

Punjab Engineering College, Chandigarh
End-Term Examination

Programme: **B.E (Electrical)**

Course Name: Electrical Machines-II

Maximum Marks: 100

Course Instructor: Prof. Dhiraj Bharat

Year/Semester: 2122_2

Course Code: **EL1006**

Time allowed: **3 Hrs**

Date & Time: 13th May 2022, 9:30-12:30 Hrs

- All questions are compulsory.
- Unless stated otherwise, the symbols have their usual meanings in context with subject. Assume suitably and state, additional data required, if any.
- The candidates, before starting to write the solutions, should please check the question paper for any discrepancy, and also ensure that they have been delivered the question paper of right **course code**.

Q.No	Question	Marks												
1.A	<p>A 220 V, three phase, two pole, 50-Hz induction motor is running at a per unit slip of 0.05. Find the following</p> <p>i. The speed of the rotating magnetic field in rpm. ii. The speed of the rotor in rpm. iii. The slip speed of the rotor in rpm. iv. The rotor frequency in Hz.</p>	10												
1.B	<p>The test data on a 208-V, 60-Hz, 4-pole, Y-connected, three-phase induction motor rated at 1710 rpm are as follows:</p> <table border="1" style="margin-left: auto; margin-right: auto;"> <tr> <th></th><th style="text-align: center;">No Load Test</th><th style="text-align: center;">Blocked Rotor Test</th></tr> <tr> <td>Power Input</td><td style="text-align: center;">450 W</td><td style="text-align: center;">59.4 W</td></tr> <tr> <td>Line Current</td><td style="text-align: center;">1.562 A</td><td style="text-align: center;">2.77 A</td></tr> <tr> <td>Line Voltage</td><td style="text-align: center;">208 V</td><td style="text-align: center;">27 V</td></tr> </table> <p>The stator resistance (dc) between any two terminals = 2.4Ω. Evaluate the equivalent circuit parameters of the induction motor and draw its per phase equivalent circuit with respect to the stator. Also evaluate the maximum value of the torque that the machine can supply. At what speed this maximum torque is generated?</p>		No Load Test	Blocked Rotor Test	Power Input	450 W	59.4 W	Line Current	1.562 A	2.77 A	Line Voltage	208 V	27 V	10
	No Load Test	Blocked Rotor Test												
Power Input	450 W	59.4 W												
Line Current	1.562 A	2.77 A												
Line Voltage	208 V	27 V												
2.A	<p>A 440 V, 3-phase, 50 Hz, 6 pole, delta connected induction motor has the following parameters referred to the stator:</p> <p style="text-align: center;">$R_s = 2 \Omega, R_r' = 2 \Omega, X_s = 3\Omega, X_r' = 4 \Omega, X_m = 100 \Omega$</p> <p>When driving a load whose torque varies linearly with speed, at rated voltage it runs at rated speed. If the motor speed is controlled using stator voltage control.</p> <p>i. Motor terminal voltage, current and torque at 800 rpm. ii. Motor speed, current and torque for the terminal voltage of 280 V.</p>	12												
2.B	<p>Write short notes on the following:</p> <p>i. PMBLDC Motor. ii. Split Phase Induction Motor.</p>	8												

