EE140 Introduction to Communication Systems

Lecture 7

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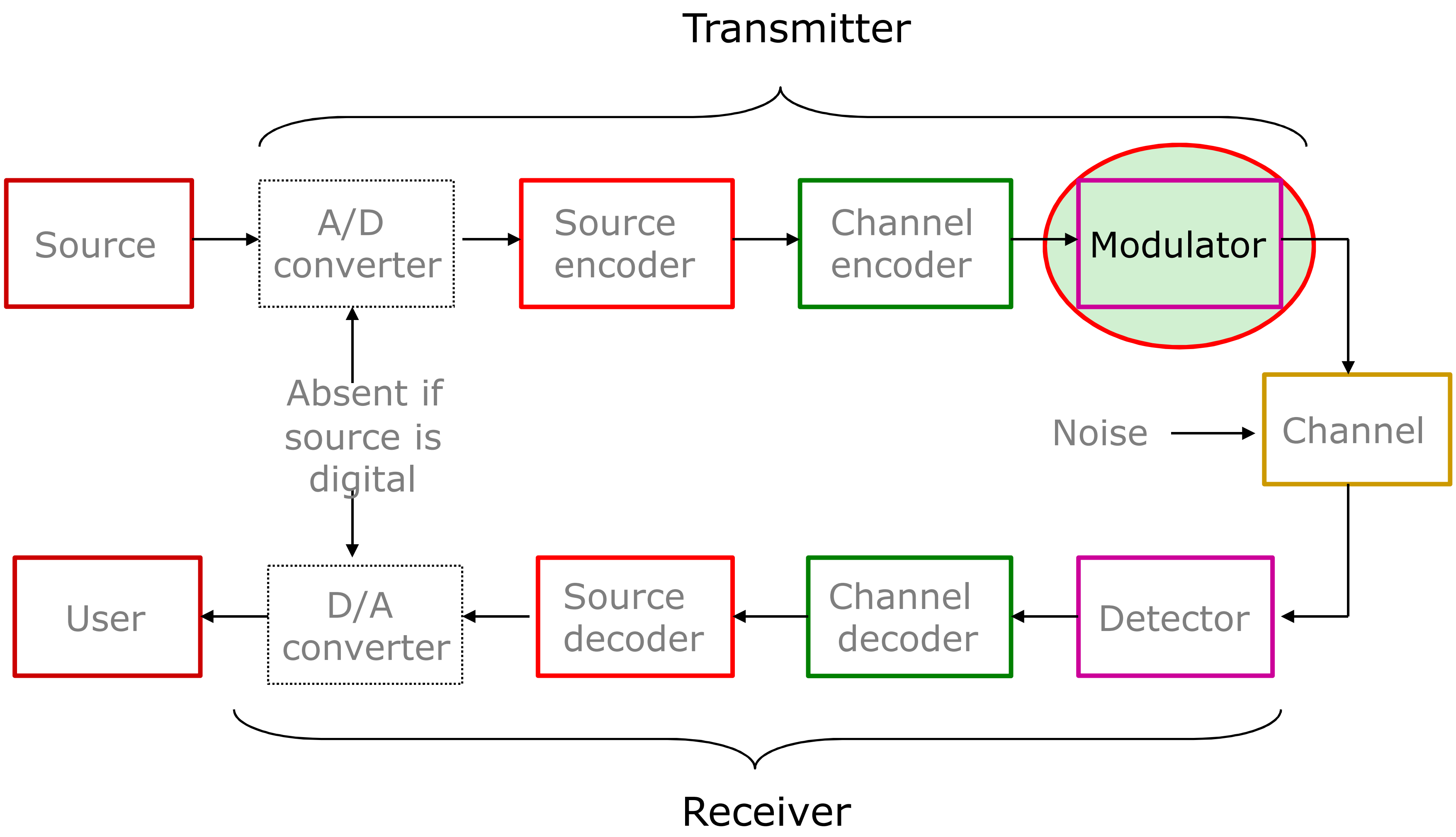
ShanghaiTech University, Fall 2022

Architecture of a (Digital) Communication System



Contents

- Analog Modulation
  - Amplitude modulation
  - Pulse modulation
  - Angle modulation (phase/frequency)

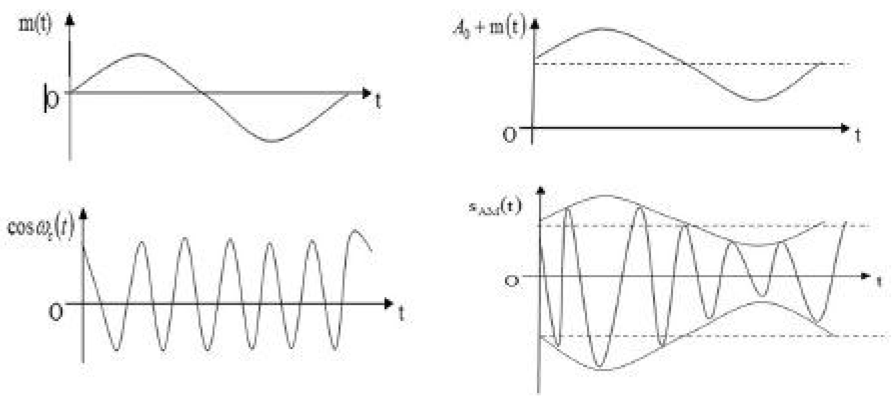
Analog Modulation

- Characteristics that can be modified in the carrier

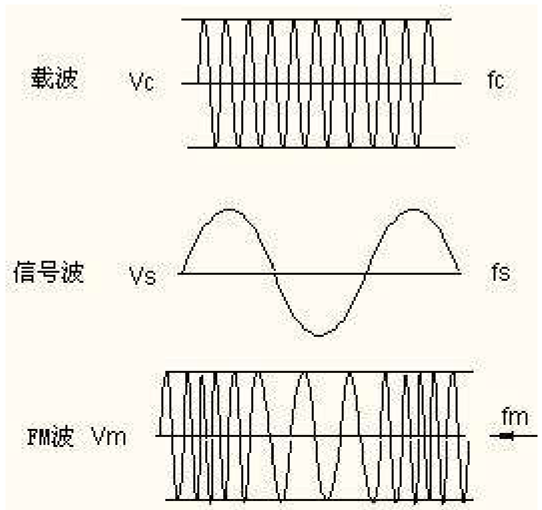
$$C(t) = A(t)\cos(2\pi f(t)t + \theta(t))$$

  - Amplitude $\Rightarrow$ Amplitude modulation
  - Frequency
  - Phase

  $\left.\begin{array}{l}\text{Frequency}\\ \text{Phase}\end{array}\right\} \Rightarrow$ Angle modulation



AM



PM

Angle Modulation

- Either phase or frequency of the carrier is varied according to the message signal
- General form

$c(t) = A_c \cos(2\pi f_c t)$

$$x_c(t) = A_c \cos[2\pi f_c t + \phi(t)]$$

– Instantaneous phase

$$\theta_i(t) = 2\pi f_c t + \phi(t)$$

phase deviation

– Instantaneous frequency

$$\omega(t) = \frac{d\theta_i(t)}{dt} = \omega_c + \frac{d\phi(t)}{dt}$$

frequency deviation

$$f(t) = \frac{1}{2\pi}\frac{d\theta_i(t)}{dt} = f_c + \frac{1}{2\pi}\frac{d\phi(t)}{dt}$$

PM and FM

- Phase modulation

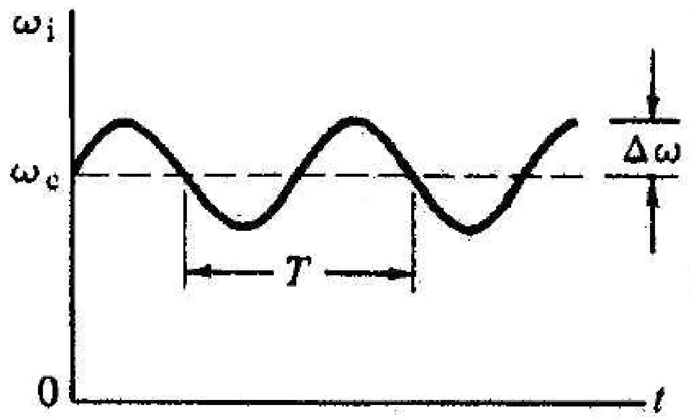
$\phi(t) = k_p m(t)$, where k_p is phase deviation constant（调相灵敏度)

