

FEE321 – E.C.T IIA – Oct 2020

Lecture 9: Laplace Transform (3) (1 hr)

Lecturer: *Prof H A Ouma*

16/12/2020

Overview

Today's class continues the look at LT application

- Examples of LT application in circuit analysis (continued)

Content

- **Examples of LT application in circuit analysis (continued)**

LT application[10]

Example 3

A series RLC circuit is supplied from a dc source of V volts. The source is switched on at $t = 0$. At $t = 0$ there is zero voltage across the capacitor, and no inductor current

- i. Dc source switched on at $t = 0 \Rightarrow v(t) = Vu(t), i_L(0^-) = 0$
- ii. Zero initial voltage $\Rightarrow v_C(0^+) = 0$, inductor ensures $i_L(0^+) = i_L(0^-) = 0$

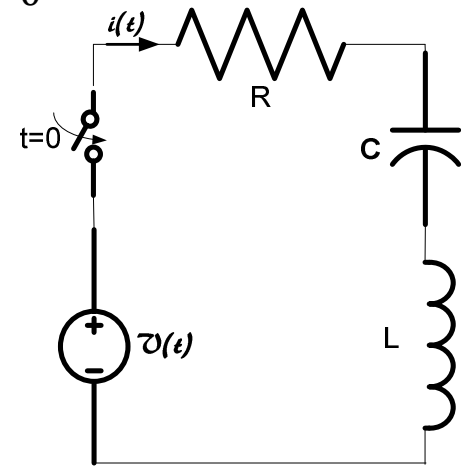
Circuit LDE is given by

$$\frac{1}{C} \int_{-\infty}^t i(t) dt + Ri(t) + L \frac{di(t)}{dt} = Vu(t) \quad ; t > 0$$

Applying LT $\mathcal{L} \left[\frac{1}{C} \int_{-\infty}^t i(t) dt + Ri(t) + L \frac{di(t)}{dt} = Vu(t) \right]$

$$\Rightarrow \mathcal{L} \left[\frac{1}{C} \int_{-\infty}^0 i(t) dt + \frac{1}{C} \int_0^t i(t) dt \right] + \mathcal{L}[Ri(t)] + \mathcal{L} \left[L \frac{di(t)}{dt} \right] = \mathcal{L}[Vu(t)]$$

$$\Rightarrow \mathcal{L} \left[v_C(0^+) + \frac{1}{C} \int_0^t i(t) dt \right] + \mathcal{L}[Ri(t)] + \mathcal{L} \left[L \frac{di(t)}{dt} \right] = \mathcal{L}[Vu(t)]$$



LT application[11]

Example 3 (continued)

Expanding the integral term

$$\Rightarrow \mathcal{L} \left[v_C(0^+) + \frac{1}{C} \int_0^t i(t) dt \right] + \mathcal{L}[Ri(t)] + \mathcal{L} \left[L \frac{di(t)}{dt} \right] = \mathcal{L}[Vu(t)]$$

Applying LT

$$\Rightarrow \frac{v_C(0^+)}{s} + \frac{I(s)}{sC} + RI(s) + L[sI(s) - i(0^+)] = \frac{V}{s}$$

$$\Rightarrow I(s) \left\{ \frac{1}{sC} + R + sL \right\} = \frac{V - v_C(0^+)}{s} + Li(0^+)$$

$$\Rightarrow I(s) \left\{ \frac{1 + sRC + s^2LC}{sC} \right\} = \frac{V - v_C(0^+)}{s} + Li(0^+)$$

Thus

$$\begin{aligned} \Rightarrow I(s) &= \frac{C(V - v_C(0^+))}{1 + sRC + s^2LC} + \frac{sCLi(0^+)}{1 + sRC + s^2LC} \\ &= \frac{CV}{1 + sRC + s^2LC} \quad \text{when } i(0^+), v_C(0^+) = 0 \end{aligned}$$

LT application[12]

Example 3 (continued)

- i. The transform equation then needs to be converted back to time domain
- ii. Terms need to be organized in the forms for which LT pairs exist or LT properties may be applied, otherwise the ILT integral has to be used

$$I(s) = \frac{CV}{1 + sRC + s^2LC} = \frac{V/L}{\frac{1}{LC} + s\frac{R}{L} + s^2} = \frac{V/L}{s^2 + s\frac{R}{L} + \frac{1}{LC}}$$

A completing the square in the denominator term, so it looks more like the transform pairs that we know, gives us

$$I(s) = \frac{V/L}{\left(s + \frac{R}{2L}\right)^2 + \left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}$$

This is now clearly relates to $e^{-at} \sin(\omega t) \Leftrightarrow \frac{\omega}{(s + a)^2 + \omega^2}$

