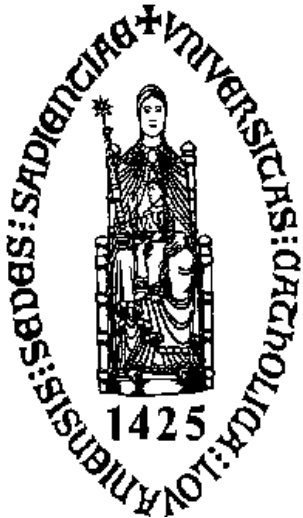

Class AB and driver amplifiers



Willy Sansen

KULeuven, ESAT-MICAS

Leuven, Belgium

willy.sansen@esat.kuleuven.be

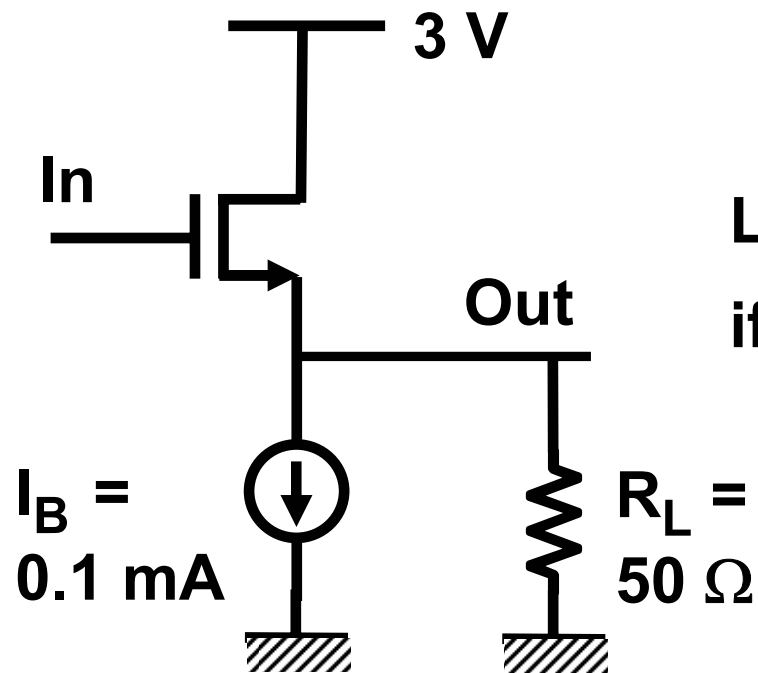


Outline

- **Problems of class AB drivers**
 - **Cross-coupled quads**
 - **Adaptive biasing**
 - **I_Q control with translinear circuits, etc.**
 - **Current feedback and other principles**
 - **Low-Voltage realizations**

Ref.: W. Sansen : Analog Design Essentials, Springer 2006

CMOS Output stage problem



Low power consumption:

if $I_B = 0.1 \text{ mA}$: $V_{\text{out, peak}} = 5 \text{ mV}_{\text{peak}}$

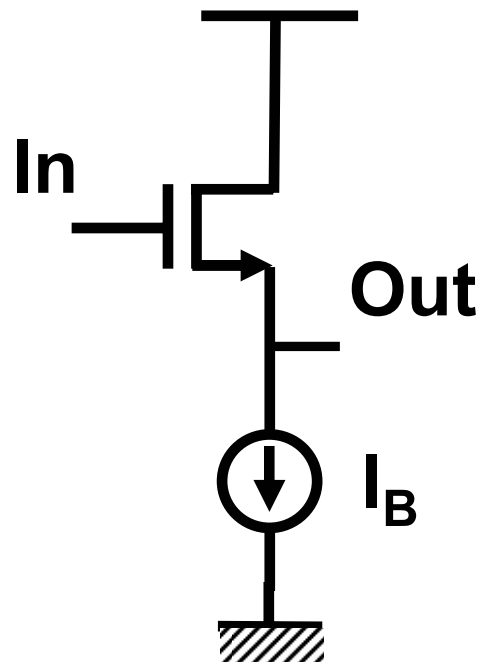
$$I_{\text{max}} < I_B$$

$$V_{\text{Out}} = V_{\text{In}} - V_{\text{GS}}$$

For $V_{\text{out, peak}} = 1 \text{ V}_{\text{peak}}$: $I_B = 20 \text{ mA}$

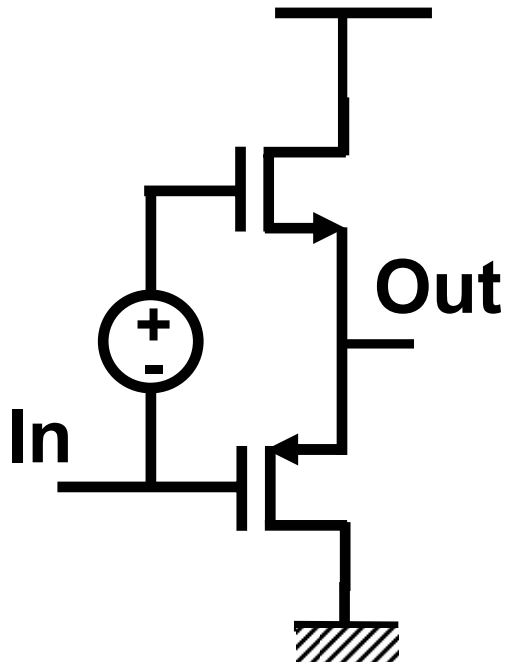
High power consumption !