	A 9-kVA, 208-V, 60-Hz, Y Connected, three phase alternator has a synchronous impedance of $0.1 + j3 \Omega$ per phase. The field winding resistance is 25Ω and the applied field voltage is 120-V (dc). The per phase OCC data at rated speed is as under																									
3.A	<table border="1"> <thead> <tr> <th>$i_f(A)$</th><th>0</th><th>0.5</th><th>1</th><th>1.5</th><th>2</th><th>2.5</th><th>3</th><th>3.5</th><th>4</th><th>4.5</th><th>5</th></tr> </thead> <tbody> <tr> <td>$E_a(V)$</td><td>0</td><td>90</td><td>140</td><td>185</td><td>209</td><td>223</td><td>230</td><td>236</td><td>238</td><td>248</td><td>250</td></tr> </tbody> </table> <p>If the rotation loss is 800 W, determine the voltage regulation and efficiency of the generator when it supplies the rated load at 0.9 pf lagging. What must be the external resistance in the field winding circuit.</p>	$i_f(A)$	0	0.5	1	1.5	2	2.5	3	3.5	4	4.5	5	$E_a(V)$	0	90	140	185	209	223	230	236	238	248	250	10
$i_f(A)$	0	0.5	1	1.5	2	2.5	3	3.5	4	4.5	5															
$E_a(V)$	0	90	140	185	209	223	230	236	238	248	250															
3.B	Condition for “unity internal power factor” is a preferred condition in the operation of synchronous generators. Determine the governing dynamics for operation of unity internal power factor for a cylindrical rotor synchronous generator in terms of armature current, power factor angle, synchronous reactance and per phase terminal voltage. Also determine the absolute limit of armature current beyond which condition of unity internal power factor cannot be imposed. Neglect armature resistance.	10																								
4.A	A 2200-V, 60-Hz, three-phase, Y connected, 8 pole synchronous motor has synchronous impedance of $0.8 + j8 \Omega$. At no load, the field excitation is adjusted so that the excitation voltage is equal in magnitude to the applied voltage. When the motor is loaded the torque angle is 22° (lagging). Compute the torque developed by the motor.	10																								
4.B	<p>A 208-V, 60-Hz, three-phase, Y-connected, salient pole synchronous motor operates at full load and draws a current of 40 A at 0.8 pf lead. The d-axis and q-axis reactance are 2.7Ω and 1.7Ω, respectively. The armature winding resistance is negligible and rotational loss is 5% of the power developed by the motor. Determine the following</p> <ol style="list-style-type: none"> Per phase excitation voltage \widetilde{E}_a. Synchronous power and salient power. Torque angle. 	10																								
5.A	<p>A 208-V, three-phase, Y connected, synchronous motor takes 7.2 kW at 0.8 pf leading. The synchronous reactance of the motor is 4Ω and the armature winding resistance is negligible. Determine the new torque angle, armature current and power factor if</p> <ol style="list-style-type: none"> The field excitation is adjusted to decrease the excitation voltage by 50% while the load on the motor remains same. The field excitation is adjusted to obtain a unity power factor while the load on the motor remains same. 	10																								
5.B	A salient pole synchronous motor has negligible armature resistance. It is connected to infinite bus and giving a constant power output. Derive the differential equation indicating the governing dynamics of change of power angle with change in the induced voltage with induced voltage as independent variable and power angle as the dependent variable.	10																								

End Semester Examination Solutions

Electrical Machines - II

2021-22 - 2, DOE - 13th May 2022

Ans 1. (A) 220 V, 3Ø, 2 pole, 50 Hz

$$s = 0.05$$

$$\text{Speed of rotating MF} = \frac{120f}{P} = \frac{120 \times 50}{2} = 3000 \text{ rpm} \\ = N_s$$

$$N_m = SN_s = (1-s)N_s = 0.95 \times 3000 \\ = 2850 \text{ rpm}$$

Slip speed = slip (pu) \times Base

$$= 0.05 \times 3000 \\ = 150 \text{ rpm}$$

$$f_s = sf = 0.05 \times 50 = 2.5 \text{ Hz}$$

$$\underline{\text{Ans 1. (B)}} \quad W_{NL} = 450 \quad W_{NL/\text{phase}} = \frac{450}{3} = 150 \text{ W}$$

$$I_{NL} = 1.562 \text{ A} = I_{NL/\text{phase}}$$

$$V_{NL} = \frac{208}{\sqrt{3}} \Rightarrow V/\text{phase} = \frac{208}{\sqrt{3}} = 120.088$$

$$R_{dc} = 2.4 \Rightarrow R_s = \frac{2.4}{2} = 1.2 \Omega$$

$$\frac{(V/\text{phase})^2}{R_c} = W_{NL/\text{phase}} = 150$$

$$\Rightarrow \frac{\left(\frac{208}{\sqrt{3}}\right)^2}{R_c} = 150 \Rightarrow R_c = \frac{(208)^2}{3 \times 150} \\ = 96.1422 \Omega$$

$$\Theta_{NL/\text{phase}} = \sqrt{S_{NL/\text{phase}}^2 - W_{NL/\text{phase}}^2} \quad (1) \\ = \sqrt{\left(\frac{208}{\sqrt{3}} \times 1.562\right)^2 - (150)^2} = 112.63127 \text{ VAR}$$

$$\frac{V_{NL}/\text{phase}^2}{X_m} = \theta_{NL}/\text{phase}$$

$$\frac{\left(\frac{208}{\sqrt{3}}\right)^2}{X_m} = 112.63127$$

$$\Rightarrow X_m = 128.04 \Omega$$

$$W_{br} = 59.4 \text{ W} \quad W_{br}/\text{phase} = 19.8 \text{ W}$$

$$I_{br} = 2.77 \text{ A} = \frac{I_{br}/\text{phase}}{V_{br}/\text{phase}} = \frac{27}{\sqrt{3}} = 15.5884 \text{ V}$$

