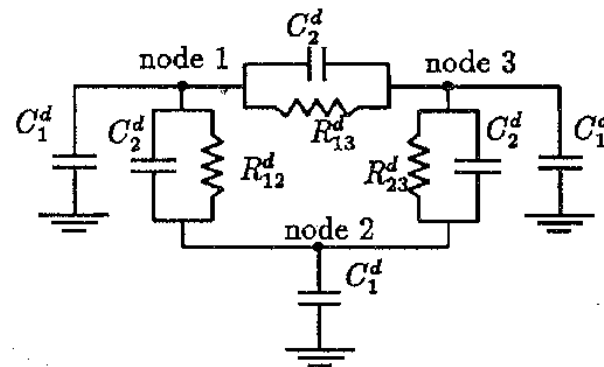


Fig. 13. Area coordinate.



# Element and Global Matrices: Assembly

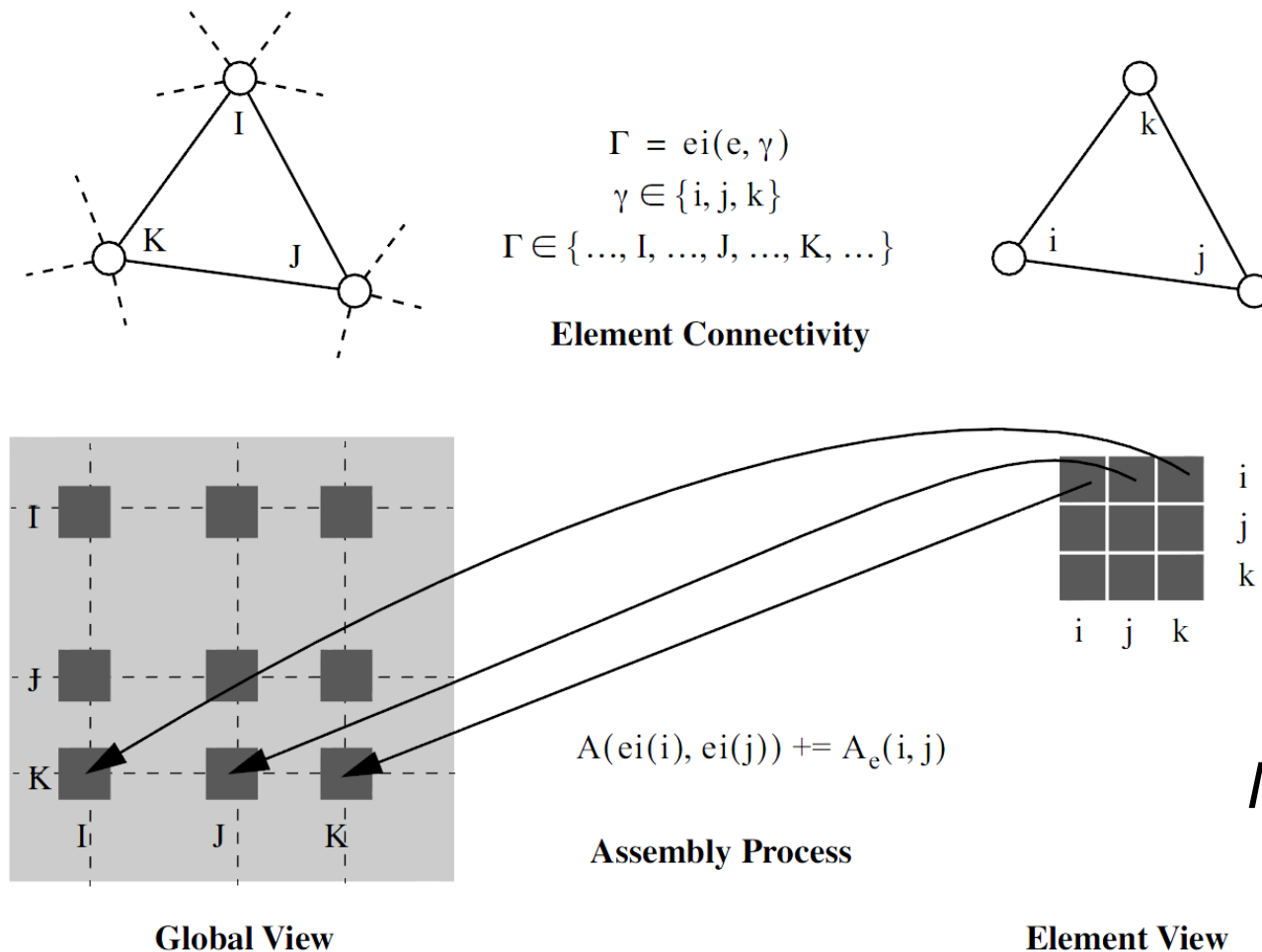
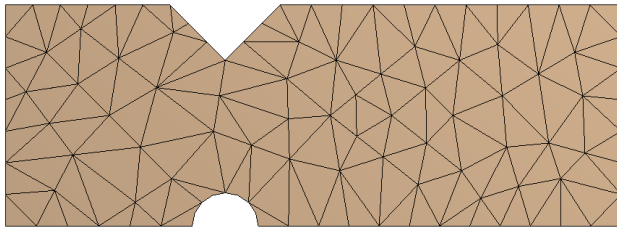
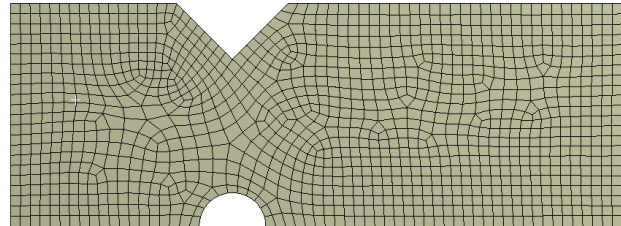


