
Low-Noise Amplifiers



Willy Sansen

**KULeuven, ESAT-MICAS
Leuven, Belgium**

willy.sansen@esat.kuleuven.be



Receiver Topology

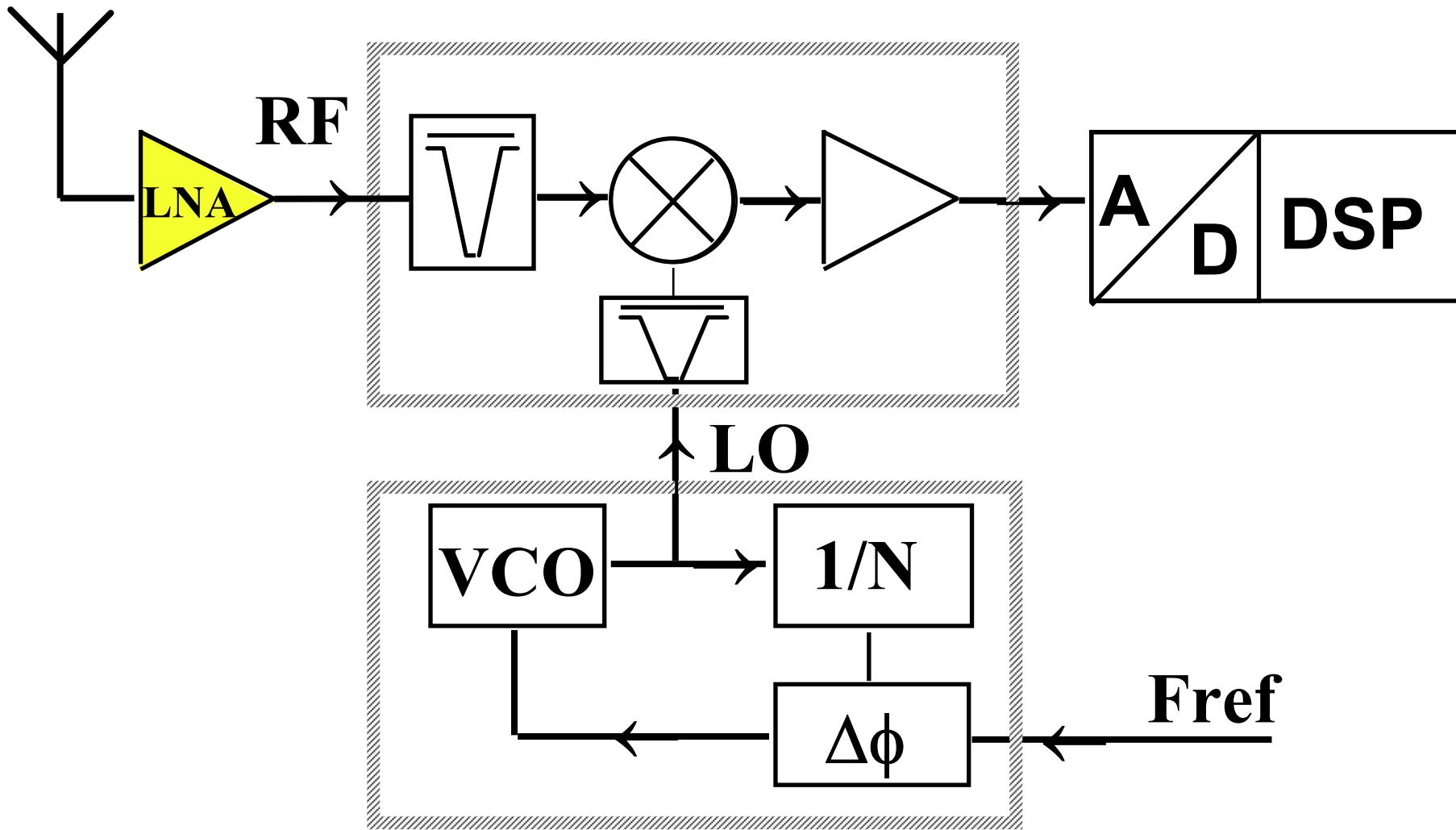
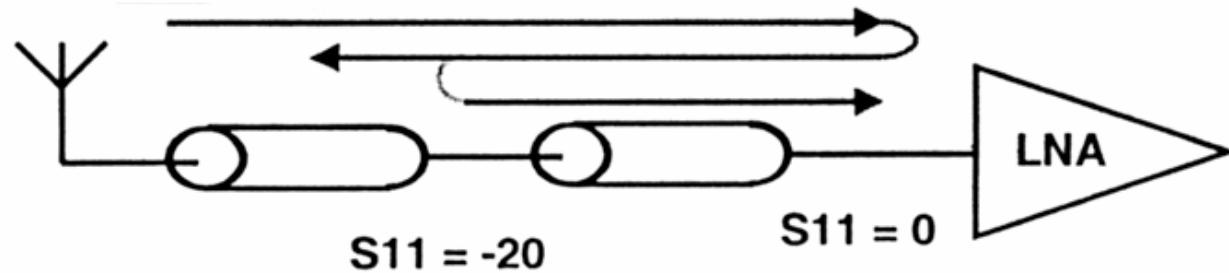


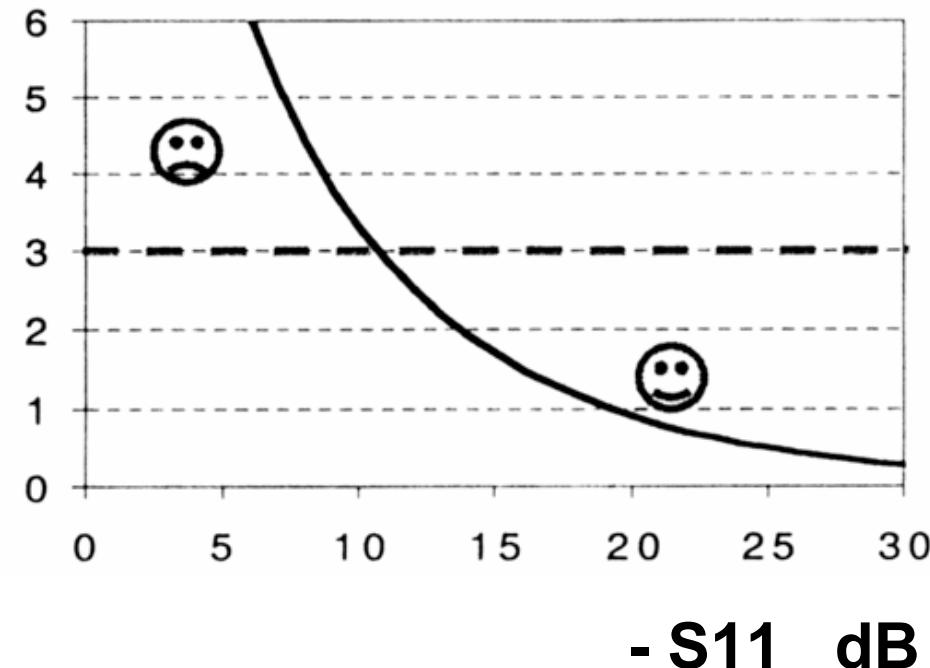
Table of contents

- Noise Figure and Impedance Matching
- LNA specifications and linearity
- Input amplifier or cascode
- Non-quasi-static MOST model
- More realizations
- Inductive ESD protection

Transmission line effects



**Unwanted Signal
over Signal in -dB**



Noise Figure

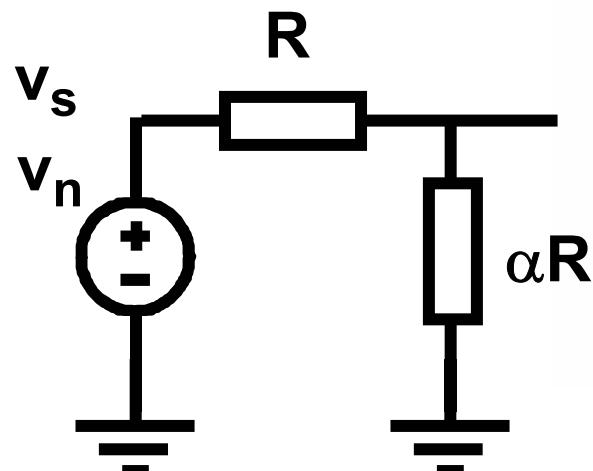
$$V_n = \sqrt{4RkTB}$$

$$V_s = \sqrt{4R.S}$$

$$NF = \frac{\text{total output noise power}}{\text{output noise due to input source}}$$

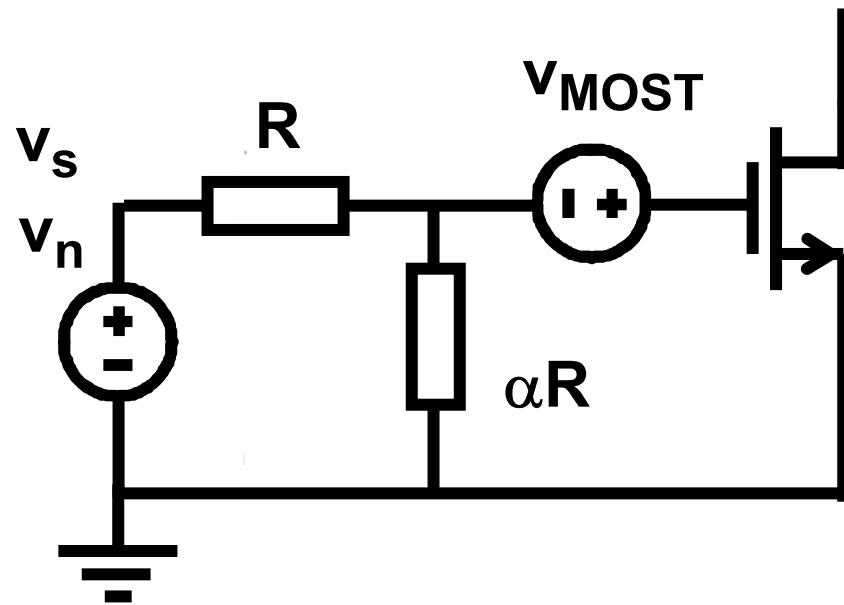
$$NF = \frac{4kTB \left[\frac{\alpha}{(1+\alpha)^2} + \frac{1}{(1+\alpha)^2} \right]}{4kTB \frac{\alpha}{(1+\alpha)^2}}$$

$$NF = \frac{1+\alpha}{\alpha}$$

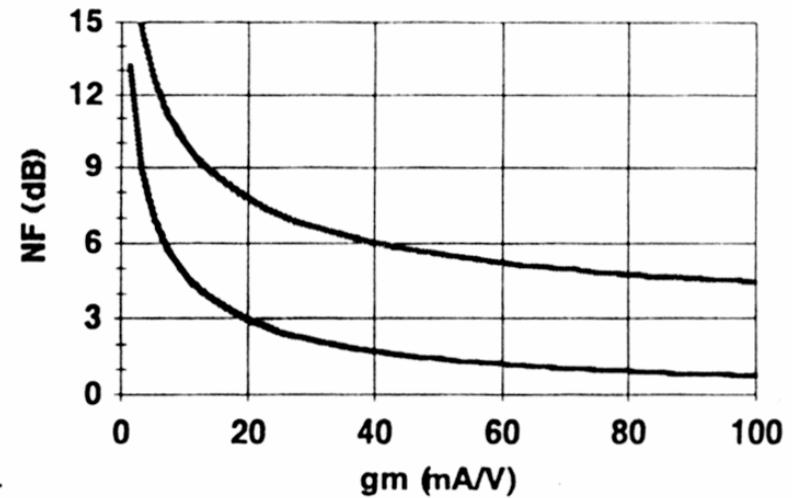


Resistive match : $\alpha = 1$: $NF = 3 \text{ dB}$

MOST amplifier with Resistive termination



$$v_{\text{MOST}} = 4kT \frac{2}{3 g_m}$$



$$NF = \frac{1 + \alpha}{\alpha} + \left(\frac{1 + \alpha}{\alpha} \right)^2 \frac{1}{gm \cdot R}$$

$\alpha = 1$ (Matched):

$\alpha = \infty$ (Open circuit):

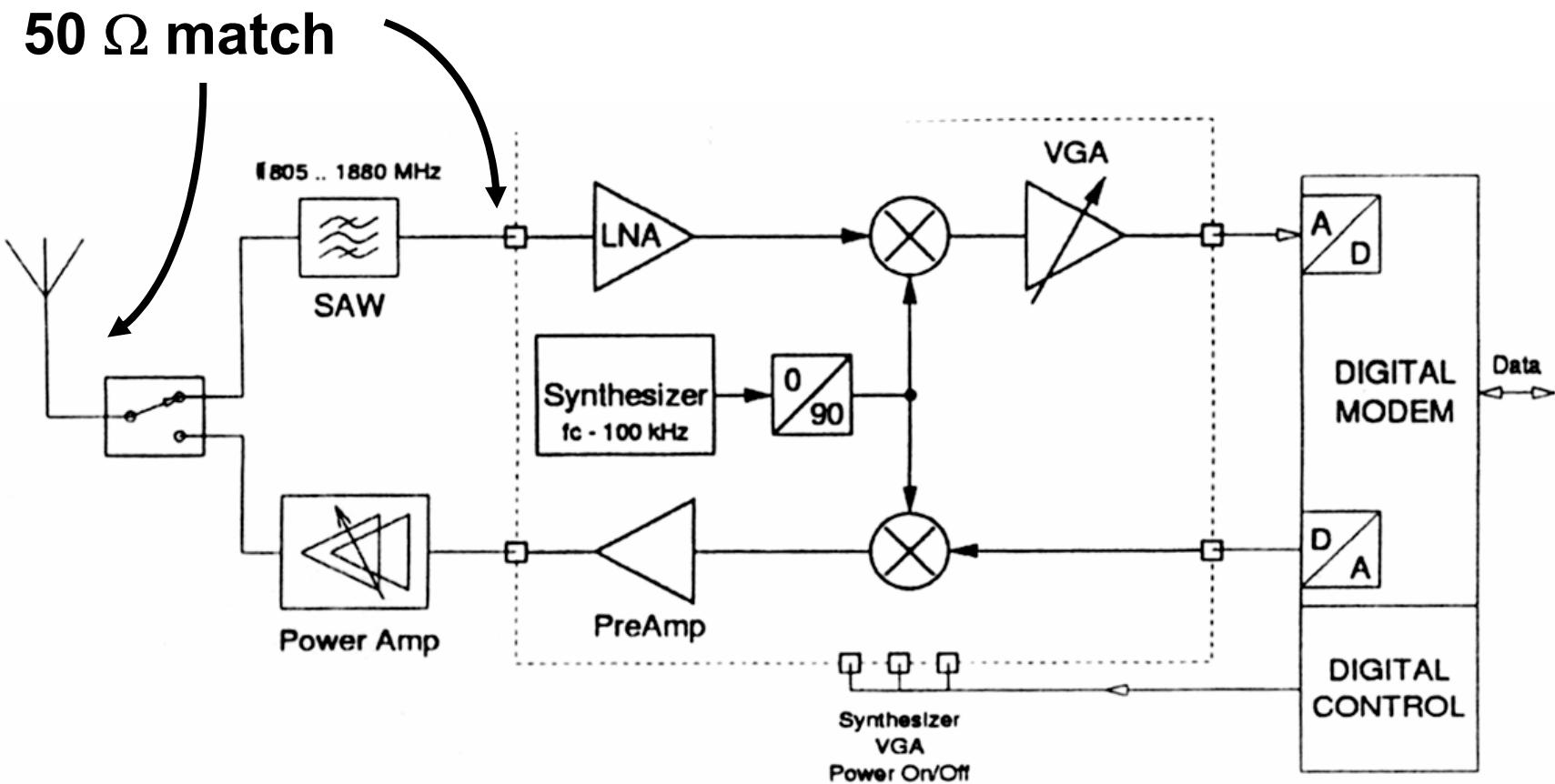
$$NF = 2 + \frac{4}{gm \cdot R}$$

$$NF = 1 + \frac{1}{gm \cdot R}$$

Table of contents

- Noise Figure and Impedance Matching
- LNA specifications and linearity
- Input amplifier or cascode
- Non-quasi-static MOST model
- More realizations
- Inductive ESD protection

Transceiver



Minimum NF and IIP3 for DCS-1800

Sensitivity -100 dBm

SNR 9 dB

Input noise -109 dBm

kT = -174 dBm

Bandwidth (200 kHz) + 53 dB

NF : -109 - (-174+53) = 12 dB

Attenuating blocking filter : 3 dB NF < 9 dB

+ 3 dB Sensitivity -97 dBm

SNR (-49 dBm sine) 9 dB

IIP3 = -49 + (-49- (-106/2)) = -20.5 dBm

With attenuating blocking filter : 3 dB IIP3 < -23.5 dBm

Linearity CMOS amplifier

Velocity saturation

$v_{\max} \approx 10^7 \text{ cm/s}$

$\Theta L \approx 0.2 \mu\text{m/V}$

$$I_{ds} = \frac{\mu_0 C_{ox}}{2n} \cdot \frac{W}{L} \cdot \frac{(V_{GS} - V_T)^2}{1 + \Theta \cdot (V_{GS} - V_T)}$$

$$\Theta = \theta + \frac{\mu_0}{L_{eff} \cdot v_{\max} \cdot n}$$

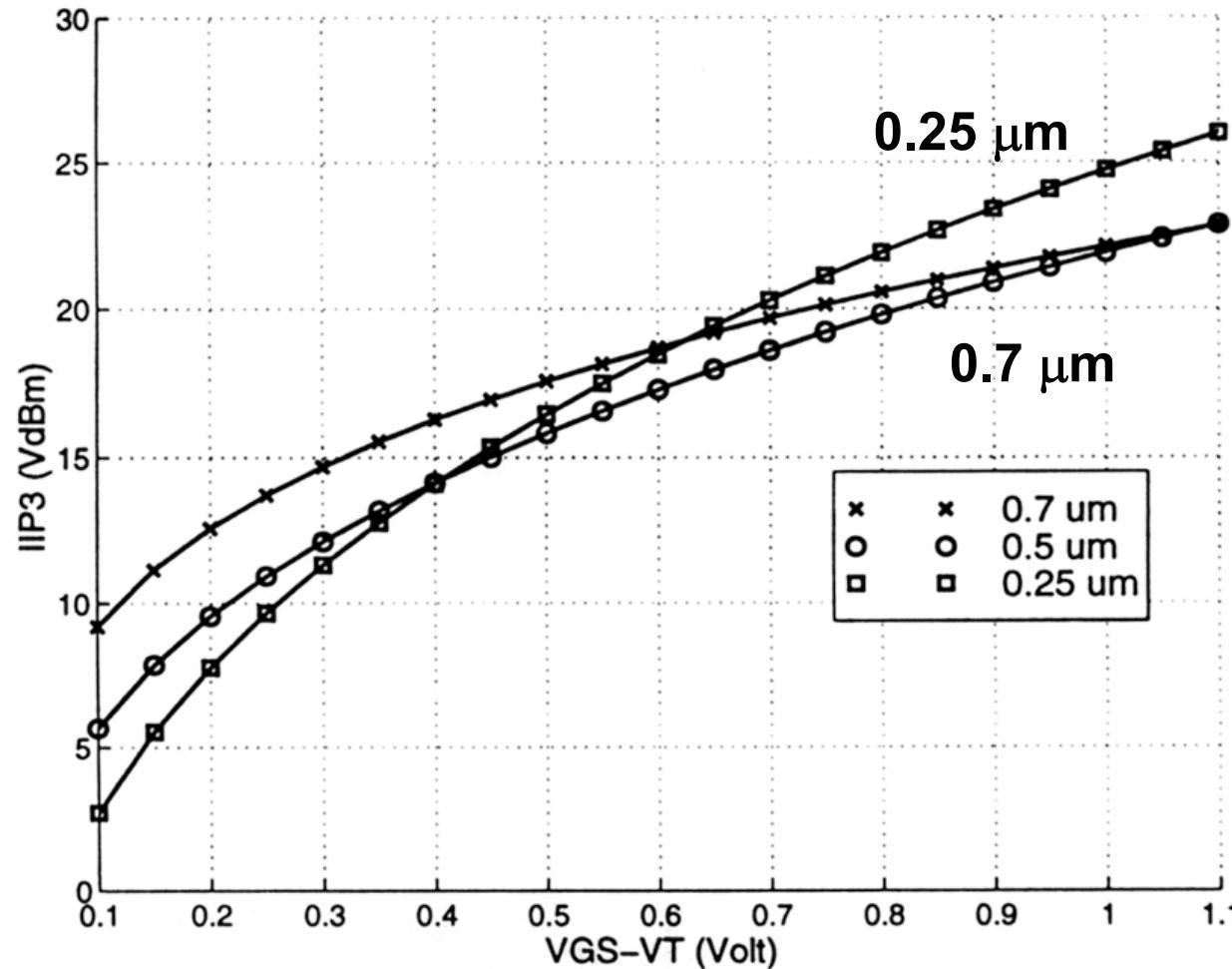
$$IM2 = \frac{v}{V_{GS} - V_T} \cdot \frac{1}{(1+r) \cdot (2+r)}$$

$$r = \Theta \cdot (V_{GS} - V_T)$$

$$IM3 = \frac{3}{4} \frac{v^2}{(V_{GS} - V_T)} \cdot \frac{\Theta}{(1+r)^2 \cdot (2+r)}$$

$$IIP3 \cong 11.25 + 10 \cdot \log_{10} \left((V_{GS} - V_T) \cdot (1+r)^2 \cdot (2+r) / \Theta \right)$$