$$V_{br} = 27 \text{ V}$$

$$(I_{br})^2 R_e = W_{br}/\text{phase}$$

$$(2.77)^2 R_e = 19.8 \Rightarrow R_e = 2.5805 \Omega$$

$$\Rightarrow R_s + R_r' = 2.5805 \Omega$$

$$\Rightarrow R_r' = 2.5805 - 1.2 = 1.3805 \Omega$$

$$\theta_{br}/\text{phase} = \sqrt{S_{br}/\text{phase}^2 - W_{br}/\text{phase}^2}$$

$$= \sqrt{\left(\frac{27}{\sqrt{3}} \times 2.77\right)^2 - (19.8)^2}$$

$$= 38.3728 \text{ VAR}$$

(2)

$$(I_{br}/\text{phase})^2 X_e = \theta_{br}/\text{phase}$$

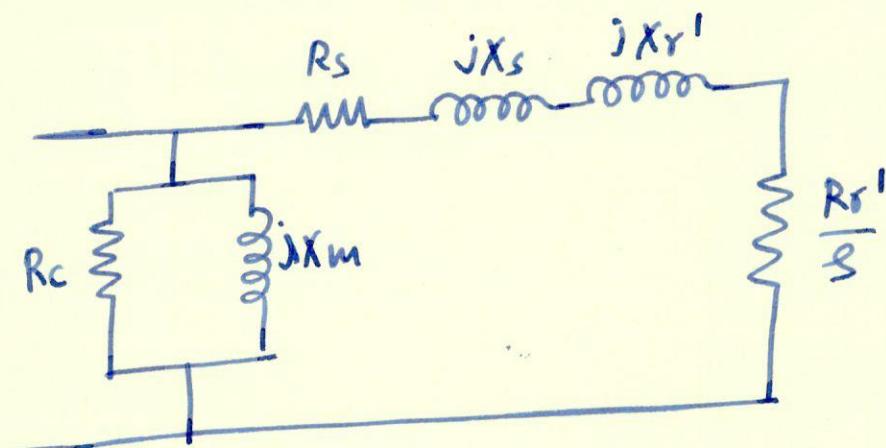
$$X_e = \frac{(38.3728)^2}{(2.77)^2} = 5.0010 \Omega$$

$$\Rightarrow X_S = X_{r'} \approx 0.5 X_e \approx 2.5 \Omega$$

$$R_S = 1.2 \Omega \quad R_{r'} = 1.3805$$

$$X_S = X_{r'} = 2.5 \Omega$$

$$R_C = 96.1422 \Omega, \quad X_m = 128.04 \Omega$$



$$\begin{aligned} W_{ma} &= \frac{120f}{P} \times \frac{2\pi}{60} \\ &= \frac{120 \times 60}{4} \times \frac{2\pi}{60} \\ &= 188.4955 \text{ rad/sec.} \end{aligned}$$

$$\alpha = \frac{3 V_1^2 R_{r'}}{W_{ma}} = \frac{3 \left(\frac{208}{\sqrt{3}}\right)^2 1.3805}{188.4955} = 316.856$$

$$A = R_S^2 + X_e^2 = (1.2)^2 + (5.001)^2 = 26.45$$

$$B = 2 R_S R_{r'} = 2 (1.2) (1.3805) = 3.3132$$

$$C = R_{r'}^2 = 1.90578$$

$$T_{max(motoring)} = \frac{\alpha}{B + 2\sqrt{AC}} = \frac{316.856}{3.3132 + 2\sqrt{26.45 \times 1.90578}} = \underline{18.0927 \text{ N-m.}}$$

$$\delta_{(max T, motoring)} = + \sqrt{\frac{C}{A}} = + \sqrt{\frac{1.90578}{26.45}}$$

$$= \underline{0.2684}$$

(3)

$$\begin{aligned} \text{Speed (max T)} &= (1 - 0.2684) \times 1800 \\ &= \underline{1316.8343 \text{ rpm}} \end{aligned}$$

Ans 2(A) 440 V, 3Ø, 50 Hz, 6 pole, 975 rpm
 Δ connected

$$R_s = 2 \Omega \quad R_r' = 2 \Omega \quad X_s = 3 \Omega \quad X_r' = 4 \Omega$$

$$X_m = 100 \Omega \quad W_{m0} = \frac{120 \times 50}{6} \times \frac{2\pi}{60} = \frac{104.7197}{rad/sec}$$

$T_L = K W_m$ → at rated voltage it runs at rated speed.