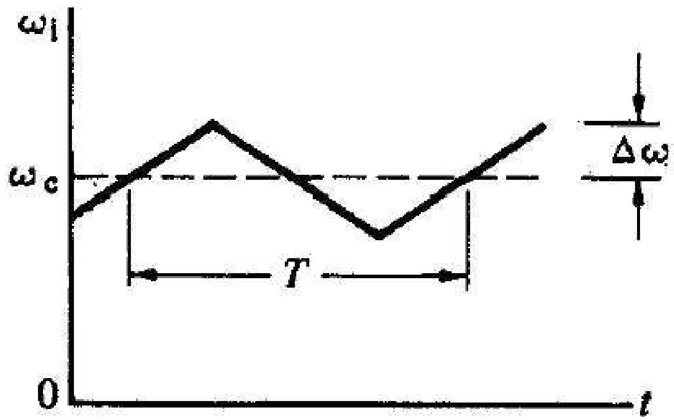
  – Overall output $x_c(t) = A_c \cos[\,2\pi f_c t + k_p m(t)]$

- Frequency modulation

$\frac{d\phi(t)}{dt} = k_f m(t) = 2\pi f_d m(t)$, where f_d is frequency deviation constant (调频灵敏度)

  – Overall output $x_c(t) = A_c \cos[\,2\pi f_c t + 2\pi f_d \int_0^t m(\tau)d\tau + \phi_0]$





	$x(t)$	FD	PD
FM			
PM			

Example

FD	PD
$f_d\, m(t)$	$2\pi f_d \int^t m(\tau)\,d\tau$
$\frac{k_p}{2\pi}\frac{d\,m(t)}{dt}$	$k_p\, m(t)$

FM $\quad x_c(t) = A_c \cos\left(2\pi f_c t + 2\pi f_d \int^t m(\tau)\,d\tau\right)$

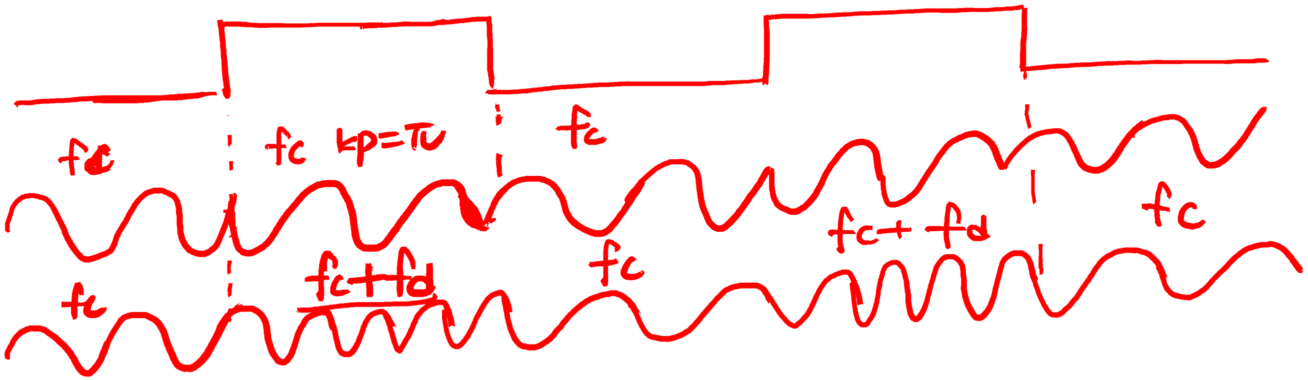
PM $\quad x_c(t) = A_c \cos\left(2\pi f_c t + k_p m(t)\right)$

Example 1.

m(t)

PM:

FM



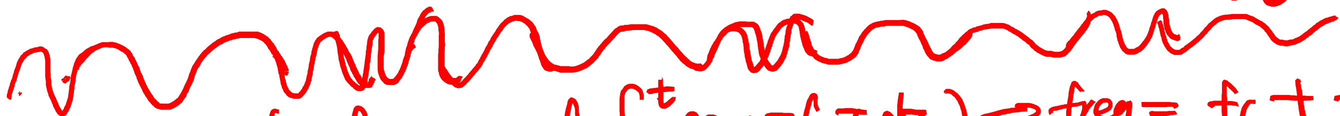
fc is constant
phase Discont.

f is Discont.
phase is cont.

Example 2.

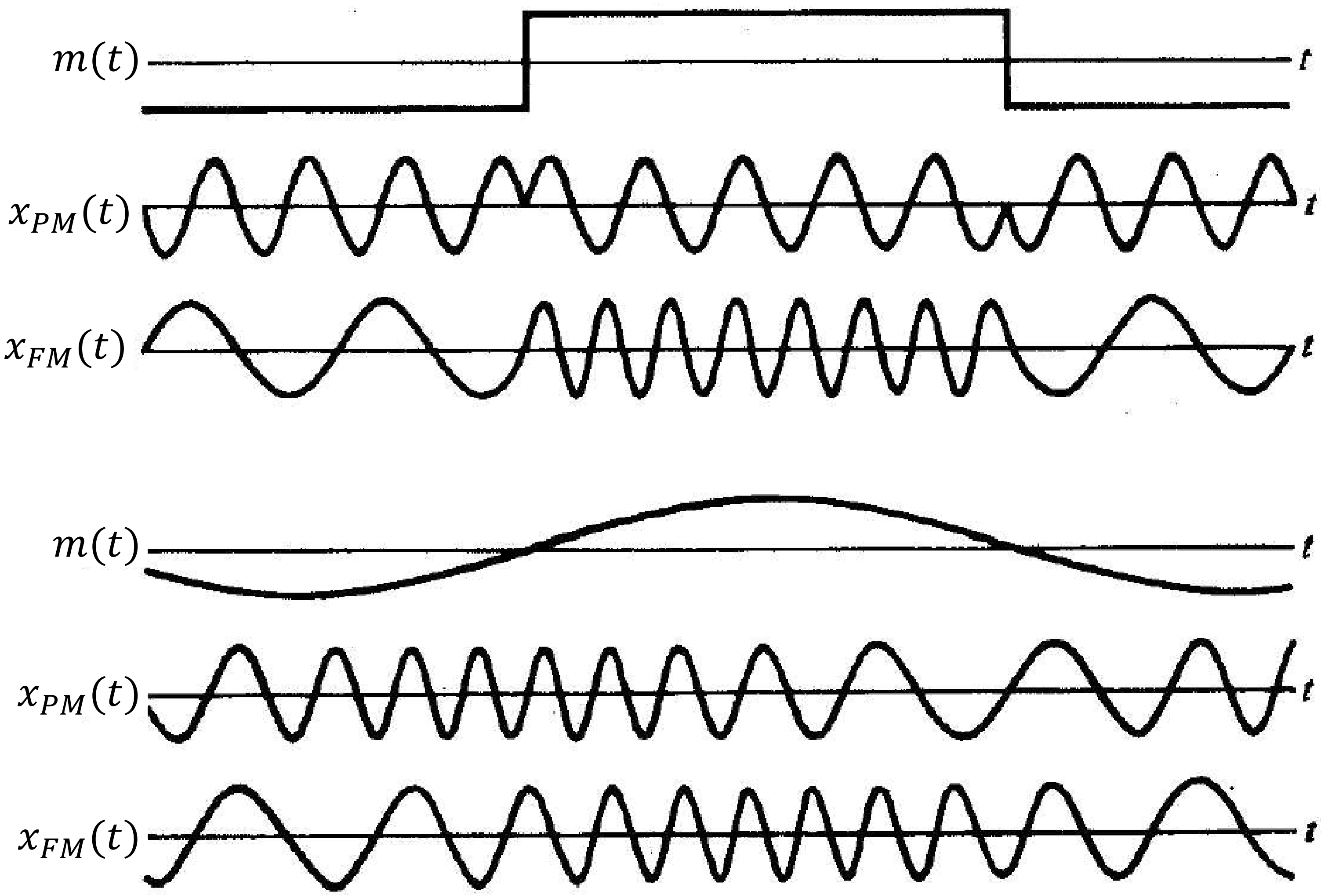
$m(t) = \cos(2\pi f_m t)$

PM $\quad x_c(t) = A\cos(2\pi f_c t + k_p \cos 2\pi f_m t) \Rightarrow \text{freq.} = f_c + k_p \frac{d \cos 2\pi f_m t}{dt}$