IIP₃ for different CMOS technologies



Velocity saturation

$v_{max} \approx 10^7 \text{ cm/s}$

$\Theta L \approx 0.2 \mu\text{m/V}$

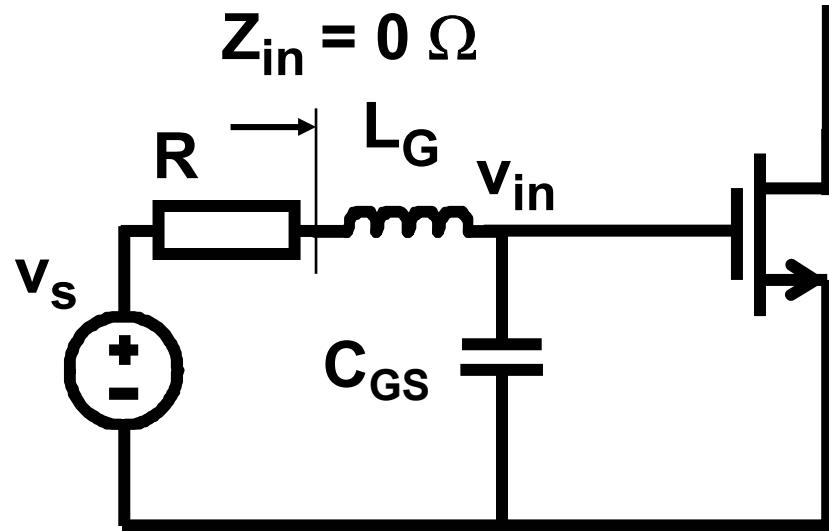
$L = 0.7 \mu\text{m} \quad \Theta \approx 0.5 \text{ V}^{-1}$

$L = 0.25 \mu\text{m} \quad \Theta \approx 1.2 \text{ V}^{-1}$

Table of contents

- Noise Figure and Impedance Matching
- LNA specifications and linearity
- Input amplifier or cascode
- Non-quasi-static MOST model
- More realizations
- Inductive ESD protection

Inductive input : gain



$$Z_{in} = \frac{1}{j\omega C_{GS}} + j\omega L_G$$

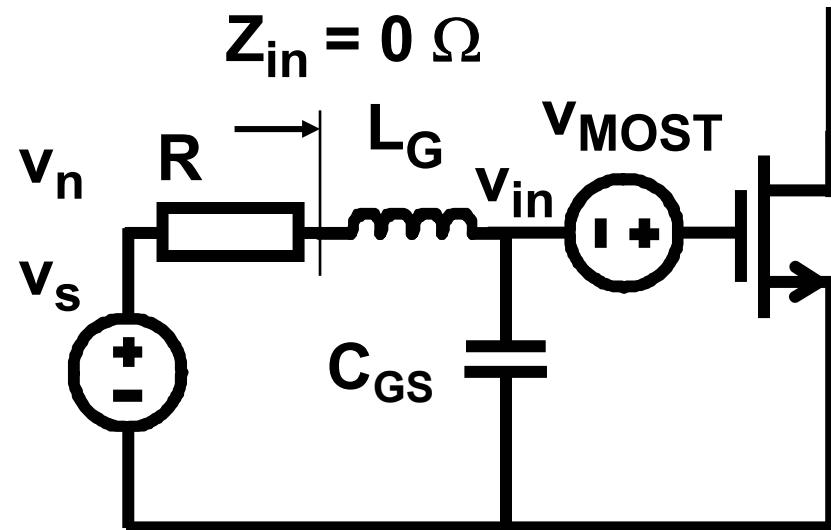
(1) $L_G = \frac{1}{C_{GS} \omega_{in}^2}$

At $f_{in} = \frac{1}{2\pi\sqrt{L_G C_{GS}}}$ (2) $\frac{v_{in}}{v_s} = \frac{1}{R\sqrt{C_{GS}/L_G}} = \frac{1}{2\pi RC_{GS}\omega_{in}}$

Extra Gain ≈ 10 dB

$L_G = 15$ nH; $C_{GS} = 0.5$ pF; $f_{in} = 1.8$ GHz ; $R = 50 \Omega$;

Inductive input : noise



$$v_{MOST} = 4kT \frac{2}{3 g_m}$$

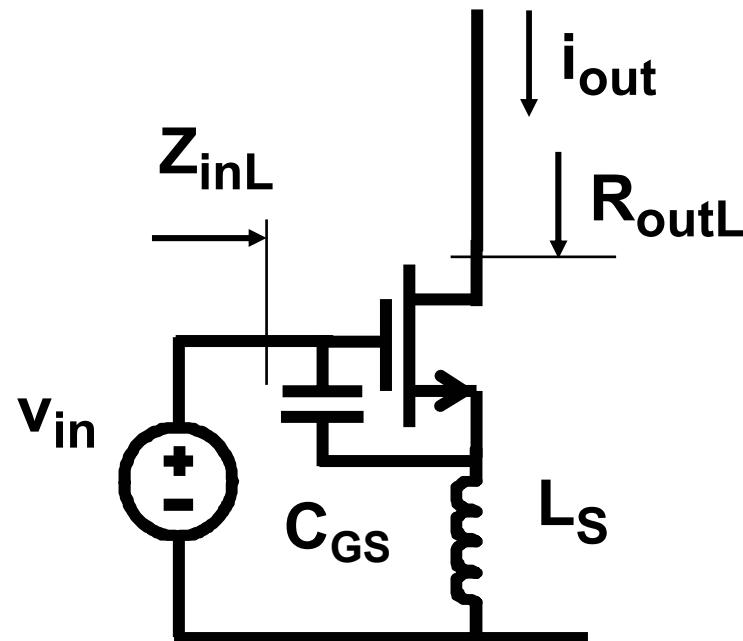
$$\frac{v_{in}}{v_s} = \frac{1}{R \sqrt{C_{GS} / L_G}}$$

$$NF = 1 + \frac{(R \sqrt{C_{GS} / L_G})^2}{g_m R} = 1 + \frac{R C_{GS}}{g_m L_G} = 1 + g_m R \left(\frac{\omega_{in}}{\omega_T} \right)^2$$

$$NF_{gmR=1} \approx 0.4 \text{ dB}$$

$L_G = 15 \text{ nH}$; $C_{GS} = 0.5 \text{ pF}$; $f_{in} = 1.8 \text{ GHz}$

Inductive degeneration in the Source



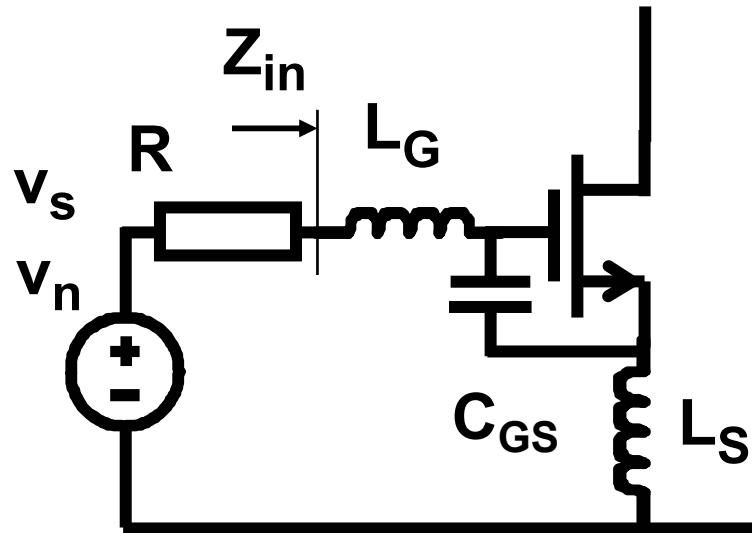
$$g_{mL} = \frac{g_m}{1 + g_m L_S s}$$

$$R_{outL} = r_{DS} (1 + g_m L_S s)$$

$$Z_{inL} = g_m \frac{L_S}{C_{GS}} + \frac{1 + L_S C_{GS} s^2}{s C_{GS}}$$

$$Z_{inL} = L_S \omega_T + L_S s + \frac{1}{s C_{GS}}$$

Inductive degeneration in Source and Gate



$$Z_{in} = \frac{1}{j\omega C_{GS}} + j\omega (L_G + L_S) + \omega_T L_S$$

1

$$L_G + L_S = \frac{1}{C_{GS} \omega_{in}^2}$$

2

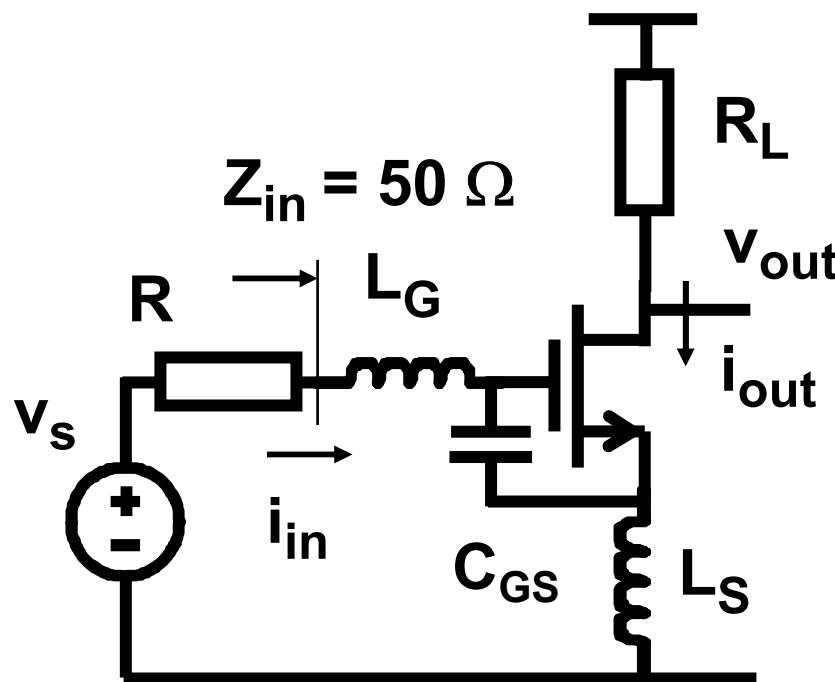
$$L_S = \frac{R C_{GS}}{g_m} = \frac{R}{\omega_T}$$

Impedance Match :

$\text{Re}(Z_{in}) = R_{in} = R \text{ at } \omega_{in}$

$\text{Im}(Z_{in}) = 0$

Inductive degeneration : gain



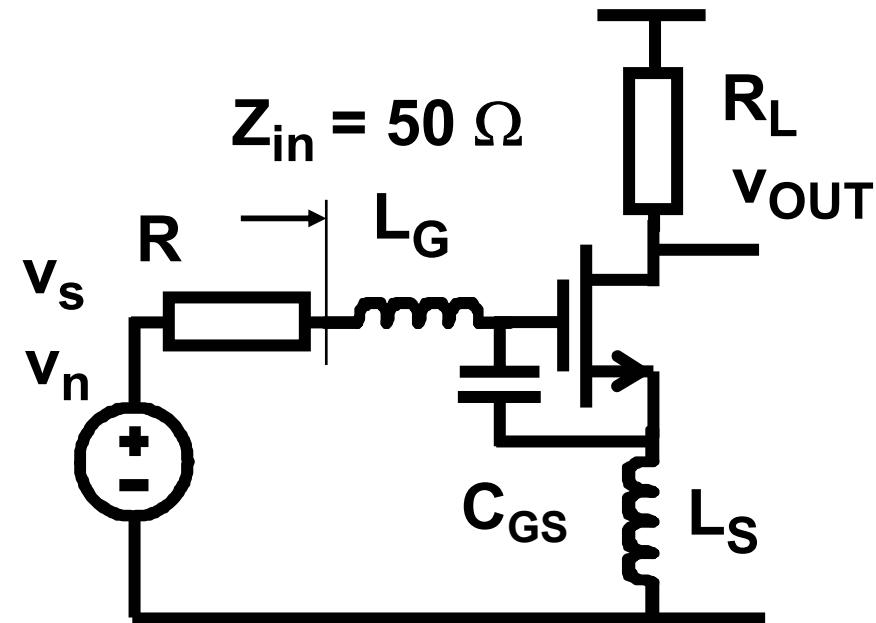
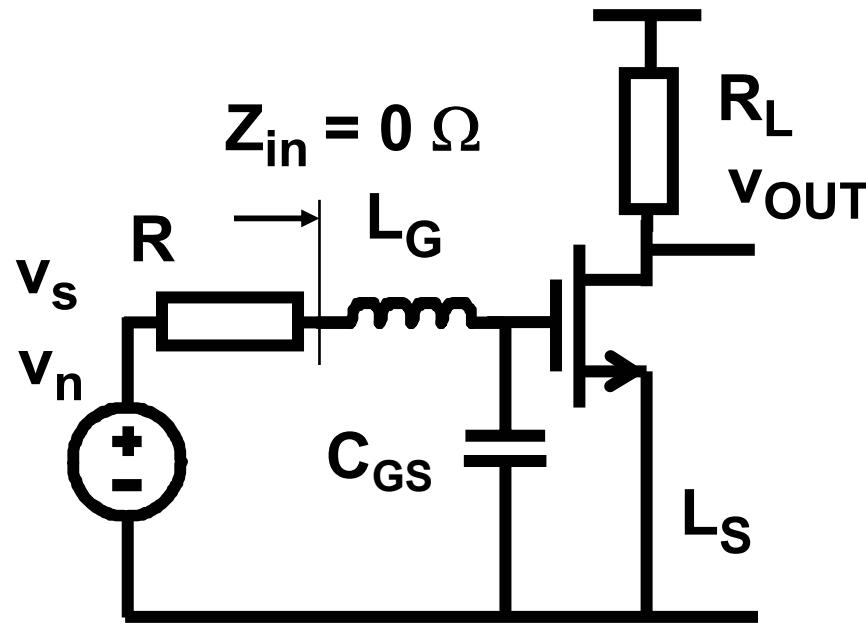
Under matching :

$$\frac{i_{out}}{i_{in}} = \frac{\omega_I}{\omega_{in}}$$

$$\frac{v_{out}}{v_{in}} = \frac{i_{out}}{i_{in}} \frac{R_L}{2R}$$

$$G_P = \frac{P_{out}}{P_{in}} = \left(\frac{\omega_I}{\omega_{in}} \right)^2 \frac{R_L}{2R}$$

Inductive degeneration : gain



$$G_v = \frac{g_m}{\sqrt{C_{GS}/L_G}} \frac{R_L}{R}$$

$$G_v = \frac{g_m}{\sqrt{C_{GS}/(L_G + L_S)}} \frac{R_L}{2R}$$

$$G_v / G_{v,R=50\Omega} = 2x$$

Inductive degeneration : Noise Figure

$$NF = 1 + \frac{dv_{in}^2}{dv_R^2} = 1 + \frac{R C_{GS}}{g_m (L_G + L_S)}$$

$$dv_{in}^2 = 4kT \frac{2/3}{g_m} df \approx 4kT \frac{1}{g_m} df$$

$$dv_R^2 = 4kT R df$$

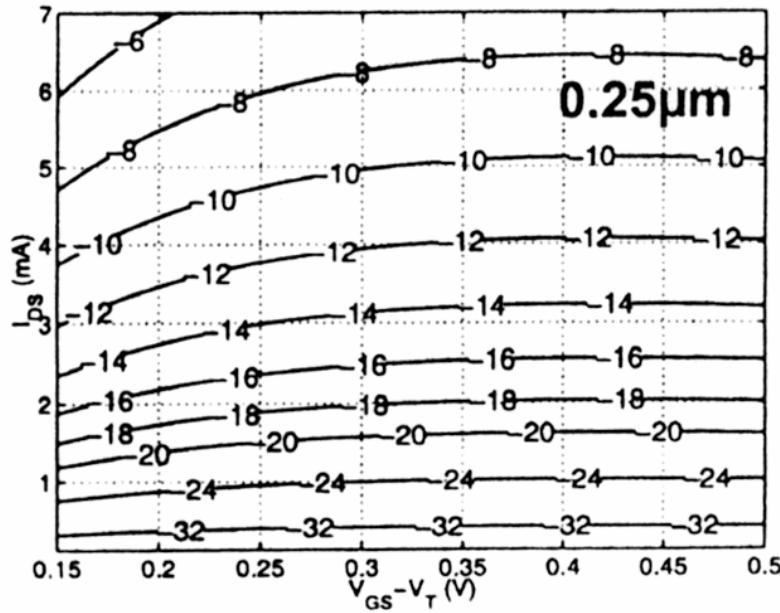
$$NF = 1 + g_m R \left(\frac{\omega_{in}}{\omega_T} \right)^2$$

Inductive degeneration : IIP3 vs IDS

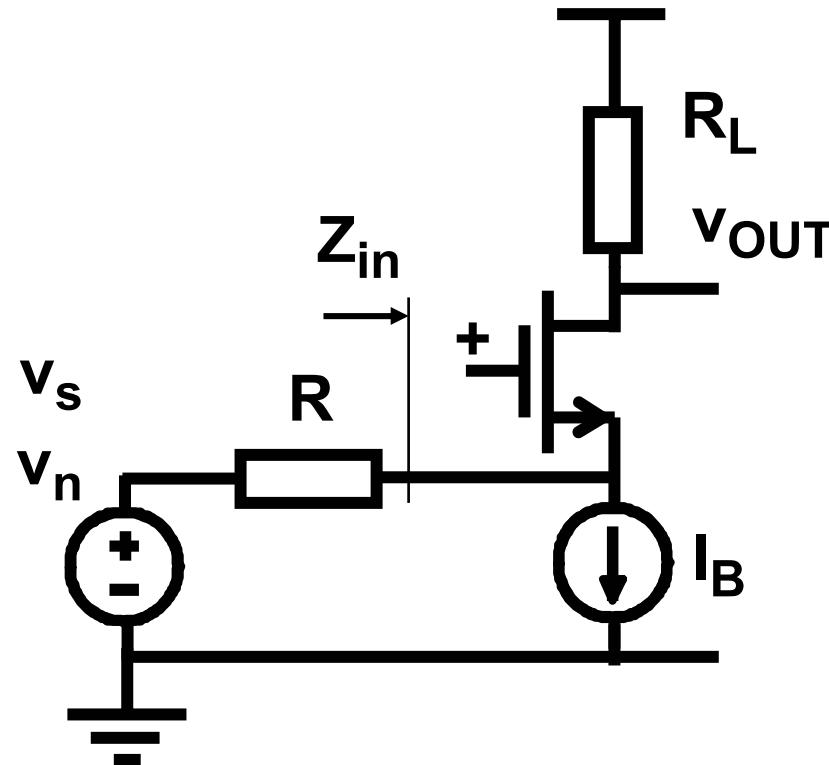
$$IIP3 \approx 11.25 + 20 \log_{10} \left(\underbrace{\frac{Vgst(2+r)^2(1+r)}{\Theta} \frac{1+\Theta Vgst}{Vgst^2} \cdot \omega_{in} \frac{100}{\mu_0} I_D L^2}_{\approx Cst} \right)$$

$$IIP3 \approx Cst + 20 \log_{10} \left(\frac{\omega_{in} I_D L^2}{\mu_0} \right)$$

$$r = \Theta V_{gst} = \Theta (V_{GS} - V_T)$$



Cascode or current input : Z_{in}



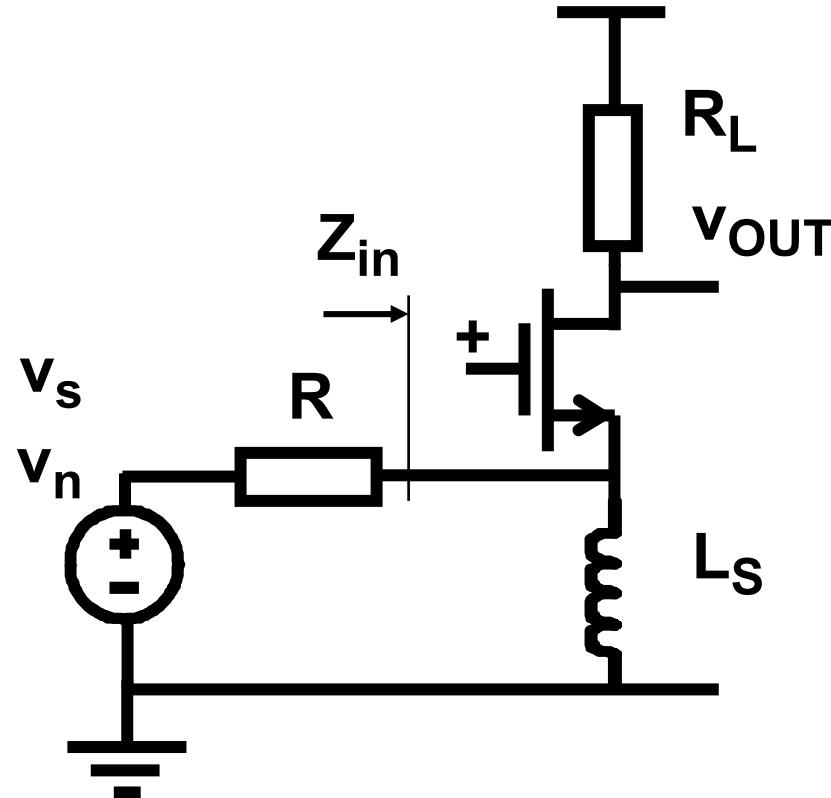
$$R_{in} = \frac{1}{g_m}$$

$= 50 \Omega \text{ at } 20 \text{ mS}$

$$R_{in} = \frac{1}{g_m} \frac{1}{n} \left(1 - \frac{R_L}{2r_{DS}} \right)$$

Depends on r_{DS} !

