

(Kaliske, 1997)

- Initialize storage for previous time steps.

$$\text{DEV} \underline{\underline{S}}_0^n, \underbrace{\underline{\underline{H}}_1^n, \underline{\underline{H}}_2^n}_{\text{internal stress variables}}$$

↑
elastic stress

- Initialize material constants based on Abaqus per (Garimella, 2017).

$$g_1 = 0.65425, \quad g_2 = 0.0149$$

$$\tau_1 = 0.0066940, \quad \tau_2 = 0.15642$$

Note:

Set $K_1 = K_2 = 0$, so that Abaqus does not apply viscosity to hydrostatic stress.

- Convert material constants to Kaliske notation.

$$g_\infty + \sum_{i=1}^N g_i = 1 \rightarrow g_\infty = 1 - g_1 - g_2 \rightarrow \gamma_i = \frac{g_i}{g_\infty}$$

(Abaqus)

↓ Kaliske
↑ Abaqus

- Calculate elastic PK2 stress at current time $\underline{\underline{S}}_0^{n+1}$.

- Calculate $\underline{\underline{C}} = \underline{\underline{F}}^T \underline{\underline{F}}$ for current time.

- Calculate the deviatoric component of $\underline{\underline{S}}_0^{n+1}$ w.r.t. the reference configuration.

$$\text{DEV} \underline{\underline{S}}_0^{n+1} = 1 - \frac{1}{3} \left[\underline{\underline{C}} : \underline{\underline{S}}_0^{n+1} \right] \underline{\underline{C}}^{-1}$$

↑
 $\underline{\underline{C}} : \underline{\underline{S}}_0^{n+1} = \text{tr}(\underline{\underline{C}}^T \underline{\underline{S}}_0^{n+1}) = \text{tr}(\underline{\underline{C}} \underline{\underline{S}}_0^{n+1})$

- Calculate internal stress variables at current time $\underline{\underline{H}}_1^{n+1}$ and $\underline{\underline{H}}_2^{n+1}$.

$$\underline{\underline{H}}_j^{n+1} = \exp\left(-\frac{\Delta t}{\tau_j}\right) \underline{\underline{H}}_j^n + \gamma_j \frac{1 - \exp\left(-\frac{\Delta t}{\tau_j}\right)}{\frac{\Delta t}{\tau_j}} \left[\text{DEV} \underline{\underline{S}}_o^{n+1} - \text{DEV} \underline{\underline{S}}_o^n \right]$$

\downarrow current time step from n to $n+1$
 \uparrow previous time step from storage.
 \uparrow previous time step from storage.

- Calculate the modified deviatoric PK2 stress $\text{DEV} \underline{\underline{S}}^{n+1}$.

$$\text{DEV} \underline{\underline{S}}^{n+1} = \text{DEV} \underline{\underline{S}}_o^{n+1} + \sum_{j=1}^N \underline{\underline{H}}_j^{n+1}$$

- Transform the modified deviatoric PK2 stress $\text{DEV} \underline{\underline{S}}^{n+1}$ to the modified deviatoric Kirchhoff stress $\text{dev} \underline{\underline{\tau}}^{n+1}$.

$$\text{dev} \underline{\underline{\tau}}^{n+1} = \underline{\underline{F}}^{n+1} \text{DEV} \underline{\underline{S}}^{n+1} (\underline{\underline{F}}^{n+1})^T$$

- Calculate the total Kirchhoff stress $\underline{\underline{\tau}}^{n+1}$.

$$\underline{\underline{\tau}} = J^{n+1} U'^{n+1} \underline{\underline{I}} + \text{dev} \underline{\underline{\tau}}^{n+1}$$

where

$$U' = \frac{\partial U}{\partial J} \quad \hat{U}(J) \text{ volumetric strain energy function}$$

Note:

$$\text{Mooney-Rivlin: } W = C_{10} (\bar{I}_1 - 3) + C_{01} (\bar{I}_2 - 3) + \underbrace{\frac{1}{D_1} (J-1)^2}_{\hat{U}(J)}$$

$$\text{Ogden (N=1): } W = \frac{2\mu_1}{\alpha_1^2} \left[\bar{\lambda}_1^{\alpha_1} + \bar{\lambda}_2^{\alpha_1} + \bar{\lambda}_3^{\alpha_1} - 3 \right] + \underbrace{\frac{1}{D_1} (J-1)^2}_{\hat{U}(J)}$$