CMOS Output stages



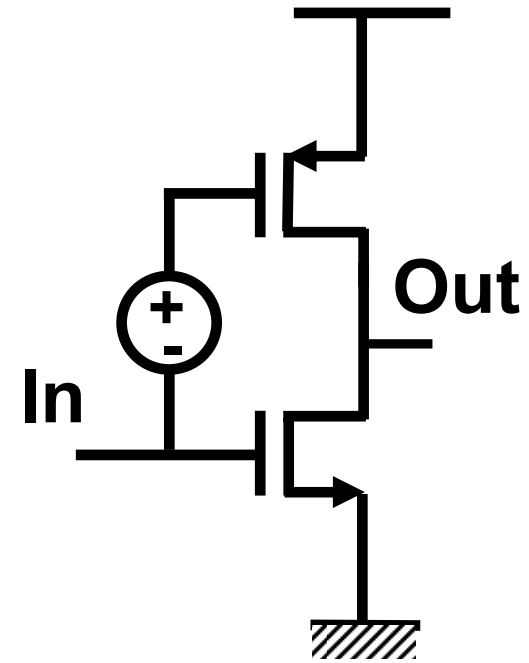
$$I_{\max} < I_B$$

$$V_{\text{Out}} = V_{\text{In}} - V_{\text{GS}}$$



Push-Pull

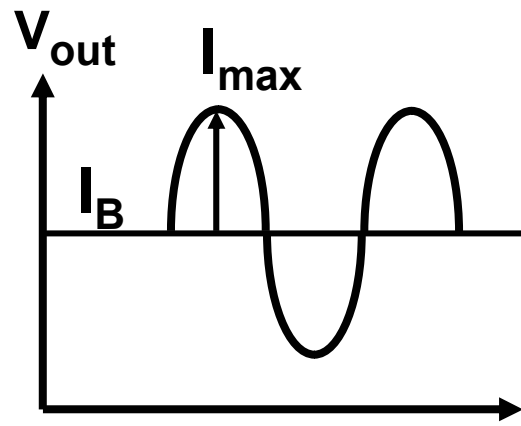
$$V_{\text{out,max}} = V_{\text{DD}} - 2V_{\text{GS}}$$



Amplifier

Rail-to-rail

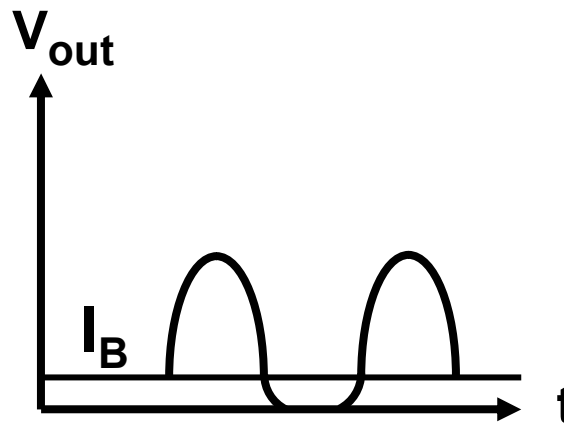
Class A, AB, B, etc



$$I_B > I_{max}$$

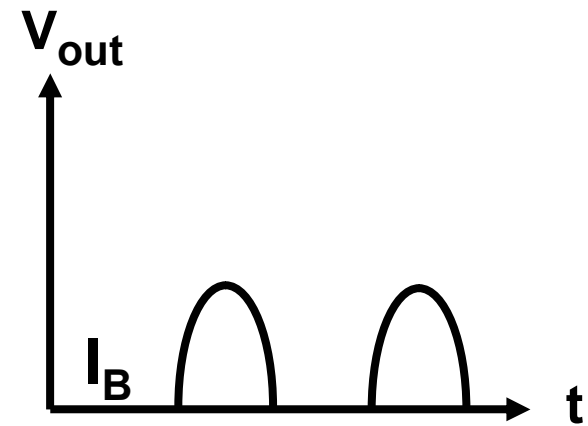
Class A

High power !