Cascode or current input : Gain & NF



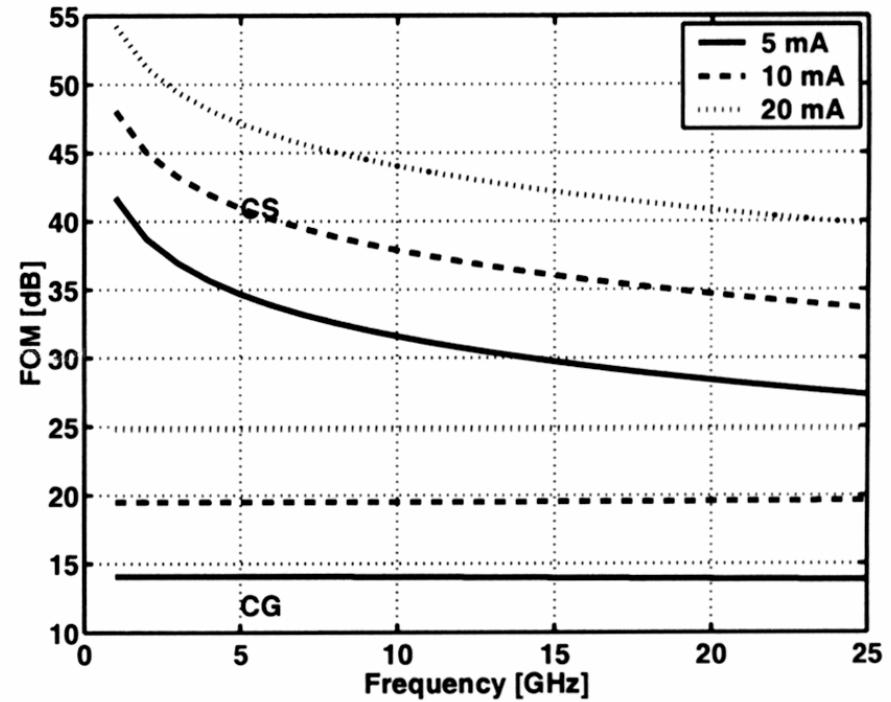
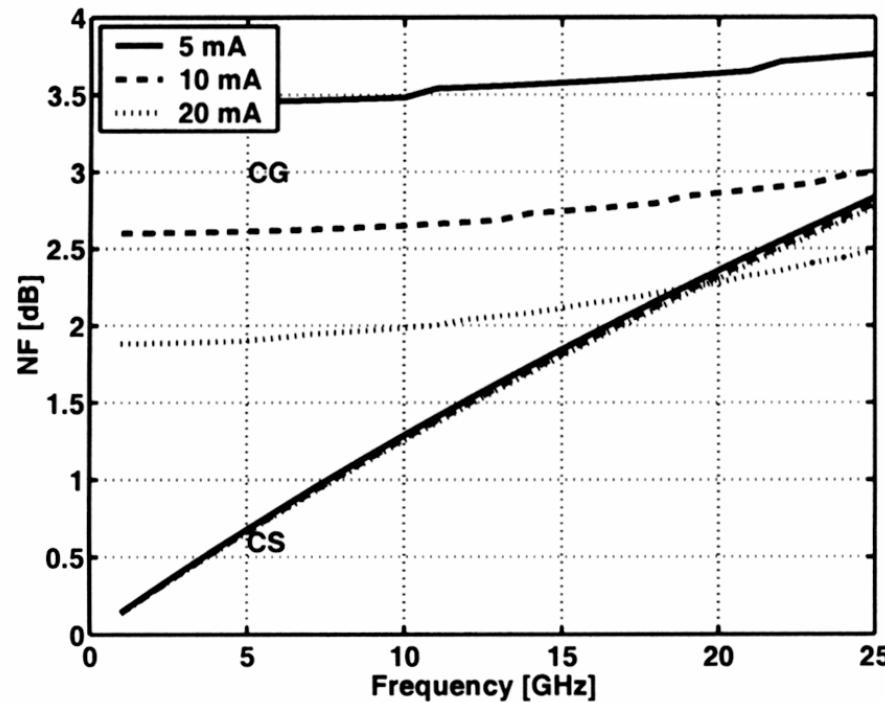
$$\frac{i_{out}}{i_{in}} = 1$$

$$G_P = \frac{P_{out}}{P_{in}} = \frac{R_L}{4R}$$

$$NF = 1 + \frac{1}{g_m R}$$

Match : $NF = 3 \text{ dB}$

LNA : amplifier versus cascode

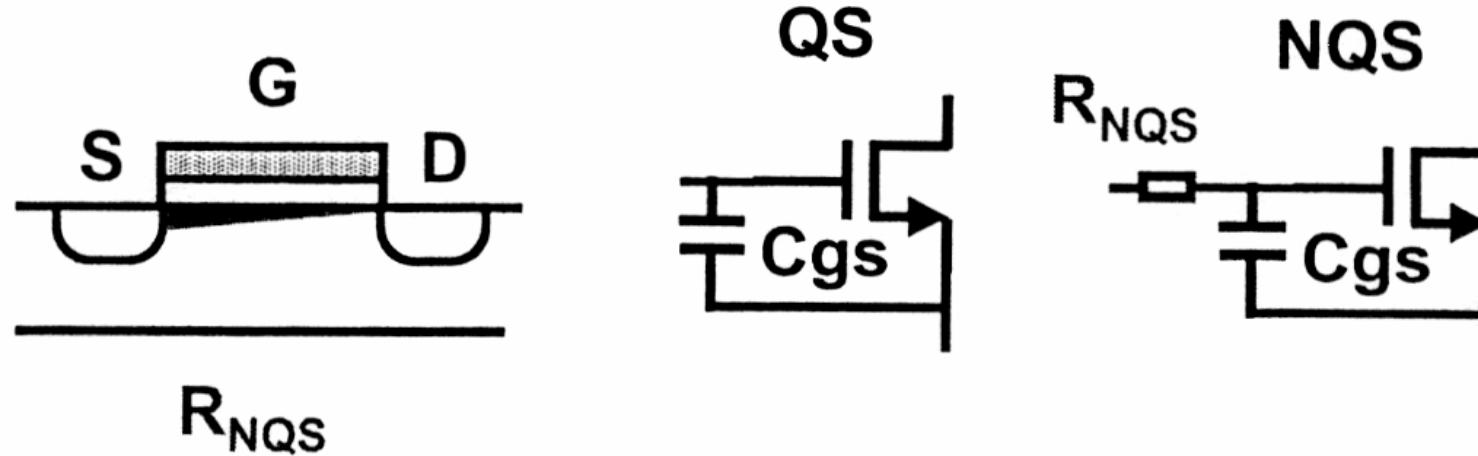


$$FOM = \frac{G_P IIP_3}{NF - 1}$$

Table of contents

- Noise Figure and Impedance Matching
 - LNA specifications and linearity
 - Input amplifier or cascode
 - Non-quasi-static MOST model
-
- More realizations
 - Inductive ESD protection

Non-quasi static MOST model



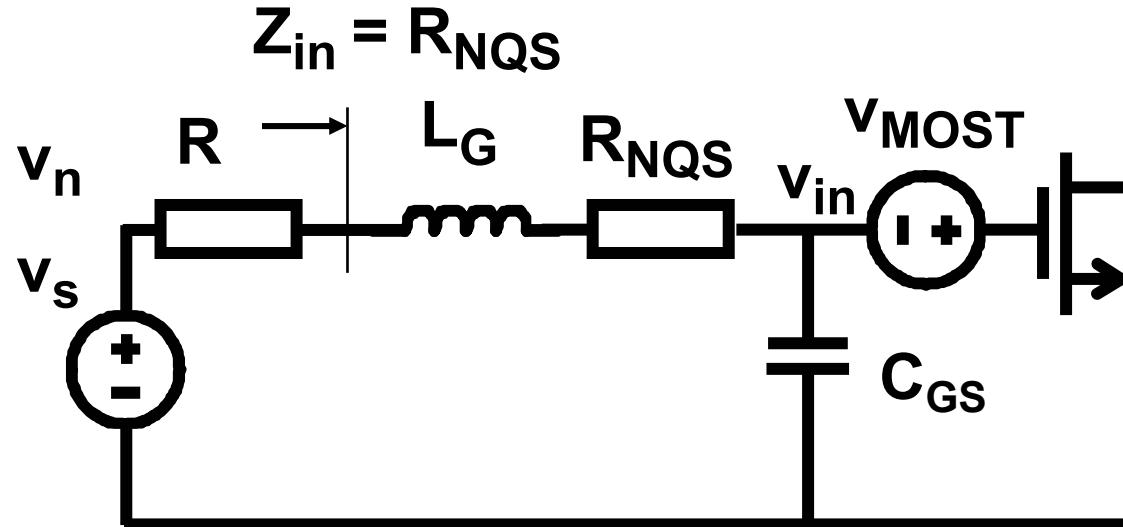
$$R_{NQS} = \frac{1}{5 g_m}$$

Normally important for $f > f_T / 5$

C_{GS} is tuned out by L_G !!

Ref.Janssens, ACD 1998

Inductor in input

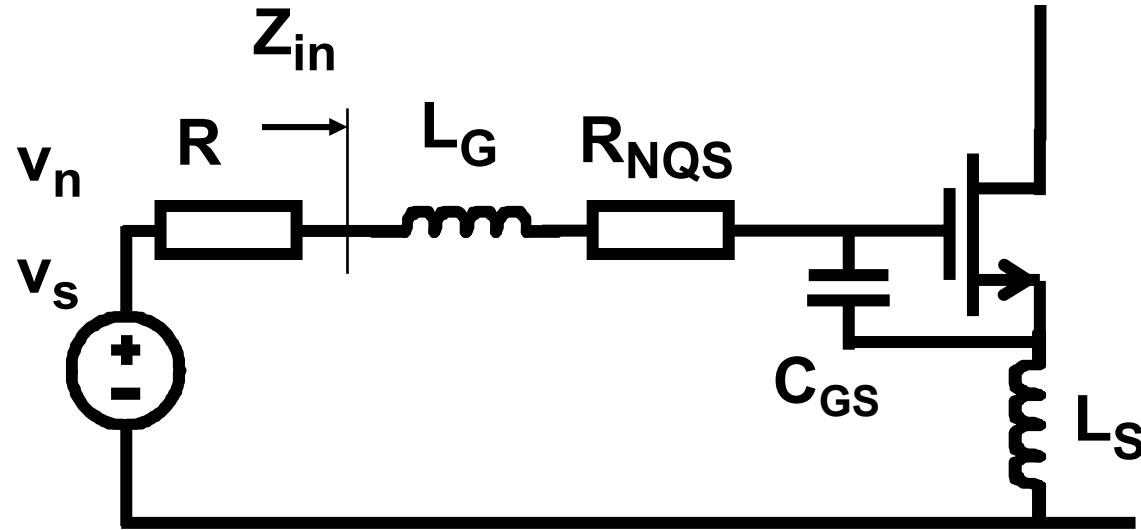


$$NF = 1 + \frac{R \cdot C_{gs}}{gm \cdot L_g} \left(1 + \frac{R_{NQS}}{R}\right)^2 + \frac{R_{NQS}}{R}$$

$$\text{NF}_{gm=20mS} = 1.2 \text{ dB}$$

$$NF = 1 + \frac{R \cdot C_{gs}}{gm \cdot L_g} \left(1 + \frac{1}{5gmR}\right)^2 + \frac{1}{5gmR}$$

Inductive degeneration with NQS model



$$\omega^2 C_{gs} (L_g + L_s) = 1$$

$$L_s = \frac{(R - R_{NQS})C_{gs}}{gm}$$

$$NF = 1 + \frac{R.C_{gs}}{gm(L_g + L_s)} \left(1 + \frac{R_{NQS}}{R}\right)^2 + \frac{R_{NQS}}{R}$$

$$NF_{gm=20mS} = 1.2 \text{ dB}$$

Noise matching

$$NF = 1 + \frac{R.Cgs}{gm.(Lg + Ls)} \left(1 + \frac{1}{5gmR}\right)^2 + \frac{1}{5gmR}$$

Optimum $R = \frac{1}{5gm} \cdot \sqrt{1 + \frac{5.(Lg + Ls)gm^2}{Cgs}} = 80\Omega$

NF ≈ 1 dB (g_m = 20 mS)

L_G+L_S = 15 nH; C_{GS} = 0.5 pF; f = 1.8 GHz

Noise matching (Optimum design)

$$NF = 1 + \frac{R.Cgs}{gm.(Lg + Ls)} \left(1 + \frac{1}{5gmR}\right)^2 + \frac{1}{5gmR}$$

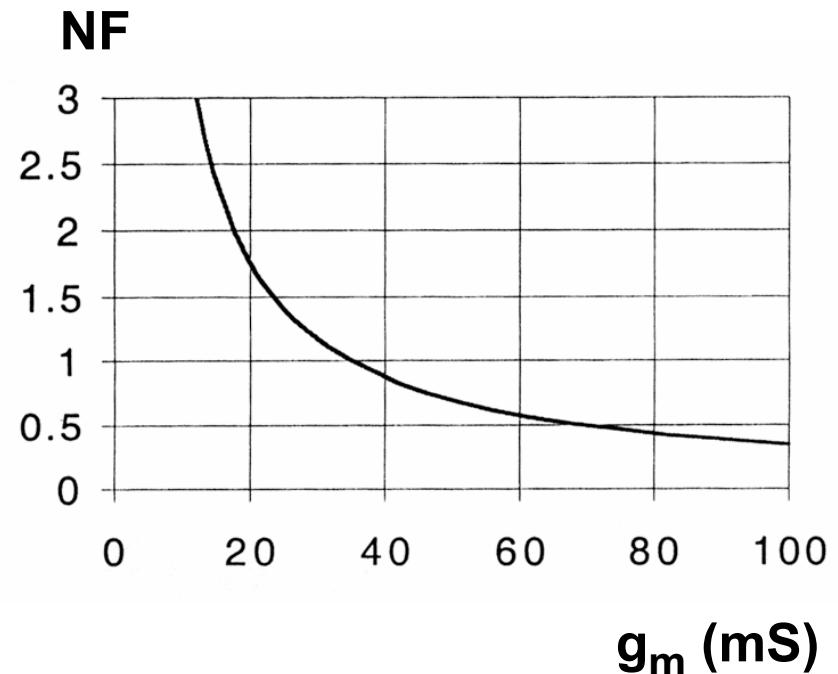
Opt. $Cgs = \frac{5.(Lg + Ls)gm^2}{(5.Rgm)^2 - 1}$

$$NF = 1 + \frac{5gmR}{(5gmR)^2 - 1} \left(1 + \frac{1}{5gmR}\right)^2 + \frac{1}{5gmR}$$

$$NF \approx 1 + \frac{2}{5gmR}$$

$g_m R > 1$

Lower NF requires more power !