Figure from "MEMS and NEMS Simulation". In MEMS: A Practical Guide to Design, Analysis, and Applications, William Andrew Publishing, 2005.

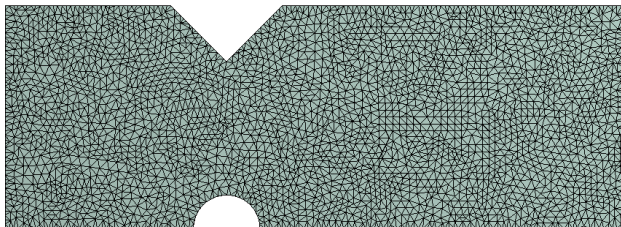
# Meshing and Accuracy – Structural Mechanics



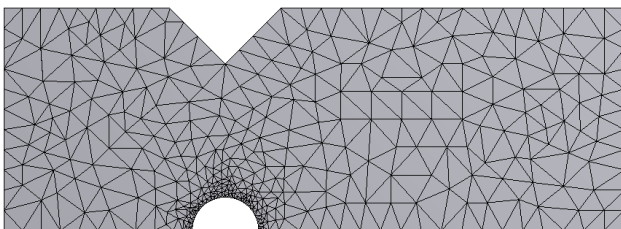
Coarse Tet Mesh



Moderately Fine Hex Mesh



Fine Tet Mesh



Locally Refined Tet Mesh

	Max Deformation	Max Principle Stress	No of Nodes
<b>Coarse Tet</b>	0,192	95,4	1086
<b>Fine Tet</b>	0,2	125	38950
<b>Locally Refined Tet</b>	0,198	126	7702
<b>Hex</b>	0,199	125	14511

# Workflow

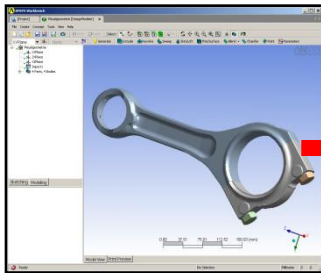
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- Preprocessing
  - Import geometry and simplify if possible
  - Material properties
  - Boundary conditions
  - Loads
  - Meshing
  
- Solution
  
- Postprocessing
  - Visualization
  - Reports

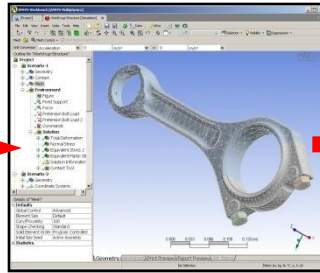


# The Simulation Workflow

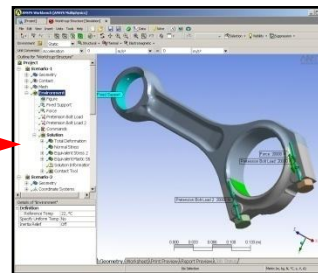
## Geometry



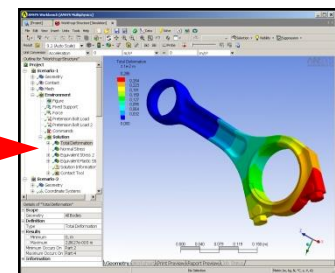
## Meshing



## Simulation



## Results

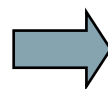


# What is the Analysis Goal

- Structural deformation
- Structural stresses
- Temperatures
- Fluid Velocities
- Fluid Pressures
- Electric Current
- Electric Voltage
- Magnetic field
- .....