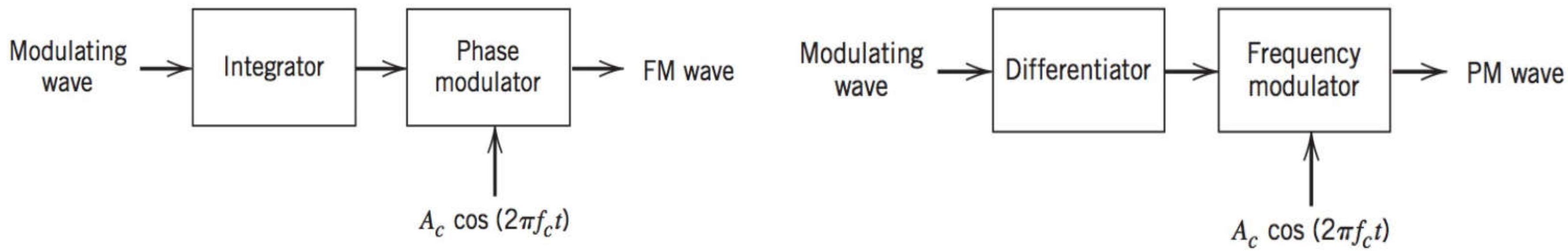


FM $\quad x_c(t) = A_c \cos\left(2\pi f_c t + 2\pi f_d \int^t \cos 2\pi f_m \tau\, d\tau\right) \Rightarrow \text{freq} = f_c + f_d \cos 2\pi f_m t$

PM and FM: Graphic Interpretation



FM and PM



- Transform between FM and PM
  - FM: PM with the modulation wave $\int_0^t m(\tau)d\tau$.
  - PM: FM with the modulation wave $\frac{dm(t)}{dt}$.
  - Deduce the property of PM from FM.
  - We concentrate on FM signal.

FM and PM

- Amplitude modulation (AM) is linear
  - $x_c(t) = (A_c + m\ (t)) \cos 2\, \pi f_c t$

$$\Downarrow$$

$$\frac{dx_c(t)}{dm(t)} \text{ is independent of } m(t)$$

- Angle modulation (PM and FM) is nonlinear

$$x_c(t) = A_c \cos[2\pi f_c t + \phi(t)] = \text{Re}\left\{A_c e^{j2\pi f_c t}\, e^{j\phi(t)}\right\}$$
$$= \text{Re}\left\{A_c e^{j2\pi f_c t}\left[1 + j\phi(t) - \frac{1}{2!}\phi^2(t) - j\frac{1}{3!}\phi^3(t) + \ \cdots\right]\right\}$$
$$= A_c\left[\cos(2\pi f_c t) - \phi(t)\sin(2\pi f_c t) - \underline{\frac{\phi^2(t)}{2!}\cos(2\pi f_c t) + \frac{\phi^3(t)}{3!}\sin(2\pi f_c t) + } \cdots\right]$$

“Linear” Angle Modulation

- Nonlinear angle modulation: the sidebands arising in angle modulation do not obey the principle of superposition.

- However, if $|\phi(t)| << 1$, the high-order terms in $x_c(t)$ can be ignored

$$x_c(t) \approx A_c\,[\cos(2\pi f_c t) - \phi(t)\sin(2\pi f_c t)]$$

$\Downarrow$

Approximately linear!

$\Downarrow$

Narrowband Angle Modulation

Narrowband FM (NBFM)

- FM– sinusoidal modulating signal

$$x_c(t) = A_c \cos[\,2\pi f_c t + k_f \int_0^t m(\tau)d\tau + \phi_0]$$

- Given $m(t) = A_m \cos 2\,\pi f_m t$ and $\phi_0 = 0$

$$\phi(t) = k_f \int_0^t m(\tau)d\tau = \frac{A_m k_f}{2\pi f_m} \sin 2\,\pi f_m t$$

$$= \frac{A_m f_d}{f_m} \sin 2\,\pi f_m t = \frac{\Delta f}{f_m} \sin 2\,\pi f_m t = \beta \sin 2\,\pi f_m t$$

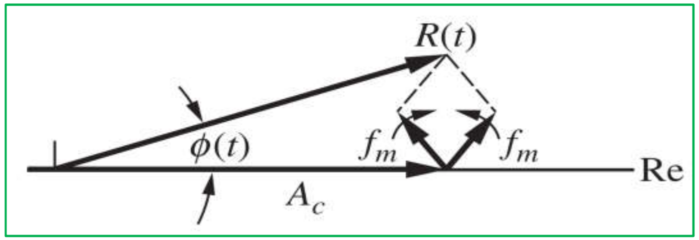
  - Where $\Delta f = A_m f_d$ is the peak frequency deviation, and $\beta = \frac{A_m f_d}{f_m}$ is the modulation index.

- FM signal $x_c(t) = A_c \cos[\,2\pi f_c t + \beta \sin 2\,\pi f_m t]$
  - Narrowband FM (NBFM): $0 < \beta \ll 1$ (small β)
  - Wideband FM (WBFM): $\beta \gg 1$ (large β)

NBFM (Cont'd)

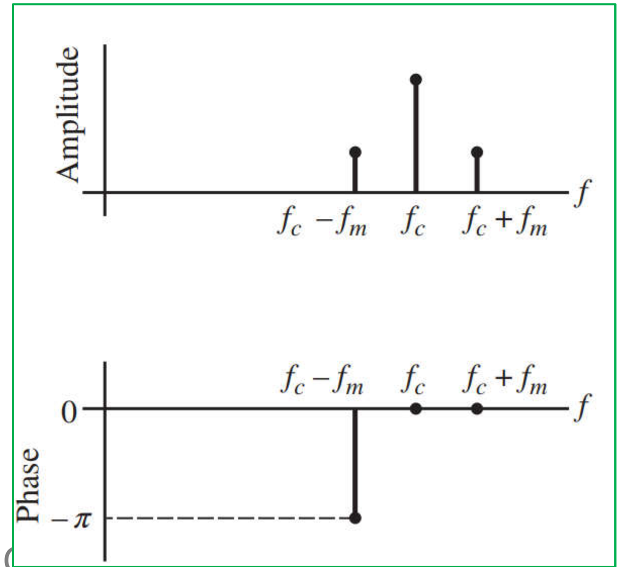
- If $0 < \beta << 1$ (i.e. $|\phi(t)| << 1$), the narrowband FM signal is given by

$$x_c(t) = A_c \cos[2\pi f_c t + \beta \sin 2\pi f_m t]$$
$$\approx A_c \cos 2\pi f_c t - A_c \beta \sin 2\pi f_m t \sin 2\pi f_c t$$
$$= A_c \cos 2\pi f_c t + \frac{1}{2} A_c \beta \{\cos[2\pi(f_c + f_m)t] - \cos[2\pi(f_c - f_m)t]\}$$
$$= A_c \mathrm{Re}\left\{e^{j2\pi f_c t}\left(1 + \frac{\beta}{2}e^{j2\pi f_m t} - \frac{\beta}{2}e^{-j2\pi f_m t}\right)\right\}$$