The expression may therefore be rewritten as

$$I(s) = \frac{V/L}{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}} \times \frac{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}}{\left(s + \frac{R}{2L}\right)^2 + \left\{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}\right\}^2}$$

LT application[13]

Example 3 (continued)

We can then do the time domain expression

$$\begin{aligned} i(t) &= u(t) \left\{ \frac{\frac{V}{L}}{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}} \times e^{-\frac{R}{2L}t} \sin\left(\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}t\right) \right\} \\ &= u(t) \left\{ \frac{V}{\sqrt{\left(\frac{L}{C} - \frac{R^2}{4}\right)}} \times e^{-\frac{R}{2L}t} \sin\left(\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}t\right) \right\} = \frac{Vu(t)e^{-\frac{R}{2L}t}}{\sqrt{\left(\frac{L}{C} - \frac{R^2}{4}\right)}} \sin\left(\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}t\right) \text{ A} \end{aligned}$$

- We notice that in this case we shall have a **decaying sinusoid** current response
- And this despite there being no sinusoidal input
- The response is due to the exchange of stored energy between the capacitor and the inductor; the magnetic field and the electric field
- The rate of decay is determined by $\frac{R}{2L}$
- For the same value of L , the larger the value of R , the faster the decay
- Since the resistor is the one that dissipates the energy, this makes sense
- The **circuit time constant**, the time it takes the amplitude to reduce to $1/e$, is $\frac{2L}{R}$ seconds
- At steady state, inductor is a short circuit, capacitor is open circuit and no current flows

LT application[14]

Example 3 (continued)

- Consider

$$i(t) = u(t) \left\{ \frac{V/L}{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}} \times e^{-\frac{R}{2L}t} \sin\left(\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)} t\right) \right\}$$

- If the term under the square root is zero, what happens?
- We have to go back to the s-domain expression to answer this question

$$I(s) = \frac{V/L}{\left(s + \frac{R}{2L}\right)^2 + \left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)} \quad \rightarrow \quad I(s) = \frac{V/L}{\left(s + \frac{R}{2L}\right)^2}$$

- This would now correspond to $u(t)te^{-at} \Leftrightarrow \frac{1}{(s+a)^2}$
- Note that this is obtained by either applying **complex shift** property to the LT of $t \cdot u(t)$ **or** applying the **multiplication by t** property to the LT of $u(t)e^{-at}$
- Under this special condition therefore, the circuit current response shall be $i(t) = \frac{V}{L} t \cdot u(t) e^{-\frac{R}{2L}t}$
- As $t \rightarrow 0$, the **initial value** property of LT gives us $i(t) = 0$, since $sI(s) \rightarrow 0$ as $s \rightarrow \infty$
- As $t \rightarrow \infty$, the **final value** property of LT gives us $i(t) = 0$, since $sI(s) \rightarrow 0$ as $s \rightarrow 0$

LT application[15]

Example 3 (continued)

If the initial conditions were not zero then

$$\begin{aligned}
 \Rightarrow I(s) &= \frac{C(V - v_C(0^+))}{1 + sRC + s^2LC} + \frac{sCLi(0^+)}{1 + sRC + s^2LC} = \frac{\frac{1}{L}\{V - v_C(0^+)\}}{s^2 + s\frac{R}{L} + \frac{1}{LC}} + \frac{s \cdot i(0^+)}{s^2 + s\frac{R}{L} + \frac{1}{LC}} \\
 &= \frac{\frac{1}{L}\{V - v_C(0^+)\}}{\left(s + \frac{R}{2L}\right)^2 + \left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)} + \frac{s \cdot i(0^+)}{\left(s + \frac{R}{2L}\right)^2 + \left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)} \\
 &= \frac{\frac{1}{L}\{V - v_C(0^+)\} - \frac{R}{2L}i(0^+)}{\left(s + \frac{R}{2L}\right)^2 + \left\{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}\right\}^2} + \frac{\left(s + \frac{R}{2L}\right) \cdot i(0^+)}{\left(s + \frac{R}{2L}\right)^2 + \left\{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}\right\}^2} \\
 &= \frac{\frac{1}{L}\left\{V - v_C(0^+) - \frac{R}{2}i(0^+)\right\}}{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}} \times \frac{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}}{\left(s + \frac{R}{2L}\right)^2 + \left\{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}\right\}^2} + i(0^+) \frac{\left(s + \frac{R}{2L}\right)}{\left(s + \frac{R}{2L}\right)^2 + \left\{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}\right\}^2}
 \end{aligned}$$

And

$$i(t) = u(t) \left\{ \frac{\left\{V - v_C(0^+) - \frac{R}{2}i(0^+)\right\}}{\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}} \times e^{-\frac{R}{2L}t} \sin\left(\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}t\right) + i(0^+) \times e^{-\frac{R}{2L}t} \cos\left(\sqrt{\left(\frac{1}{LC} - \frac{R^2}{4L^2}\right)}t\right) \right\} A$$