$$\alpha = \frac{3 V_1^2 R_r'}{W_{m0}} = \frac{3 (440)^2 2}{104.7197} = 11092.4629$$

$$A = R_s^2 + X_e^2 = 2^2 + 7^2 = 53$$

$$B = 2 R_s R_r' = 2(2)(2) = 8$$

$$C = R_r'^2 = 4$$

$$\xi_{rated} = 1 - S_{rated} = 1 - \frac{975}{1000} = 0.055$$

$$T_e = \frac{\alpha s}{As^2 + Bs + C} = \frac{(11092.4629)(0.055)}{53(0.055)^2 + 8(0.055) + 4} \\ = 13.061133 N-m.$$

$$\Rightarrow K W_{m(rated)} = T_L = T_e = 13.061133$$

$$\Rightarrow K = \frac{13.061133}{995 \times \frac{2\pi}{60}} = 0.131983$$

$$(i) W_m = 800 rpm = 83.7758 rad/sec$$

$$T_L = K W_m = 11.05698 N-m.$$

$$\xi_{800rpm} = 1 - \frac{800}{1000} = 0.2$$

$$T_e = \frac{\alpha s}{As^2 + Bs + C} = T_L$$

(4)

$$\frac{d_{(800 \text{ rpm})} s_{800}}{A s_{800}^2 + B s_{800} + C} = 11.05698$$

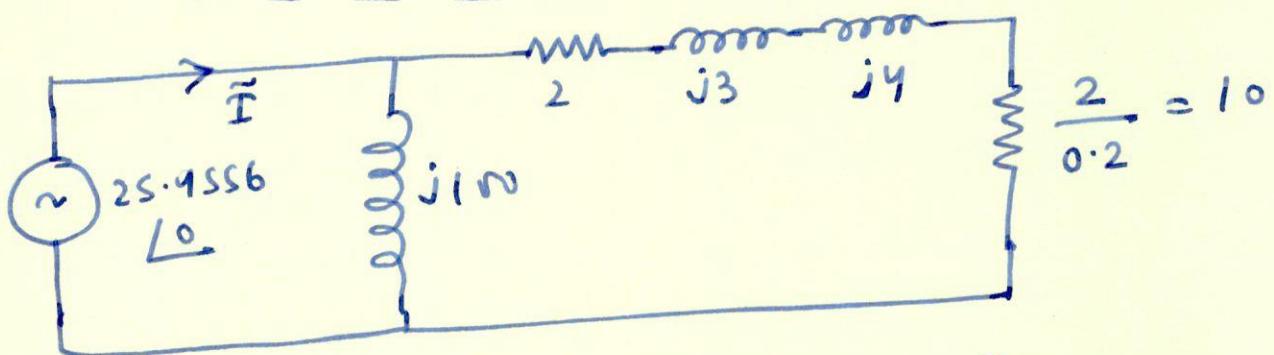
$$d_{(800 \text{ rpm})} 0.2 = (11.05698)(53(0.2)^2 + 8(0.2) + 4)$$

$$d_{(800 \text{ rpm})} = 38.6$$

$$\Rightarrow \frac{3 V_{(800)}^2 Rr'}{W_{\text{ms}}} = 38.6$$

$$\Rightarrow \frac{3 V_{(800)}^2 \times 2}{104.7197} = 38.6$$

$$\Rightarrow V_{800} = 25.9556 \text{ V}$$



$$\tilde{I} = \frac{25.9556 L^0}{j1w} + \frac{25.9556 L^0}{12 + 7j}$$

$$= 2.01164 \angle -36.6553^\circ$$

$$I_{\text{line}} = \sqrt{3} \times 2.01164 = 3.48426 \text{ A}$$

$$T_{\text{e}}(800 \text{ rpm}) = T_L(800 \text{ rpm}) = 11.05698$$

(5)

$$(ii) \quad V_L = 280^\circ = \nu_{\text{phase}}.$$

$$\frac{\alpha s}{As^2 + Bs + C} = K W_m = K S W_{\text{ms}}$$

$$= K(1-s) W_{\text{ms}}.$$

$$\alpha = \frac{3 \times (280)^2 2}{104.7197} = 4491.991478$$

$$A = 53, \quad B = 8, \quad C = 4, \quad K = 0.131983.$$

$$\Rightarrow \frac{4491.991478 s}{53s^2 + 8s + 4} = \frac{(0.131983)(104.7197)}{(1-s)}$$