Gain vs Rin for optimal NF

$$G = \frac{gm}{\sqrt{\frac{5gm^2}{(5gmR)^2 - 1}}} \cdot \frac{R_L}{(R + R_{in})}$$

Gain + 2dB

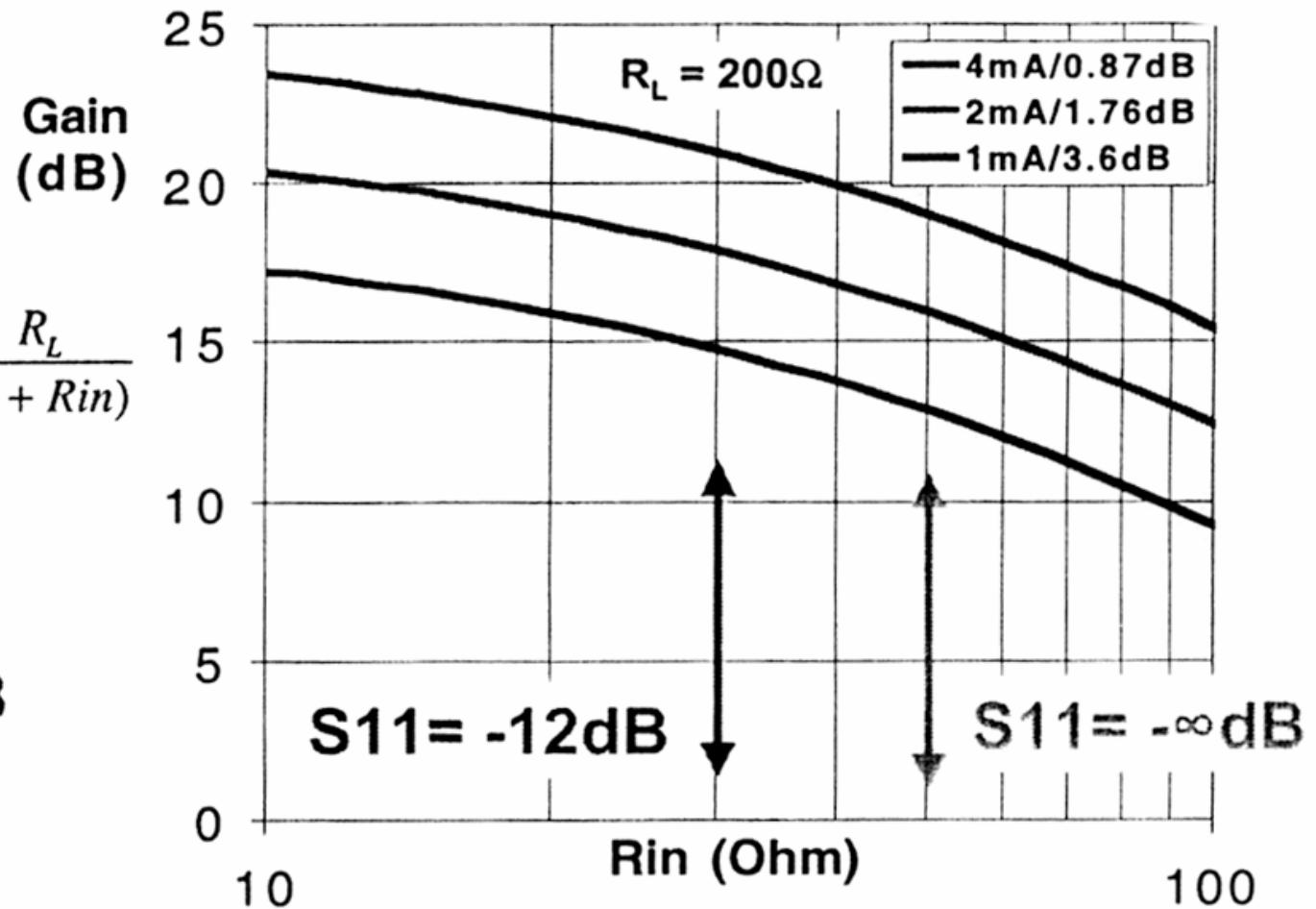
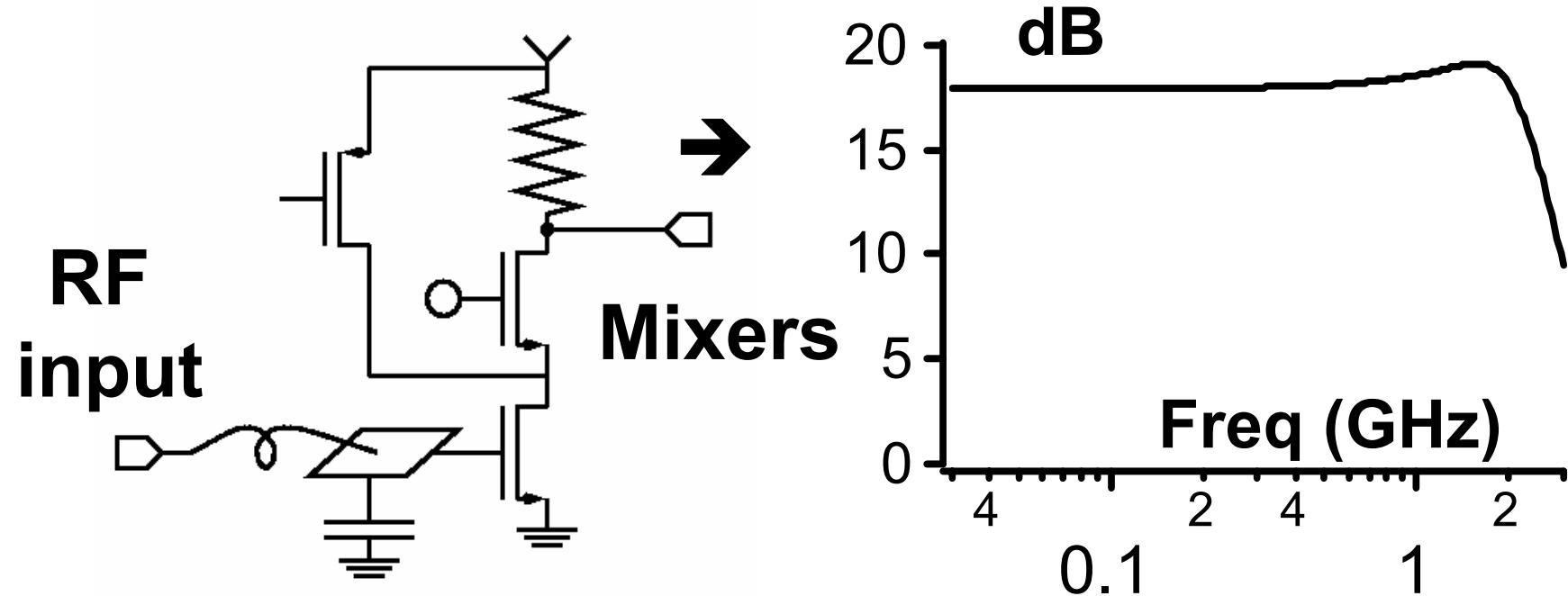


Table of contents

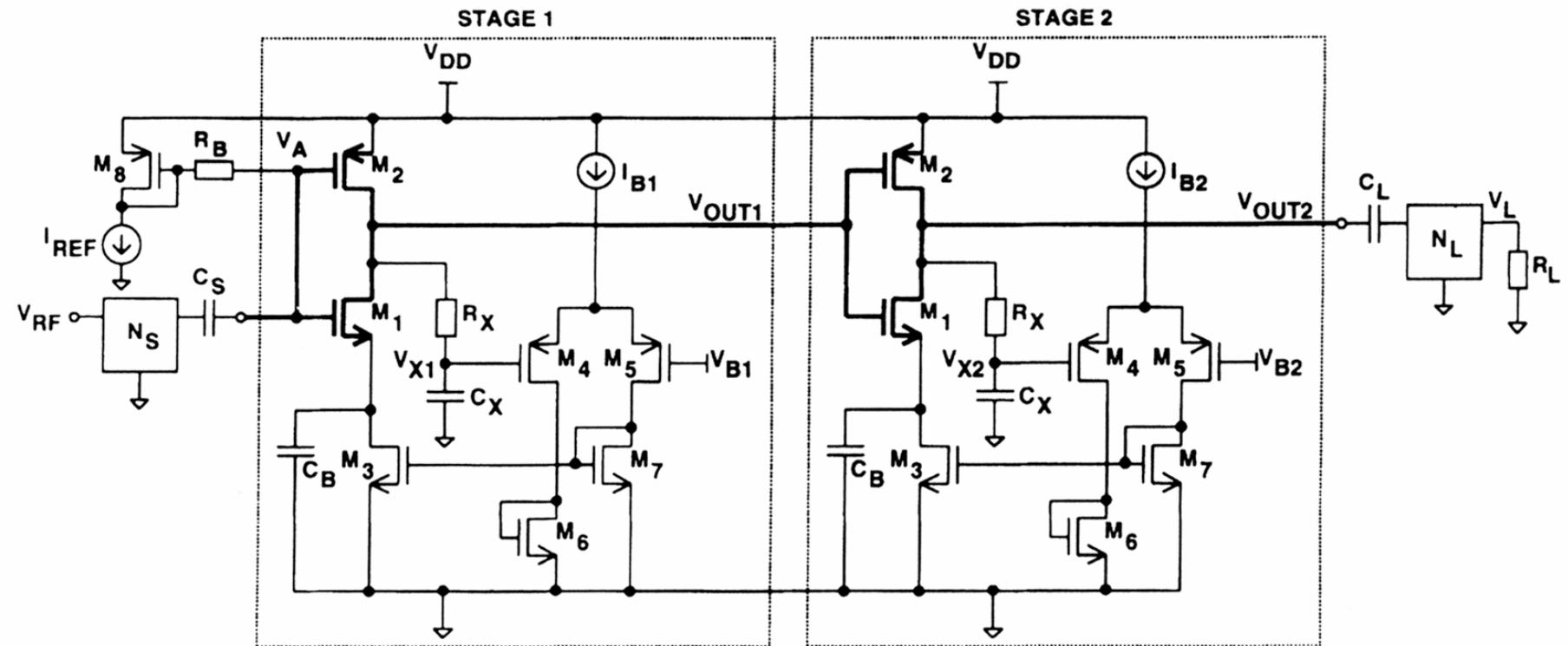
- Noise Figure and Impedance Matching
- LNA specifications and linearity
- Input amplifier or cascode
- Non-quasi-static MOST model
- More realizations
- Inductive ESD protection

Low-noise amplifier



Broad-Band Topology : multi-mode possible

LNA 900 MHz with reuse



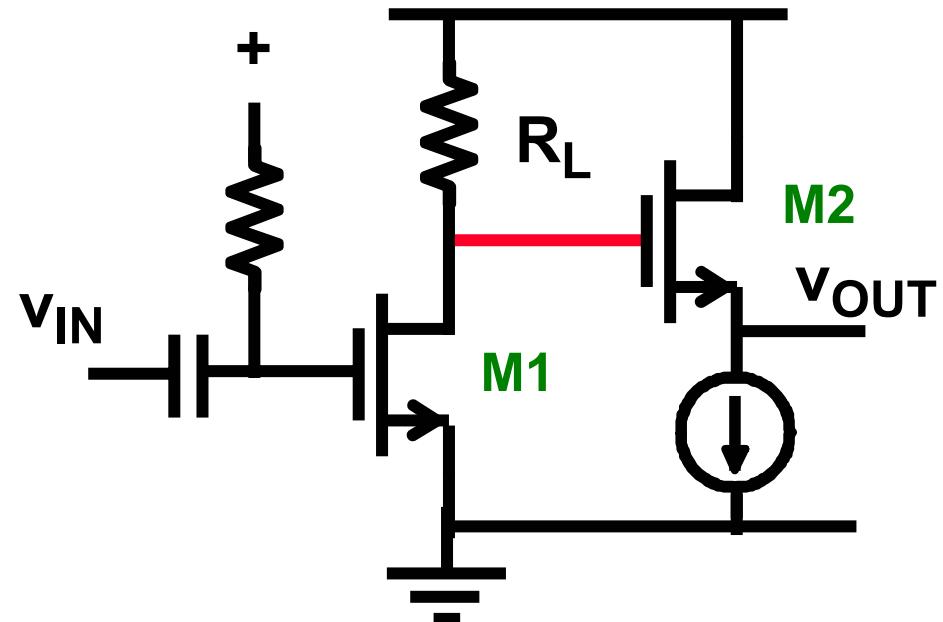
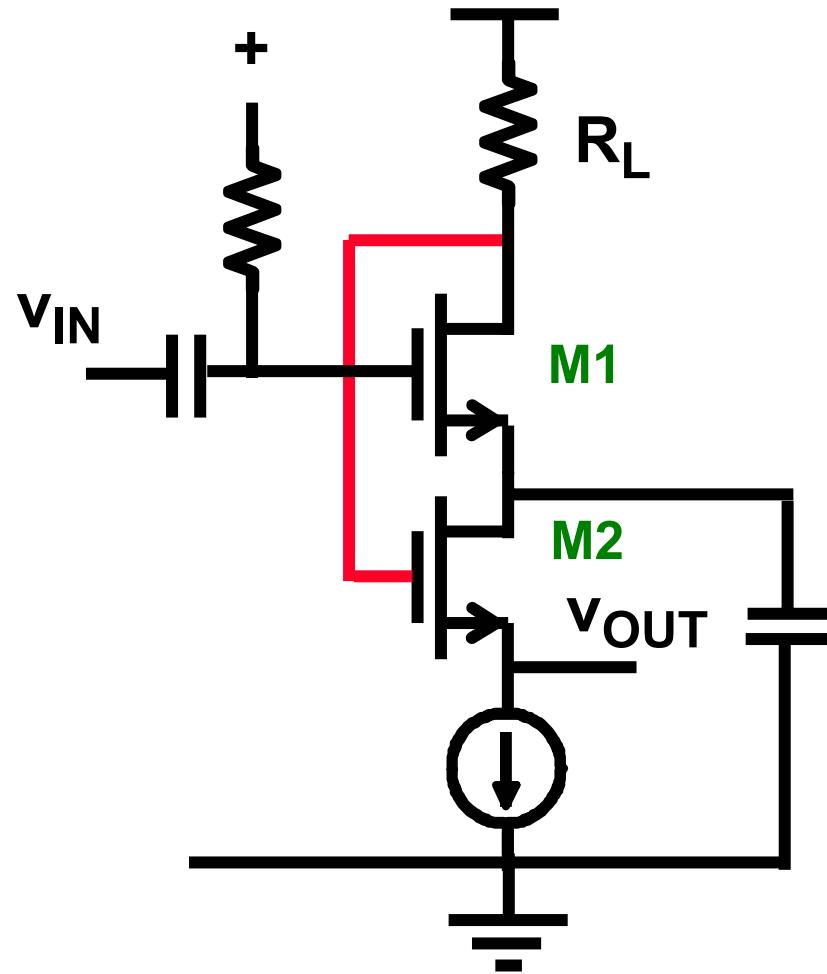
$NF = 2.2 \text{ dB}$

$G = 15.6 \text{ dB}$

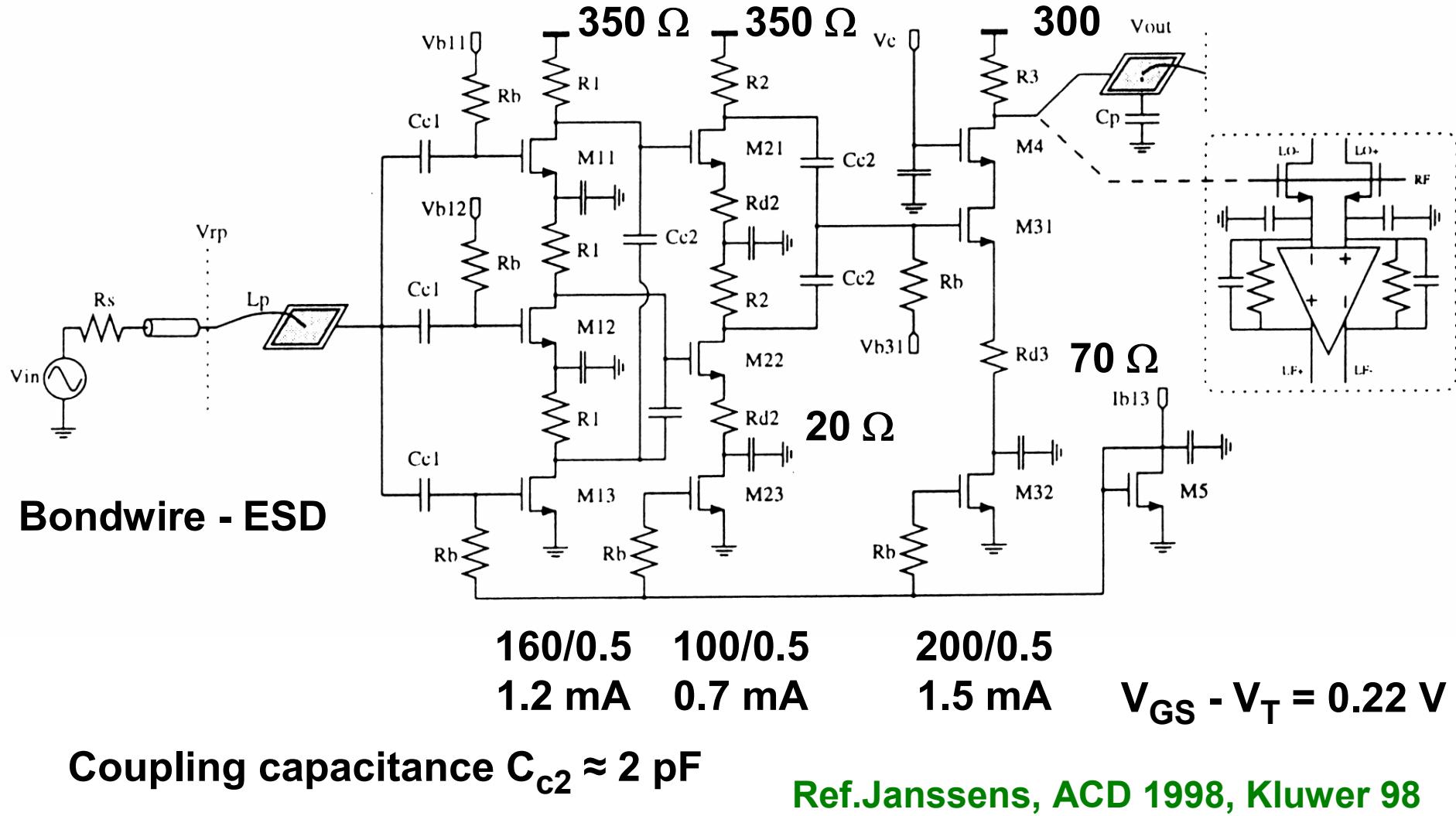
$P = 20 \text{ mW (2.7 V)}$

Karanicolas, JSSC Dec 96, 1939-1944

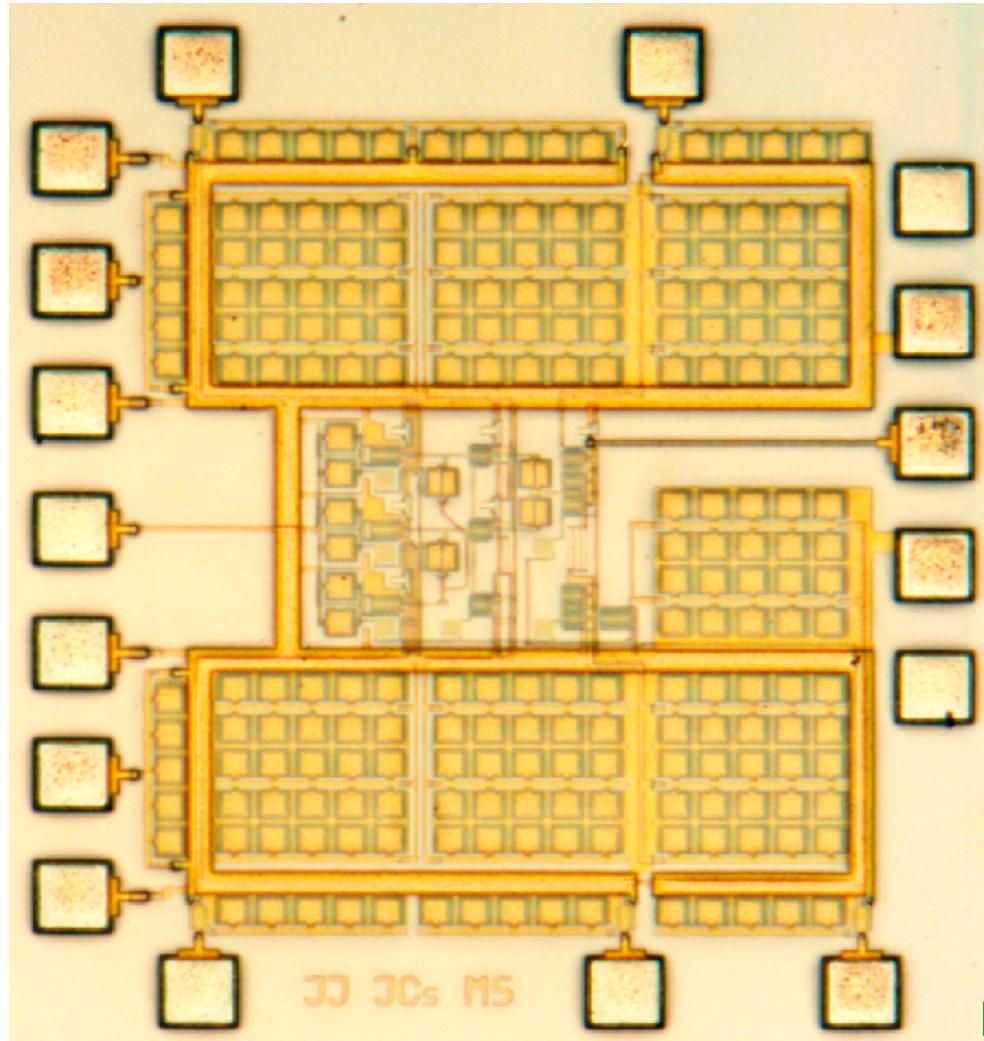
LNA with reuse



LNA with reuse : realization



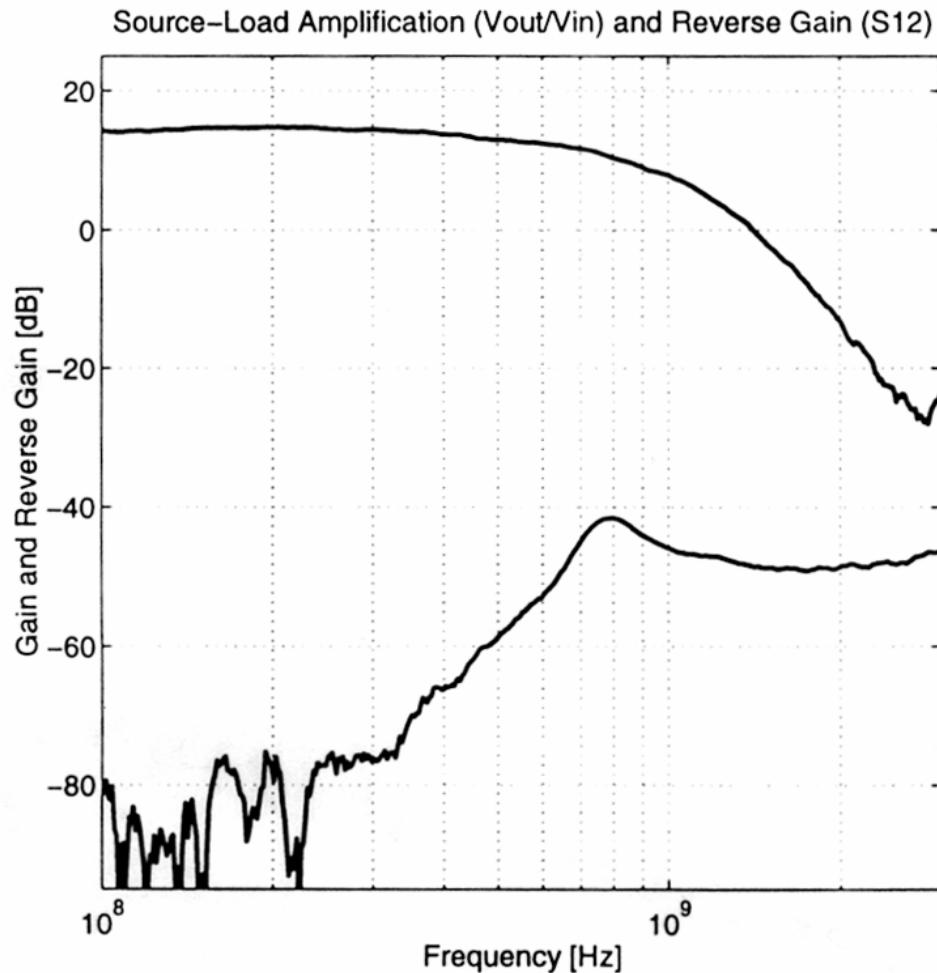
CMOS LNA with reuse



Fin	900 MHz
Power	10 mW
NF	2.3-3.3 dB
Gain	14.8 dB
IIP3	-4.7 VdBm
S11	-7 dB
Area	0.12 mm²