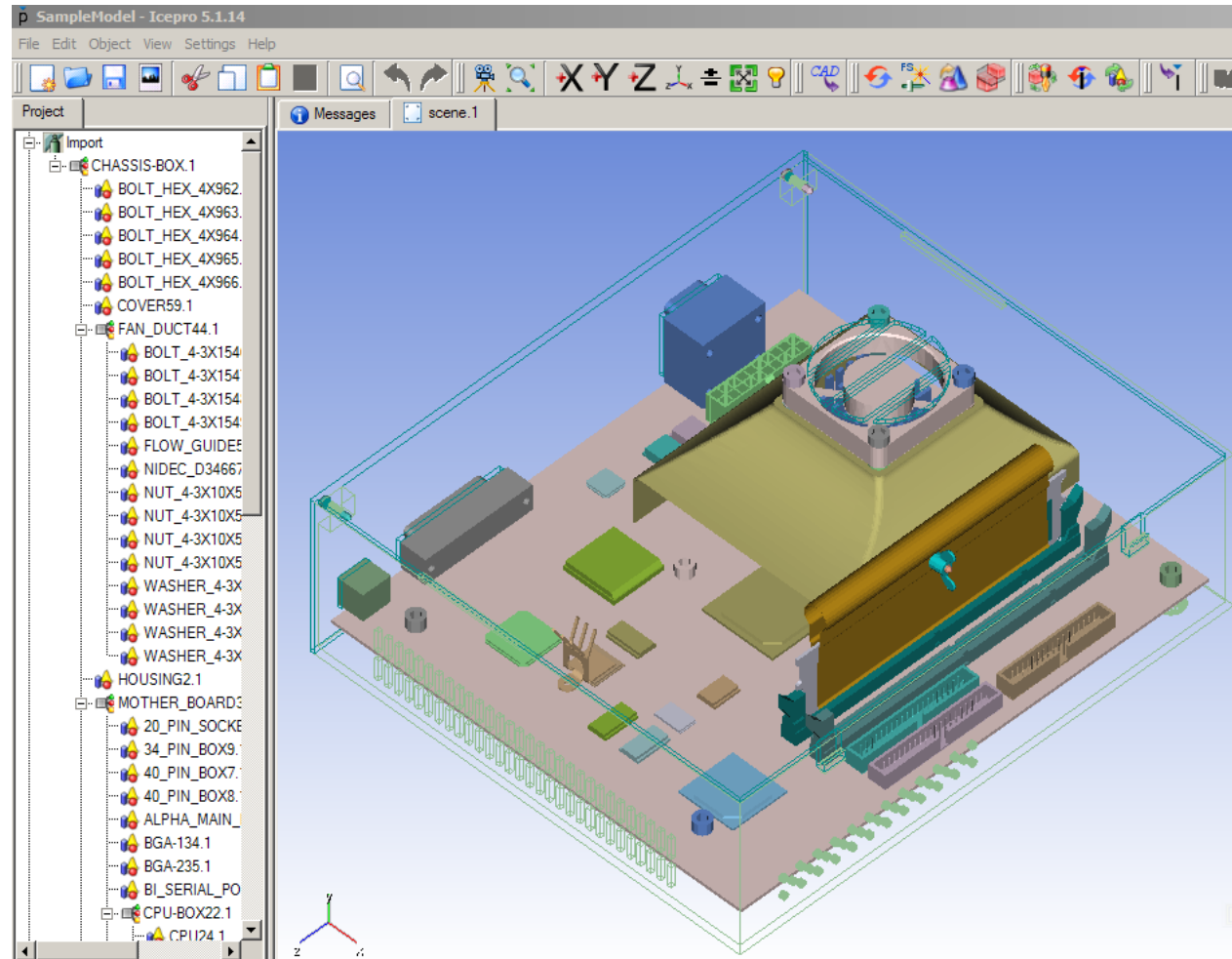
Geometry imported from  
CAD-system



