

# Homework Set 2

# Linear Algebra

Revision: 13-Jan-2019

# 2.1 Analysis

## 2.1.1 Uniqueness

Let **A** be a given square matrix. Show that if  $\mathbf{A}\mathbf{x} = \mathbf{b}$  has at least one solution for any **b**, then it has exactly one solution for any **b**.

## 2.1.2 Companion matrix

A companion matrix has the form

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & & & \vdots & \\ 0 & 0 & 0 & \cdots & 1 \\ -a_k & -a_{k-1} & -a_{k-2} & \cdots & -a_1 \end{bmatrix}$$
(2.1)

1. Show that the characteristic equation is

$$\lambda^k + a_1 \lambda^{k-1} + \dots + a_k = 0 \tag{2.2}$$

where  $\lambda$  is an eigenvalue.

2. If k = 3 show that eigenvectors  $\mathbf{v}$  have the form

$$\mathbf{v} = \begin{bmatrix} 1 & \lambda & \lambda^2 \end{bmatrix}^T \tag{2.3}$$

### 2.1.3 Similarity

Consider the matrix  $\mathbf{A} \in \mathbb{R}^{n \times n}$ , and the orthogonal matrix  $\mathbf{Q} \in \mathbb{R}^{n \times n}$ .

- Show that  $\mathbf{B} = \mathbf{Q}^T \mathbf{A} \mathbf{Q}$  has the same eigenvalues as  $\mathbf{A}$ .
- Also, comment on the eigenvectors of **B**.

### 2.1.4

Show that the linear independence of eigenvectors given by

$$\alpha_1 \mathbf{v}_1 + \alpha_2 \mathbf{v}_2 + \dots + \alpha_n \mathbf{v}_n = \mathbf{0} \tag{2.4}$$

is true by making use of the orthogonality property of eigenvectors.



#### Some hand calculations 2.2

#### 2.2.1Determinant

Compute (by hand) the determinant of

$$\mathbf{A} = \begin{bmatrix} 2 & -1 & 0 & 0 & 1 \\ -1 & 2 & -1 & 0 & 0 \\ 0 & -1 & 2 & -1 & 0 \\ 0 & 0 & -1 & 2 & -1 \\ -1 & 0 & 0 & -1 & 2 \end{bmatrix}$$
 (2.5)

check your result using Matlab.

### 2.2.2 Rank

Determine the rank of the following matrix by elimination

$$\mathbf{A} = \begin{bmatrix} 1 & 0 & 1 \\ 1 & 1 & 2 \\ 1 & 1 & q \end{bmatrix} \tag{2.6}$$

#### 2.2.3Inverse

Using Gaussian Elimination, compute the inverse of the following matrices

$$\mathbf{A} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 1 & 2 & 1 & 0 \\ 1 & 3 & 3 & 1 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} 1 & 0 & 1 \\ 1 & 1 & 2 \\ 1 & 1 & q \end{bmatrix}$$
(2.8)

$$\mathbf{B} = \begin{bmatrix} 1 & 0 & 1 \\ 1 & 1 & 2 \\ 1 & 1 & q \end{bmatrix} \tag{2.8}$$

#### 2.3 Some programming

#### 2.3.1BLAS

Here are some general questions about BLAS implementations

- 1. What is the BLAS function(s) that multiplies a general matrix and a vector (in double precision)? Also, explain each input/output of the routine.
- 2. What does dsymv do?
- 3. Write a daxpy-equivalent function in Matlab.

#### 2.3.2 Matrix Multiplication

Implement a naïve (simple loop-based) function that multiplies two rectangular matrices. Check the performance against the built-in matrix multiply on a range of random matrices of increasing size.

#### 2.3.3Determinant

Find the largest determinant of a 6 by 6 matrix whose entries are 1's and -1's.



# 2.4 Eigenvalues and differential equations

Initial value problems in LTI differential equations, without an input, can be written as

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) \tag{2.9}$$

$$\mathbf{x}(0) = \mathbf{x}_0. \tag{2.10}$$

The general solution to this involves the so-called matrix exponential  $e^{\mathbf{A}t}$ :

$$\mathbf{x}(t) = e^{\mathbf{A}t}\mathbf{x}_0 \tag{2.11}$$

which can be computed in many ways. One such method is the use of the Laplace transform which results in

$$e^{\mathbf{A}t} = \mathcal{L}^{-1} \left[ (s\mathbf{I} - \mathbf{A})^{-1} \right]. \tag{2.12}$$