$$\Rightarrow 4491.991478 s = 13.82122 (1-s)(53s^2 + 8s + 4)$$

$$\Rightarrow 325.00688 = 53s^2 + 8s + 4$$

$$- 53s^3 - 8s^2 - 4s$$

$$\Rightarrow 325.00688 = -53s^3 + 45s^2 + 4s + 4$$

$$\Rightarrow 53s^3 - 45s^2 + 321.00688 - 4 = 0$$

$$s = \frac{-0.012482, 0.41828 + 2.423i,}{0.41828 - 2.423i}$$

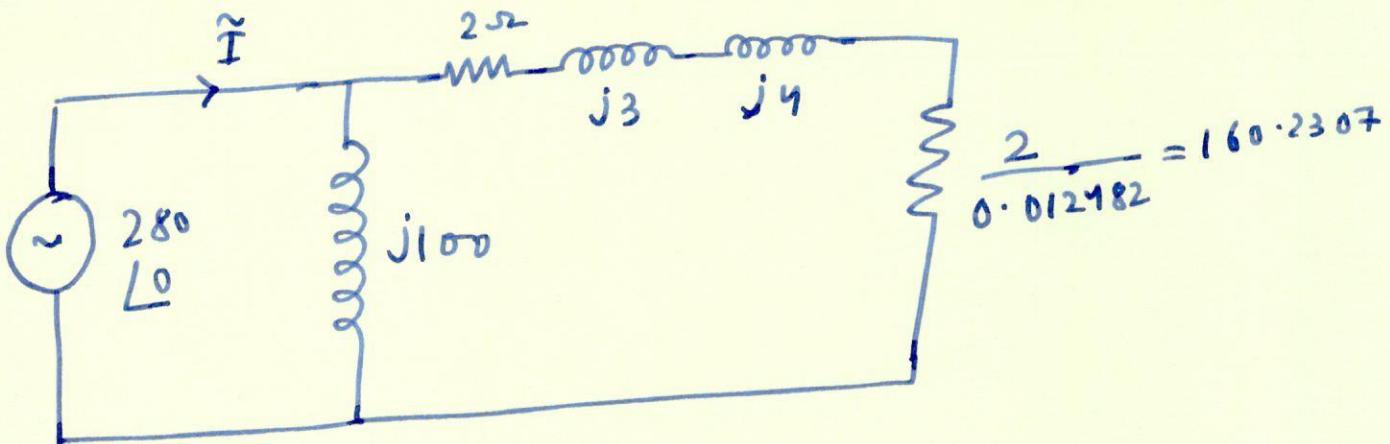
$$\Rightarrow s = \underline{-0.012482} \Rightarrow s = 0.987518$$

$$W_m(280v) = 0.987518 \times 1000 = 987.518 \text{ rpm.}$$

$$T_e = T_L = K W_m = 0.131983 \times 987.518 \times \frac{2\pi}{60}$$

$$= \underline{13.6487 \text{ N-m.}}$$

(6)



$$\tilde{I} = \frac{280 \angle 0^\circ}{100j} + \frac{280 \angle 0^\circ}{162.2307 + 7j}$$

$$= 3.351057 \angle -59.06366^\circ$$

$$\Rightarrow I_{\text{LINE}} = 3.351057 \sqrt{3} = 5.8042 \text{ A}$$

Ans 2(B) → Theory

Ans 3(A) 9 kVA, 208V, 60Hz, Y connected, 3Ø
Synchronous generator
 $Z_s = 0.1 + j3 \Omega/\text{phase}$ $R_f = 25 \Omega$
 $V_f = 120 \text{ V(d.c.)}$

$$P_T = 800 \text{ W}$$

$$\text{per phase kVA} = \frac{9}{3} = 3 \text{ kVA}$$

$$\text{per phase voltage} = \frac{208}{\sqrt{3}}$$

$$\Rightarrow \text{rated load current} = \frac{3000}{208/\sqrt{3}} = 24.9815 \text{ A}$$

$$\tilde{V}_t = \frac{208}{\sqrt{3}} \angle 0^\circ = 120.088 \angle 0^\circ \quad (7)$$

$$\tilde{I}_a = 24.9815 \angle -25.8419^\circ \text{ (0.9 pf lag).}$$

$$\tilde{E}_a - \tilde{I}_a Z_s = \tilde{V}_t \Rightarrow \hat{E}_a = \tilde{V}_t + \tilde{I}_a Z_s$$

$$\tilde{E}_a = 120.088 \angle 0^\circ + (24.9815 \angle -25.8419) \\ (0.1 + j3) \\ = 168.611966 \angle 23.177^\circ$$