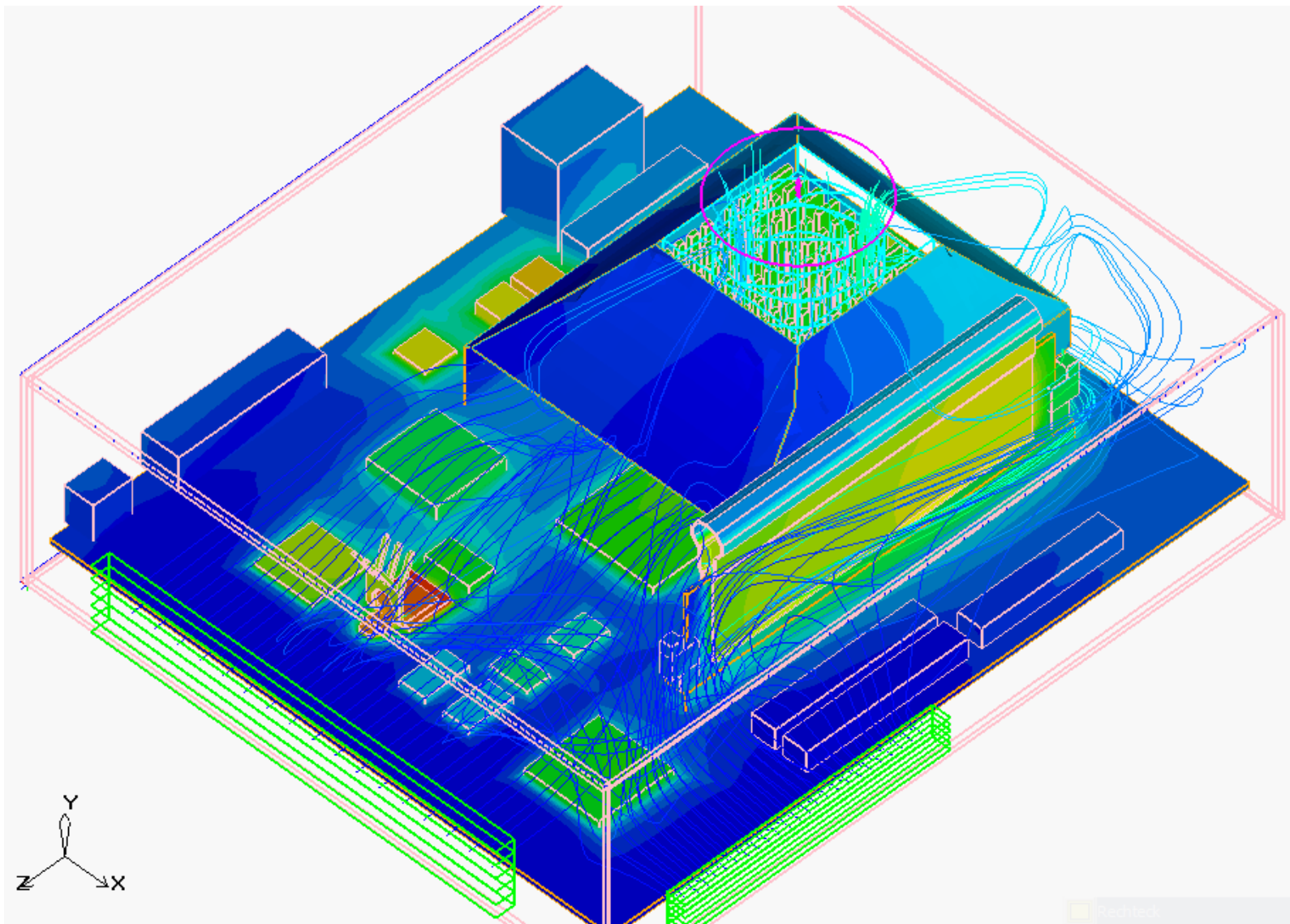
The simulation is done with a mathematical model derived from the CAD-geometry