LT application[16]

Example 3 (numerical)

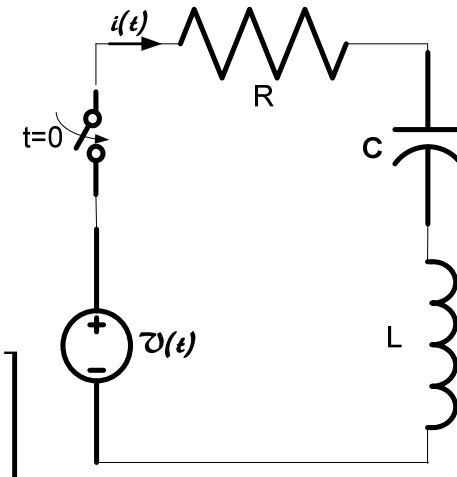
A series RLC circuit is supplied from a dc source of 20 volts. The source is switched on at $t = 0$. Assume that at $t = 0$ there is zero voltage across the capacitor, and no inductor current. Let $R = 10\Omega$, $C = 0.04F$ and $L = 1.25H$

Circuit LDE is given by

$$\frac{1}{C} \int_{-\infty}^t i(t) dt + Ri(t) + L \frac{di(t)}{dt} = Vu(t) \quad ; t > 0$$

Substituting in values

$$\mathcal{L} \left[25 \int_{-\infty}^t i(t) dt + 10i(t) + 1.25 \frac{di(t)}{dt} = 20u(t) \right]$$



Expanding the integral

$$\Rightarrow \mathcal{L} \left[25 \int_{-\infty}^0 i(t) dt + 25 \int_0^t i(t) dt \right] + \mathcal{L}[10i(t)] + \mathcal{L} \left[1.25 \frac{di(t)}{dt} \right] = \mathcal{L}[20u(t)]$$

$$\Rightarrow \mathcal{L} \left[v_C(0^+) + 25 \int_0^t i(t) dt \right] + \mathcal{L}[10i(t)] + \mathcal{L} \left[1.25 \frac{di(t)}{dt} \right] = \mathcal{L}[20u(t)]$$

LT application[17]

Example 3 (numerical continued)

Starting at

$$\mathcal{L}\left[v_C(0^+) + 25 \int_0^t i(t) dt\right] + \mathcal{L}[10i(t)] + \mathcal{L}\left[1.25 \frac{di(t)}{dt}\right] = \mathcal{L}[20u(t)]$$

Applying LT

$$\Rightarrow \frac{v_C(0^+)}{s} + \frac{25I(s)}{s} + 10I(s) + 1.25[sI(s) - i(0^+)] = \frac{20}{s}$$

$$\Rightarrow I(s) \left\{ \frac{25}{s} + 10 + 1.25s \right\} = \frac{20 - v_C(0^+)}{s} + 1.25i(0^+)$$

$$\Rightarrow I(s) \left\{ \frac{25 + 10s + 1.25s^2}{s} \right\} = \frac{20 - v_C(0^+)}{s} + 1.25i(0^+)$$

Thus

$$\Rightarrow I(s) = \frac{20 - v_C(0^+)}{25 + 10s + 1.25s^2} + \frac{1.25s \cdot i(0^+)}{25 + 10s + 1.25s^2}$$

$$= \frac{0.8(20 - v_C(0^+))}{s^2 + 8s + 20} + \frac{s \cdot i(0^+)}{s^2 + 8s + 20}$$

LT application[18]

Example 3 (numerical continued)

Continuing to work with **non-zero** initial conditions then

$$\begin{aligned}\Rightarrow I(s) &= \frac{0.8(20 - v_C(0^+))}{s^2 + 8s + 20} + \frac{s \cdot i(0^+)}{s^2 + 8s + 20} \\ &= \frac{0.8\{20 - v_C(0^+)\}}{(s + 4)^2 + (20 - 16)} + \frac{s \cdot i(0^+)}{(s + 4)^2 + (20 - 16)}\end{aligned}$$

$$= \frac{0.8\{20 - v_C(0^+)\} - 4i(0^+)}{(s + 4)^2 + 2^2} + \frac{(s + 4) \cdot i(0^+)}{(s + 4)^2 + 2^2}$$

$$= 0.4\{20 - v_C(0^+) - 5i(0^+)\} \frac{2}{(s + 4)^2 + 2^2} + i(0^+) \frac{s + 4}{(s + 4)^2 + 2^2}$$

And

$$i(t) = u(t)e^{-4t} \{ [8 - 0.4v_C(0^+) - 2i(0^+)] \sin(2t) + i(0^+) \cos(2t) \} \quad A$$

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Summary

Today's class looked at Laplace transform application

- Examples in circuit analysis

QUESTIONS?