$$I_B < I_{max}$$

Class AB



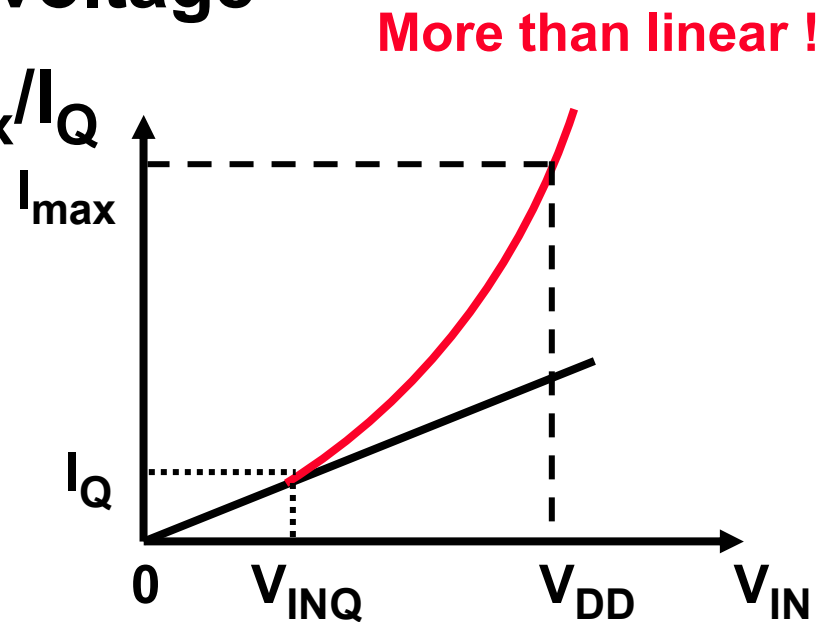
$$I_B = 0$$

Class B

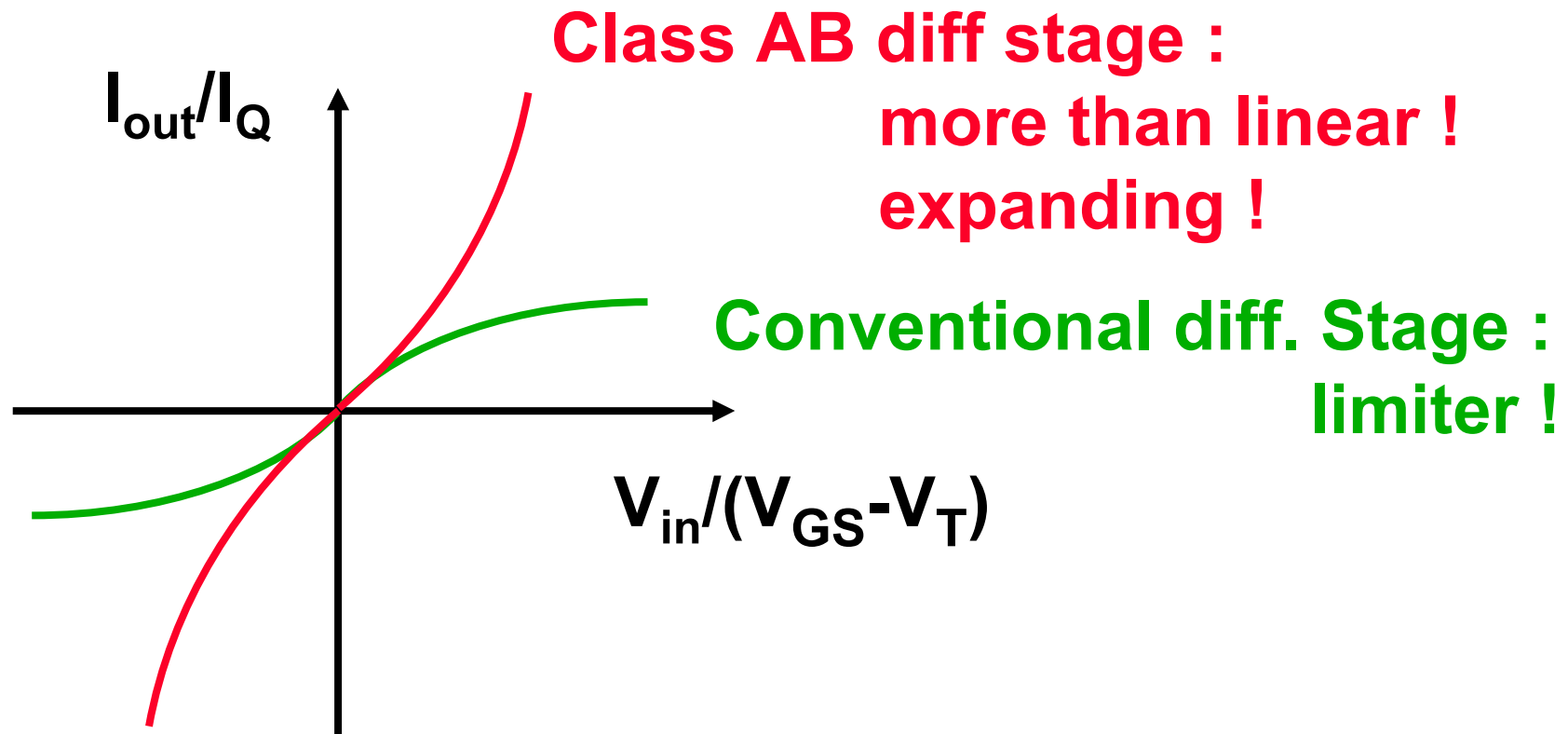
Distortion !