# Geometry Simplification

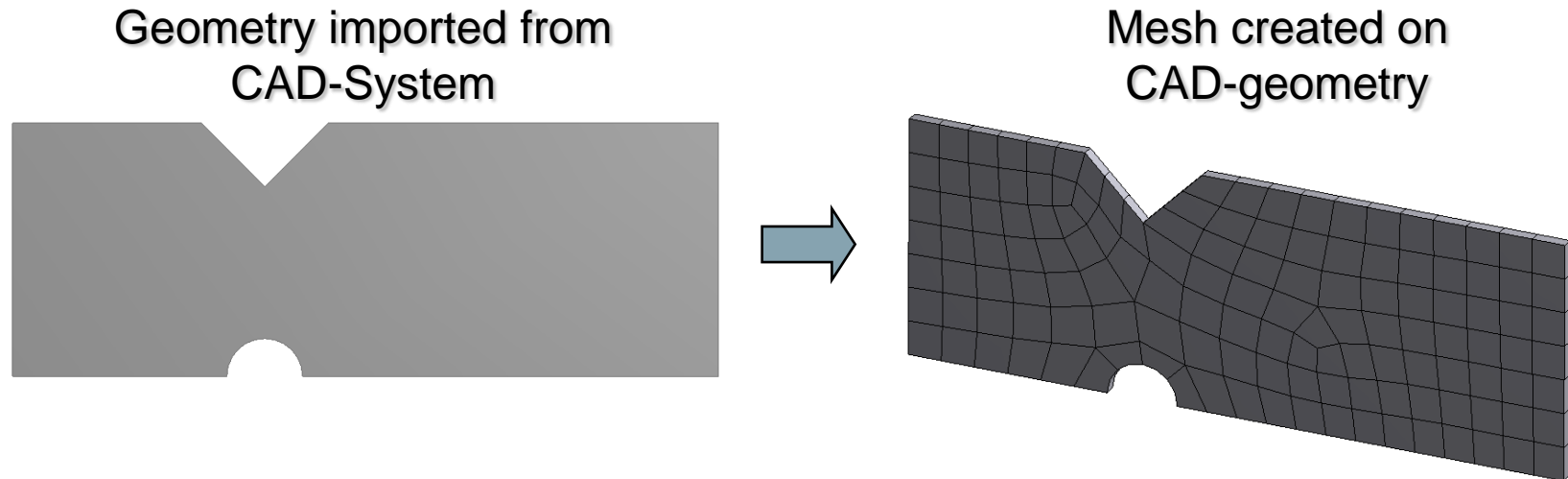
- There are tools to simplify the model.
- Strategy:
  - Divide the model to functional components;
  - Simplify them and save into the Icepak library;
  - Load necessary components to the Icepak project from the library.



# Simulation with simplified model



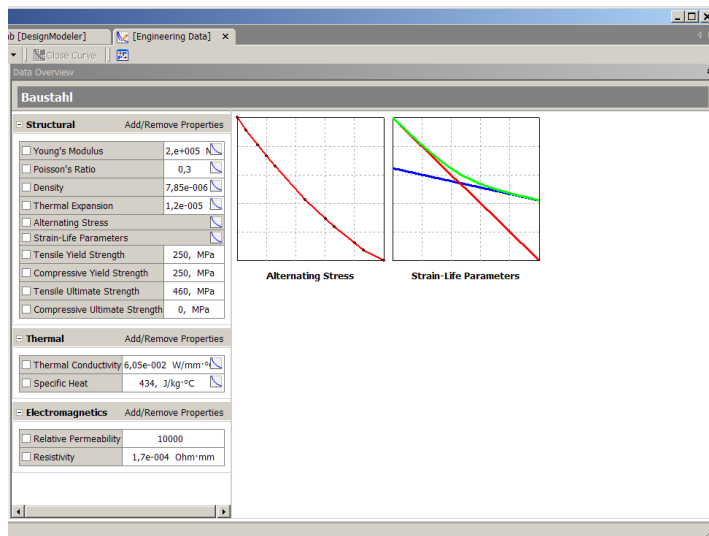
# The Meshing Process



- The geometry is subdivided into and thus represented by elements and nodes
- The required mesh density is strongly governed by the
  - The size of geometric details
  - The desired accuracy
  - The physics to be solved

# Simulation – Definition of Material Properties

For all elements physical properties must be defined.