Phasor diagram

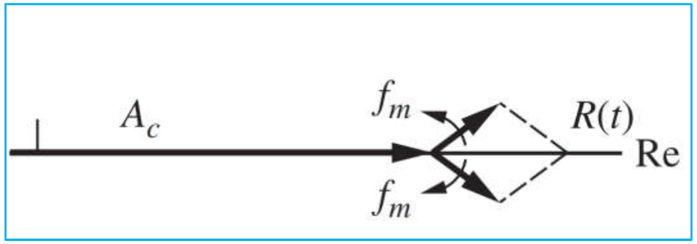
Spectrum



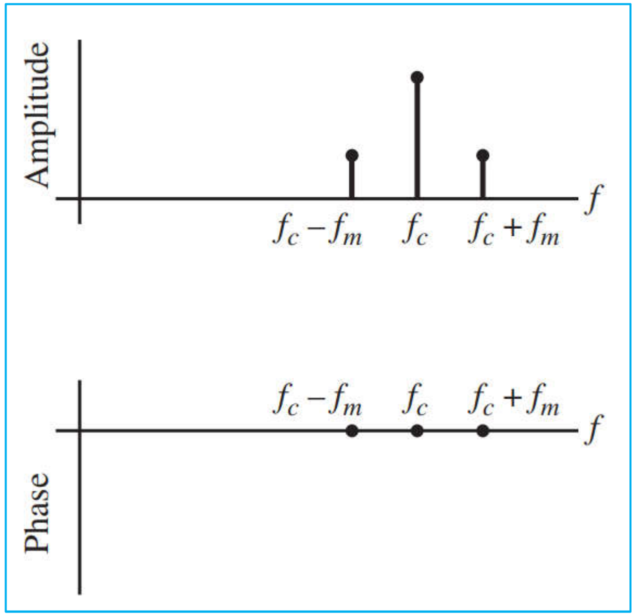
NBFM (Cont'd)

- Compared with DSB-LC (AM)

$$
\begin{aligned}
x_c(t) &= A_c(1 + a\cos 2\pi f_m t)\cos 2\pi f_c t \\
&= A_c \cos 2\pi f_c t + A_c a\cos 2\pi f_m t \cos 2\pi f_c t \\
&= A_c \cos 2\pi f_c t + \frac{1}{2} A_c a\{\cos[2\pi(f_c+f_m)t] + \cos[2\pi(f_c-f_m)t]\} \\
&= \mathrm{Re}\left\{A_c e^{j2\pi f_c t}\left(1 + \frac{a}{2}e^{j2\pi f_m t} + \frac{a}{2}e^{-j2\pi f_m t}\right)\right\}
\end{aligned}
$$



Phasor diagram



Spectrum

Comparison between NBFM & AM
1. Same transmission bandwidth (B=2fm)
2. NBFM: diff phase with carrier, approximately same amplitude
3. AM: same phase, different amplitude

Narrowband PM (NBPM)

- PM– sinusoidal modulating signal

$$x_c(t) = A_c \cos[2\pi f_c t + k_p m(t)]$$

- Given $m(t) = A_m \cos 2\pi f_m t$ and $\phi_0 = 0$

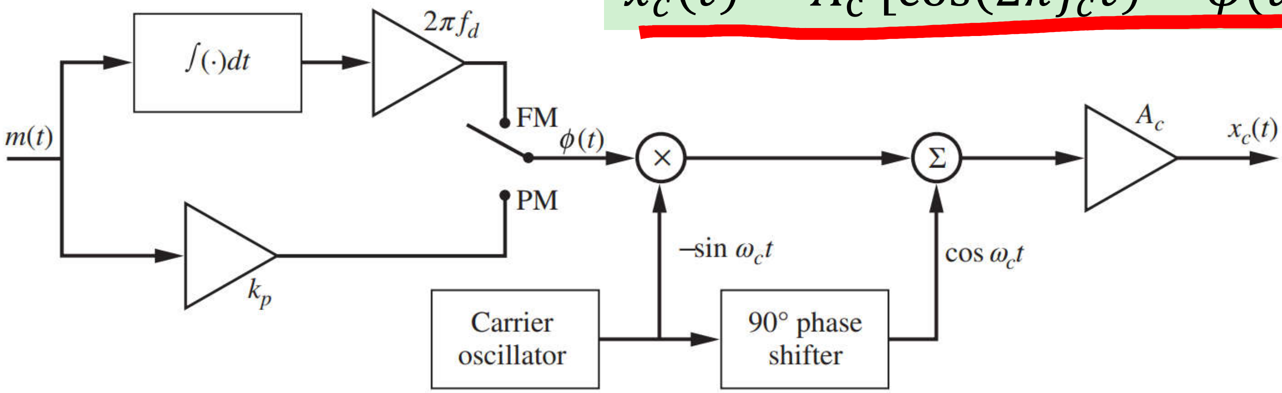
$$\phi(t) = k_p A_m \cos 2\pi f_m t = \beta \cos 2\pi f_m t$$

  - $\beta = k_p A_m$ is the modulation index.
- PM signal $x_c(t) = A_c \cos[2\pi f_c t + \beta \cos 2\pi f_m t]$
  - Narrowband PM (NBPM): $0 < \beta \ll 1$ (small β)
  - Wideband PM (WBPM): $\beta \gg 1$ (large β)

Narrowband Angle Modulation

- If $0 < \beta << 1$, $x_c(t)$ is approximately linear.
- DSB-LC(AM), NBPM and NBFM are examples of linear modulation.
- If the modulating signal bandwidth is f_m, the narrowband angle-modulated signal will have a bandwidth of $2f_m$.
- Generation of Narrowband angle modulation

$$x_c(t) = A_c\,[\cos(2\pi f_c t) - \phi(t)\sin(2\pi f_c t)]$$



Wideband FM

- If modulation index is NOT small, the spectral density of a general angle-modulated signal cannot be obtained by Fourier transform.

$$x_c(t) = A_c \cos[\,2\pi f_c t + 2\pi f_d \int_0^t m(\tau)d\tau + \phi_0]$$

- Wideband FM: given $m(t) = A_m \cos 2\,\pi f_m t$ and $\phi_0 = 0$

$$x_c(t) = A_c \cos\left[2\pi f_c t + \frac{A_m f_d}{f_m} \sin 2\,\pi f_m t\right] = A_c \cos[2\pi f_c t + \beta \sin 2\,\pi f_m t]$$

$$= \mathrm{Re}\left\{A_c e^{j2\pi f_c t} \underline{e^{j\beta \sin 2\pi f_m t}}\right\}$$

  - Modulation index

$$\beta = \frac{\Delta f}{f_m} = \frac{f_d A_m}{f_m}$$

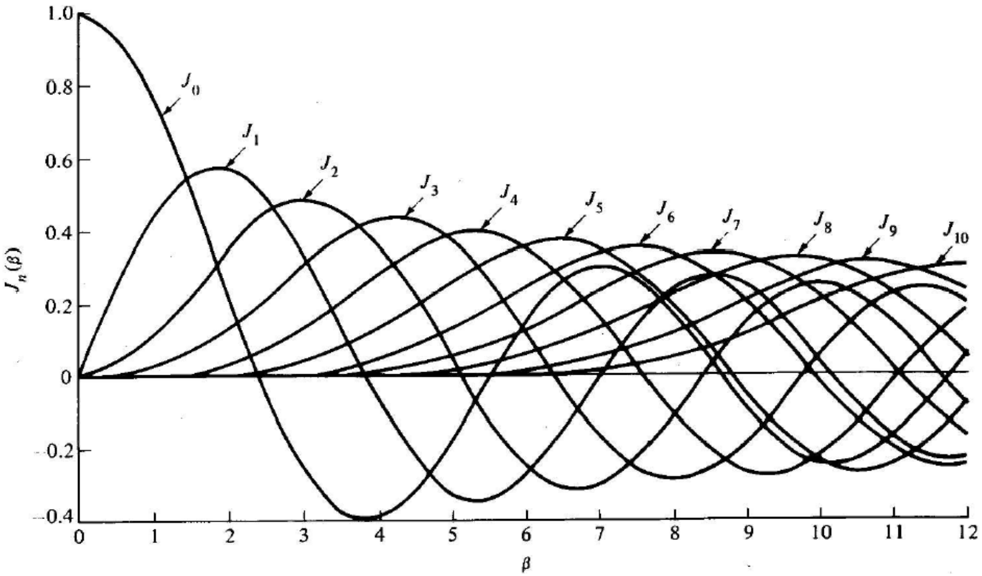
Wideband FM

- $e^{j\beta \sin 2\pi f_m t}$ is a periodic function of time with a fundamental frequency of f_m. Its Fourier series representation is

$$e^{j\beta \sin 2\pi f_m t} = \sum_{n=-\infty}^{\infty} F_n \, e^{j2\pi n \omega_m t}, \quad \text{where } F_n = \frac{1}{T}\int_{-T/2}^{T/2} e^{j\beta \sin 2\pi f_m t} e^{-j2\pi n f_m t} dt$$