Ref.Janssens, M.Steyaert, CICC'98

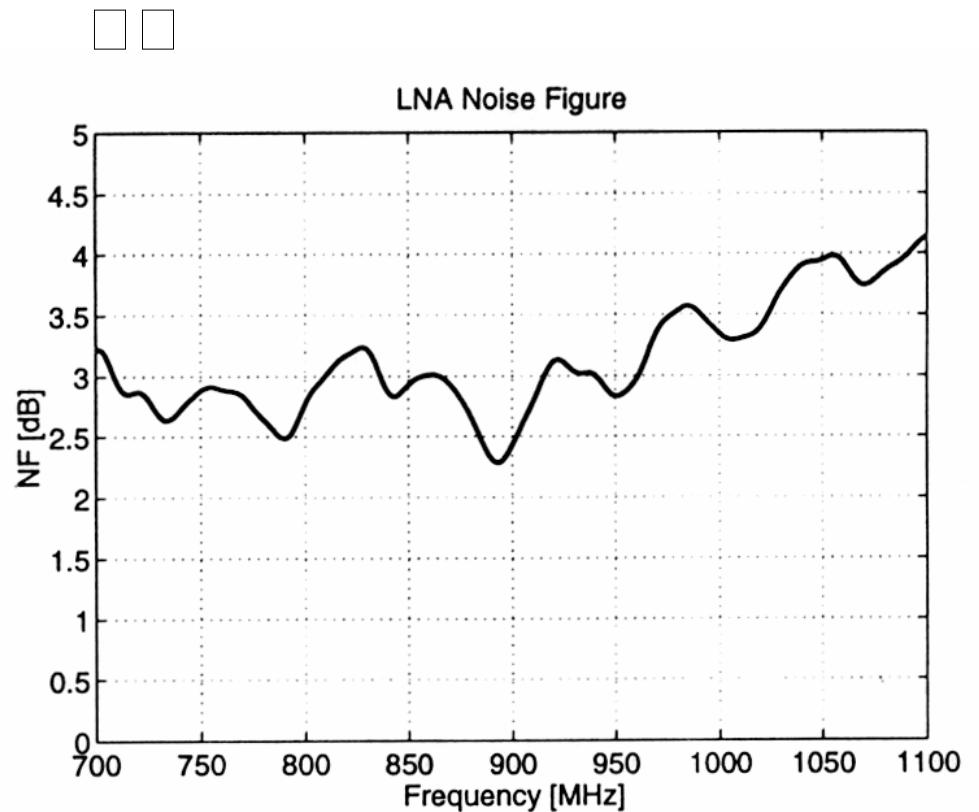
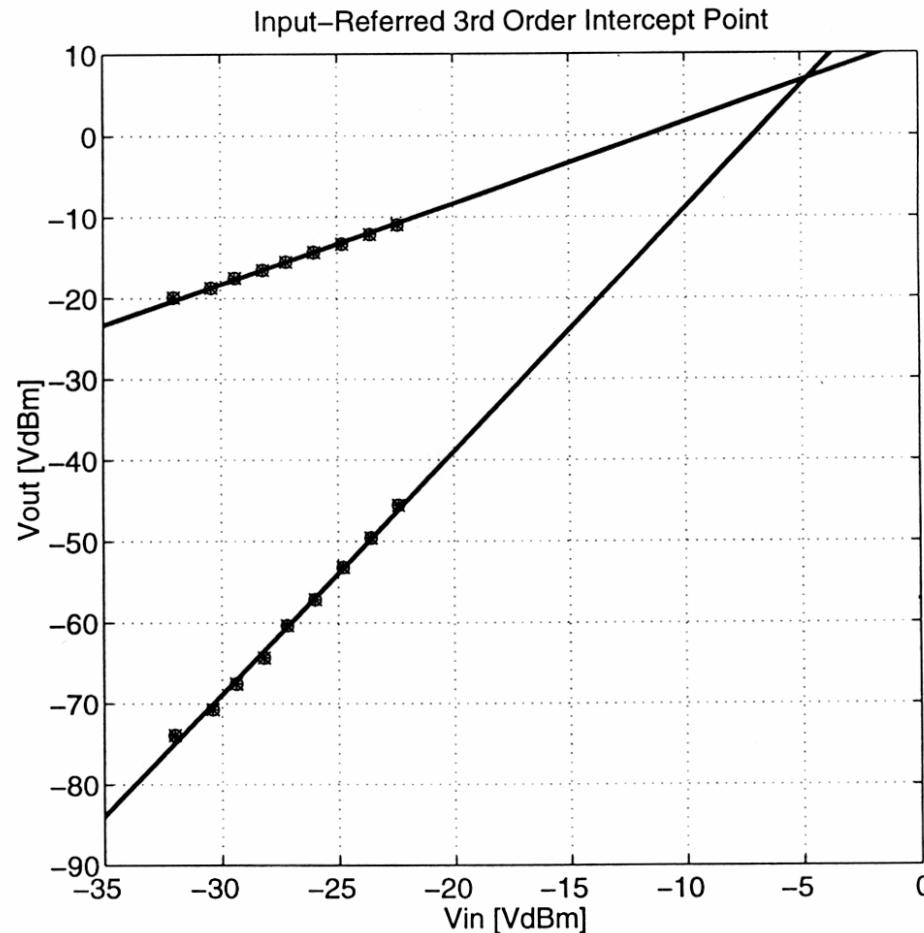
Measurements - 1



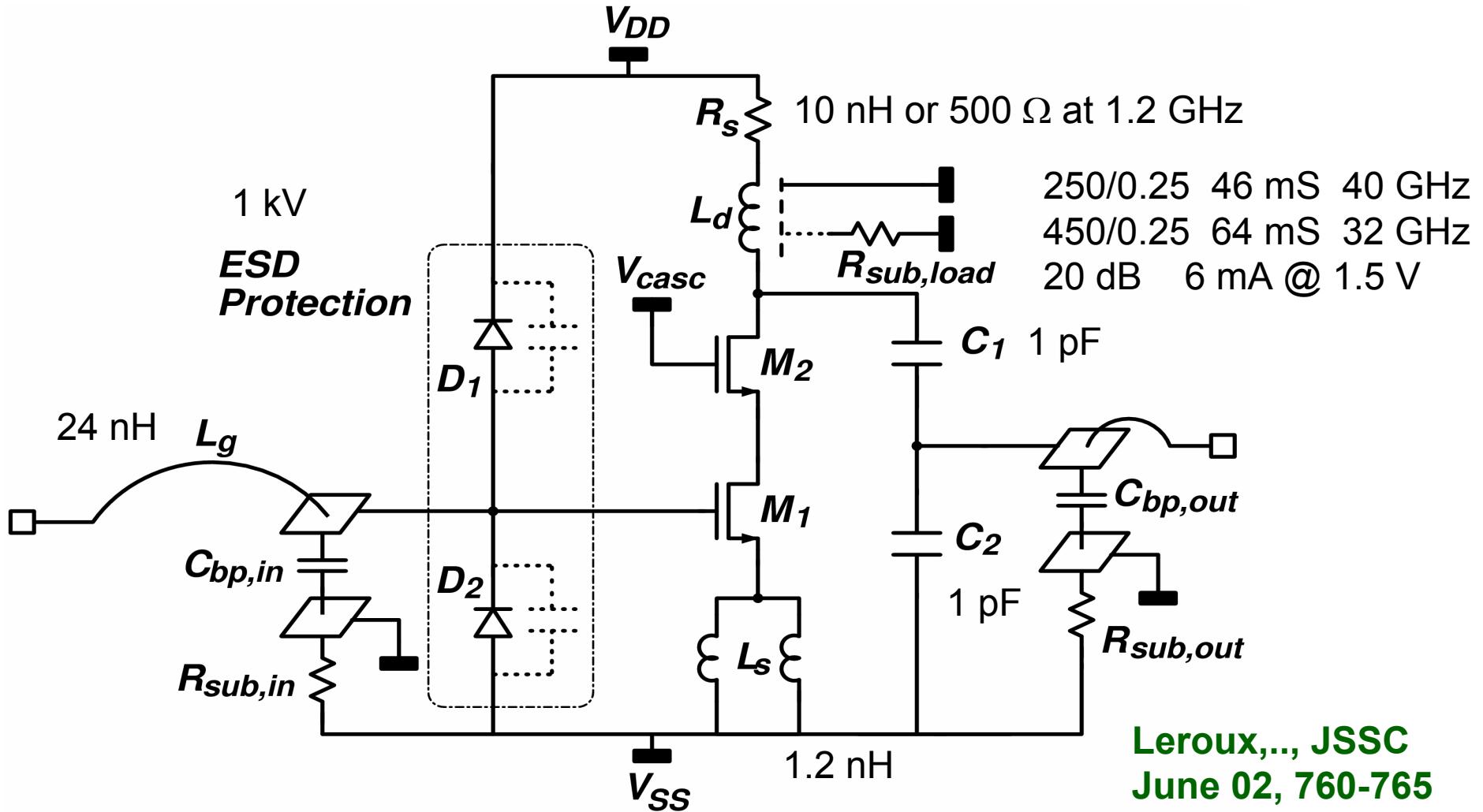
Forward & Reverse gain

Parameter	Value
Supply voltage	3.0 Volt
Power dissipation	10 mW
-3dB band	50 - 700 MHz
Noise figure	2.3 - 3.3 dB
In-band gain	14.8 dB
Gain at 900 MHz	9 dB
Reverse isolation	> 41 dB
Input IP3	-4.7 VdBm
Die area	1.0 x 1.2 mm ²