$$\text{Approximate linearized slope} = \frac{45}{0.5}$$

$$\Rightarrow \frac{45}{0.5} = \frac{168.611966 - 140}{I_f - 1}$$

$$\Rightarrow I_f - 1 = 0.31791$$

$$\Rightarrow I_f = 1.31791 \text{ A}$$

$$\frac{V_f}{R_f + R_{ex}} = I_f = 1.31791$$

$$\Rightarrow R_f + R_{ex} = 91.0532$$

$$\Rightarrow R_{ex} = 66.0532 \Omega$$

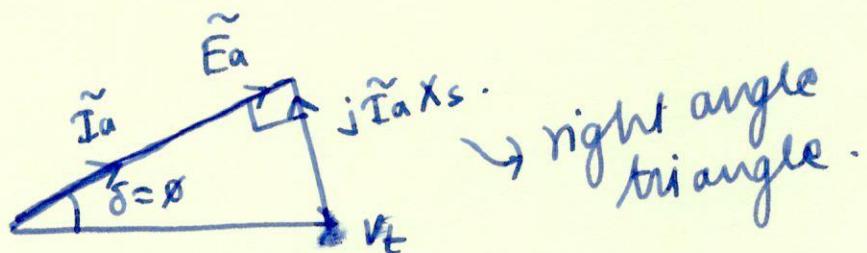
$$\therefore VR = \frac{\frac{E_a - V_t}{\sqrt{3}} \times 100}{\frac{208}{\sqrt{3}}} = \frac{-208}{\sqrt{3}} + 168.611966 \\ = 40.407 \%$$
(8)

$$P_0 = 3V_t I_a \cos \phi = 3 \frac{208}{\sqrt{3}} (24.9815)(0.9) = 8099.999 \text{ W}$$

$$\eta = \frac{P_0}{P_0 + \text{losses.}} = \frac{8099.999}{8099.999 + (1.31791)^2 (91.0532)} \\ + 3(24.9815)^2 (0.1) \\ = \frac{8099.999 + 800}{8099.999 + 158.1492 + 187.2226 + 800}$$

$$\therefore \eta = \frac{8099.999}{9245.3708} \times 100 = 87.6114\%$$

Ans 3(B)



for unity internal power factor $\delta = 0^\circ$.

$$\sin \phi = \frac{I_a X_s}{V_t} \rightarrow \text{governing dynamics for unity internal power factor}$$

$$\sin \phi \leq 1$$

$$\Rightarrow \frac{I_a X_s}{V_t} \leq 1 \Rightarrow$$

$$I_a \leq \frac{V_t}{X_s}$$

$$I_a (\text{absolute maxima}) = \frac{V_t}{X_s}$$

Ans 4.(A) 2200V, 60Hz, 3Ø, Y connected
8 pole, synchronous motor

$$Z_s = 0.8 + j8 \Omega$$

$$\text{at no load } E_a = \frac{220}{\sqrt{3}} = 1270 \cdot 170592 V$$

$$|\delta| = 22^\circ \text{ or } \delta = -22^\circ$$

(9)

$$\tilde{V}_t = \frac{2200}{\sqrt{3}} \angle^{\circ} = 1270.170592 \angle^{\circ}$$

$$\tilde{E}_a = \frac{2200}{\sqrt{3}} \angle^{-22^{\circ}} = 1270.170592 \angle^{-22^{\circ}}$$

$$\begin{aligned}\tilde{I}_a &= \frac{\tilde{V}_t - \tilde{E}_a}{Z_s} \rightarrow \delta \\ &= 60.289 \angle^{-5.2894}\end{aligned}$$

$$\begin{aligned}P_{in} &= 3 \operatorname{Re}(\tilde{V}_t \tilde{I}_a^*) = 3 V_t I_a \cos \delta \\ &= 3 \frac{2200}{\sqrt{3}} \times 60.289 \times \cos(5.2894) \\ &= 228753.6931 \text{ W}\end{aligned}$$

$$\begin{aligned}P_d &= P_{in} - P_{scw} \\ &= 228753.6931 - 3 \times (60.289)^2 \times 0.8 \\ &= 220030.2607 \text{ W} \\ &= 3 \operatorname{Re}(\tilde{E}_a \tilde{I}_a^*)\end{aligned}$$

$$P_d = T_d \text{ Wms} \Rightarrow T_d = \frac{220030.2607}{\frac{120 \times 60}{8} \times \frac{2\pi}{60}}$$

$$T_d = \underline{2334.5935 \text{ N-m}}$$

* In this problem, Power developed cannot be evaluated by $\frac{3E_a V_t}{X_s} \sin \delta$ as this is valid only when $R_a = 0$. ☺