  - Fourier coefficients: Bessel functions of the first kind

$$F_n = J_n(\beta)$$



Wideband FM

- $e^{j\beta \sin 2\pi f_m t} = \sum_{n=-\infty}^{\infty} F_n\, e^{j2\pi n\omega_m t} = \sum_{n=-\infty}^{\infty} J_n(\beta) e^{j2\pi n\omega_m t}$
- Modulated signal

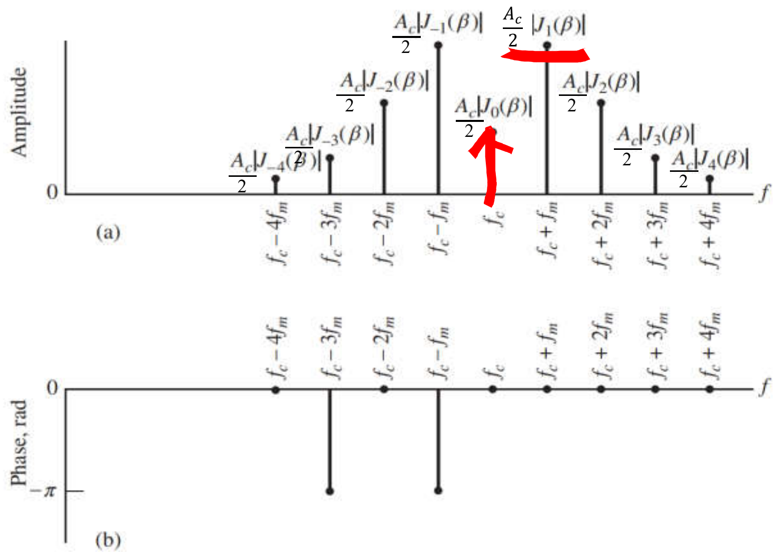
$$x_c(t) = A_c \cos[2\pi f_c t + \beta \sin 2\,\pi f_m t] = \mathrm{Re}\{A_c e^{j2\pi f_c t} e^{j\beta \sin 2\pi f_m t}\}$$
$$= \mathrm{Re}\{(A_c \sum_{n=-\infty}^{\infty} J_n(\beta) e^{j2\pi n\omega_m t}) e^{j2\pi f_c t}\}$$
$$= A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos[2\pi(f_c + n f_m)t]$$

- Spectrum

$$X_c(f) = \frac{A_c}{2} \sum_{n=-\infty}^{\infty} J_n(\beta)\, [\delta(f - f_c - n f_m) + \delta(f + f_c + n f_m)]$$

  - n=0: carrier component with amplitude $\frac{A_c}{2} J_0(\beta)$
  - n=1,2,…: side frequencies with amplitude $\frac{A_c}{2} J_n(\beta)$

f_m



Wideband FM

- The spectrum of angle modulated signal
  - Properties of Bessel function $J_n(\beta)$
    - Even n: $J_n(\beta) = J_{-n}(\beta)$; odd n: $J_n(\beta) = -J_{-n}(\beta)$.
    - If $\beta \ll 1$: $J_0(\beta) \simeq 1; J_1(\beta) \simeq \frac{\beta}{2}$; $J_n(\beta) \simeq 0, n \geq 2$.
    - $\sum_{n=-\infty}^{\infty} J_n^2(\beta) = 1$.

$B = 2nf_m$

$\beta << 1 \quad n = 1$

$B >> 1 \quad n = \infty$

  - For $\beta \ll 1$: narrowband FM
  - Total Average Power

$$P = \frac{A_c^2}{2} \sum_{n=-\infty}^{\infty} J_n^2(\beta) = \frac{A_c^2}{2} = P_c$$

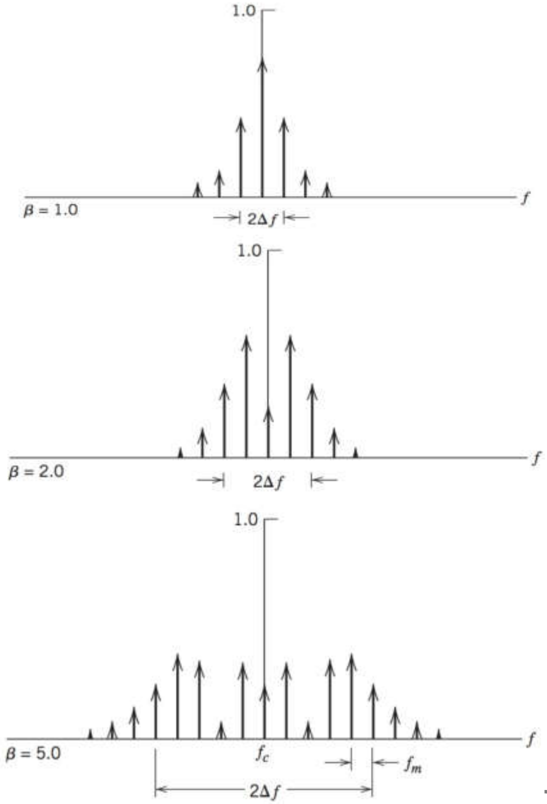
constant

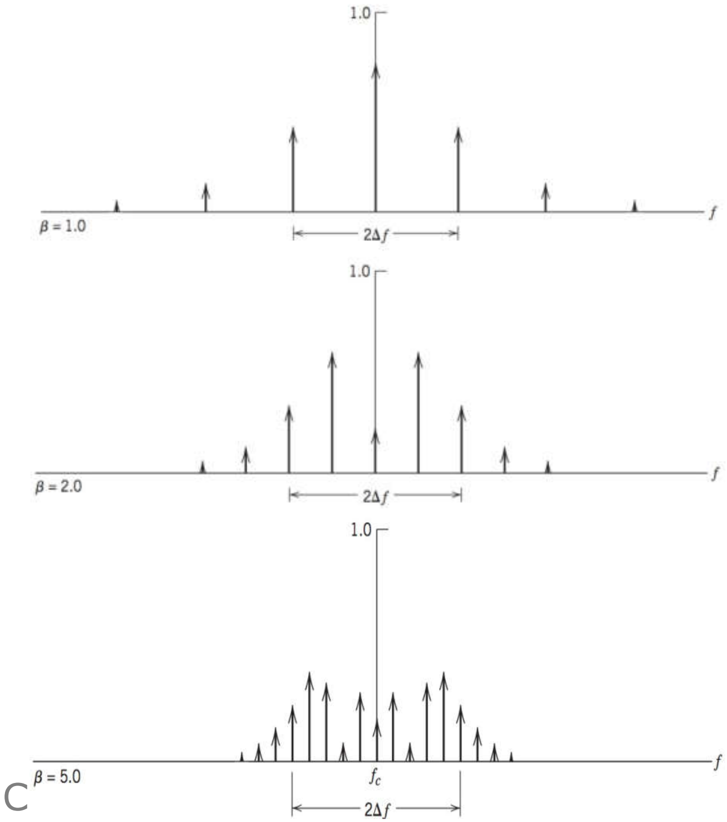
WBFM: Spectra of FM Signal

- Total average power in an FM signal is a constant.