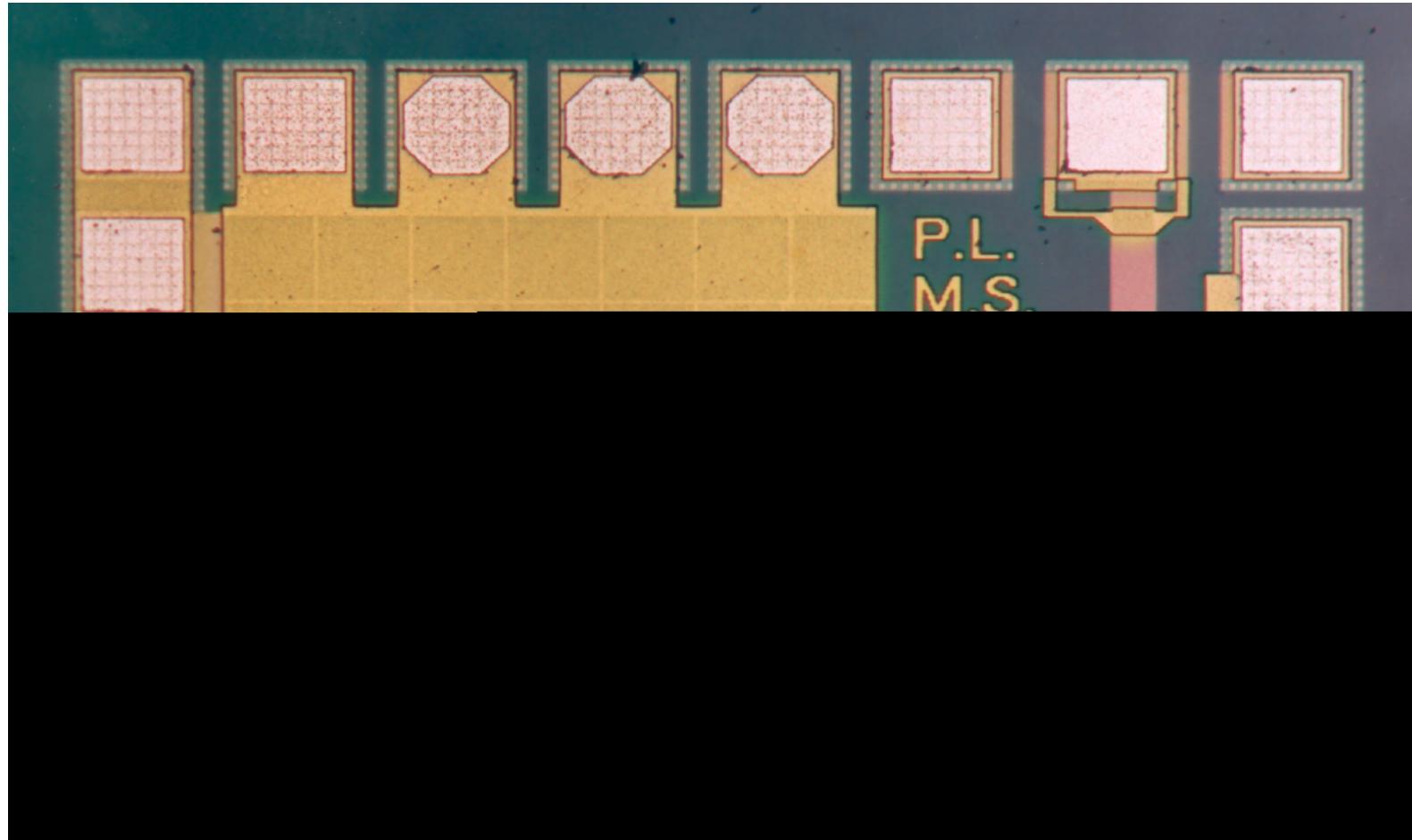
Measurements - 2



1.2 GHz LNA with C-ESD protection



LNA Micrograph

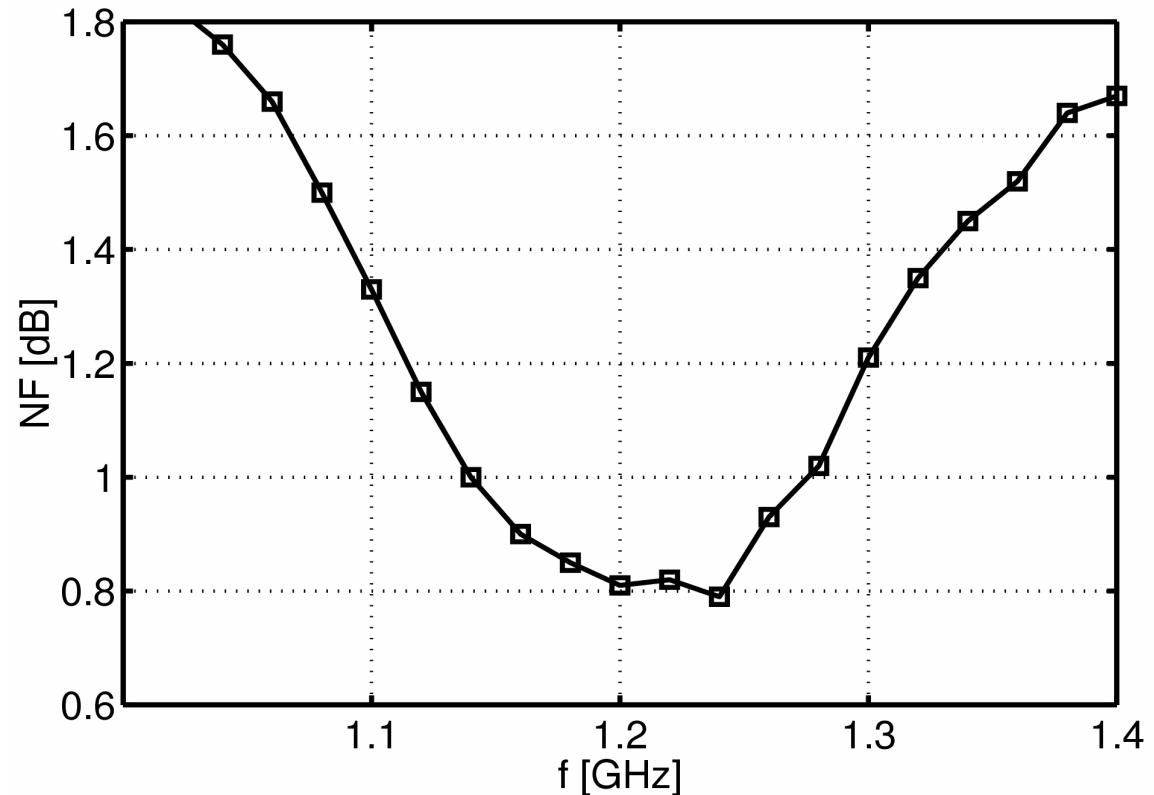


Leroux,.., JSSC June 02, 760-765

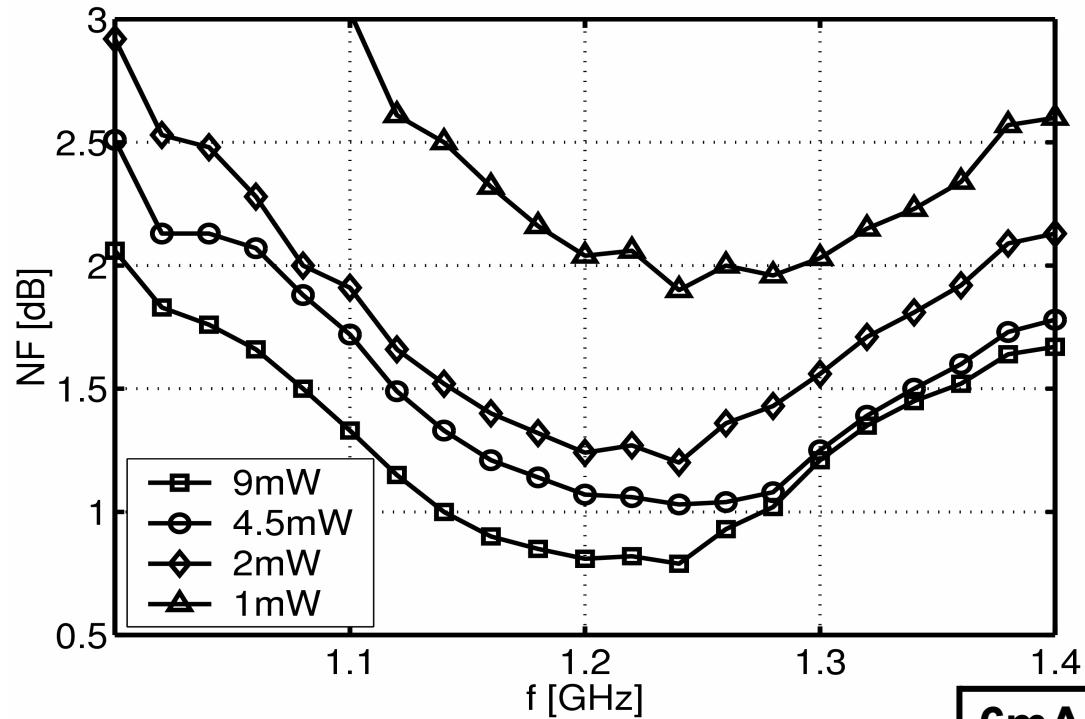
Willy Sansen 10-05 2340

Noise Figure

- **Min. NF = 0.8 dB**
- **BW (NF<1dB) = 130 MHz**



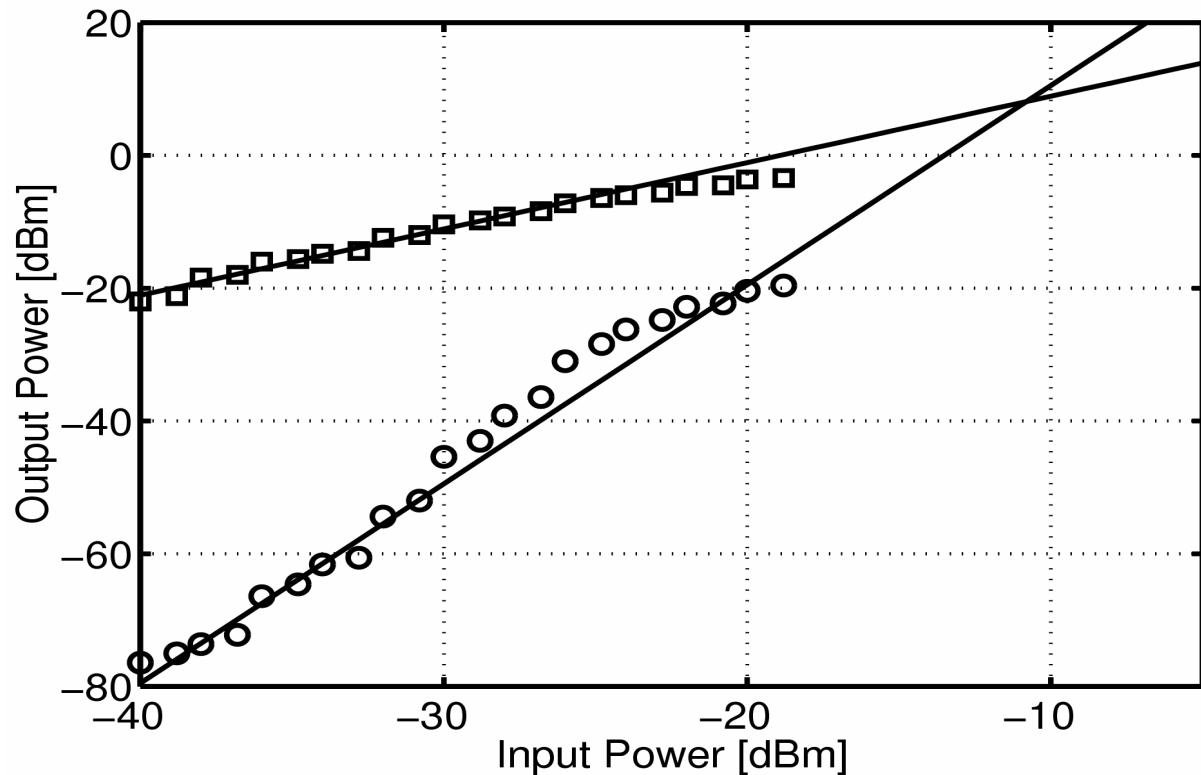
Noise Figure



NF @ min	
6mA @ 1.5V	0.8dB
3mA @ 1.5V	1 dB
2mA @ 1V	1.2dB
1mA @ 1V	1.9dB

Linearity performance

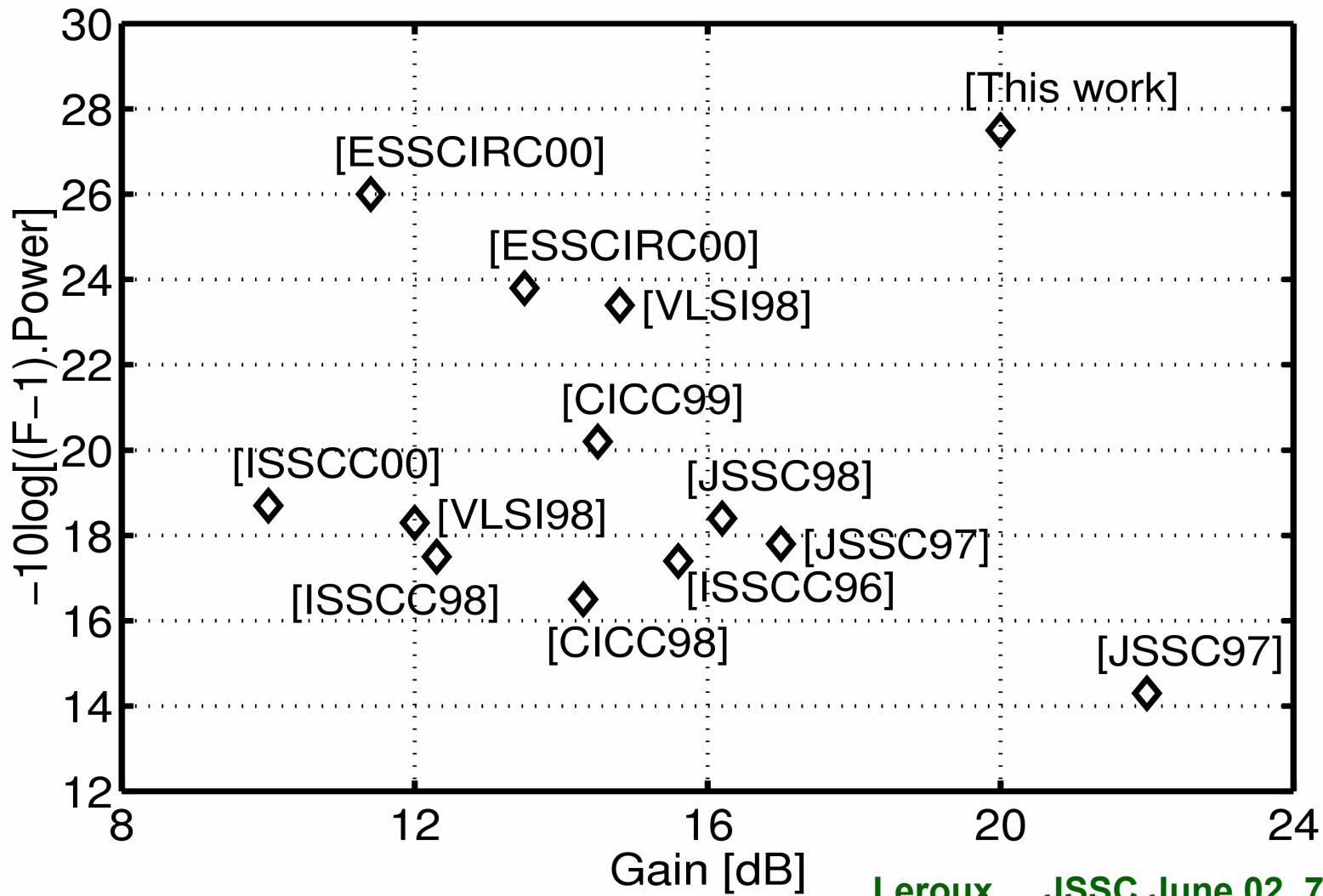
- Input IP3 = -10.8 dBm
- Input 1dB C_p = -24 dBm



Performance summary

<i>Parameter</i>	<i>Specification</i>	<i>Measurement</i>
Supply voltage	1.5 Volt	1.5 Volt
Power dissipation	10 mW	9 mW
Noise figure	1 dB	0.79 dB
Power gain @ 1.23 GHz	Max.	20 dB
S11 at 1.23 GHz	-10 dB	-11 dB
S22 at 1.23 GHz	-10 dB	-11 dB
Reverse isolation	30 dB	31 dB
Input IP3	-20 dBm	-10.8 dBm
HBM ESD-protection	0.5 kV	0.6 kV / -1.4 kV
Die area	-	0.6 x 1.1 mm ²

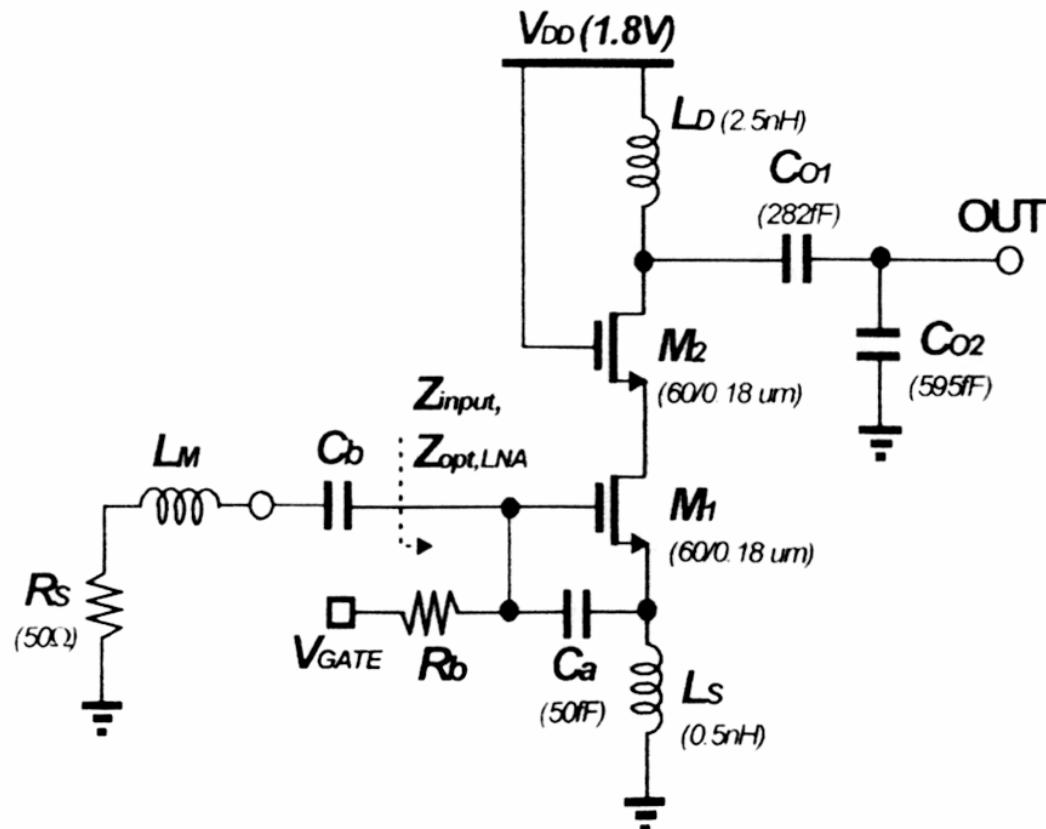
Performance comparison



Leroux..., JSSC June 02, 760-765

Willy Sansen 10-05 2345

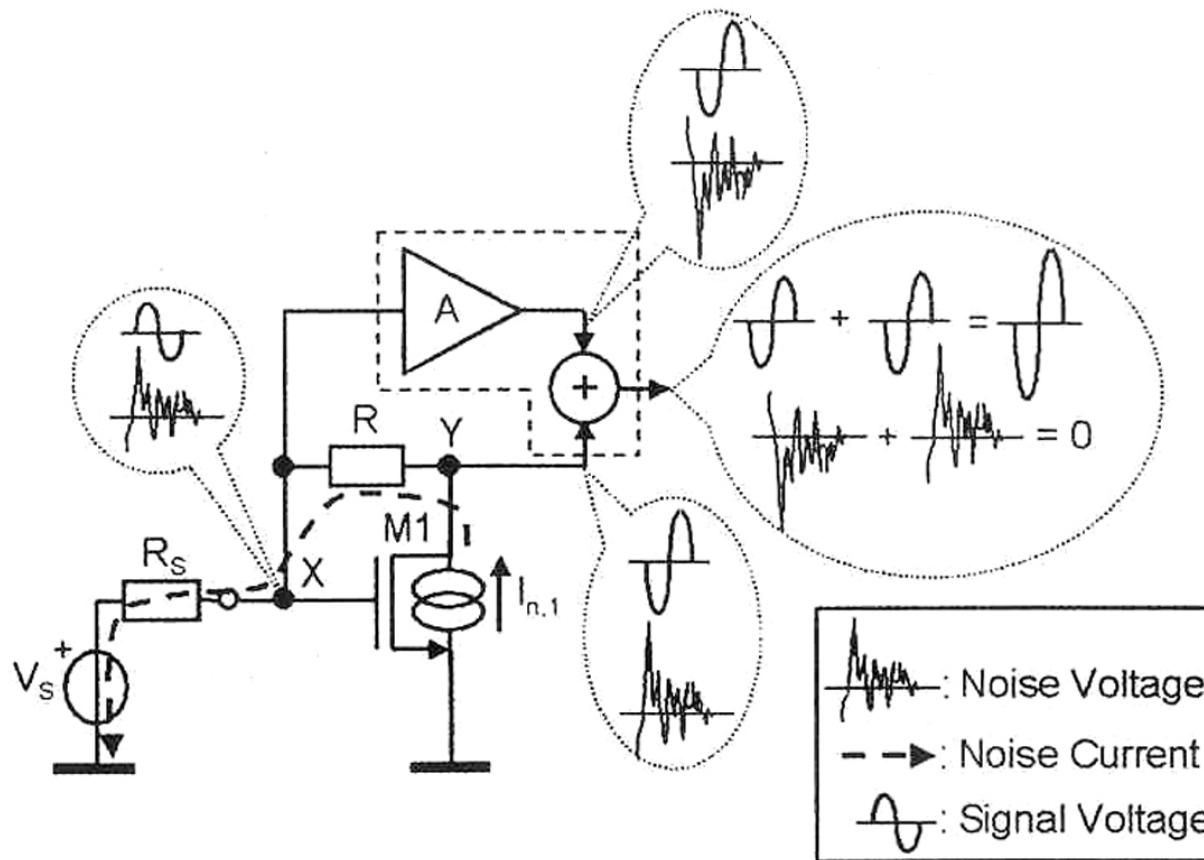
5.2 GHz LNA



5.2 GHz
Gain 16 dB
NF 1.1 dB
1.8 V
12.4 mW

Han..., JSSC March 05, 726-735

Noise-cancellation principle



$$v_x = \frac{R_s I_{n,1}}{1 + g_m R_s}$$

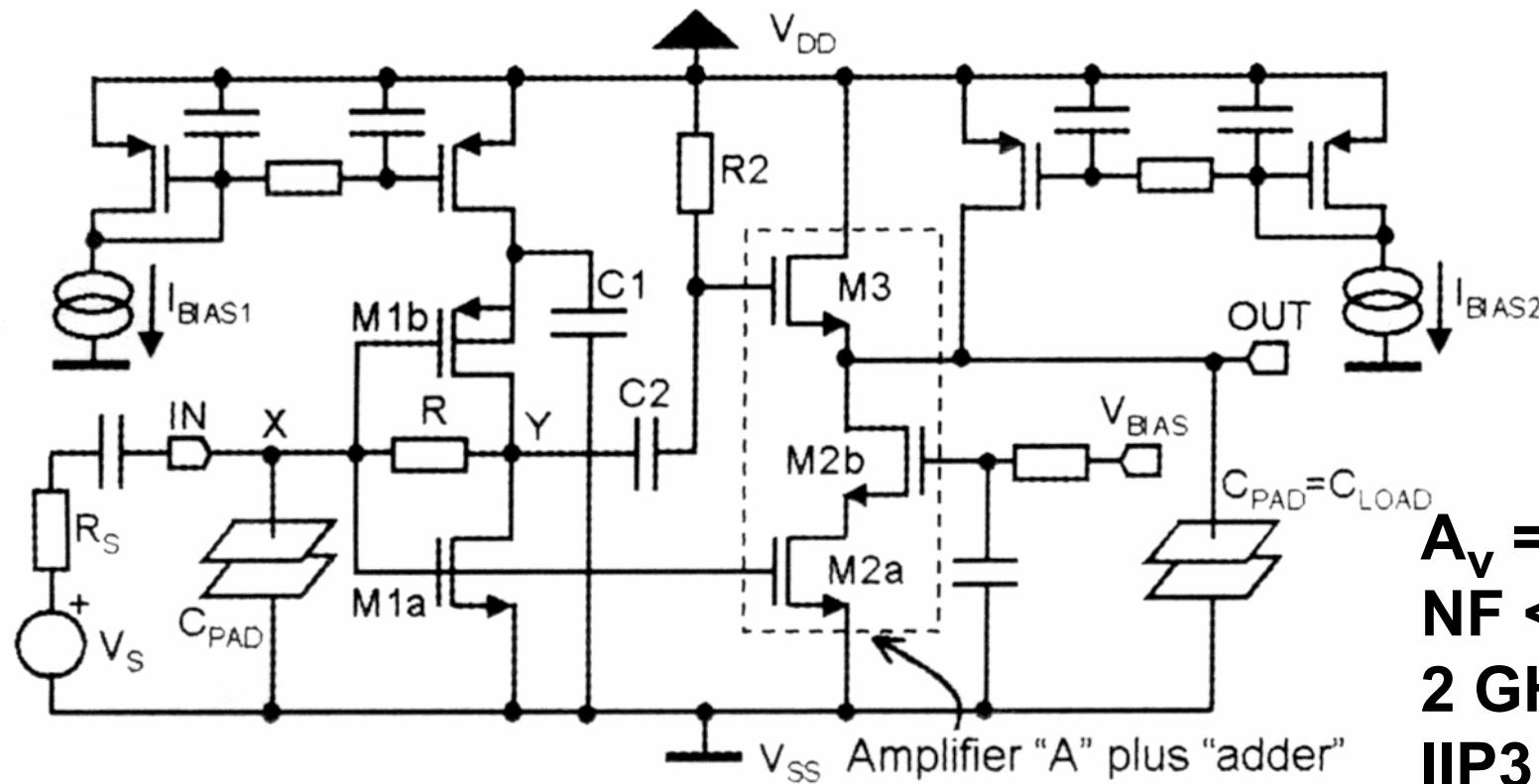
$$v_y = \frac{(R + R_s) I_{n,1}}{1 + g_m R_s}$$

$$v_{\text{OUT}} = A v_x + v_y$$

cancels the noise

Brucoleri..., JSSC Febr.04, 275-282

Noise-cancelling LNA

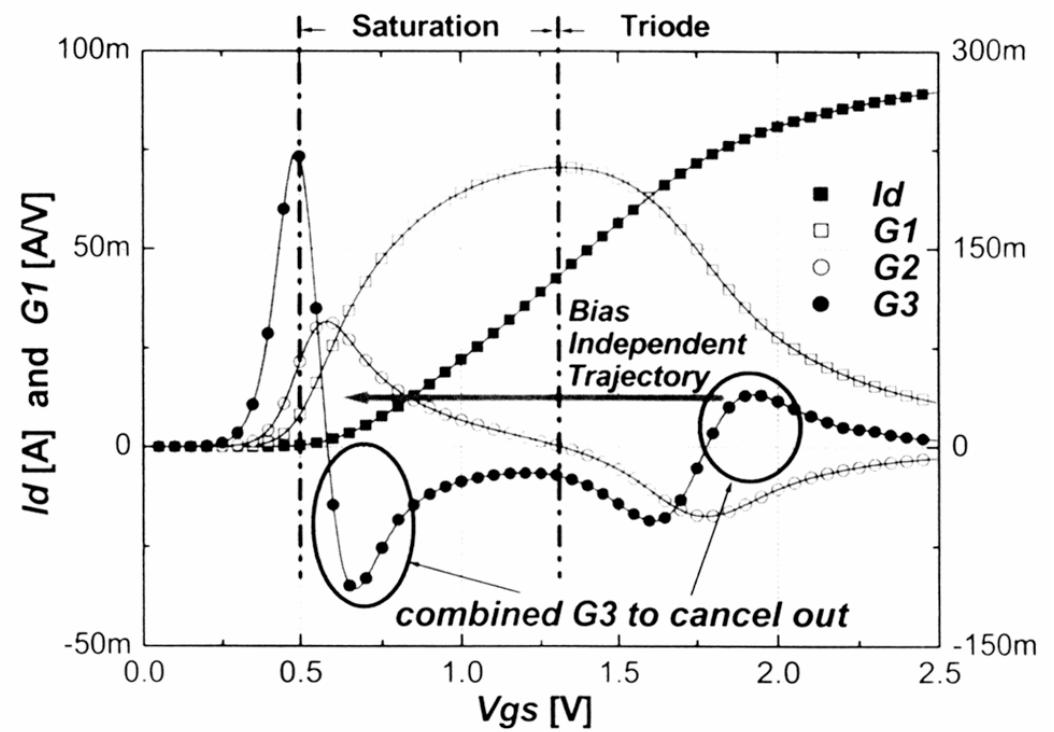
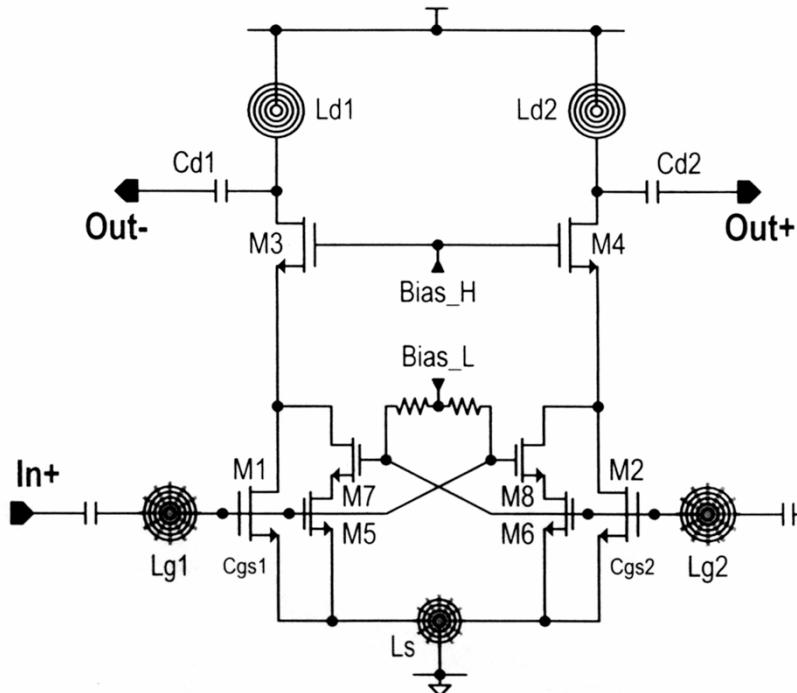


