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DEPARTMENT OF ELECTRONICS ENGINEERING
ELECTRONIC CIRCUITS
Multi-transistor circuits

Numerical 1

The parameters for each circuit shown in figure 1 are $\beta_1 = \beta_2 = 110$ & $V_A = \infty$

- Determine small signal parameters
- Determine small signal voltage gain assuming V_{o1} is connected to o.c, then determine small signal voltage gain for stage 2.
- Determine the overall small signal voltage gain

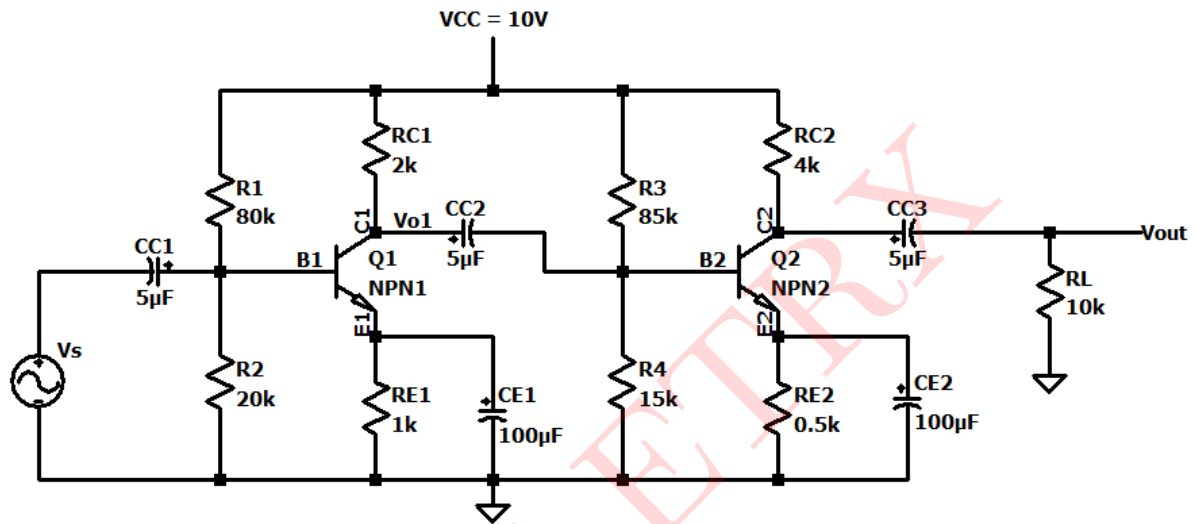


Figure 1: Circuit for Numerical 1

Solution: The above circuit is a 2-stage RC coupled CE-CE amplifier

DC Analysis: During DC analysis, capacitors become open circuit.

Since both the stages are different, DC analysis for both the stages will be different.

STAGE-1:

From figure 1 we get,

$$R_{th1} = R_1 \parallel R_2 = 80k \parallel 20k$$

$$\therefore R_{th1} = 16k\Omega$$

$$V_{th1} = \frac{R_2}{R_1 + R_2} \times V_{CC} = \frac{20k}{20k + 80k} \times 10$$

$$\therefore V_{th1} = 2V$$

The thevenin's equivalent circuit for stage-1 is shown in figure 2

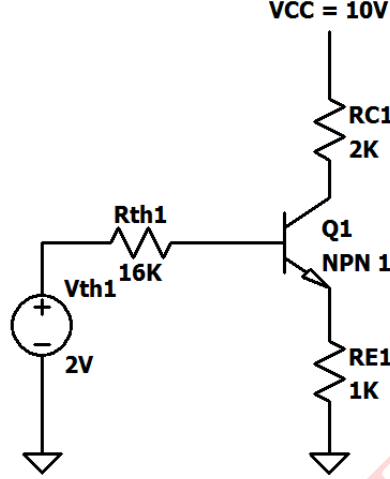


Figure 2: Thevenin's Equivalent Circuit for Stage-1

Applying KVL to the B-E loop for figure 2 we get,

$$V_{th1} - I_{BQ1}R_{th1} - V_{BE1} - I_{E1}R_{E1} = 0$$

$$V_{th1} - I_{BQ1}R_{th1} - V_{BE1} - (1 + \beta_1)I_{BQ1}R_{E1} = 0 \quad (\because I_E = (1 + \beta)I_B)$$

$$I_{BQ1} = \frac{V_{th1} - V_{BE1}}{R_{th1} + (1 + \beta_1)R_{E1}} = \frac{2V - 0.7V}{16k + (1 + 110) \times 1K}$$

$$\therefore I_{BQ1} = 10.23\mu A$$

$$I_{CQ1} = \beta_1 \times I_{BQ1} = 110 \times 10.23\mu A$$

$$\therefore I_{CQ1} = 1.126mA$$

Applying KVL to C-E loop of figure 2 we get,

$$V_{CC} - I_{CQ1}R_{C1} - V_{CEQ1} - I_{CQ1}R_{E1} = 0$$

$$V_{CEQ1} = V_{CC} - I_{CQ1}(R_{C1} + R_{E1}) = 10 - 1.126mA(2k + 1k)$$

$$\therefore V_{CEQ1} = 6.622V$$

Calculation of small signal parameters:

$$g_{m1} = \frac{I_{CQ1}}{V_T} = \frac{1.126mA}{0.026}$$

$$\therefore g_{m1} = 43.30mA/V$$

$$r_{\pi1} = \frac{\beta_1 V_T}{I_{CQ1}} = \frac{110 \times 26mV}{1.126mA}$$

$$\therefore r_{\pi1} = 2.5k\Omega$$

$$r_{o1} = \infty \quad (\because V_A = \infty)$$

STAGE-2:

From figure 1 we get,

$$R_{th2} = R_3 \parallel R_4 = 85k \parallel 15k$$

$$\therefore R_{th2} = 12.75k\Omega$$

$$V_{th2} = \frac{R_4}{R_3 + R_4} \times V_{CC} = \frac{15k}{15k + 85k} \times 10$$

$$\therefore V_{th2} = 1.5V$$

The thevenin's equivalent circuit for stage-2 is shown in figure 3

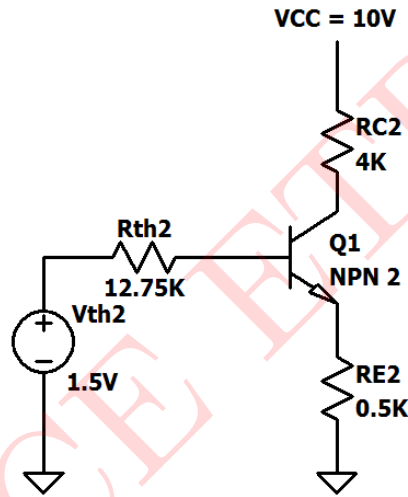


Figure 3: Thevenin's Equivalent Circuit for Stage-2

Applying KVL to the B-E loop for figure 2 we get,

$$V_{th2} - I_{BQ2}R_{th2} - V_{BE2} - I_{E2}R_{E2} = 0$$

$$V_{th2} - I_{BQ2}R_{th2} - V_{BE2} - (1 + \beta_2)I_{BQ2}R_{E2} = 0 \quad (\because I_E = (1 + \beta_2)I_B)$$

$$I_{BQ2} = \frac{V_{th2} - V_{BE2}}{R_{th2} + (1 + \beta_2)R_{E2}} = \frac{1.5V - 0.7V}{12.75k + (1 + 110) \times 0.5k}$$

$$\therefore I_{BQ1} = 11.722\mu A$$

$$I_{CQ2} = \beta_2 \times I_{BQ2} = 110 \times 11.722\mu A$$

$$\therefore I_{CQ2} = 1.289mA$$

Applying KVL to C-E loop of figure 3 we get,

$$V_{CC} - I_{CQ2}R_{C2} - V_{CEQ2} - I_{CQ2}R_{E2} = 0$$

$$V_{CEQ2} = V_{CC} - I_{CQ2}(R_{C2} + R_{E2}) = 10 - 1.289mA(4k + 0.5k)$$

$$\therefore V_{CEQ2} = 4.199V$$

Calculation of small signal parameters:

$$g_{m2} = \frac{I_{CQ2}}{V_T} = \frac{1.289mA}{0.026}$$

$$\therefore g_{m2} = 49.576mA/V$$

$$r_{\pi2} = \frac{\beta_2 V_T}{I_{CQ2}} = \frac{110 \times 26mV}{1.289mA}$$

$$\therefore r_{\pi2} = 2.2k\Omega$$

$$r_{o2} = \infty \quad (\because V_A = \infty)$$

AC Analysis:

Mid band small signal equivalent circuit is shown in figure 4

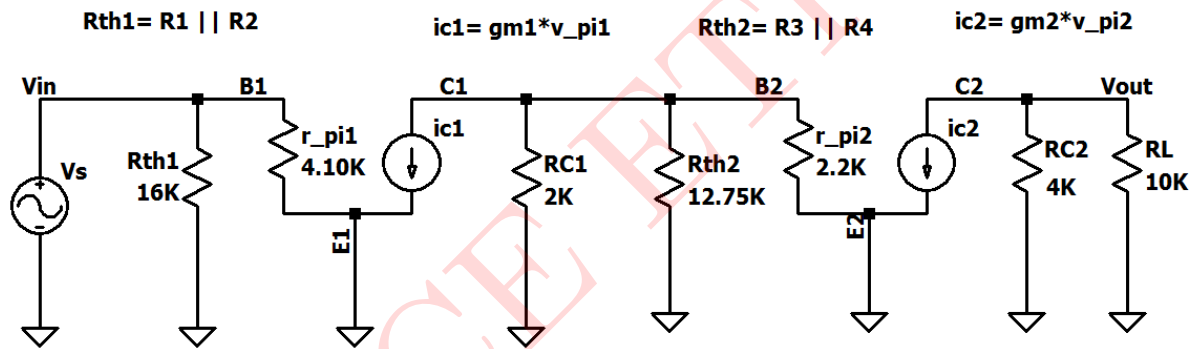


Figure 4: Small Signal Equivalent Circuit

Calculation of voltage gain:

$$A_{V(mid)} = \frac{V_{out}}{V_{in}} = \frac{V_{out}}{V_{o1}} \times \frac{V_{o1}}{V_{in}}$$

For Stage-1:

$$A_{V1} = \frac{V_{o1}}{V_{in}} = -g_{m1}(R_{C1} \parallel R_{th2} \parallel r_{\pi2}) = -43.30mA/V(2k \parallel 12.75k \parallel 2.2k)$$

$$A_{V1} = -41.91$$

For Stage-2:

$$A_{V2} = \frac{V_{out}}{V_{o1}} = -g_{m2}(R_{C2} \parallel R_L) = -49.576mA/V(4k \parallel 10k)$$

$$A_{V2} = -141.645$$

The overall voltage gain $A_{V(mid)}$

$$A_{V(mid)} = -141.645 \times -41.91 = 5936.34$$

$$A_{V(mid)(dB)} = 20\log(5936.34)$$

$$A_{V(\text{mid})}(\text{dB}) = 75.47\text{dB}$$

SIMULATED RESULTS:

Above circuit is simulated in LTspice and results are as follows:

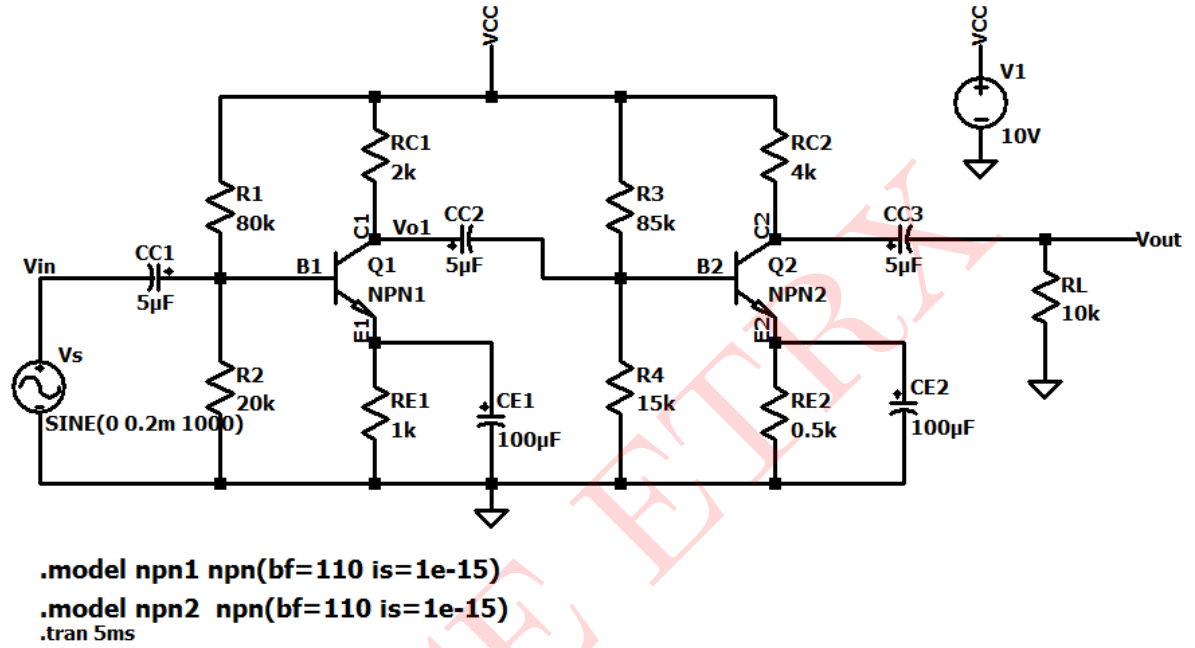


Figure 5: Circuit Schematics: Results

Output Waveforms:

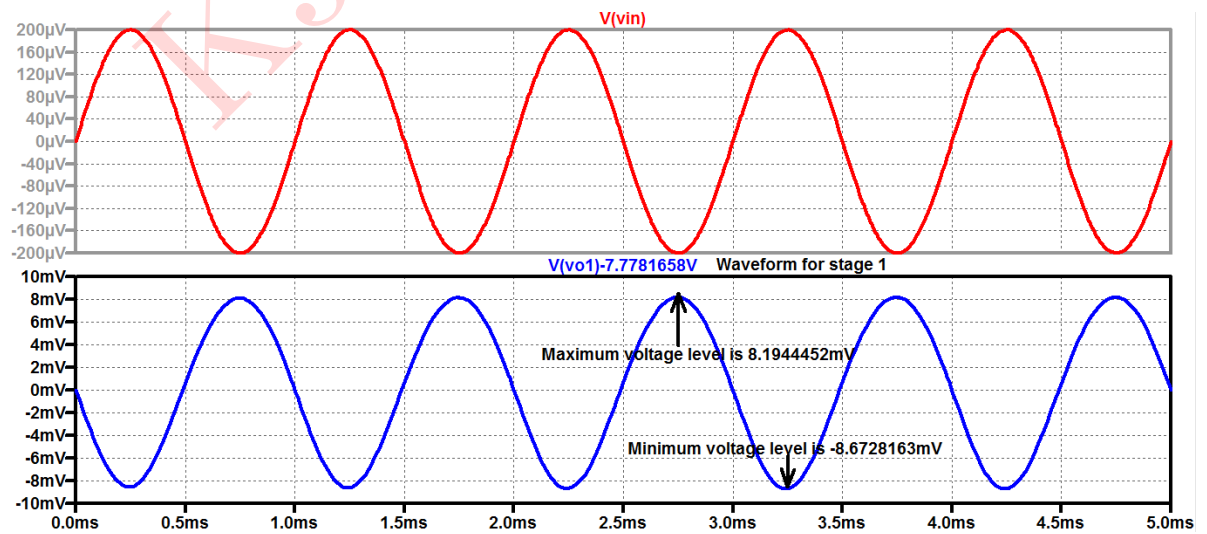


Figure 6: Input and Output Waveforms for 1st Stage

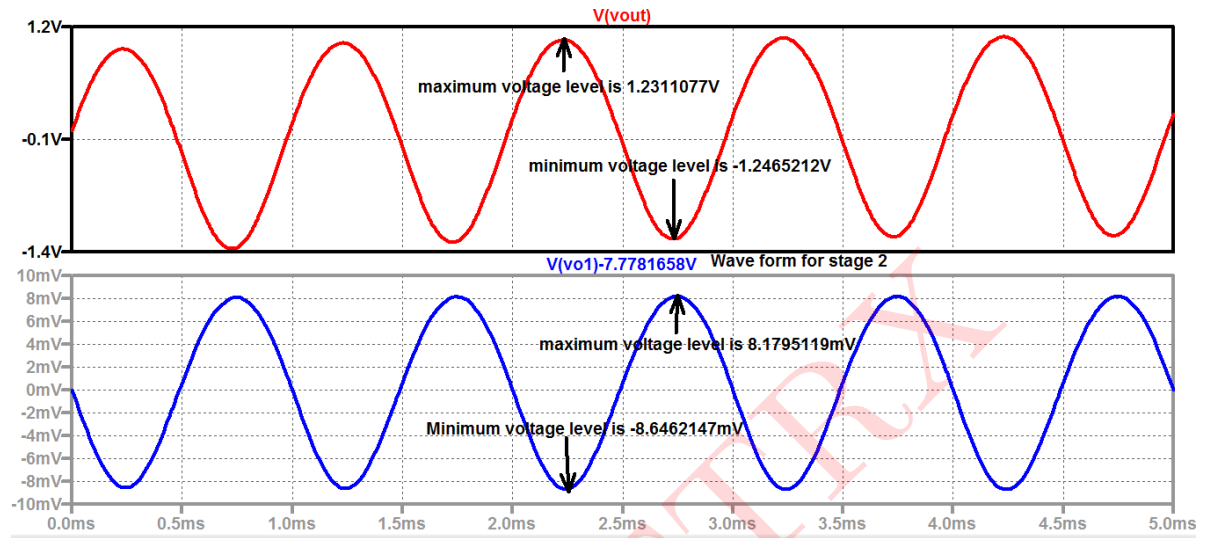


Figure 7: Input and Output Waveforms for 2nd Stage

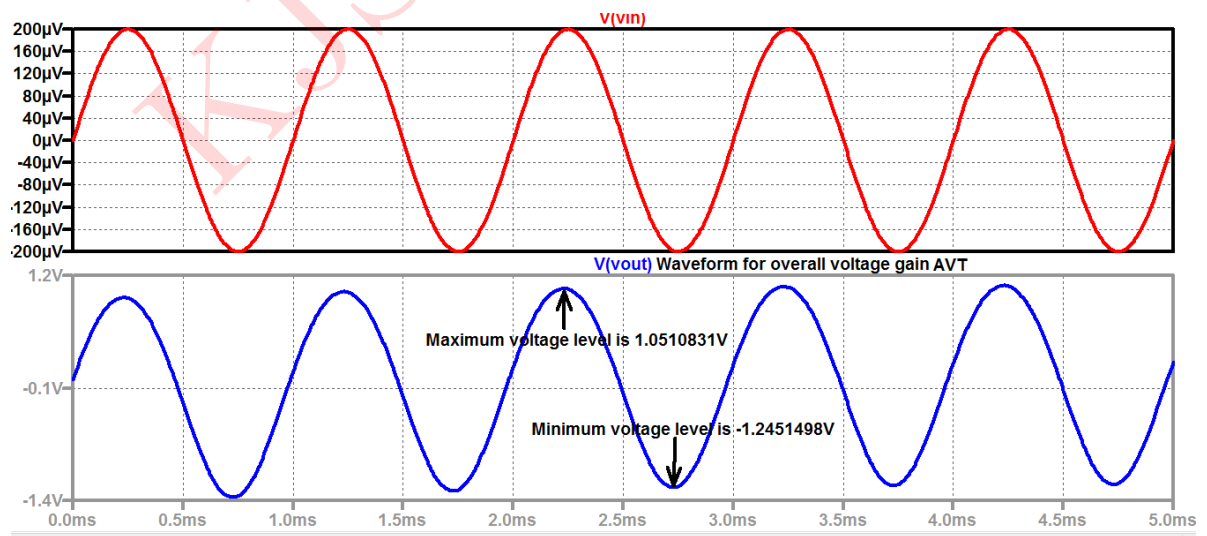


Figure 8: Input and Output Waveforms for the circuit

Comparison between theoretical and simulated values is given below:

Parameters	Simulated Values	Theoretical Values
Stage-1: I_{CQ_1}	$1.11mA$	$1.126mA$
Stage-1: V_{CEQ_1}	$6.65V$	$6.622V$
Stage-2: I_{CQ_2}	$1.25mA$	$1.289mA$
Stage-2: V_{CEQ_2}	$4.34V$	$4.199V$
Stage-1: Voltage gain	-42.1	-41.91
Stage-2: Voltage gain	-138.52	-141.645
Overall voltage gain A_V in dB	$75.155dB$	$75.47dB$

Table 1: Numerical 1

Numerical 2

Calculate the DC bias, output impedance, voltage gain and resulting voltage for cascade amplifier shown in figure 9. Calculate the load voltage if $10k\Omega$ is connected across the output.

Given: $R_L = 10k\Omega$, $I_{DSS} = 10mA$, $V_P = -4V$

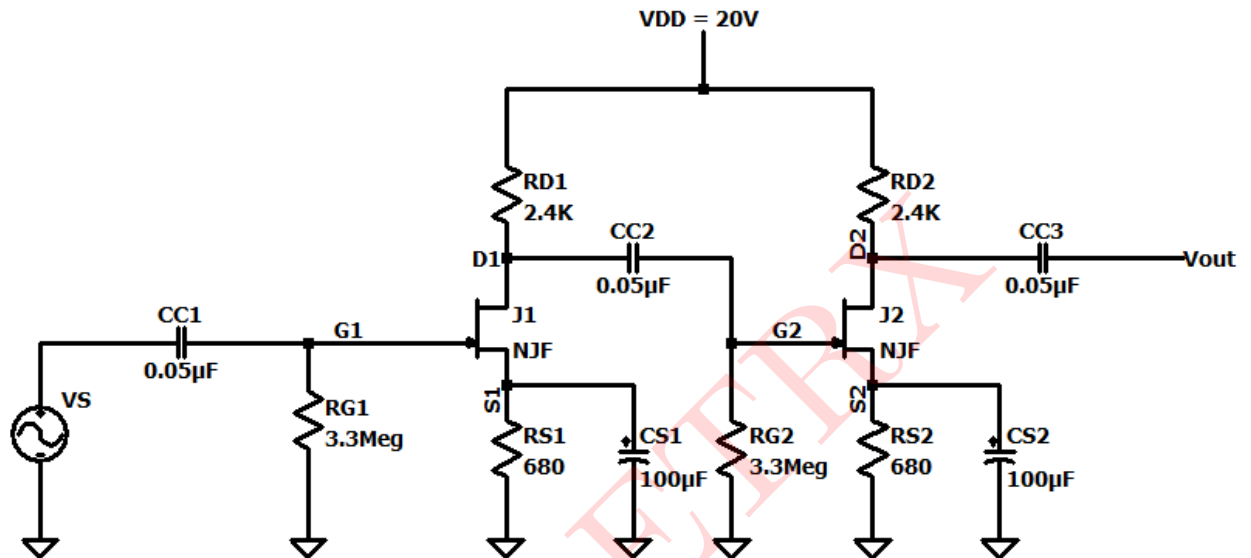


Figure 9: Circuit for Numerical 2

Solution: The above circuit is a 2-stage RC coupled cascaded amplifier

DC Analysis: During DC analysis, capacitors become open circuit.