Requirements class -AB stages

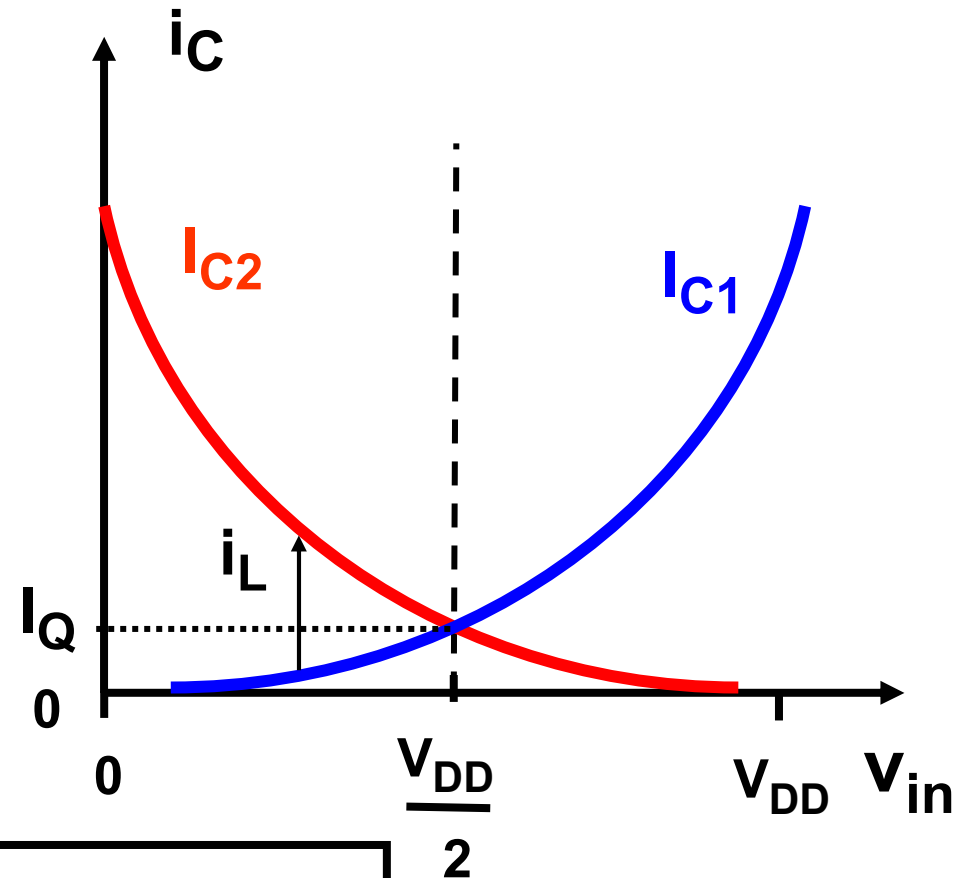
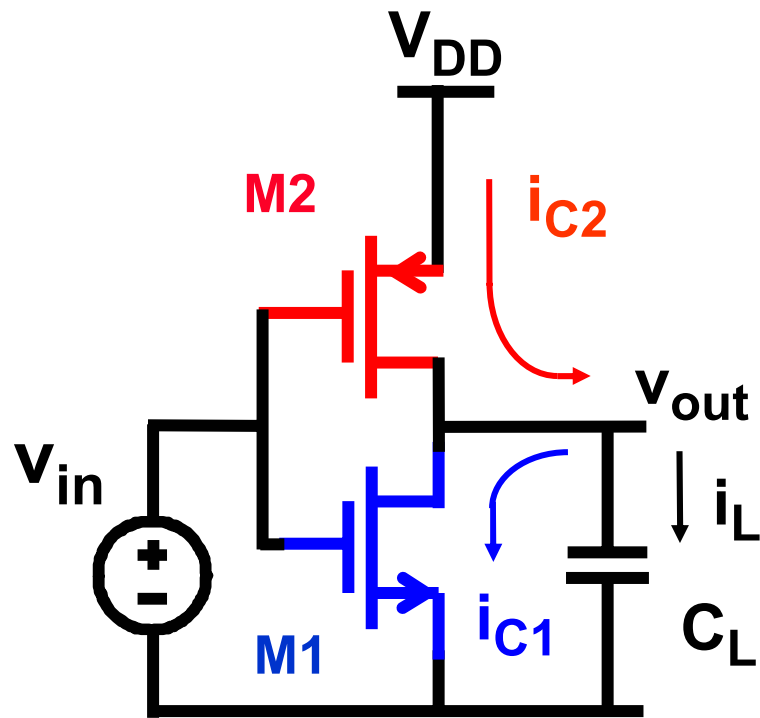
- Rail-to-rail output swing
- Accurate control of quiescent current I_Q
 - Must be low
 - Independent of supply voltage
- Large drive capability I_{\max}/I_Q
- Small area