$$\beta = \frac{A_m f_d}{f_m} = \frac{\Delta f}{f_m} \qquad m(t) = A_m \cos 2\pi f_m t$$

Case 1: Fix f_m, increase $A_m(\Delta f)$	Case 2: Fix $A_m(\Delta f)$, decrease f_m





WBFM: Bandwidth of FM Signals

- Bandwidth of FM signals, theoretically unlimited.

$$\boxed{\beta = \frac{\Delta f}{f_m}}$$

- Significant sideband $B = 2n\,f_m$
  - For large β: $J_n(\beta)$ diminish rapidly for $n > \beta$. Assume there are $n = \beta$ significant sidebands, $B = 2n\,f_m \approx 2\beta\,f_m = 2\,\Delta f$. (wideband FM)
  - For small β: only $J_0(\beta)$ and $J_1(\beta)$ have significant magnitude. Assume $n = 1$, $B \approx 2f_m$. (Narrowband FM)

β

- Carson's rule:

$$B \approx 2\,(\Delta f + f_m) = 2(1+\beta)\,f_m = 2(1+1/\beta)\,\Delta f$$

β Δf B

$m(t) = A_m \cos 2\pi f_m t$

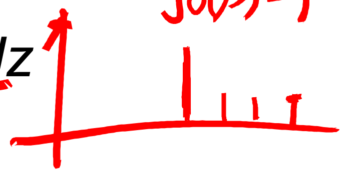
  - An approximation of the bandwidth.
- Arbitrary m(t)
  - Deviation Ratio: $D = \frac{f_d \max|m(t)|}{W}$, $B \approx 2\,(1+D)W$

Example

$f_c = 10 MHz$ $\Delta f = 50 kHz$

- A 10 MHz carrier is frequency-modulated by a sinusoidal signal such that the peak frequency deviation is 50 kHz. Determine the approximate bandwidth of the FM signal when modulating frequency is (a) 500 kHz; (b) 500 Hz; (c) 10 kHz.
- Solution: f_m''
  - (a) $\beta = \frac{\Delta f}{f_m} = \frac{50}{500} = 0.10 \ll 1 \rightarrow B \approx 2f_m = 1\ MHz$
    - Carson's rule gives: $B \approx 2f_m(1+\beta) = 1.1\ MHz$
  - (b) $\beta = \frac{\Delta f}{f_m} = \frac{50000}{500} = 100 \gg 1 \rightarrow B \approx 2\,\Delta f = 100\ kHz$

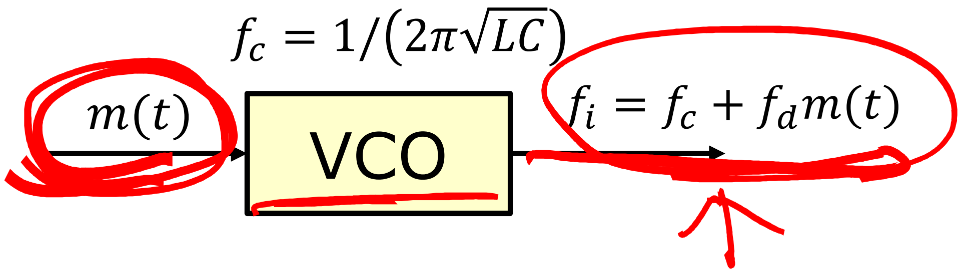
$J_0(\beta)=1$



    - Carson's rule gives: $B \approx 2f_m(1+\beta) = 101\ kHz$
  - (c) $\beta = 50/10 = 5$. Check Bessel function table(P163), we have 1% basis: $n = 8, J_8(5) = 0.018,$ $B \approx 2nf_m = 160\ kHz$
    - Carson's rule gives: $B \approx 2f_m(1+\beta) = 120\ kHz$

Generation of Wideband FM Signals

- Direct method: vary the carrier frequency directly with the modulating signal *m(t)* by using the voltage-controlled oscillator (VCO).

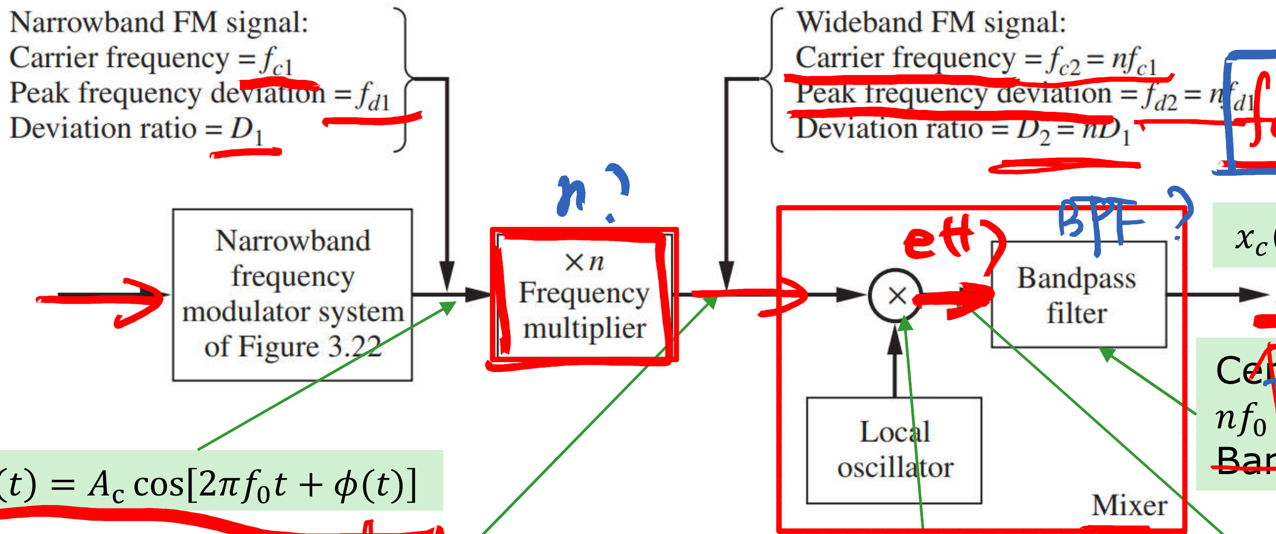


- Requirement of direct method:
  - The long-term frequency stability is not as good as the crystal-stabilized oscillators so that frequency stabilization is needed.
  - The percentage frequency deviation that can be attained in this method is quite small. (say $\beta < 0.2$ in theory)

Generation of Wideband FM Signals (Cont'd)

- Indirect method: Armstrong indirect FM transmitter
  - produce a narrowband FM signal.

$D = \frac{\Delta f}{W}$



$f_c = nf_0 - f_{LO}$

n?

e(t)

BPF?

$x_c(t) = A_c\cos[2\pi f_c t + n\phi(t)]$

Center frequency: $f_c = nf_0 + f_{LO}$ or $f_c = nf_0 - f_{LO}$

Bandwidth: Carson's rule

B

$nf_0 - f_{LO}$ $\quad$ $nf_0 + f_{LO}$

$x(t) = A_c\cos[2\pi f_0 t + \phi(t)]$

$y(t) = A_c\cos[2\pi n f_0 t + n\phi(t)]$

$e_{LO}(t) = 2\cos 2\pi f_{LO} t$

f_{LO} ?