Noise cancelling condition :

$$\frac{g_{m2}}{g_{m3}} = \frac{R + R_S}{R_S}$$

Brucoleri,Nauta,
JSSC Febr.04,
275-282

Differential LNA in 0.25 μ m CMOS : 2.4 GHz

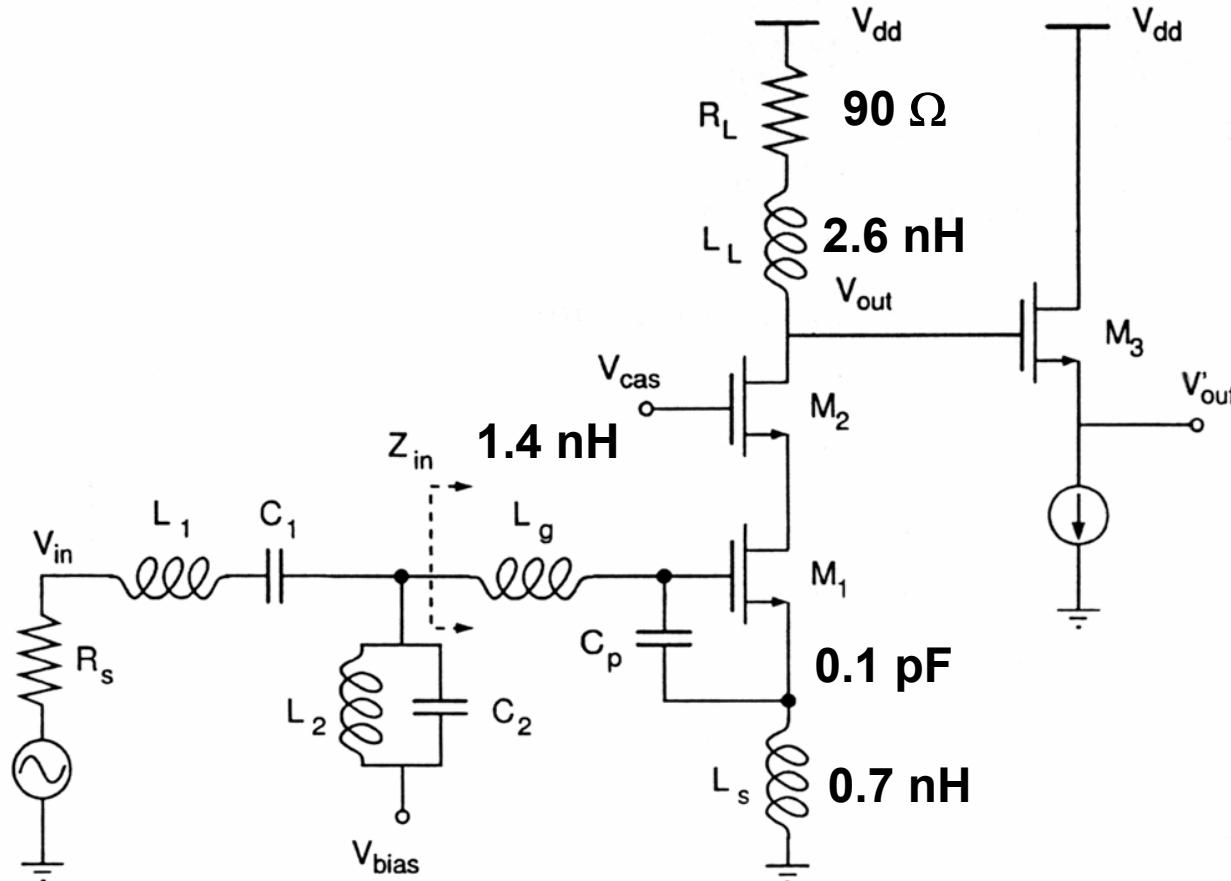


17 % More output power : 23.5 mW or +16 dBm

For same $P_{-1dB} = -5$ dBm

Youn,..., ISSCC 03, 406-407

LNA for UWB (3 - 10 GHz)



A_V = 9.3 dB

NF < 4 dB

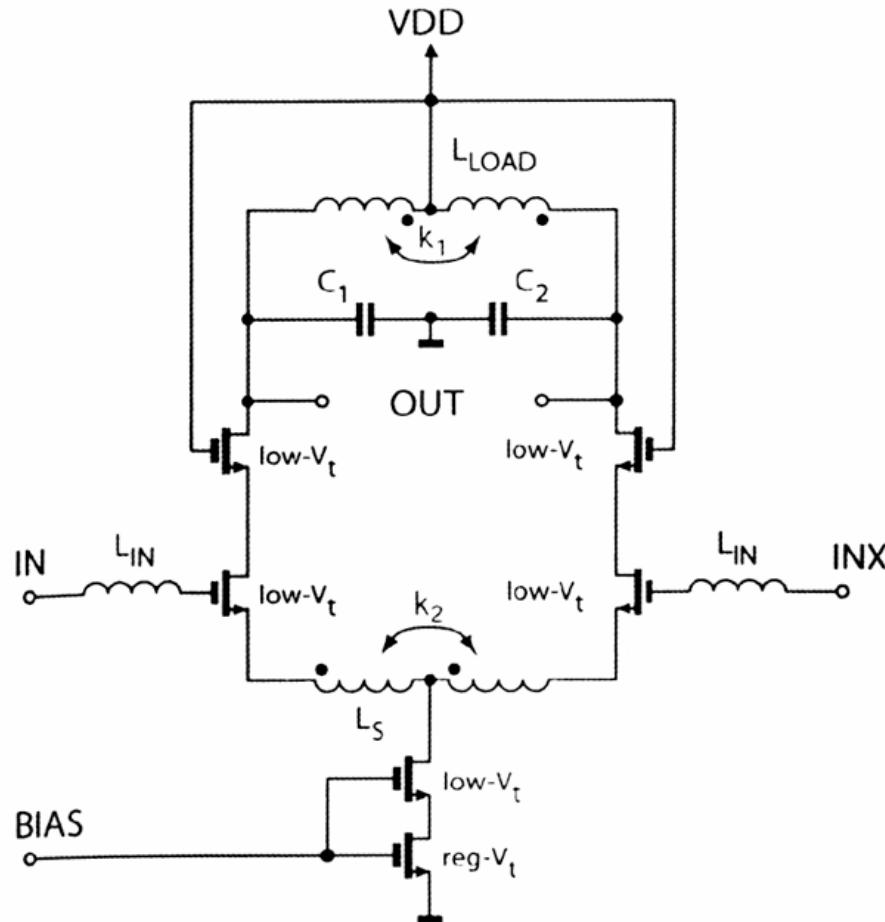
IIP3 = 6.7 dBm

1.5 V 5 mA

0.18 μm CMOS

Bevilacqua,.., JSSC Dec.01, 2259-2268

Differential LNA at 17 GHz



WLAN ISM 17 GHz

$A_v = 25.8 \text{ dB}$

$NF < 10 \text{ dB}$

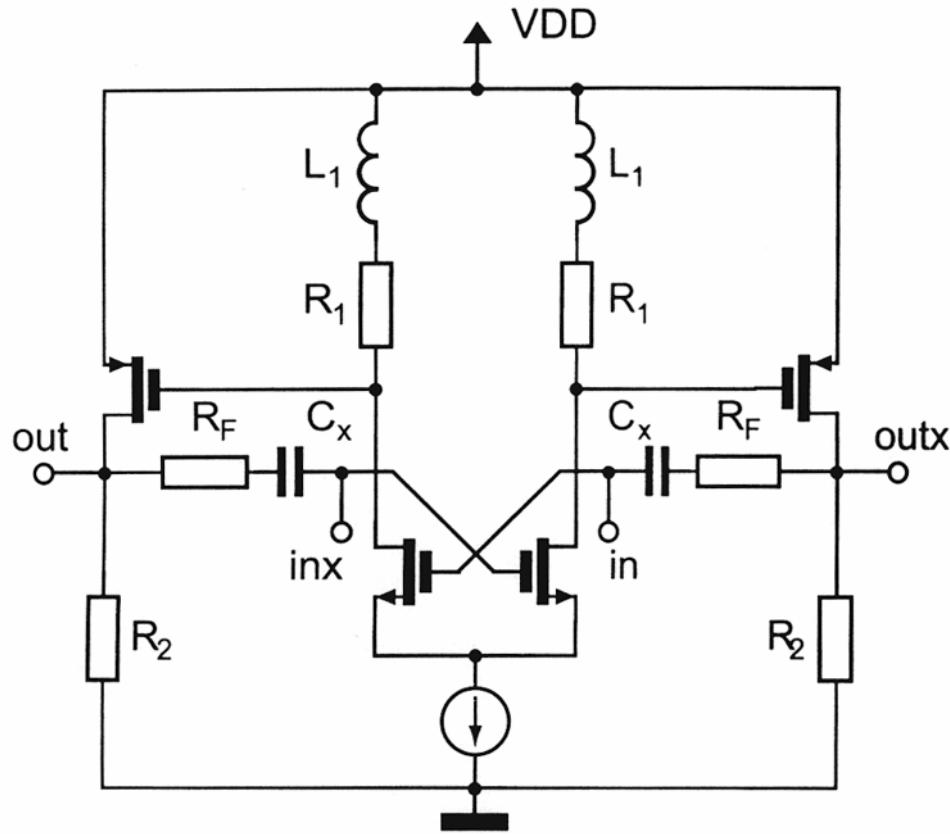
$IIP3 = -40 \text{ dBm}$

1.5 V

$0.13\mu\text{m CMOS}$

Kienmayer,.., ESSCIRC 2005, 133-136

Differential LNA at 5 GHz



UWB 3 - 5 GHz

$A_v = 25.8 \text{ dB}$

$\text{NF} < 3.6 \text{ dB}$

$\text{IIP3} = -22.7 \text{ dBm}$

$1.5 \text{ V } 45 \text{ mW}$

HBM ESD 1.5 kV

Salerno,..., ESSCIRC 2005, 219-222

Table of contents

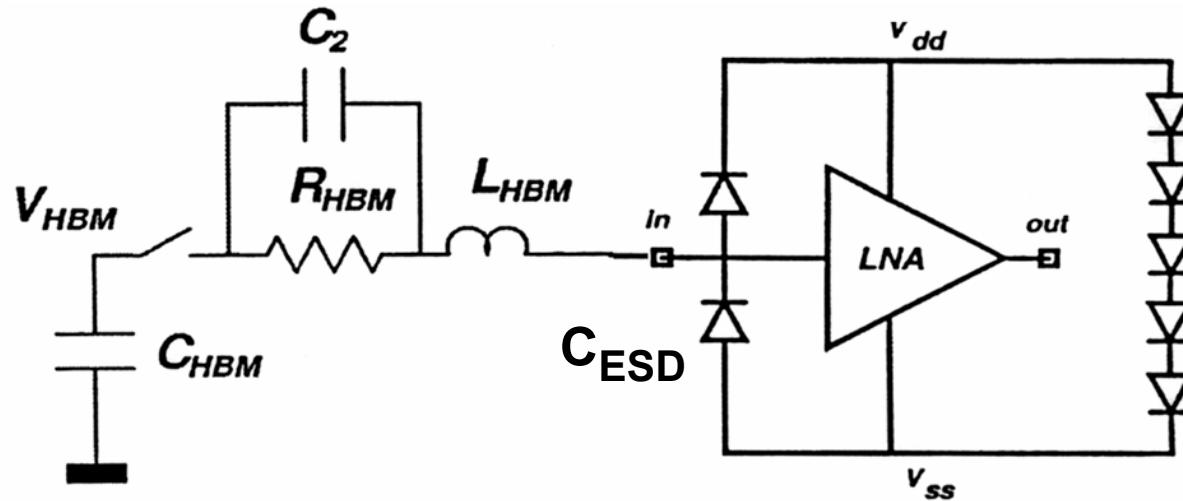
- Noise Figure and Impedance Matching
 - LNA specifications and linearity
 - Input amplifier or cascode
 - Non-quasi-static MOST model
 - More realizations
- Inductive ESD protection

ESD protection : Human Body model

- CMOS requires ESD protection
- Protection network deteriorates RF performance
- Standards for testing : Human Body Model

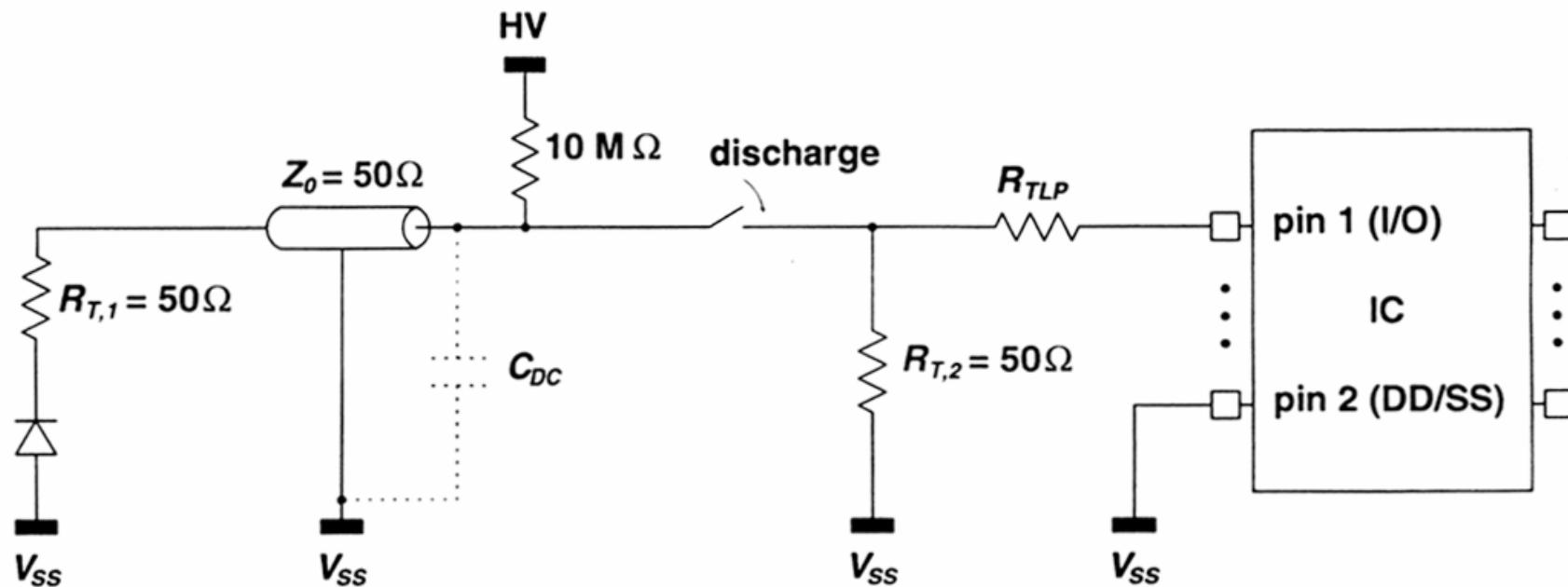
Transmission Line Pulse ...