Class -AB stages



Simple CMOS class-AB amplifier

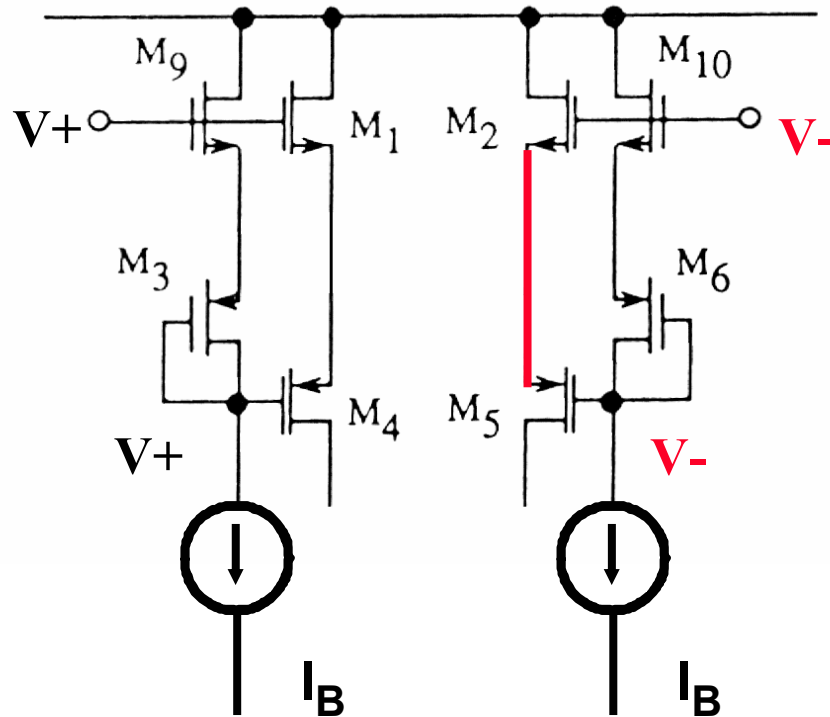


$$i_L = i_{C2} - i_{C1}$$

Outline

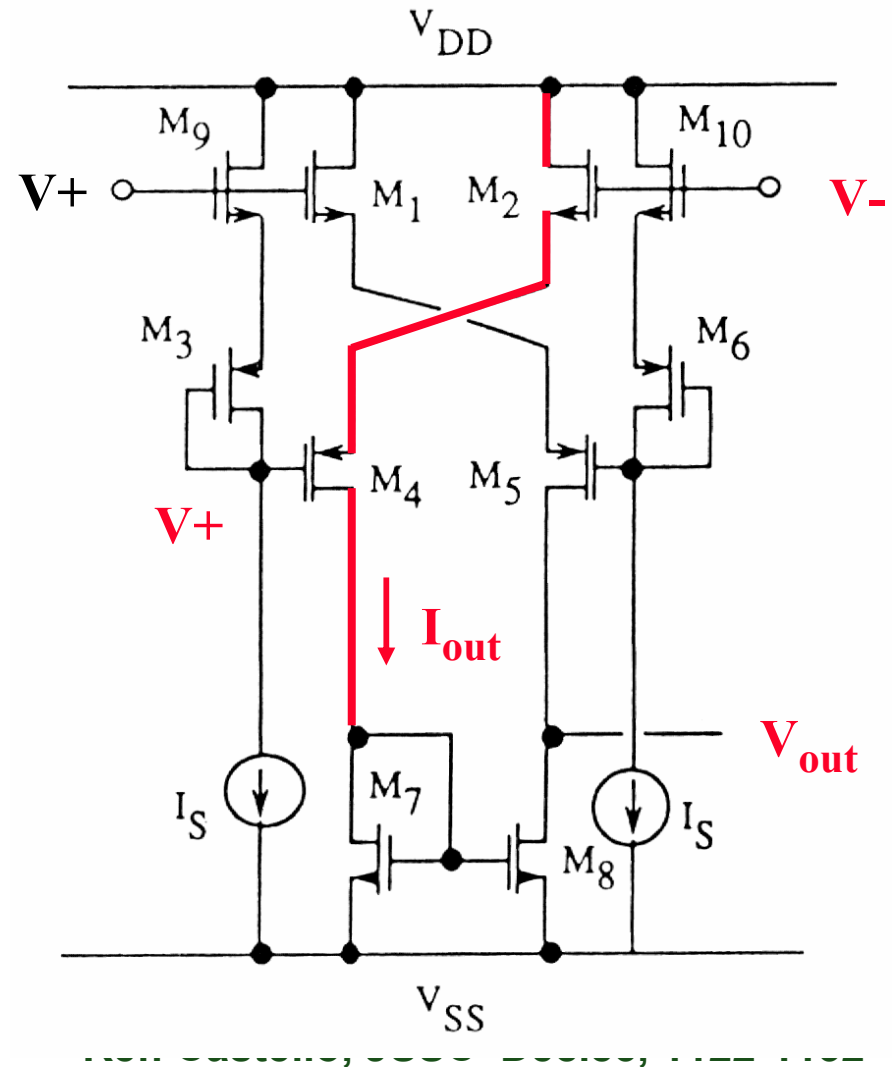
- Problems of class AB drivers
- Cross-coupled quads
- Adaptive biasing
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- Current feedback and other principles
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Cross-coupled quad