Due to RC coupling, both the stage's Q-points are isolated. Since both the stage's parameters and resistor values are identical, DC analysis of one stage will be sufficient.

The DC equivalent circuit for stage-1 is shown in figure 10

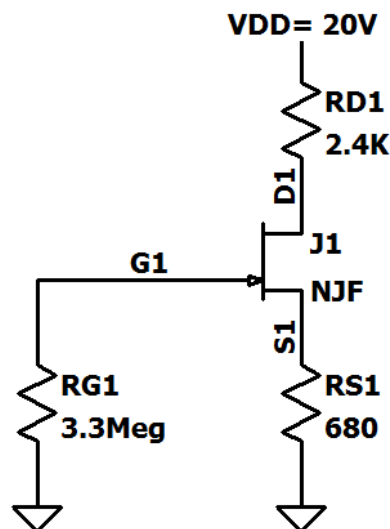


Figure 10: DC Equivalent Circuit for Stage-1

Applying KVL to G-S loop of figure 10 we get,

$$V_{GS_1} = -I_{D_1}R_{S_1}$$

$$V_{GS_1} = -I_{D_1}(680) \quad \dots(1)$$

$$I_{D_1} = I_{DSS} \left(1 - \frac{V_{GS_1}}{V_P}\right)^2$$

$$I_{D_1} = 10mA \times \left(1 + \frac{V_{GS_1}}{4}\right)^2 \quad \dots(2)$$

Substituting (2) in (1) we get,

$$V_{GS_1} = -6.8 \left(1 + \frac{V_{GS_1}}{2} + \frac{V_{GS_1}^2}{16}\right)$$

$$V_{GS_1} = -6.8 - 3.4V_{GS_1} - 0.425V_{GS_1}^2$$

$$0.425V_{GS_1}^2 + 4.4V_{GS_1} + 6.8 = 0$$

Solving the above quadratic equation we get,

$$V_{GS_1} = -1.89V \text{ or } V_{GS_1} = -8.46V$$

$$V_{GS_1} = -1.89V \quad (\because V_{GS} > V_P)$$

$$I_{D_1} = 10mA \times \left(1 - \frac{(-1.89V)}{(-4)}\right)^2$$

$$I_{D_1} = 2.779mA$$

Both the stages are identical so, $V_{GS_1} = V_{GS_2} = -1.89V$ & $I_{D_1} = I_{D_2} = 2.779mA$

Calculation of small signal parameters:

$$g_{m_1} = \frac{2I_{DSS}}{|V_P|} \left(1 - \frac{V_{GS_1}}{V_P}\right) = \frac{2 \times 10mA}{|-4|} \left(1 - \frac{(-1.89V)}{(-4V)}\right)$$

$$g_{m_1} = 2.6mA/V$$

$$\text{i.e. } g_{m_1} = g_{m_2} = 2.6mA/V$$

AC Analysis:

Mid band small signal equivalent circuit is shown in figure 11

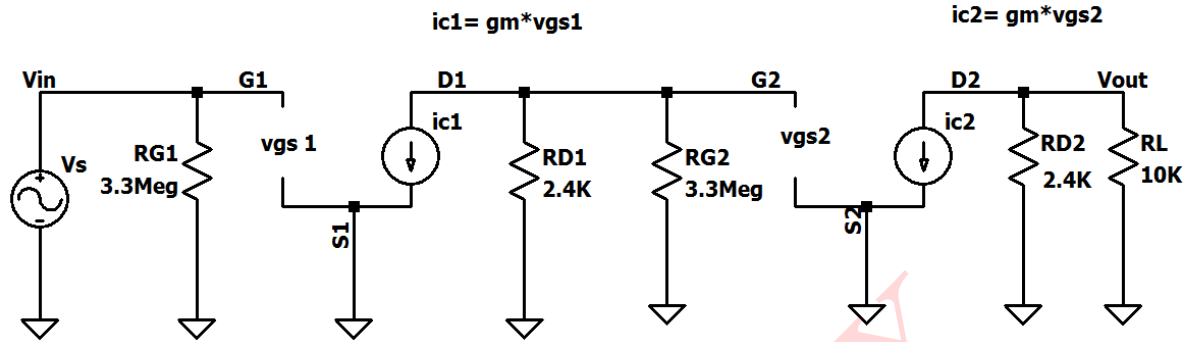


Figure 11: Small Signal Equivalent Circuit

Calculation of voltage gain:

$$A_{V(mid)} = \frac{V_{out}}{V_{in}} = \frac{V_{out}}{V_{o1}} \times \frac{V_{o1}}{V_{in}}$$

For Stage-1:

$$A_{V1} = \frac{V_{o1}}{V_{in}} = -g_{m1}(R_{D1} \parallel R_{G2}) = -2.6mA/V(2.4k \parallel 3.3M) \approx -2.6mA/V \times 2.4k$$

$$A_{V1} = -6.24$$

For Stage-2:

$$A_{V2} = \frac{V_{out}}{V_{o1}} = -g_{m2}(R_{D2}) = -2.6mA/V \times 2.4k$$

$$A_{V2} = -6.24$$

The overall voltage gain A_{VT} :

$$A_{VT} = A_{V1} \times A_{V2} = -6.24 \times -6.24$$

$$A_{VT} = 38.93$$

$$A_{VT}(dB) = 20\log_{10}(38.93)$$

$$A_{VT}(dB) = 31.80dB$$

Calculation of output voltage V_o :

$$V_o = A_{VT} \times V_i = 38.93 \times 10mV$$

$$V_o = 389.3mV$$

Calculation of input and output impedances:

$$Z_i = R_G$$

$$Z_i = 3.3M\Omega$$

$$Z_o = R_D$$

$$Z_o = 2.4k\Omega$$

The output voltage across 10k Ω load:

$$V_L = \frac{R_L}{Z_o + R_L} \times V_o = \frac{10k}{2.4k + 10k} \times 389.3mV$$

$$V_L = 313.7mV$$

SIMULATED RESULTS:

Above circuit is simulated in LTspice and results are as follows:

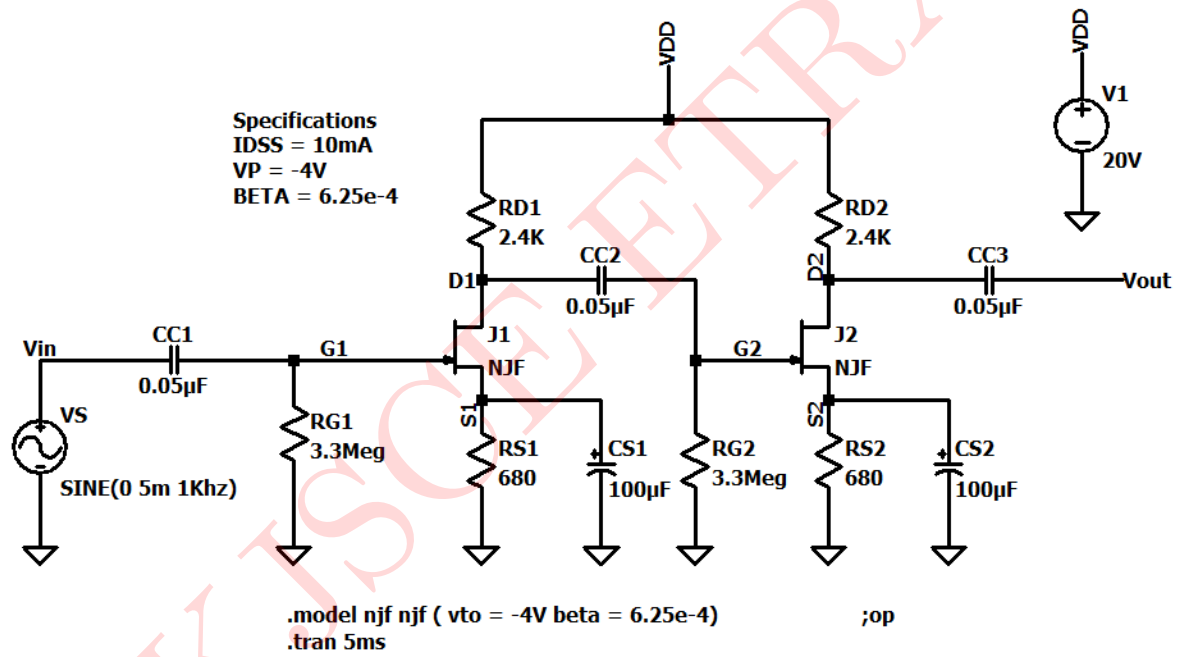


Figure 12: Circuit Schematics: Results

Output Waveforms:

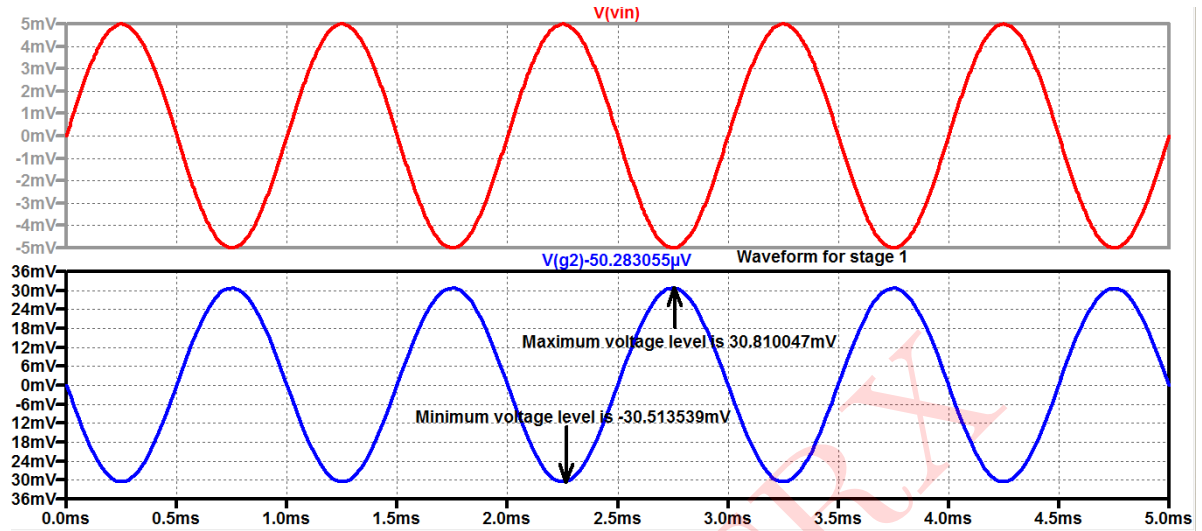


Figure 13: Input and Output Waveforms for 1st Stage

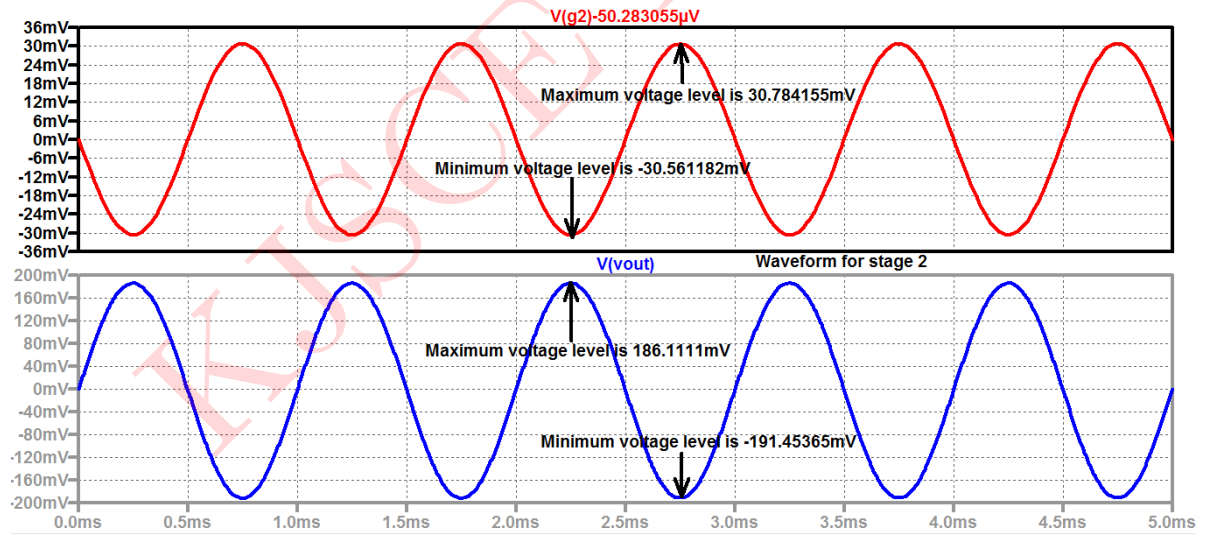


Figure 14: Input and Output Waveforms for 2nd Stage

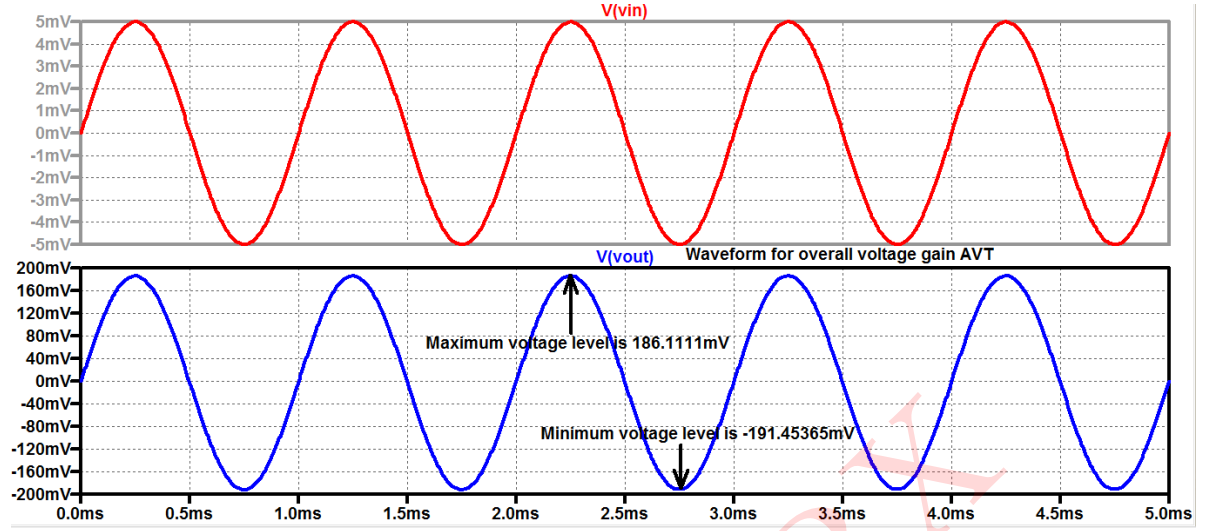


Figure 15: Input and Output Waveforms for the circuit

Comparison between theoretical and simulated values is given below:

Parameters	Simulated Values	Theoretical Values
Stage-1: I_{DQ_1}	2.78mA	2.779mA
Stage-1: V_{GSQ_1}	-1.89V	-1.89V
Stage-2: I_{DQ_2}	2.78mA	2.779mA
Stage-2: V_{GSQ_2}	-1.89V	-1.89V
Stage-1: Voltage gain A_{V_1}	-6.12	-6.24
Stage-2: Voltage gain A_{V_2}	-6.14	-6.24
Overall Voltage gain A_{V_T}	31.52dB	31.80dB
Output Voltage	0.377V	0.38V
Input impedance Z_i	—	3.3M Ω
Output impedance Z_o	—	2.4k Ω