(10)

Ans 4(B) 208 V, 60 Hz, 3Ø, Y connected
 Salient pole synchronous generator
 full load \rightarrow 40 A and $\text{pf} = 0.8$ lead.

$$X_d = 2.7 \Omega \quad X_q = 1.7 \Omega$$

R_a negligible and $P_r = 5\%$ of power developed.

$$\tilde{V}_t = \frac{208}{\sqrt{3}} \angle 0^\circ = 120.088 \angle 0^\circ$$

$$\tilde{V}_t - j \tilde{I}_d X_d - j \tilde{I}_q X_q = \tilde{E}_a$$

$$\tilde{V}_t - j \tilde{I}_d X_d - j X_q (\tilde{I}_a - \tilde{I}_d) = \tilde{E}_a$$

$$\tilde{V}_t - j \tilde{I}_d (X_d - X_q) - j \tilde{I}_a X_q = \tilde{E}_a$$

$$\Rightarrow \tilde{V}_t - j \tilde{I}_a X_q = \tilde{E}_a + j \tilde{I}_d (X_d - X_q)$$

$$= \tilde{E}'_a$$

\rightarrow Calculation of δ .

δ is angle of \tilde{E}'_a also.

$$\Rightarrow \tilde{V}_t - j \tilde{I}_a X_q = 120.088 \angle 0^\circ$$

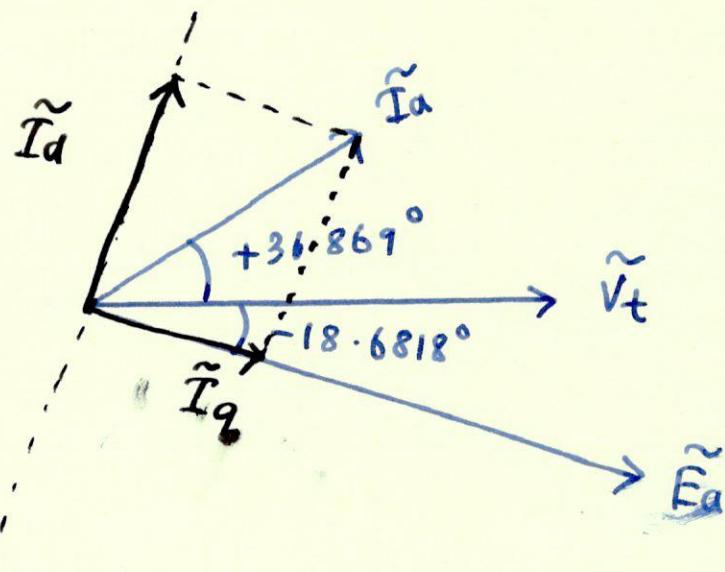
$$- j 40 \angle 36.869^\circ (1.7)$$

$$= 169.83552 \angle -18.6818^\circ$$

$$\Rightarrow \delta = -18.6818^\circ$$

(11)

torque angle = $\delta = 18.6818^\circ -$



$$\begin{aligned}\tilde{I}_q &= 40 \cos(36.869 + 18.6818) \angle -18.6818^\circ \\ &= 40 \cos(55.5508) \angle -18.6818^\circ \\ &= 22.627 \angle -18.6818^\circ\end{aligned}$$

$$\begin{aligned}\tilde{I}_d &= 40 \sin(55.5508) \angle 90^\circ - 18.6818^\circ \\ &= 32.9851 \angle 71.3182^\circ\end{aligned}$$

$$\begin{aligned}\tilde{E}_a &= \tilde{V}_t - j \tilde{I}_d X_d - j \tilde{I}_q X_q \\ &= 120.088 - j(2.7) 32.9851 \angle 71.3182^\circ \\ &\quad - j(1.7) 22.627 \angle -18.6818^\circ\end{aligned}$$

$$\boxed{\tilde{E}_a = 202.82 \angle -18.6818^\circ} \quad (12)$$

$$P_{in} = 3 V_t I_a \cos \phi = 3 \times 120.088 \times 40 \times 0.8 \\ = 11528.448 = P_d \text{ (as no Ra)}$$

$$P_{synch} = \frac{3 E_a V_t \sin \delta}{X_d} = \frac{3 (202.82)(120.088)}{2.7} \sin(18.68^\circ)$$

$$\underline{P_{synch}} = 8668.445366 \text{ W}$$

$$P_{\text{solvent}} = P_d - P_{\text{synch}}$$

$$\underline{P_{\text{solvent}} = 2860 \cdot 002634 \text{ W.}}$$

Ans 5(A) (i) 208 V, Y connected, 3Ø, Sync Motor
Takes 7.2 kW at 0.8 pf lead.