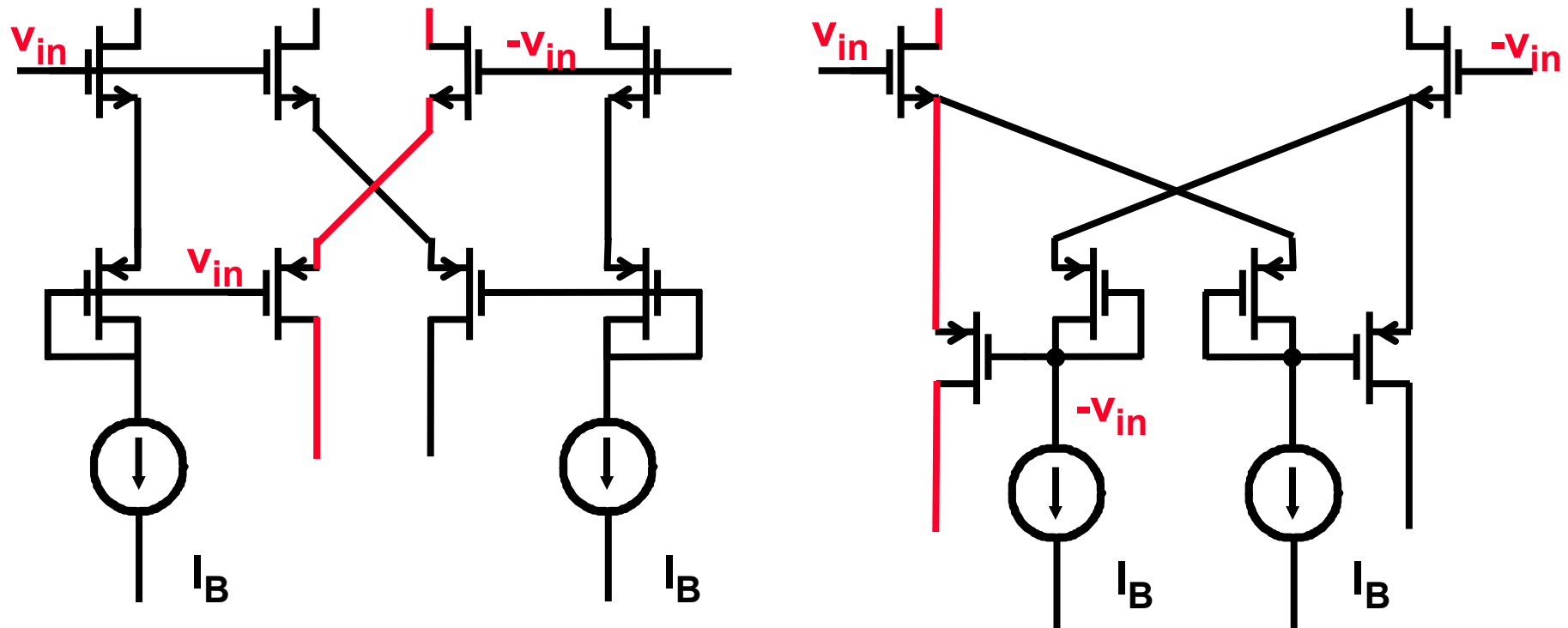


Two super-followers

Ref. Castello, JSSC Dec.85, 1122-1132

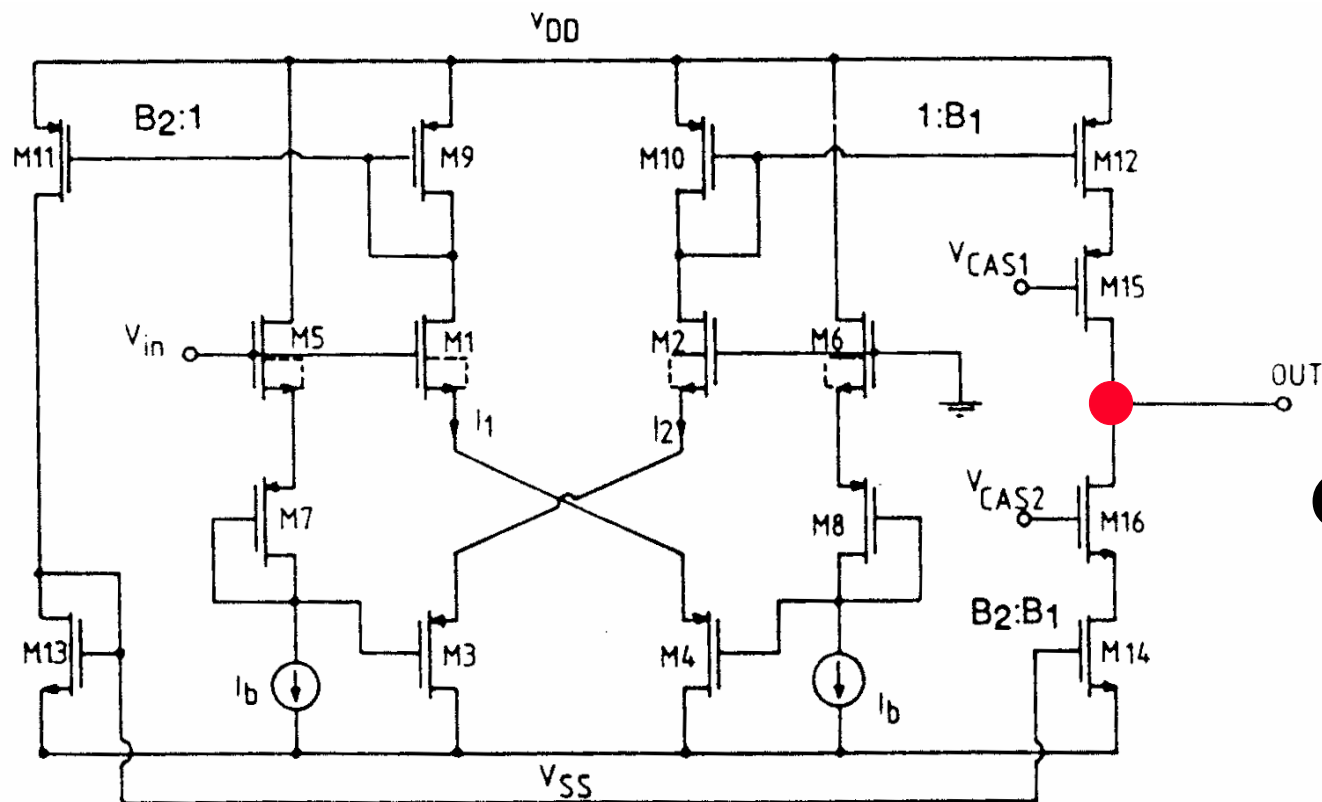


Other cross-coupled quads



Bipolar Ref. Hearn, JSSC Febr.71

Class AB Input structures