Another approach (if the **A** is diagonalizable) is to use the eigenvalues  $\lambda_i$  and the matrix of eigenvectors **V** of **A** as

$$e^{\mathbf{A}t} = \mathbf{V} \begin{bmatrix} e^{\lambda_1 t} & 0 & 0 \\ 0 & \ddots & 0 \\ 0 & 0 & e^{\lambda_n t} \end{bmatrix} \mathbf{V}^{-1}$$
 (2.13)

- 1. Using the Laplace transform and (2.11), show (2.12).
- 2. Given the matrix **A** in (2.14), compute  $e^{\mathbf{A}t}$  using (2.12).
- 3. Given the matrix **A** in (2.14), compute  $e^{\mathbf{A}t}$  using (2.13).
- 4. Are the solutions from the previous two steps the same? Should they be?

$$\mathbf{A} = \begin{bmatrix} -4 & 1 & -4 \\ 2 & -5 & 2 \\ -3 & 3 & -3 \end{bmatrix}$$
 (2.14)

### 2.5 Some mechanics

At a certain point the stress in a body made of 6061-T6 aluminum is known, and is given as the following matrix

$$\boldsymbol{\sigma} = \begin{bmatrix} 2 & 5 & 3 \\ 5 & 1 & 4 \\ 3 & 4 & 3 \end{bmatrix} 10 \text{MPa} \tag{2.15}$$

- 1. Determine the principal stresses:  $\sigma_1$ ,  $\sigma_2$ ,  $\sigma_3$ .
- 2. Determine the directions of the principal stresses.
- 3. Determine the maximum shear stress  $\tau_{\rm max}$ .
- 4. Determine the factor of safety (compared to yield strength) using the von Mises yield criterion. Compute the von Mises stress  $\sigma_v$  in three ways:



(a) Using the values in  $\sigma$ 

$$\sigma_v = \sqrt{\frac{1}{2} \left[ (\sigma_{11} - \sigma_{22})^2 + (\sigma_{22} - \sigma_{33})^2 + (\sigma_{33} - \sigma_{11})^2 + 6(\sigma_{12}^2 + \sigma_{23}^2 + \sigma_{31}^2) \right]}$$
(2.16)

(b) Using the principal stresses

$$\sigma_v = \sqrt{\frac{1}{2} \left[ (\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 \right]}$$
 (2.17)

(c) Using the second invariant of the deviatoric part of the stress tensor.

$$\sigma_{\text{dev}} = \sigma - \frac{1}{3} \text{tr} (\sigma) \mathbf{I}$$
 (2.18a)

$$J_2 = \frac{1}{2} \operatorname{tr} \left( \boldsymbol{\sigma}_{\text{dev}}^2 \right) \tag{2.18b}$$

$$\sigma_v = \sqrt{3J_2} \tag{2.18c}$$

# 2.6 Some dynamics

Given the mass-spring-damper system in Figure 2.1, assume that the contact forces are viscous friction.

1. Derive the equations of motion and state them in matrix notation.

$$\mathbf{M}\ddot{\mathbf{x}} + \mathbf{C}\dot{\mathbf{x}} + \mathbf{K}\mathbf{x} = \mathbf{f}(t) \tag{2.19}$$

2. Determine the (undamped) natural frequencies of the system. Recall that eigenvalue problem starts from assuming a harmonic free-response  $\mathbf{x}(t) = e^{j\omega t}\mathbf{v}$ , which simplifies the equation of motion to

$$-\omega^2 \mathbf{M} \mathbf{v} + \mathbf{K} \mathbf{v} = \mathbf{0} \tag{2.20}$$

where the eigenvalues are  $\omega^2$ , and their associated mode shape is  $\mathbf{v}$ .

- 3. What is the physical significance of the values of  $\omega$ ?
- 4. Bonus: What are the modeshapes of the system? Be careful here, this system is degenerate, and some eigenvalues are repeated, which means we need to find generalized eigenvectors.
- 5. If the system parameters are given in Table 2.1, numerically check your expressions for the eigenvalues (and eigenvectors if applicable) from the previous steps of the problem.

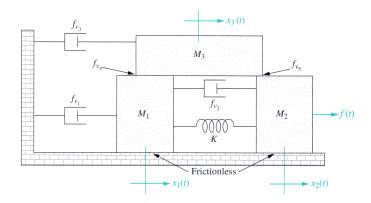


Figure 2.1: A three degree of freedom mass spring damper system.