$$X_s = 4 \Omega \quad R_a \approx 0$$

$$3 V_t I_a \cos \phi = 7200$$

$$I_a = \frac{7200}{3 \times \frac{208}{\sqrt{3}} \times 0.8} = 24.9815 \text{ A.}$$

$$\text{as } R_a \approx 0 \quad P_{\text{in}} = P_d = -3 \frac{E_a V_t}{X_s} \sin \delta.$$

$$\tilde{V}_t - j \tilde{I}_a X_s = \tilde{E}_a$$

$$\begin{aligned} \Rightarrow \tilde{E}_a &= \frac{208}{\sqrt{3}} \angle 0^\circ - j 24.9815 \frac{\angle 36.869^\circ}{4} \\ &= 120.088 - (4j)(24.9815 \angle 36.869^\circ) \\ &= 196.9922 \angle -23.942^\circ \end{aligned}$$

$$E_a' = \frac{196.9922}{2} = 98.4961$$

as the load on the motor is same hence P_d also must be same = 7200 W.

(13)

$$\Rightarrow -3 \frac{E_a' V_t}{X_s} \sin \delta' = 7200$$

$$\Rightarrow \sin \delta' = -0.8116$$

$$\Rightarrow \delta' = -54.2544^\circ.$$

\Rightarrow New torque angle = 54.2544° .

$$\tilde{E}_a' = 98.4961 \angle -54.2544^\circ$$

$$\tilde{I}_a = \frac{\tilde{V}_t - \tilde{E}_a}{j X_s}$$

$$= \frac{120.088 \angle 0^\circ - 98.4961 \angle -54.2544}{4 \angle 90^\circ}$$

$$= 25.37572 \angle -38.04^\circ$$

New armature current = 25.37572

at PF of $\cos(38.04) = 0.78758$ (lag)

$$(ii) 3 V_t I_a'' \cos \phi'' = 7200$$

$$\therefore \cos \phi'' = 1$$

$$\Rightarrow I_a'' = \frac{7200}{3 V_t} = \frac{7200}{3 \times 120.088} = 19.9853 \text{ A}$$

at UPF.

$$\tilde{E}_a = \tilde{V}_t - j \tilde{I}_a X_s$$

$$= 120.088 \angle 0^\circ - j 4 \times (19.9853 \angle 0^\circ) \quad (14)$$

$$= 144.2626 \angle -33.65124$$

New torque angle = 33.65124 new PF = unity

New armature current = 19.9853 A

Ans 5(B) Power developed by a salient pole synchronous motor can be expressed as

$$P_d = \underbrace{\left(\frac{3 V_t}{X_d} \right) \underbrace{E_a}_{A} \sin \delta + \left(\frac{3 V_t^2}{2} \right) \underbrace{\left(\frac{X_d - X_a}{X_d X_a} \right)}_{B} \sin 2\delta}$$

When connected to infinite bus, V_t is constant

Also, as the motor is delivering constant power output $\Rightarrow P_d = \text{constant } \{ \text{Neglecting } R_a \}$

$$P_d = \text{constant} = A E_a \sin \delta + B \sin 2\delta$$

$E_a \rightarrow \text{independent variable} \rightarrow X$

$\delta \rightarrow \text{dependent variable} \rightarrow Y$

$$\Rightarrow A X \sin Y + B \sin 2Y = \text{constant}$$

Differentiating wrt X we get

$$A \left(\sin Y + X \cos Y \frac{dY}{dX} \right)$$

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$$+ B \left(2 \cos 2Y \frac{dY}{dX} \right) = 0$$

$$\Rightarrow \frac{dY}{dX} \left(A X \cos Y + 2 B \cos 2Y \right) = -A \sin Y$$

$$\Rightarrow \frac{dY}{dX} = \frac{-A \sin Y}{A X \cos Y + 2 B \cos 2Y}$$

replacing X, Y with the original variables

$$\frac{d\delta}{dE_a} = \frac{-A \sin \delta}{AE_a \cos \delta + 2B \cos^2 \delta}$$

$$A = \frac{3V_t}{X_d}; B = \frac{3}{2} V_t^2 \left(\frac{X_d - X_q}{X_d X_q} \right)$$



Above differential equation governs the steady state dynamics of torque angle/power angle with change in the excitation voltage for a synchronous m/c.

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