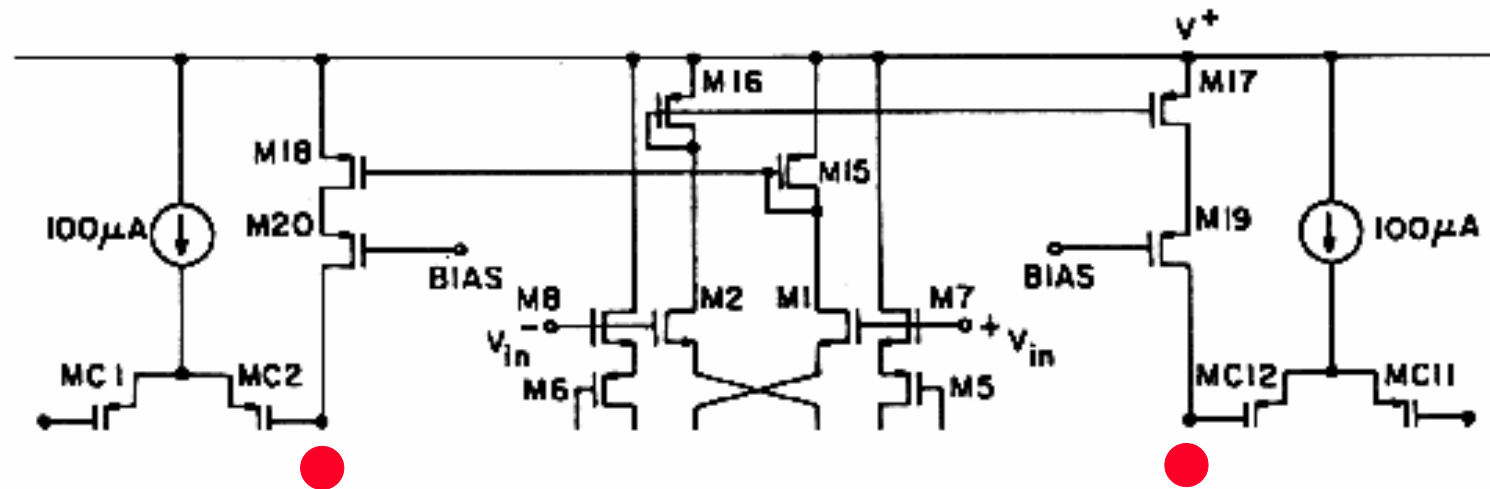


$$\text{GBW} = \frac{g_{m1}}{2\pi C_L}$$

SR  

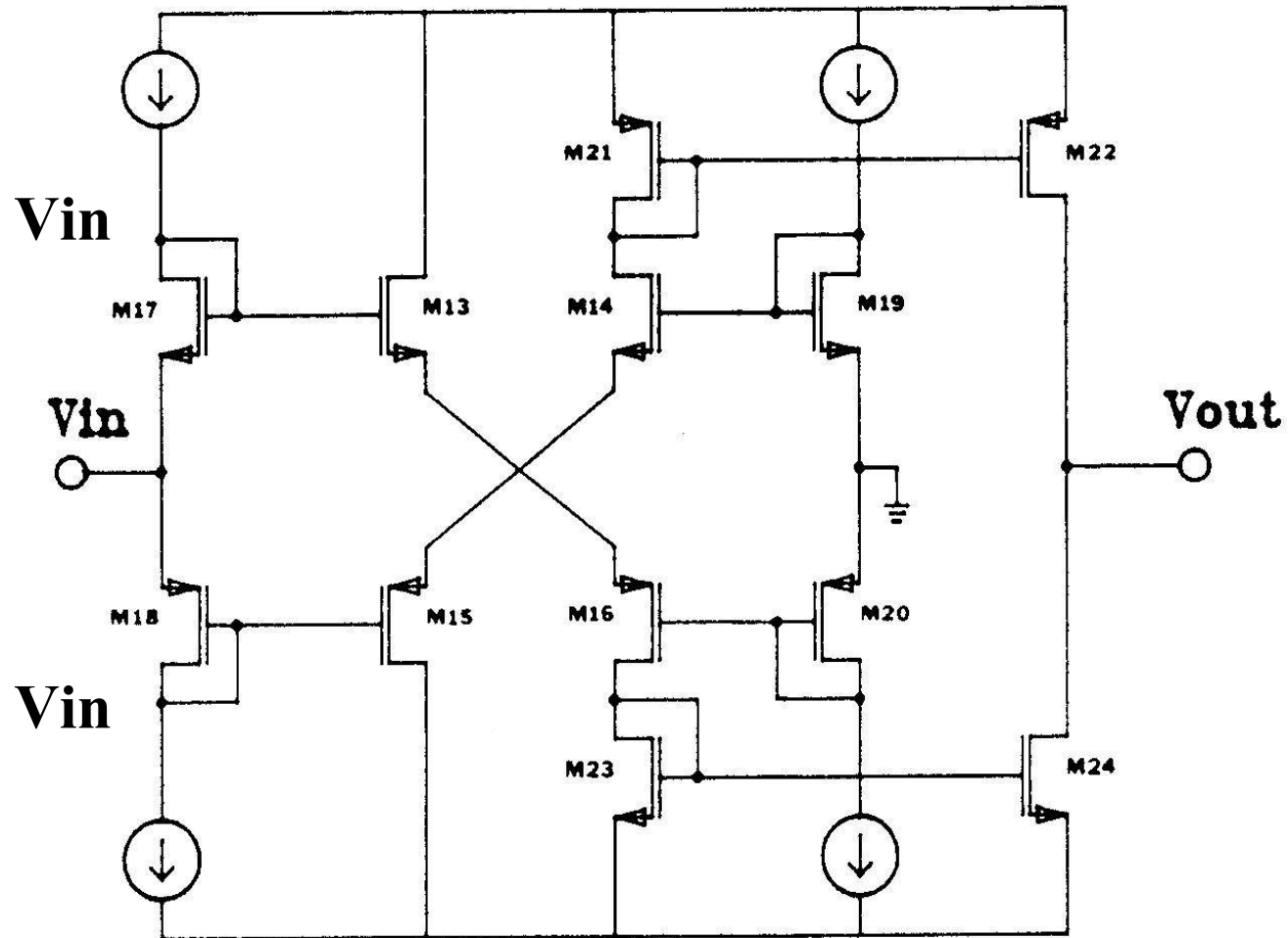
Ref. Halonen, 1987

Class AB fully differential amplifier