- Human Body Model :



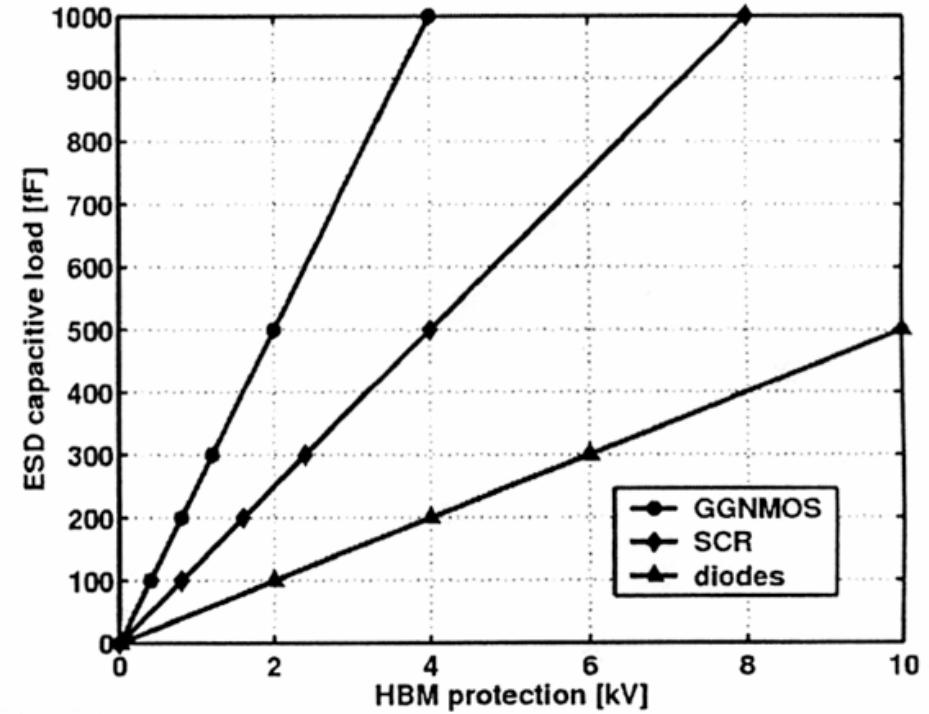
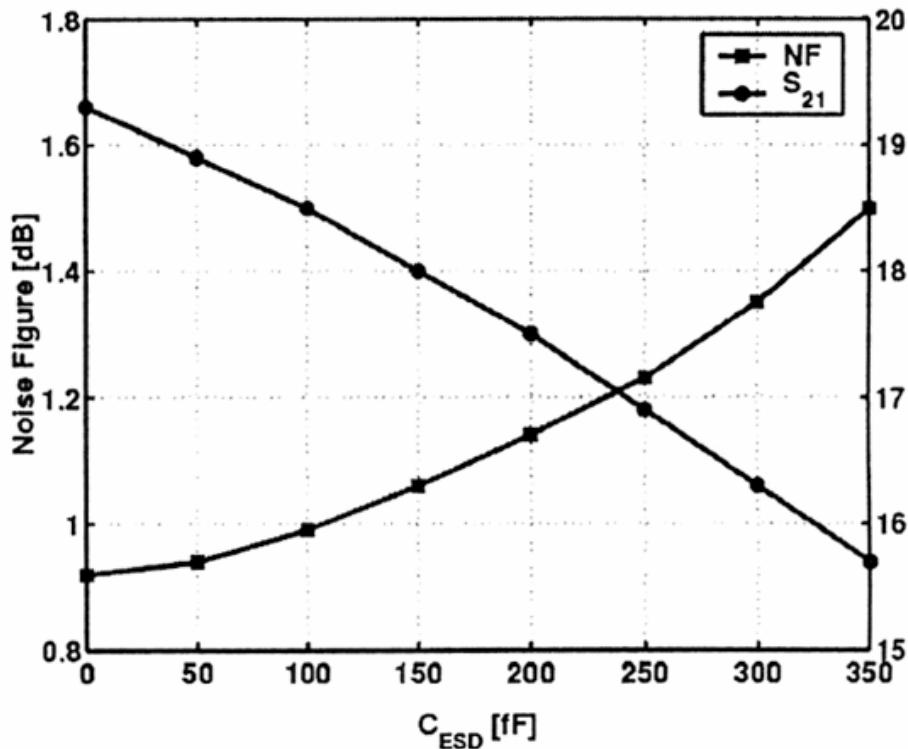
$$\begin{aligned} C_{HBM} &= 100 \text{ pF} \\ R_{HBM} &= 1.5 \text{ k}\Omega \\ V_{HBM} &= \\ I_{max} &= 0.67 \text{ A / kV} \\ \text{Required} & 2 \text{ kV !!} \end{aligned}$$

ESD protection : Transmission Line Pulse

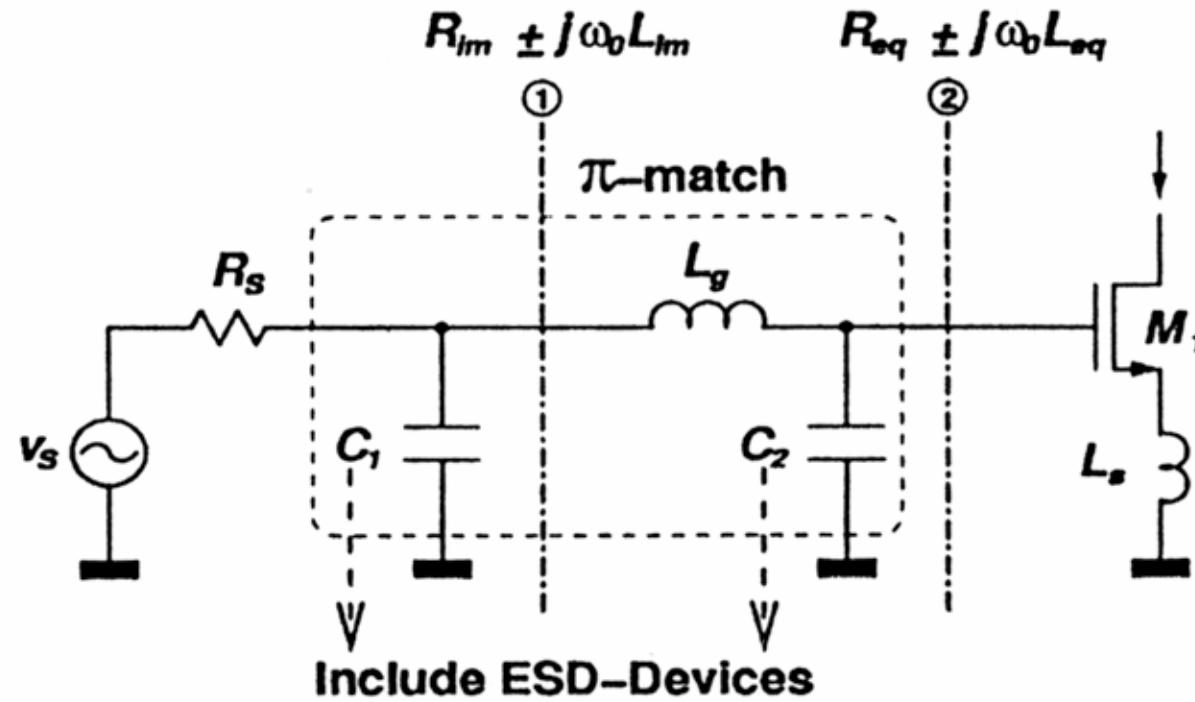


HV : High Voltage : kV's

Simulated deterioration by ESD diodes



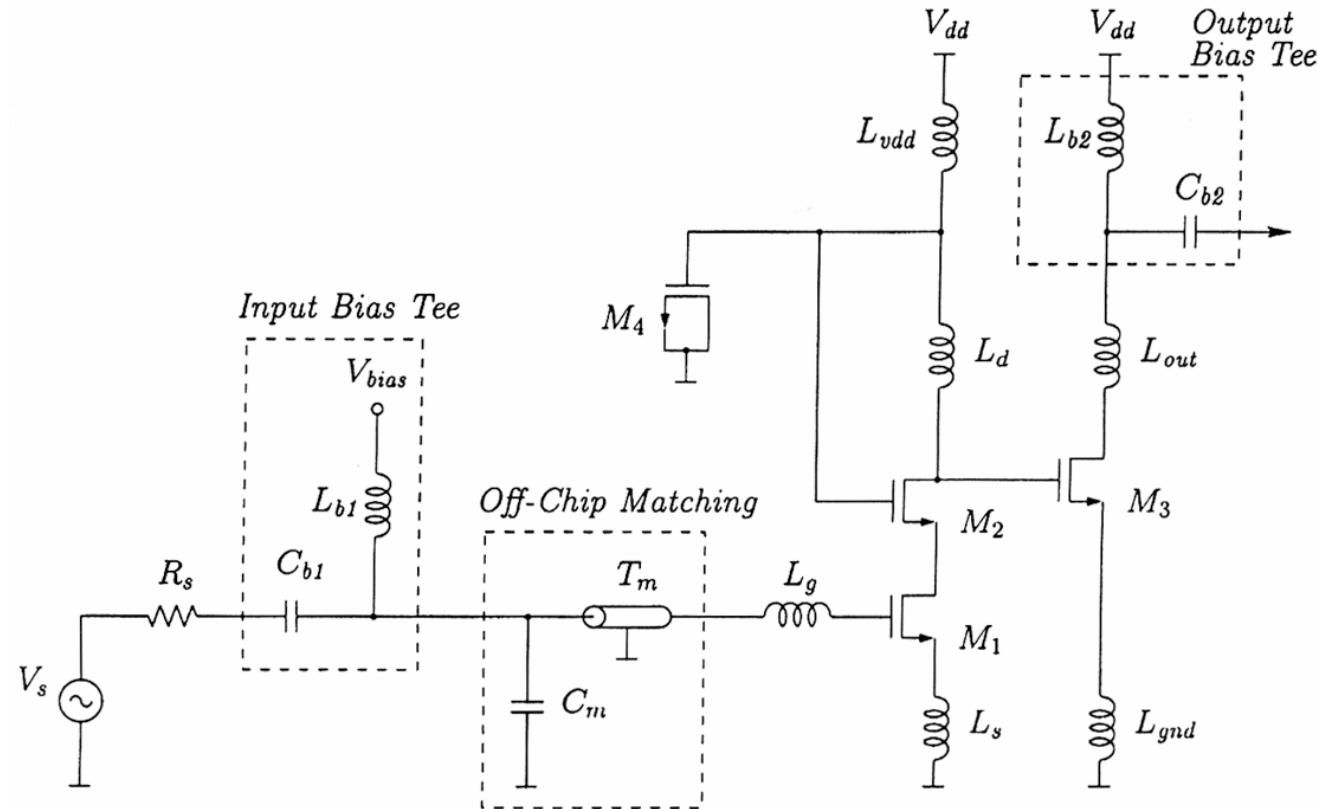
Π -network with Capacitive ESD protection



Requires on-chip inductor !

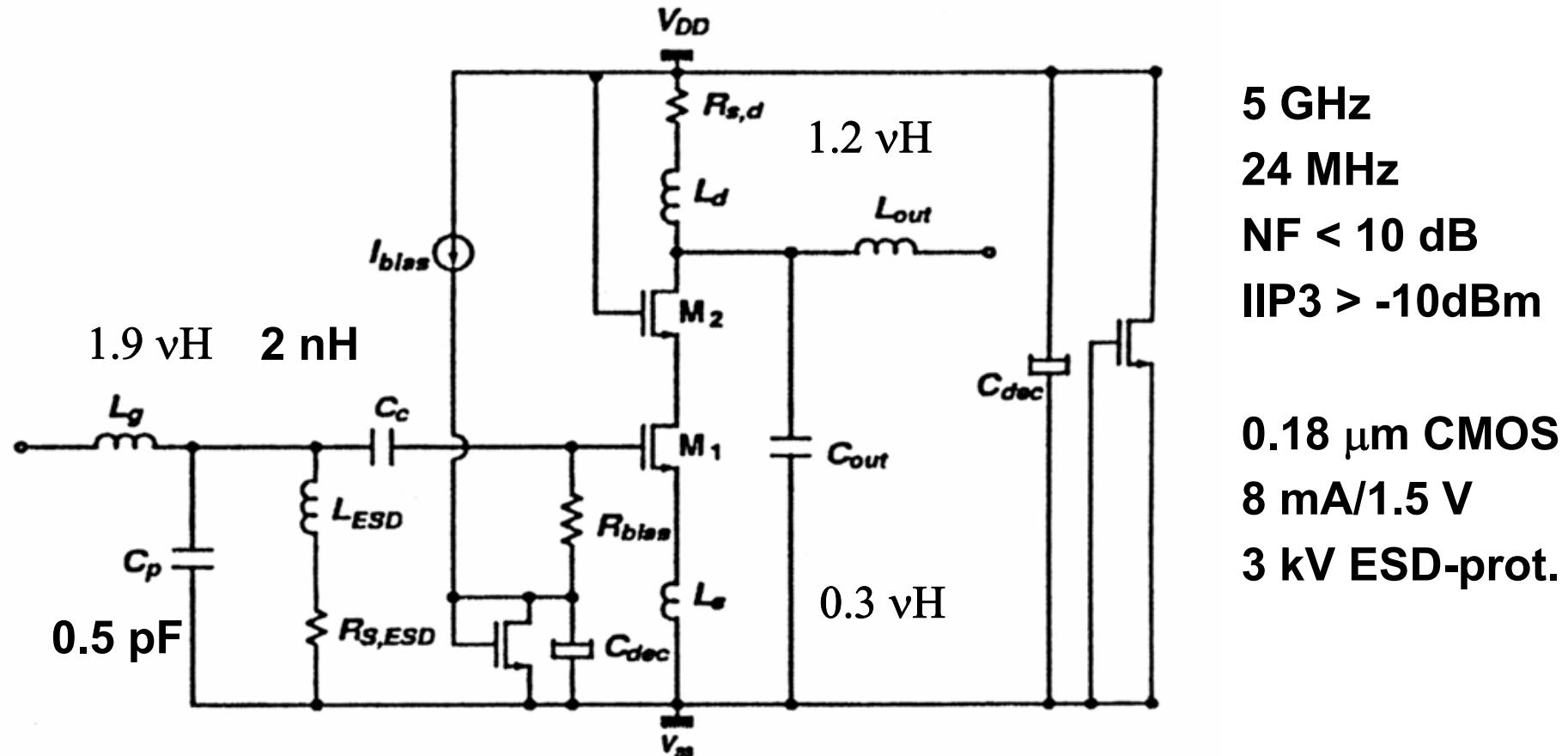
Leroux,.., Kluwer 2005

1.5 V 1.5 GHz LNA



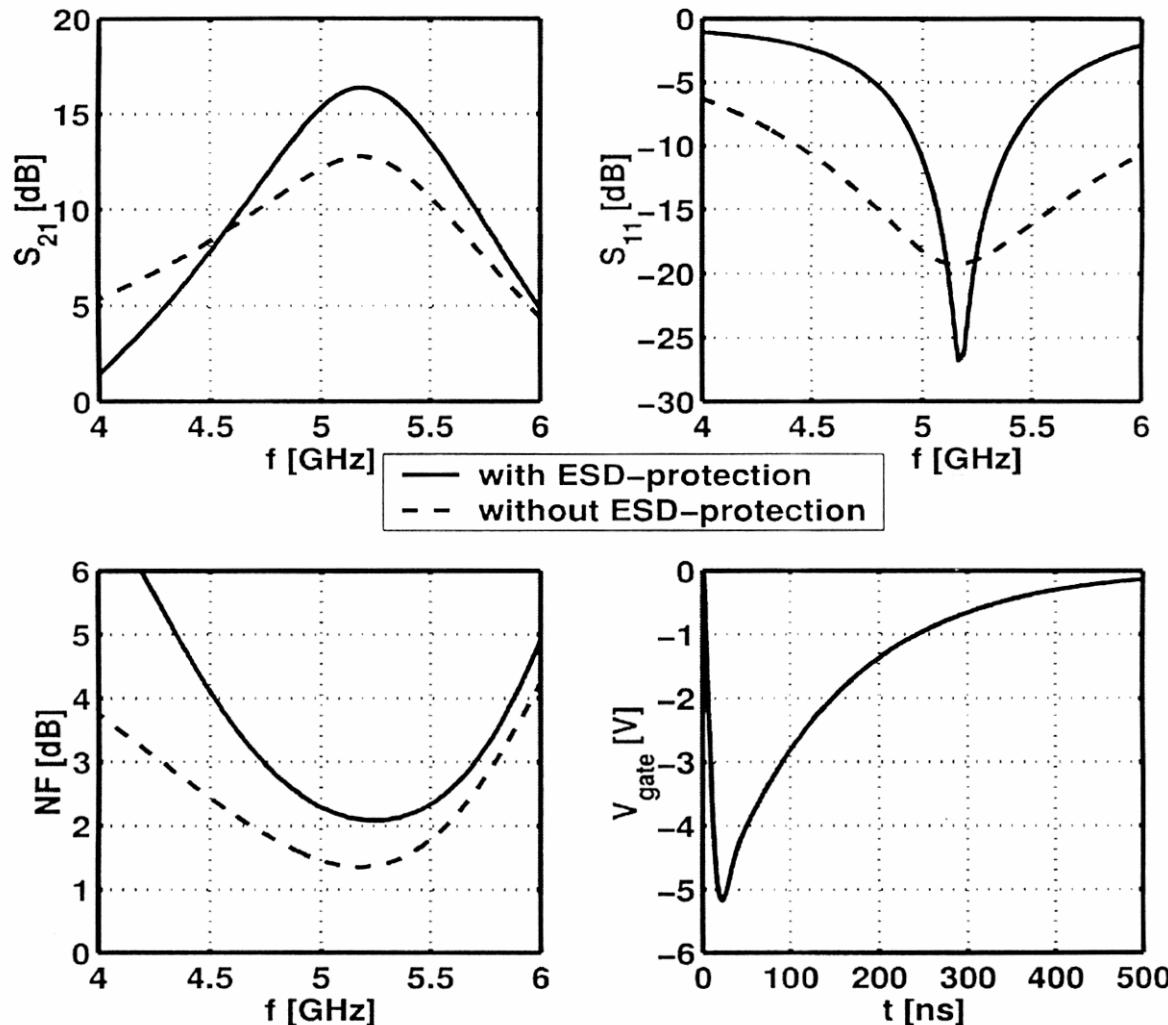
Schaeffer,.. JSSC May 97, 745-759

LNA with L-ESD protection for 5 GHz LNA

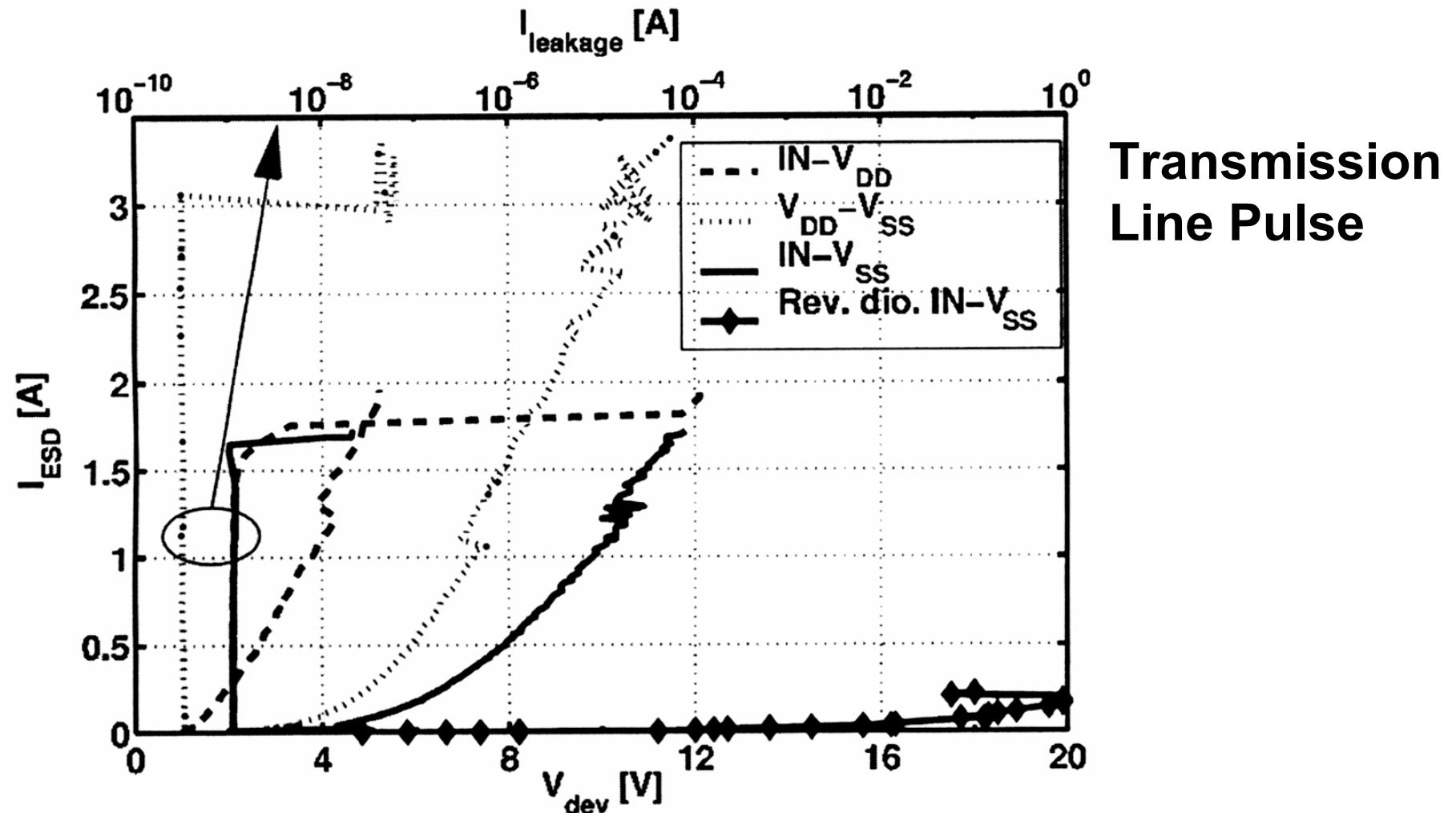


Leroux,.., AACD 2003, 207-225

Effect of ESD on performance



TLP Characteristics



Transmission
Line Pulse

Table of contents

- Noise Figure and Impedance Matching
- LNA specifications and linearity
- Input amplifier or cascode
- Non-quasi-static MOST model
- More realizations
- Inductive ESD protection