In both cases

$$U' = \frac{2}{D_1} (J-1)$$

Note: (Gurtin)

$\underline{\underline{T}}$: Cauchy stress (i.e. $\underline{\underline{\sigma}}$)

$$\underline{\underline{\sigma}} = \frac{1}{J} \underline{\underline{F}} \underline{\underline{S}} \underline{\underline{F}}^T \quad (25.10)$$

$\underline{\underline{T}}_R$: Piola Stress (i.e. $\underline{\underline{P}}$)

$$\underline{\underline{P}} = J \underline{\underline{\sigma}} \underline{\underline{F}}^{-T} \quad (24.1)$$

$\underline{\underline{T}}_{RR}$: Second Piola Stress (i.e. $\underline{\underline{S}}$)

$$\underline{\underline{S}} = \underline{\underline{F}}^{-1} \underline{\underline{P}} \quad (25.2)$$

$\underline{\underline{T}}_K$: Kirchhoff stress (i.e. $\underline{\underline{\tau}}$)

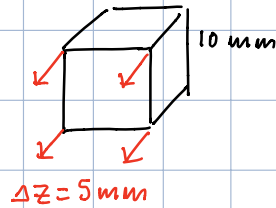
$$\underline{\underline{\tau}} = J \underline{\underline{\sigma}} \quad \text{pg. 329}$$

$$\underline{\underline{\sigma}} = \frac{1}{J} \underline{\underline{\tau}}$$

$$\underline{\underline{S}} = \underline{\underline{F}}^{-1} \underline{\underline{P}} = \underline{\underline{F}}^{-1} (J \underline{\underline{\sigma}} \underline{\underline{F}}^{-T}) = \underline{\underline{F}}^{-1} J \left(\frac{1}{J} \underline{\underline{\tau}} \right) \underline{\underline{F}}^{-T}$$

$$\underline{\underline{S}} = \underline{\underline{F}}^{-1} \underline{\underline{\tau}} \underline{\underline{F}}^{-T}$$

Test Problem - tension



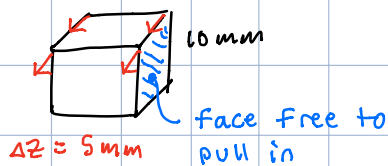
- Mooney-Rivlin.
- double precision for ABAQUS

	σ_{xx}		σ_{zz}		R_{tot}	
Δt	EEMA	ABAQUS	EEMA	ABAQUS	EEMA	ABAQUS
0.001	-2,776.26	-2,892.54	34,651.2	34,535	2.28537	2.302516
0.010	-27.838	-28.9317	24,207.3	24,206.2	1.61367	1.613756
0.100	-0.285623	-0.29577	14241.7	14,241.7	0.949451	0.949452
1.000	-0.003628	-0.00364687	13,299.5	13,299.5	0.886638	0.886636
10.000	-0.000114	-0.000105816	13,207.7	13,207.7	0.880518	0.880516
20.000	-0.000050	-0.0000462	13,203.2	13,203.2	0.880213	0.880212

$$\epsilon = \frac{\delta}{L} = \frac{5 \text{ mm}}{10 \text{ mm}} \rightarrow \epsilon = 0.5$$

$$\dot{\epsilon} = \frac{\Delta \epsilon}{\Delta t}$$

Test Problem - shear



- Mooney-Rivlin.
- double precision for ABAQUS

viscoelasticity = OFF

	τ_{yz}		σ'_{yy}		σ'_{zz}	
Δt	EEMA	ABAQUS	EEMA	ABAQUS	EEMA	ABAQUS
0.010	6769.0006	6769	-3901.3408	-3901.4	-516.8405	-516.9
0.100	6769.0006	6769	-3901.4686	-3901.48	-516.9683	-516.974

viscoelasticity = ON

	τ_{yz}		σ'_{yy}		σ'_{zz}	
Δt	EEMA	ABAQUS	EEMA	ABAQUS	EEMA	ABAQUS
0.001	19,534.8183	19,534.8	-11,417.3209	-11,418.9	-1,813.3466	-1,814.97
0.010	14,185.0155	14,185	-9,040.1743	-9,040.25	-2,840.1971	-2,840.27
0.100	8,014.5600	8,014.56	-5,008.7737	-5,008.78	-1,456.1534	-1,456.16