Material Database

## ■ Structural Mechanics

- Elasticity Module, Poisson Number
- Density, Material Damping

## ■ Heat Transfer

- Conductivity
- Density, Heat Capacity

## ■ Fluid Dynamics

- Density, Viscosity
- Conductivity, Heat Capacity

## ■ Electro-Magnetics

- Electric Conductivity
- Magnetic Permeability

# Simulation – Definition of Boundary Conditions/Loads

The interaction with adjacent parts or the environment is modeled by boundary conditions or loads.



## ■ Structural Mechanics

- Supports, displacements
- Forces, Pressures, Moments

## ■ Thermal Analysis

- Temperatures
- Heat fluxes, convection, radiation

## ■ Fluid Analysis

- Mass flow, velocities
- Pressures

## ■ Electro-Magnetics

- Electric Current
- Electric Potential
- Magnetic Flux Parallel



# Simulation – Solving the Problem

The number of nodes defines the size of the algebraic system of equations to be solved numerically



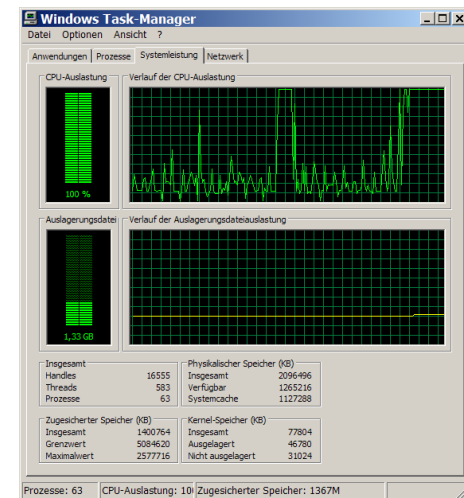
The numerical effort to solve this system of equations is limited by

- Amount of computer storage
- Acceptable CPU time



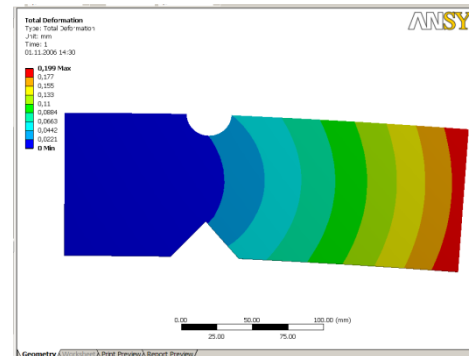
In practice one must often find a compromise between accuracy and numerical effort

$$\begin{bmatrix} a_{11} & a_{12} & a_{13} & \dots \\ a_{12} & a_{22} & a_{23} & \dots \\ \vdots & \vdots & a_{33} & \dots \\ \vdots & \vdots & \vdots & \ddots \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ \vdots \end{bmatrix} = \begin{bmatrix} b_1 \\ b_2 \\ b_3 \\ \vdots \end{bmatrix}$$

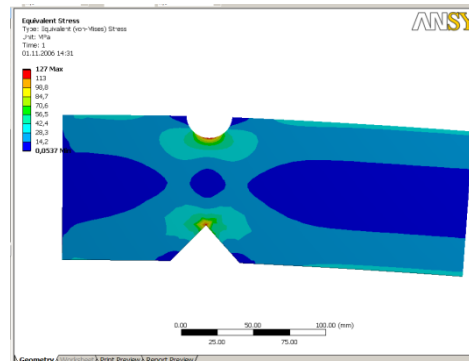


# Post Processing – Structural Mechanics

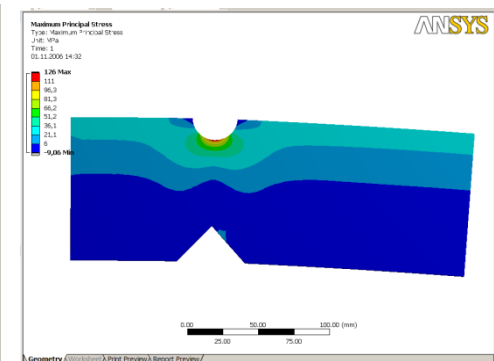
- Deformation – primary result
  - Vector sum
  - Directional Components
- Stresses – derived results
  - Equivalent stresses
  - Principle stresses
  - Stress components
  - Safety factors
  - ..