$e(t) = 2A_c\cos[2\pi n f_c t + n\phi(t)]\cos 2\pi f_{LO} t$
$= A_c\cos[2\pi(nf_0 + f_{LO})t + n\phi(t)] + A_c\cos[2\pi(nf_0 - f_{LO})t + n\phi(t)]$

Frequency multiplier: increase modulation index
Mixer: control the value of the carrier frequency

D: ~~Example~~ → 5

f_c: 100kHz → 5M → 85 MHz

Example

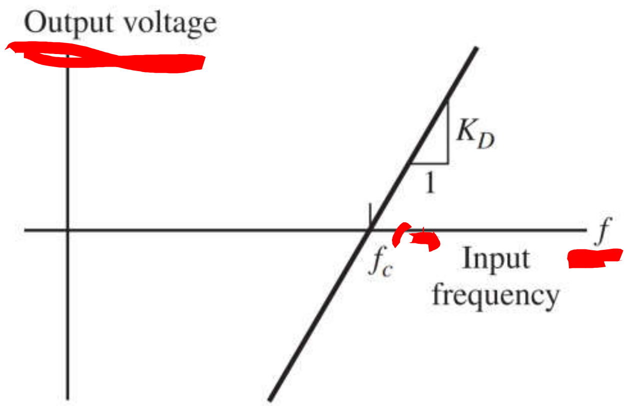
- A NB to WB converter, the output of the narrowband frequency modulator is given by $x(t) = A_c \cos[2\pi f_0 t + \phi(t)]$ with $f_0 = 100$ kHz. The peak frequency deviation is 50 Hz and the bandwidth of $\phi(t)$ is 500Hz. The wideband output $x_c(t)$ is to have a carrier frequency of 85 MHz and a deviation ratio of 5. In this example we determine the frequency multiplier factor n, two possible local oscillator frequencies and the center frequency and the bandwidth of the BP filter.

W = f_m

- Sol:
  - $D_1 = \frac{f_{d_1}}{W} = \frac{50}{500} = 0.1$, → $n = \frac{D_2}{D_1} = 50.$
  - $f_{c_2} = nf_{c_1} = 5$ MHz, $f_{LO} = f_c - f_{c_2} = 85 - 5 = 80$ MHz, or $f_{LO} = f_c + f_{c_2} = 85 + 5 = 90$ MHz.
  - The center frequency of the BP filter is 85 MHz, the bandwidth of the BP filter is $B = 2W(1 + D) = 2 * 500 * (1 + 5) = 6$ kHz.

Demodulation of Wideband FM Signals

- Demodulation: to provide an output signal whose amplitude is linearly proportional to the frequency deviation of the input FM signal.
- Direct method: use frequency discriminator
  - Frequency discriminator is the system that has a linear frequency-to-voltage transfer characteristic.



input $x_r(t) = A_c \cos[2\pi f_c t + 2\pi f_d \int_0^t m(\tau)\, d\tau + \phi_0]$

Frequency discriminator

output $y_D(t) = K_D f_d m(t)$

K_D: discriminator constant

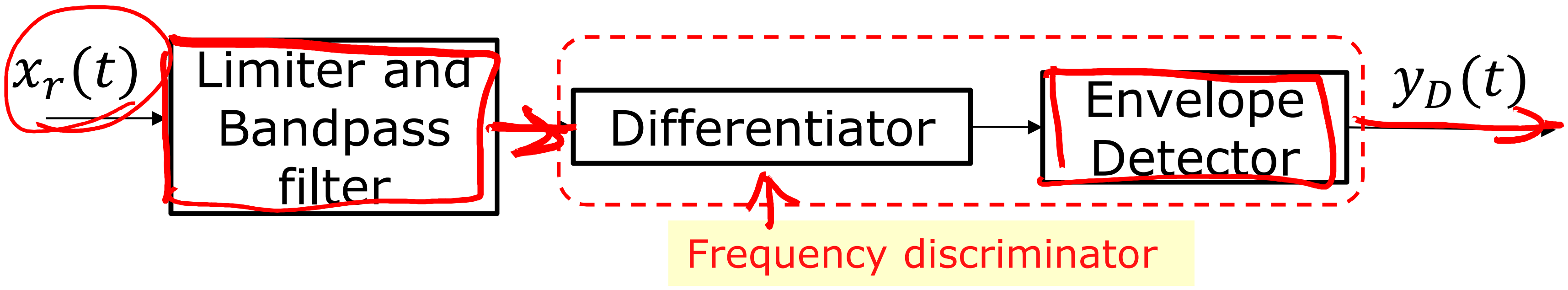
Demodulation of Wideband FM Signals

- Direct method: use frequency discriminator
  - Ideal differentiator has a linear amplitude versus frequency characteristic and therefore is a frequency discriminator.

    Input: $x_r(t) = A_c \cos[2\pi f_c t + 2\pi f_d \int_0^t m(\tau)\, d\tau + \phi_0]$

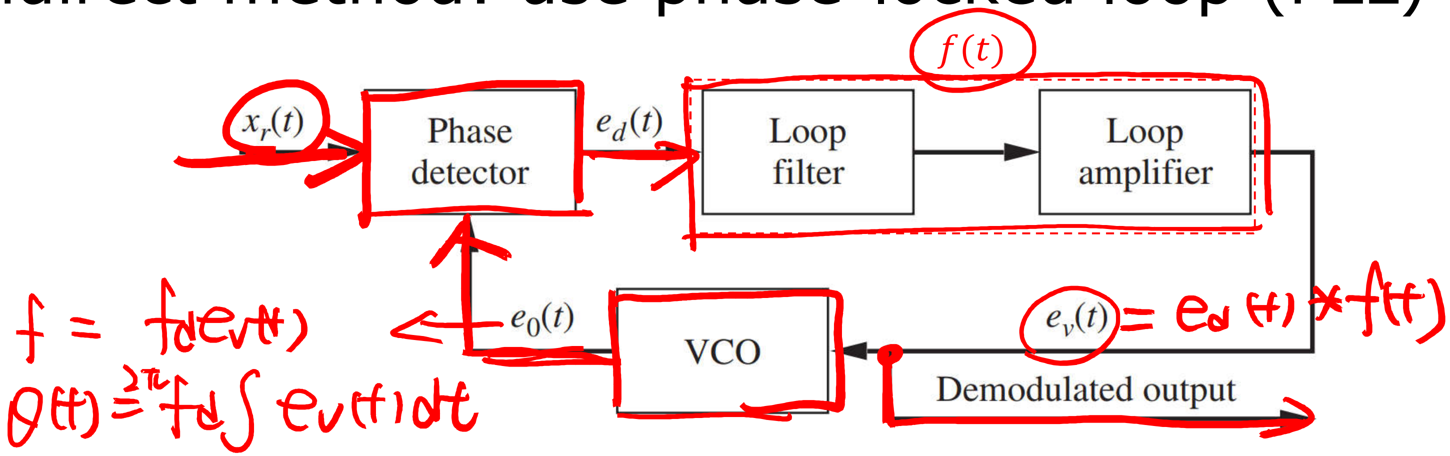
    Output: $\frac{d}{dt} x_r(t) = -A_c[2\pi f_c + 2\pi f_d m(t)] \sin\left[2\pi f_c t + 2\pi f_d \int_0^t m(\tau)\, d\tau + \phi_0\right]$

    Envelope: $A_c[2\pi f_c + 2\pi f_d m(t)]$
  - If $f_c > -f_d m(t), \forall t$, the modulating signal can then be detected by an envelope detector.
  - The output of envelope detector: $y_D(t) = 2\pi A_c f_d m(t)$



Demodulation of Wideband FM Signals (Cont’d)

- Indirect method: use phase-locked loop (PLL)