Table 2.1: Parameter values for §2.6

Quantity	Value	
$m_1$	0.5	kg
$m_2$	0.5	kg
$m_3$	2.0	kg
k	20.0	N/m
$f_{v1} = f_{v2} = f_{v3}$	0.1	Ns/m
$f_{v4} = f_{v5}$	2.0	Ns/m

## 2.7 Some controls

Consider the system of Figure 2.2 where  $m_1=m_2=1\,\mathrm{kg},\ k_1=20\,\mathrm{N/m},\ k_2=10\,\mathrm{N/m},\ c_1=0.4\,\mathrm{Ns/m},\ c_2=0.2\,\mathrm{Ns/m}.$ 

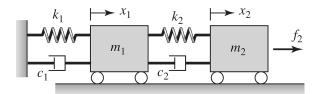


Figure 2.2: Two-mass lumped-model

- 1. Determine the equation of motion in matrix notation  $\mathbf{M}\ddot{\mathbf{x}} + \mathbf{C}\dot{\mathbf{x}} + \mathbf{K}\mathbf{x} = \mathbf{f}(t)$ , where  $\mathbf{x} = \begin{bmatrix} x_1 & x_2 \end{bmatrix}^T$ .
- 2. Determine the linear state-space representation of the system

$$\dot{\mathbf{z}} = \begin{bmatrix} \mathbf{0} & \mathbf{I} \\ -\mathbf{M}^{-1}\mathbf{K} & -\mathbf{M}^{-1}\mathbf{C} \end{bmatrix} \mathbf{z} + \begin{bmatrix} \mathbf{0} \\ \mathbf{M}^{-1}\mathbf{b} \end{bmatrix} u \tag{2.21}$$

$$y = \begin{bmatrix} 0 & 1 & 0 & 0 \end{bmatrix} \mathbf{z} \tag{2.22}$$

where  $\mathbf{z} = \begin{bmatrix} x_1 & x_2 & \dot{x}_1 & \dot{x}_2 \end{bmatrix}^T$ , the output y is  $x_2$ , the input u is  $f_2$  so  $\mathbf{b} = \begin{bmatrix} 0 & 1 \end{bmatrix}^T$ .



3. Determine the coefficients of the desired characteristic equation, if we want the system to have poles at  $\{-2\pm2j, -4\pm4j\}$ 

$$q(s) = s^4 + d_3 s^3 + d_2 s^2 + d_1 s + d_0 (2.23)$$

- 4. Show that the system is controllable. Compute the controllability matrix  $C_M$ , and determine its rank using the following ways:
  - (a) the determinant
  - (b) the QR decomposition
  - (c) the singular value decomposition
  - (d) the eigenvalue decomposition
  - (e) the rank function in Matlab.

Recall that  $C_M$  is

$$\mathbf{C}_{\mathsf{M}} = \left[ \begin{array}{cccc} \mathbf{B} & \mathbf{A}\mathbf{B} & \mathbf{A}^{2}\mathbf{B} & \cdots & \mathbf{A}^{n-1}\mathbf{B} \end{array} \right] \tag{2.24}$$

5. Design a state-feedback controller  $u=-\mathbf{kz}$  using Ackermann's formula. This was originally from (Ackermann, 1972) but it's likely easier to read in English from a text like (Åstörm and Murray, 2008) or Wikipedia. It is a handy tool to directly compute the gains in  $\mathbf{k}$  without needing to transform the system. Ackermann's formula is stated, in general, as

$$\mathbf{k} = \begin{bmatrix} 0 & 0 & \cdots & 0 & 1 \end{bmatrix} \mathbf{C}_{\mathbf{M}}^{-1} \mathbf{P} \tag{2.25}$$

where  ${f P}$  is the desired characteristic polynomial evalulated at  ${f A}$ 

$$\mathbf{P} = \mathbf{A}^{n} + d_{n-1}\mathbf{A}^{n-1} + \dots + d_{1}\mathbf{A} + d_{0}\mathbf{I}$$
 (2.26)

6. Demonstrate that your controlled system meets the desired specifications.

# **Bibliography**

Ackermann, J. (1972). "Der Entwurf linearer Regelungssysteme im Zustandsraum". Regelungstechnik und Prozess-Datenverarbeitung, 7, pp. 297–300. DOI: 10.1524/auto.1972.20.112.297.

Åstörm, K. J. and R. M. Murray (2008). Feedback Systems: An Introduction for Scientists and Engineers. Princeton University Press. URL: http://www.cds.caltech.edu/~murray/amwiki/index.php.