Total Displacement



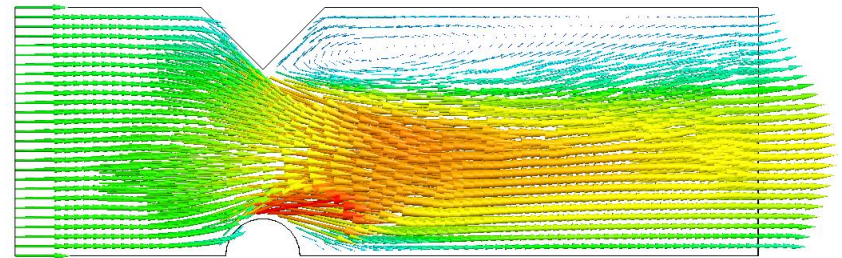
Van Mises Equivalent Stress



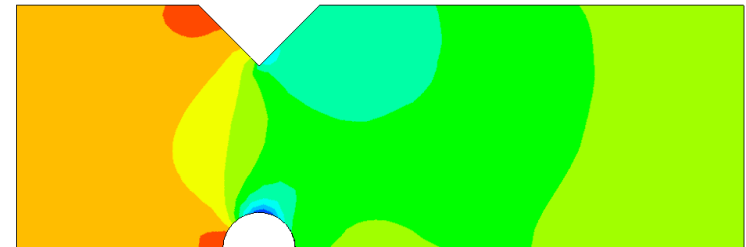
Maximum Principle Stress

# Post Processing – Fluid Mechanics

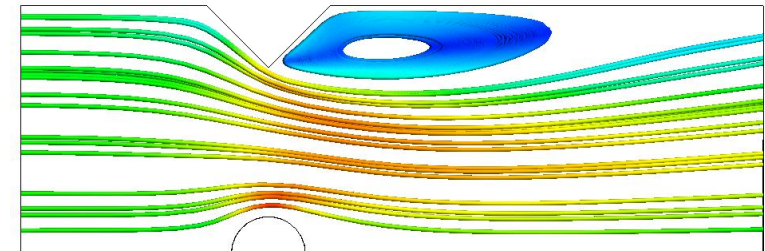
- Velocities
  - Vector Sum, Massflow
  - Directional Components
- Pressure
  - Absolute Pressure
  - Total Pressure
- Temperatures
  - Static and total temperature
  - Heat Film Coefficients
- Flow Forces
  - Pressure Forces
  - Friction Forces