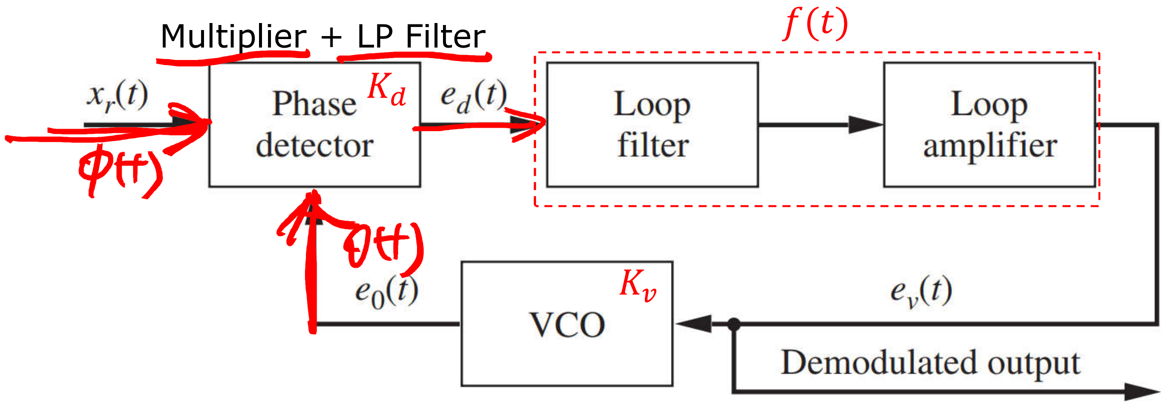


  - Phase detector detects the timing difference between the two periodic signals (with the same fundamental frequency) and produces an output voltage that is proportional to this difference.
  - Loop filter controls the dynamic response of the PLL. We have

    $e_v(t) = e_d(t) * f(t)$
  - Voltage-controlled oscillator (VCO) generates a constant-amplitude periodic waveform whose frequency deviation is proportional to the input voltage, i.e., $\frac{d\theta(t)}{dt} = K_v e_v(t)$.

Demodulation of Wideband FM Signals (Cont'd)

- Indirect method: output of PLL



  - Assume $x_r(t) = A_c \cos[2\pi f_c t + \phi(t)]$ and $e_0(t) = A_v \sin[2\pi f_c t + \theta(t)]$ the phase detector output is then

$$e_d(t) \propto \{A_c \cos[2\pi f_c t + \phi(t)]\, A_v \sin[2\pi f_c t + \theta(t)]\}_{LP}$$
$$\propto \frac{1}{2} A_c A_v K_d \sin[\phi(t) - \theta(t)]$$

  - If $\phi(t) - \theta(t)$ is small and we have $e_d(t) \approx \frac{1}{2} A_c A_v K_d [\phi(t) - \theta(t)]$.

Demodulation of Wideband FM Signals (Cont'd)

- Indirect method: output of PLL

$j2\pi f\,\Theta(f) = 2\pi K_t\,\Psi(f)F(f)$

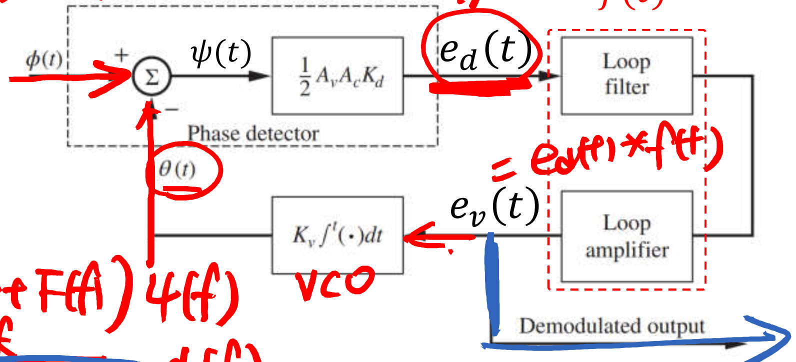
$\frac{1}{2}A_vA_cK_d(\phi(t)-\theta(t))$

$j2\pi f(\Phi(f)-\Psi(f))$

$= 2\pi K_t\,\Psi(f)F(f)$

$jf\,\Phi(f) = (jf + K_tF(f))\Psi(f)$

$\Psi(f) = \dfrac{\Phi(f)}{jf + K_tF(f)}$



$$\frac{d\theta(t)}{dt} = 2\pi K_v e_v(t) = 2\pi K_v e_d(t) * f(t) = \boxed{2\pi K_t[\phi(t)-\theta(t)] * f(t)}$$

$\frac{jf}{}$ $L(f)$

Fourier Transform

Phase error: $\phi(t)-\theta(t)=\psi(t)$

Total loop gain: $K_t = \frac{1}{2}A_cA_vK_dK_v$

$$\Psi(f) = \frac{1}{L(f)+1}\Phi(f),\ \boxed{L(f) = \frac{K_tF(f)}{jf}}$$

$K_t F(f)$

$\boxed{|L(f)| \gg 1}$

$\phi(t) \approx \theta(t)$

$\Psi(f) \to 0$

Phase lock is established

Demodulation of Wideband FM Signals (Cont'd)

- Indirect method: output of PLL (with loop)

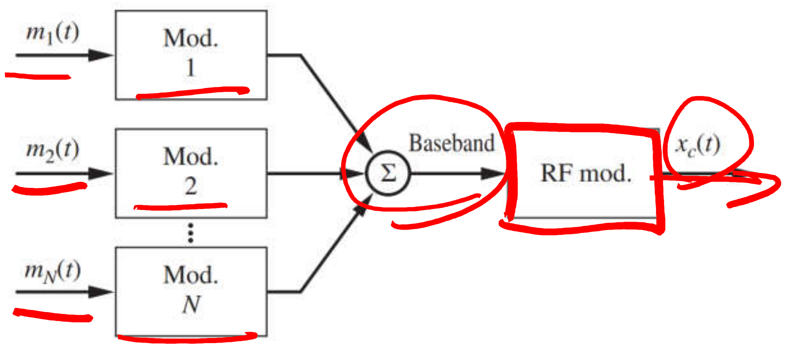
$$\phi(t) \approx \theta(t) = 2\pi K_v \int_0^t e_v(\tau)\, d\tau$$

$$e_v(t) \approx \frac{1}{2\pi K_v} \frac{d}{dt} \phi(t) \propto m(t)$$

  - Output voltage is proportional to the frequency deviation (referred to the carrier) of the input wideband FM signal.
  - The PLL demodulates the input wideband FM signal!

Multiplexing

- Frequency-Division Multiplexing



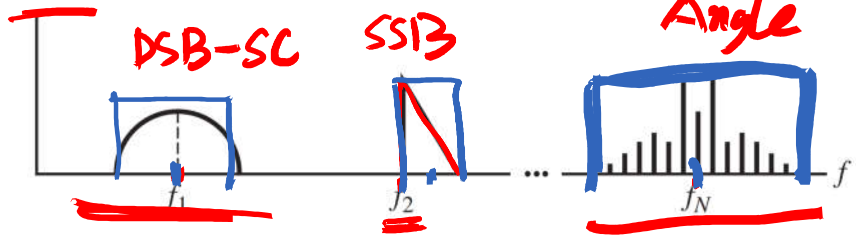
a) FDM modulator

Carson's $B_T = 2(1+\beta)f_m$

BB $B_T = 2W$ DSB-SC

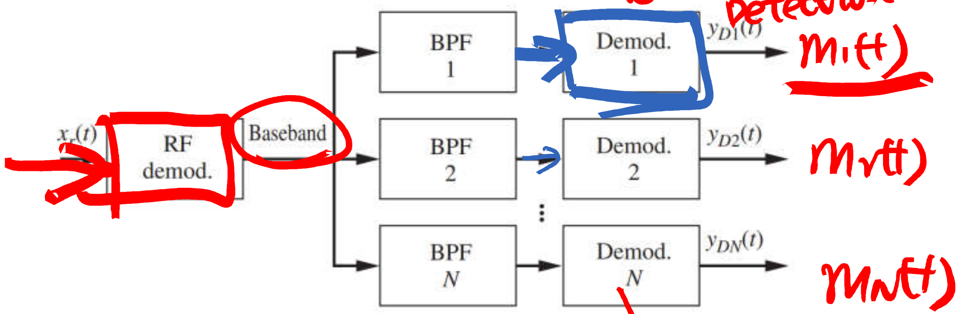
$B_T = W$ SSB

Modulation Angle



c) Assumed baseband spectrum

Coherent Detection



PLL
FD

b) FDM demodulator

Thanks for your kind attention!

Questions?