Table 2: Numerical 2

Numerical 3

A two stage circuit is shown in figure 16, its BJT parameters are $\beta_1 = \beta_2 = 20$ & $V_{BE_1} = V_{BE_2} = 0.6V$

- Determine all node voltages and terminal currents under DC analysis
- Determine the overall small signal voltage gain

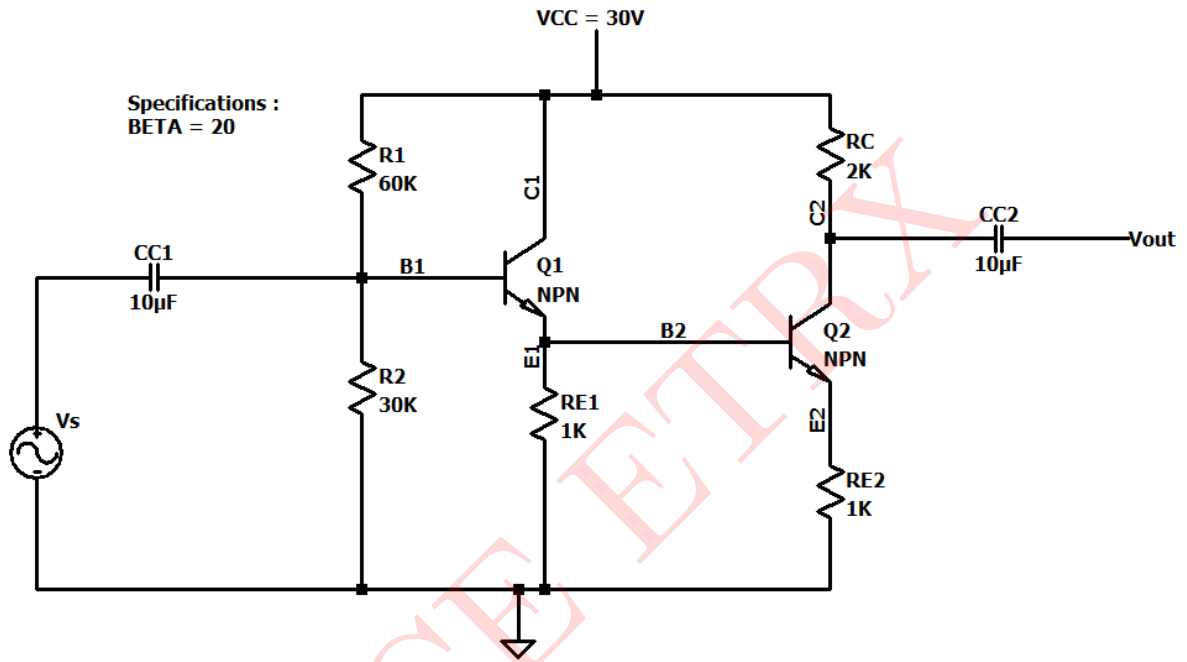


Figure 16: Circuit for Numerical 3

Solution:

DC Analysis: During DC analysis, capacitors become open circuit.

Since both the stages are different, DC analysis for both the stages will be different.

STAGE-1:

From figure 1 we get,

$$R_{th1} = R_1 \parallel R_2 = 60k \parallel 30k$$

$$R_{th1} = 20k\Omega$$

$$V_{th1} = \frac{R_2}{R_1 + R_2} \times V_{CC} = \frac{30k}{30k + 60k} \times 30V$$

$$V_{th1} = 10V$$

The thevenin's equivalent of base circuit of Q_1 is shown in figure 17

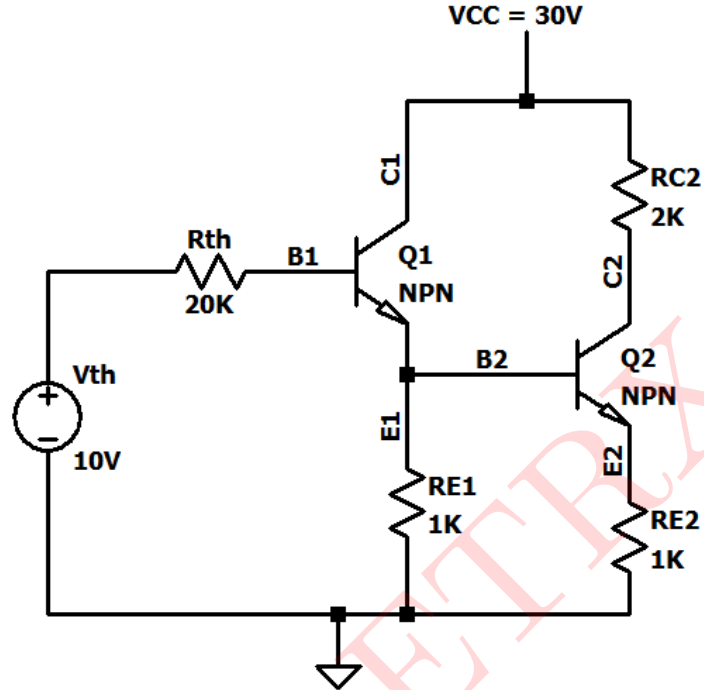


Figure 17: Thevenin's Equivalent Circuit

Calculation of terminal currents for stage-1:

Applying KVL to the B-E loop for figure 17 we get,

$$V_{th} - I_{B_1} R_{th} - V_{BE_1} - I_{E_1} R_{E_1} = 0$$

$$V_{th} - I_{B_1} R_{th} - V_{BE_1} - (1 + \beta_1) I_{B_1} R_{E_1} = 0 \quad (\because I_E = (1 + \beta) I_B)$$

$$I_{B_1} = \frac{V_{th} - V_{BE_1}}{R_{th} + (1 + \beta_1) R_{E_1}} = \frac{10V - 0.7V}{20k + (1 + 20) \times 1k}$$

$$I_{B_1} = 229.27 \mu A$$

$$I_{C_1} = \beta_1 \times I_{B_1} = 20 \times 229.27 \mu A$$

$$I_{C_1} = 4.585 mA$$

$$\text{Now, } I_{E_1} = I_{C_1} + I_{B_1} = 4.585 mA + 229.27 \mu A$$

$$I_{E_1} = 4.814 mA$$

Calculation of node voltages of stage-1:

$$V_{E_1} = I_{E_1} R_{E_1} = 4.814 mA \times 1k\Omega$$

$$V_{E_1} = 4.814 V$$

$$V_{B_1} = V_{BE_1} + V_{E_1} = 0.6V + 4.814V$$

$$V_{B_1} = 5.414 V$$

STAGE-2:**Calculation of node voltages of stage-2:**

From figure 2 we get,

$$V_{E_1} = V_{B_2}$$

$$V_{B_2} = 4.814V$$

$$V_{E_2} = V_{B_2} - V_{BE_2} = 4.814V - 0.6V$$

$$V_{E_2} = 4.214V$$

$$V_{C_2} = V_{CC} - I_{C_2} R_{C_2}$$

$$V_{C_2} = 30V - I_{C_2} \times 2k \quad \text{.....(1)}$$

Calculation of terminal currents of stage-2:

$$I_{E_2} = \frac{V_{E_2}}{R_{E_2}} = \frac{4.214V}{1k}$$

$$I_{E_2} = 4.214mA$$

$$I_{C_2} = \alpha_2 \times I_{E_2} = \frac{\beta_2}{1 + \beta_2} \times I_{E_2} = \frac{20}{21} \times 4.214mA$$

$$I_{C_2} = 4.013mA \quad \text{.....(2)}$$

$$I_{B_2} = \frac{I_{E_2}}{1 + \beta_2} = \frac{4.214mA}{21}$$

$$I_{B_2} = 200.67\mu A$$

From (1) and (2) we get,

$$V_{C_2} = 30 - 3.822mA \times 2k$$

$$V_{C_2} = 22.356V$$

Calculation of small signal parameters:

$$g_{m_1} = \frac{I_{CQ_1}}{V_T} = \frac{4.585mA}{0.026V}$$

$$g_{m_1} = 176.35mA/V$$

$$r_{\pi_1} = \frac{\beta_1 V_T}{I_{CQ_1}} = \frac{20 \times 26mV}{4.585mA}$$

$$r_{\pi_1} = 113.41\Omega$$

$$g_{m2} = \frac{I_{CQ2}}{V_T} = \frac{3.822mA}{0.026}$$

$$g_{m2} = 147mA/V$$

$$r_{\pi2} = \frac{\beta_2 V_T}{I_{CQ2}} = \frac{20 \times 26mV}{3.822mA}$$

$$r_{\pi2} = 136.054\Omega$$

AC Analysis:

Mid band small signal equivalent circuit is shown in figure 18

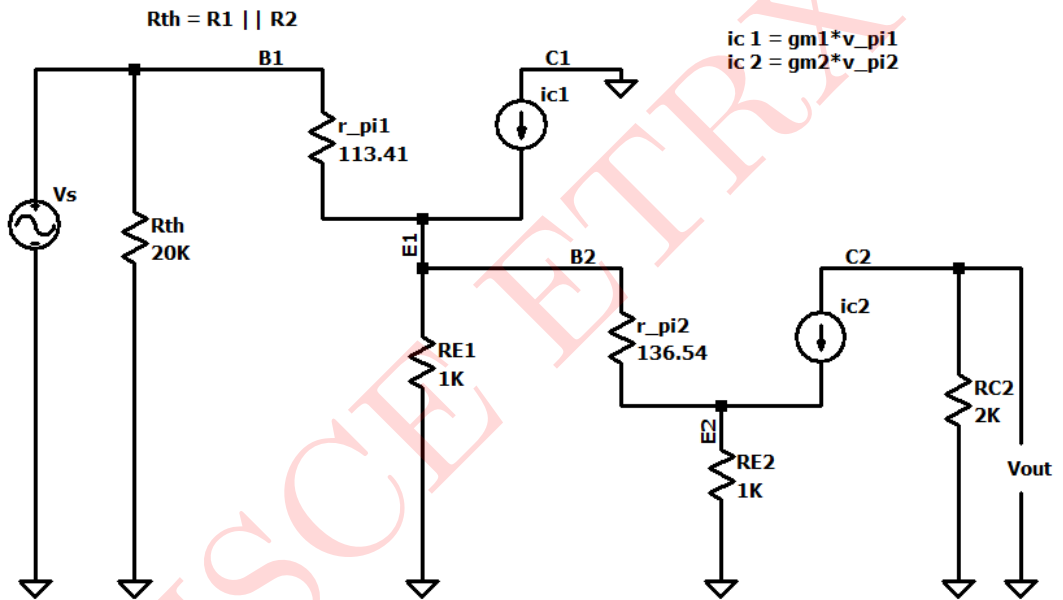


Figure 18: Small Signal Equivalent Circuit

Calculation of voltage gain:

$$A_{V_T} = \frac{V_{out}}{V_s} = \frac{V_{out}}{V_{o1}} \times \frac{V_{o1}}{V_s}$$

For Stage-1:

$$A_{V1} = \frac{V_{o1}}{V_s} = \frac{(g_{m1} V_{\pi1}) R_{E1}}{i_{b1} [r_{\pi1} + (1 + \beta) R_{E1}]}$$

$$A_{V1} = \frac{\beta i_{b1} R_{E1}}{i_{b1} [r_{\pi1} + (1 + \beta) R_{E1}]} \quad (\because ic_1 = g_{m1} V_{\pi1} = \beta i_{b1})$$

$$A_{V1} = \frac{\beta R_{E1}}{r_{\pi1} + (1 + \beta) R_{E1}}$$

$$A_{V1} = \frac{20 \times 1k}{113.41 + 21 \times 1k}$$

$$A_{V1} = -0.9473$$

For Stage-2:

$$A_{V_2} = \frac{V_{out}}{V_{o1}} = \frac{-(g_{m2} V_{\pi_2}) R_{C_2}}{i_{b_2} [r_{\pi_2} + (1 + \beta) R_{E_2}]}$$

$$A_{V_2} = \frac{-\beta i_{b_2} R_{C_2}}{i_{b_2} [r_{\pi_2} + (1 + \beta) R_{E_2}]} \quad (\because i_{c_2} = g_{m2} V_{\pi_2} = \beta i_{b_2})$$

$$A_{V_2} = \frac{-\beta R_{C_2}}{r_{\pi_2} + (1 + \beta) R_{E_2}}$$

$$A_{V_2} = \frac{-20 \times 2k}{136.054 + 21 \times 1k}$$

$$A_{V_2} = -1.8925$$

The overall voltage gain A_{V_T} :

$$A_{V_T} = A_{V_1} \times A_{V_2} = 0.9472 \times -1.8925$$

$$A_{V_T} = -1.7927$$

Calculation of output voltage:

$$V_o = A_{V_T} \times V_{in} = 1.79 \times 40mV$$

$$V_o = 71.6mV$$

SIMULATED RESULTS:

Above circuit is simulated in LTspice and results are as follows:

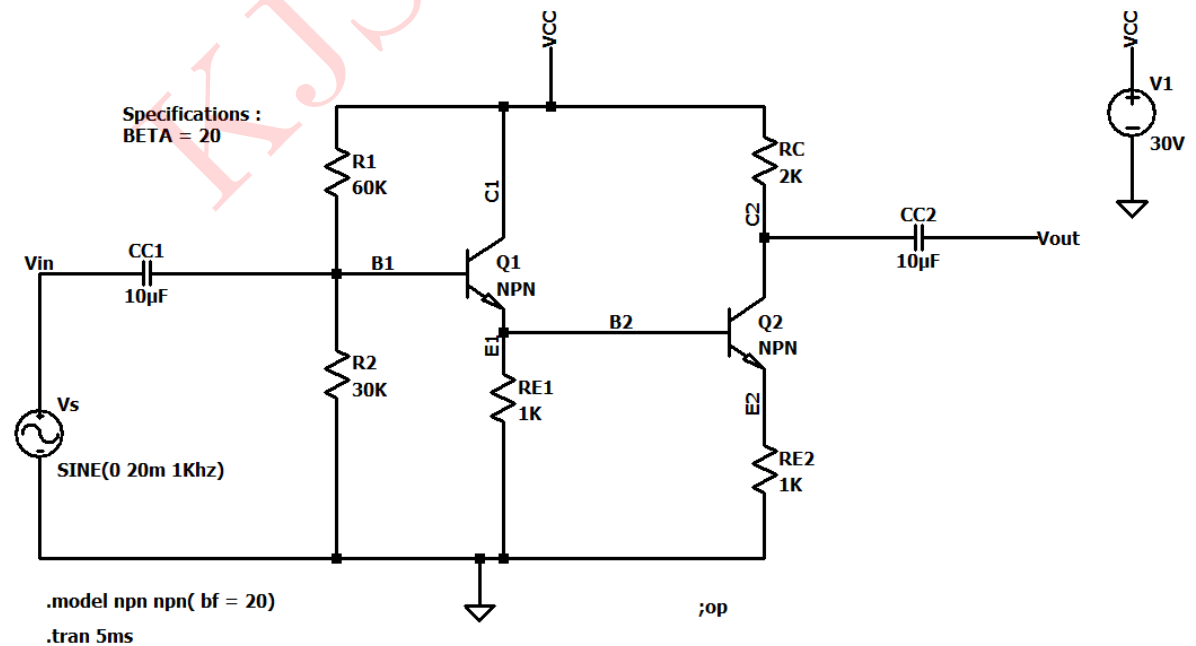


Figure 19: Circuit Schematics: Results

Output Waveforms:

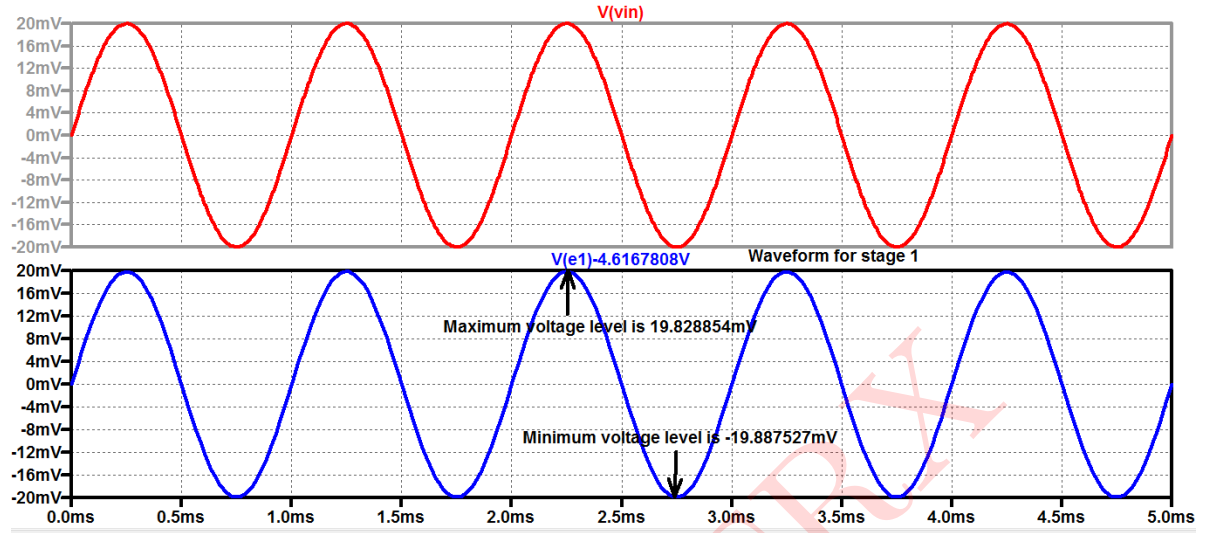


Figure 20: Input and Output Waveforms for 1st Stage

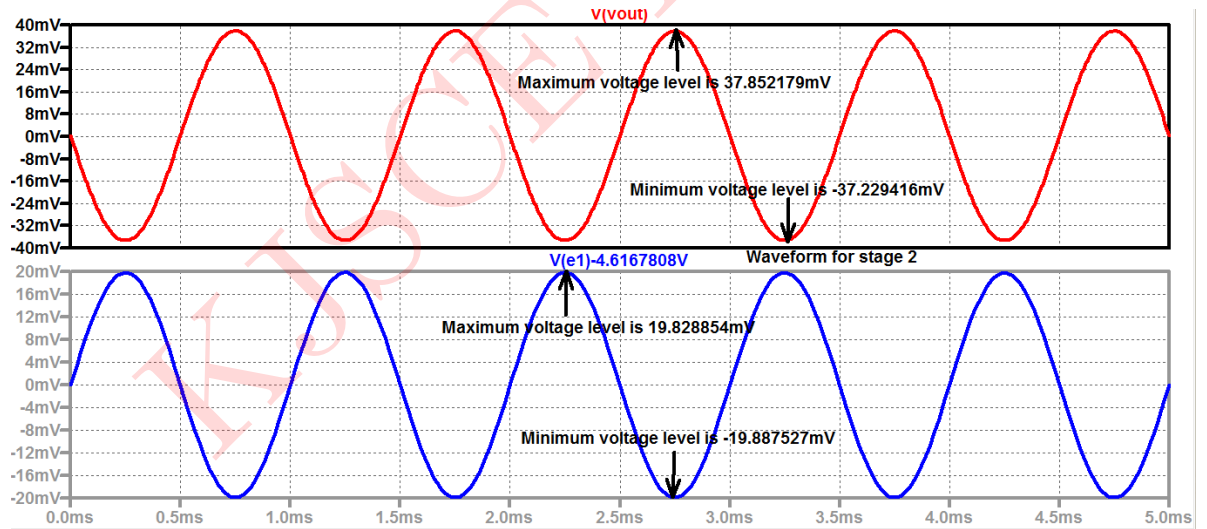


Figure 21: Input and Output Waveforms for 2nd Stage

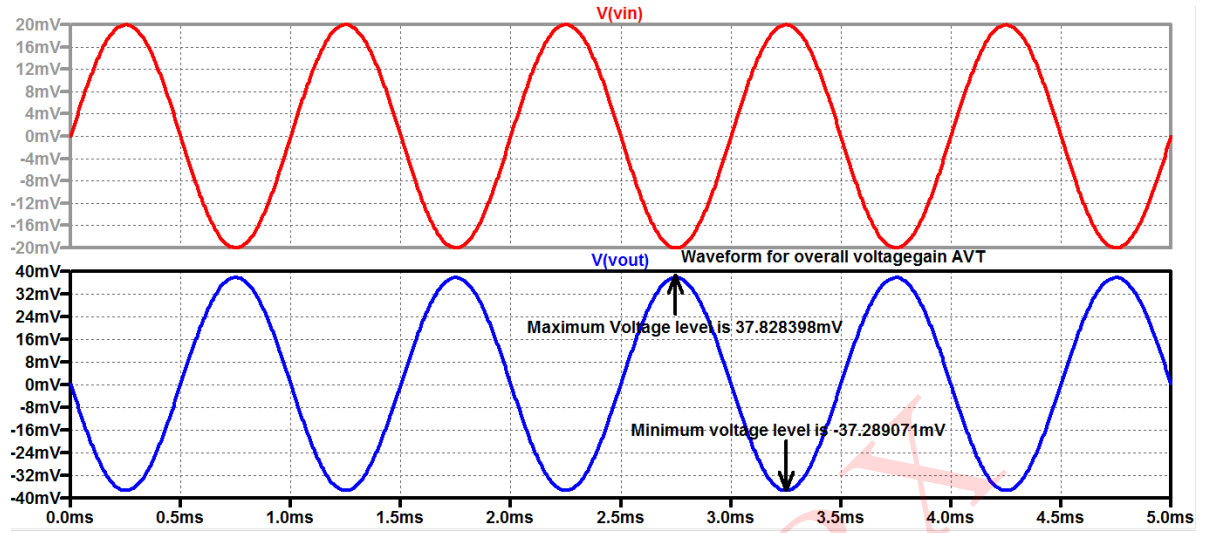


Figure 22: Input and Output Waveforms for the circuit

Comparison between theoretical and simulated values is given below:

Parameters	Simulated Values	Theoretical Values
Stage-1: I_{B_1}	$228.48\mu A$	$229.27\mu A$
Stage-1: I_{C_1}	$4.569mA$	$4.585mA$
Stage-1: I_{E_1}	$4.798mA$	$4.814mA$
Stage-1: V_{B_1}	$5.43V$	$5.414V$
Stage-1: V_{C_1}	$30V$	$30V$
Stage-1: V_{E_1}	$4.616V$	$4.814V$
Stage-2: I_{B_2}	$181.39\mu A$	$200.67\mu A$
Stage-2: I_{C_2}	$3.8mA$	$4.013mA$
Stage-2: I_{E_2}	$3.81mA$	$4.214mA$
Stage-2: V_{B_2}	$4.616V$	$4.814V$
Stage-2: V_{C_2}	$22.74V$	$22.356V$
Stage-2: V_{E_2}	$3.809V$	$4.214V$
Overall voltage gain A_{V_T}	-1.877	-1.79
Output voltage	$74.11mV$	$71.6mV$

Table 3: Numerical 3