Velocity Vectors

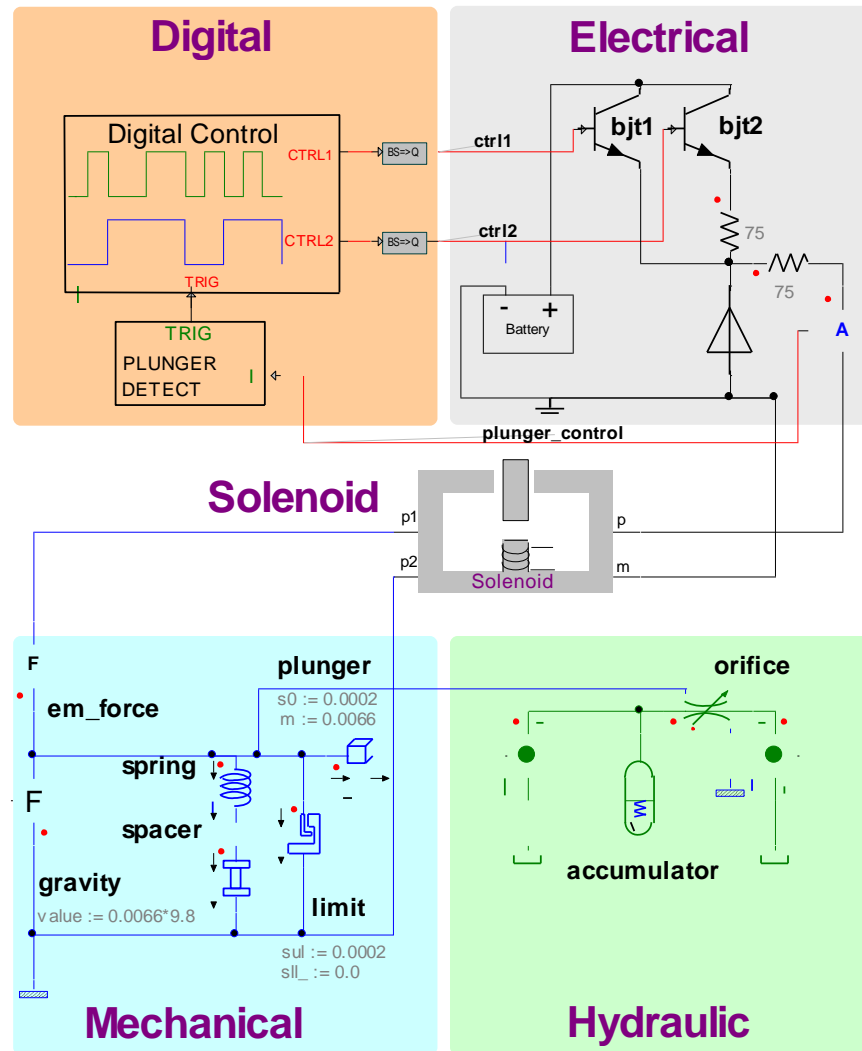


Pressure Contours

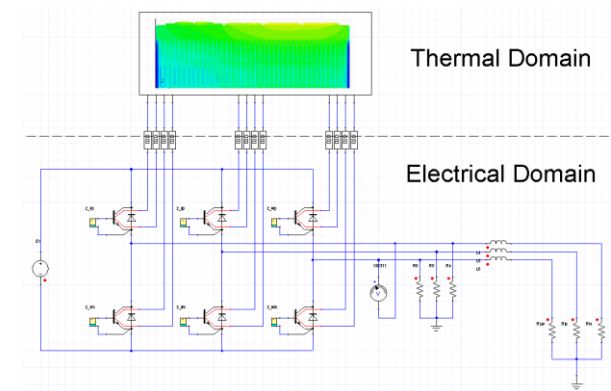
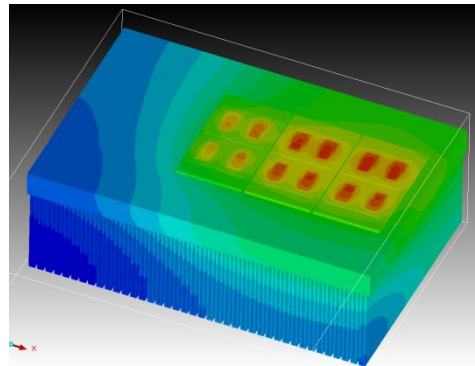
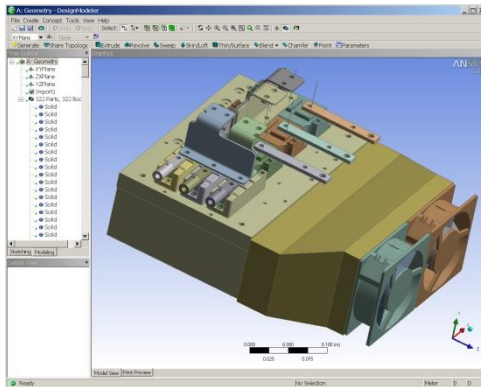
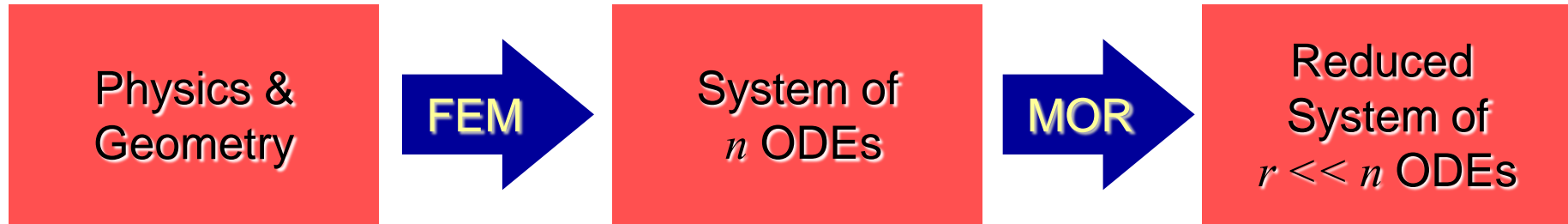


Streamlines

# Example of system level simulation



# From Finite Elements to System Simulation



- <http://ModelReduction.com>

# Summary

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- It is important to understand, that the accuracy of a simulation strongly depends on
  - Correct boundary conditions and loads
  - Correct material properties
  - Sufficient mesh resolution
- All this is the **ENGINEERS** responsibility

## However:

- The **Simulation Environment** provides all the tools that are needed for an efficient and accurate simulation