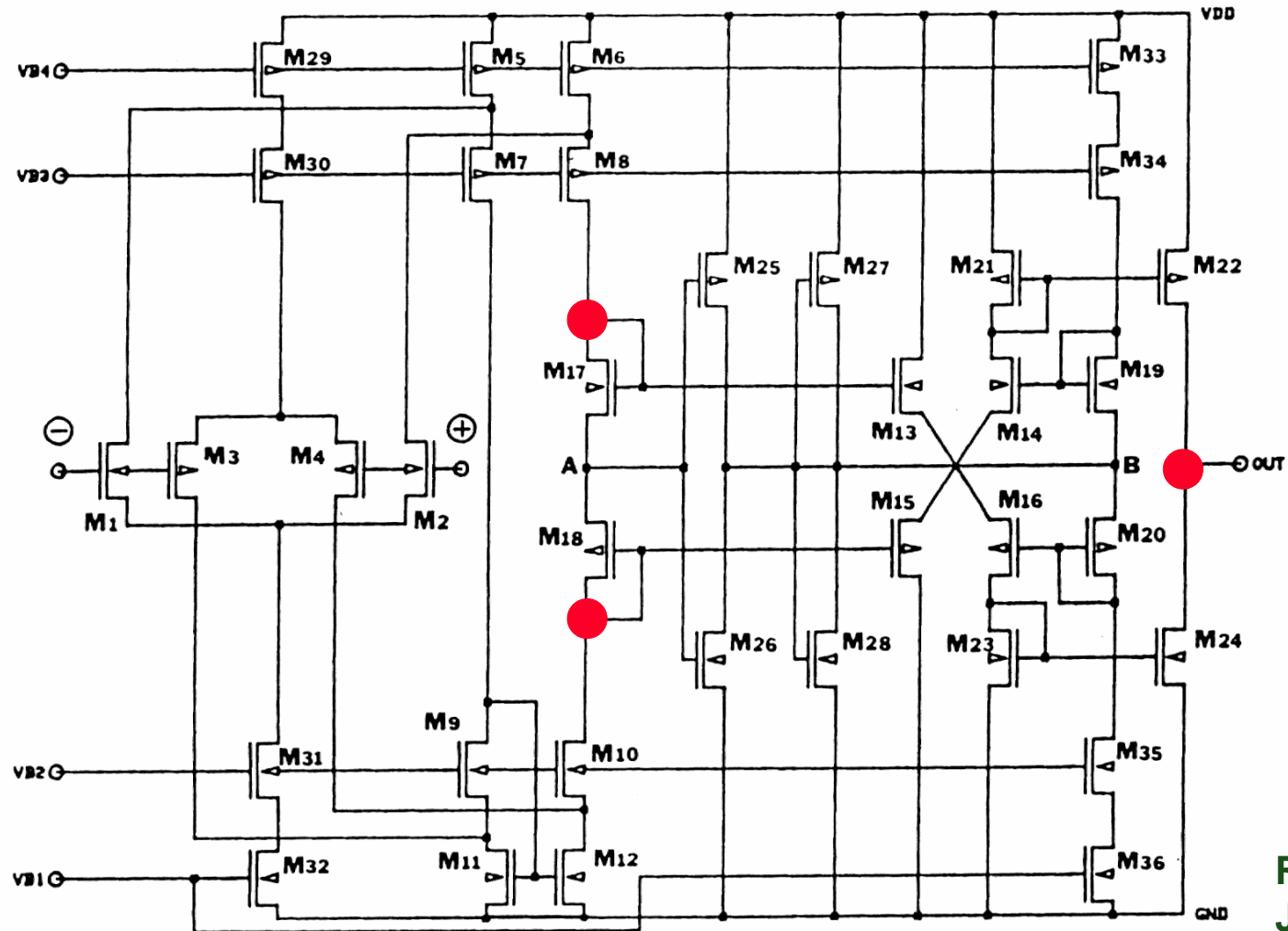
Ref.Lee,
JSSC
Dec.85,
1103-1113

Double-Push



Ref. Fischer, JSSC June 87, 330-340

Double-Push amp (Fischer)

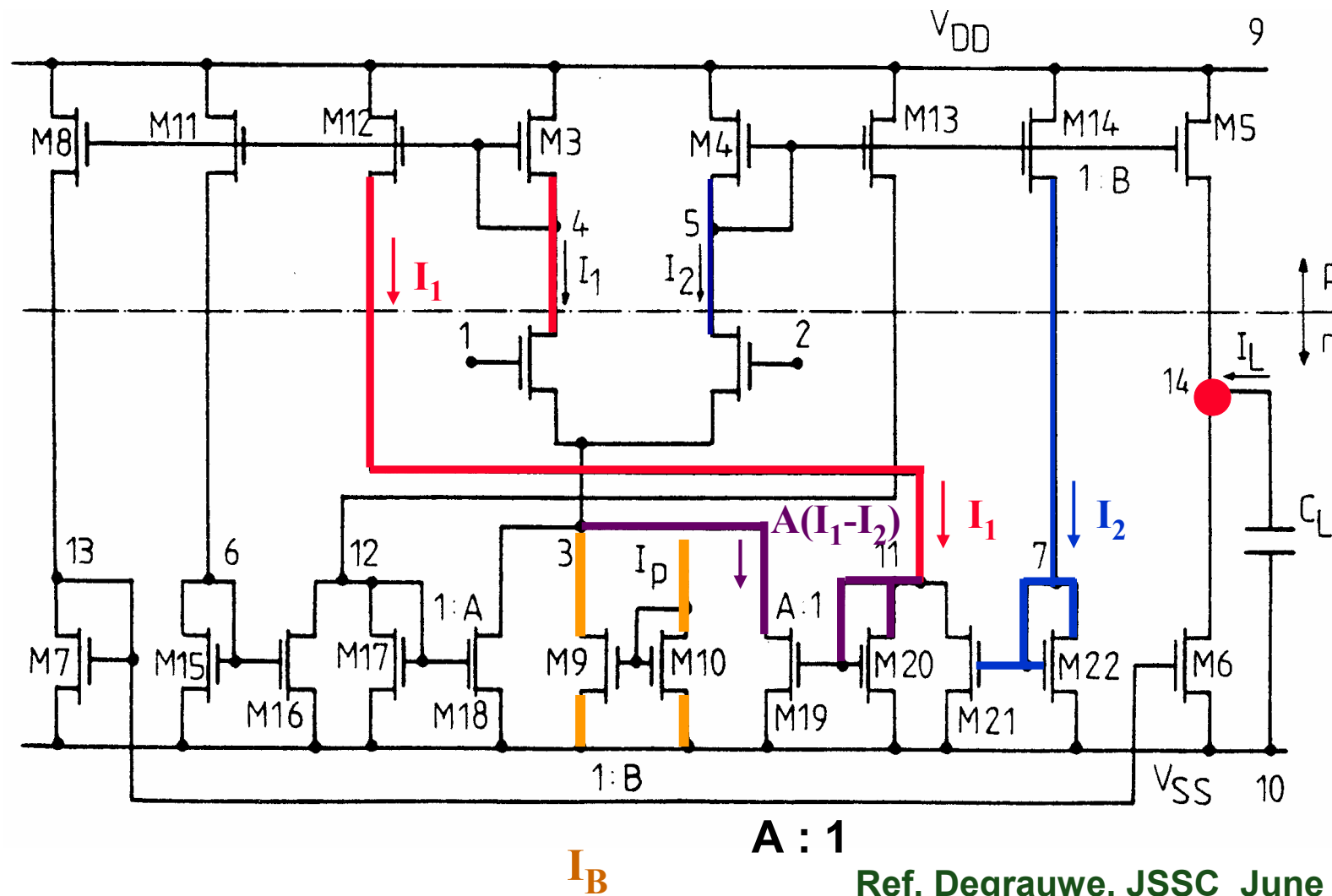


Ref. Fischer, JSSC
June 87, 330-340

Outline

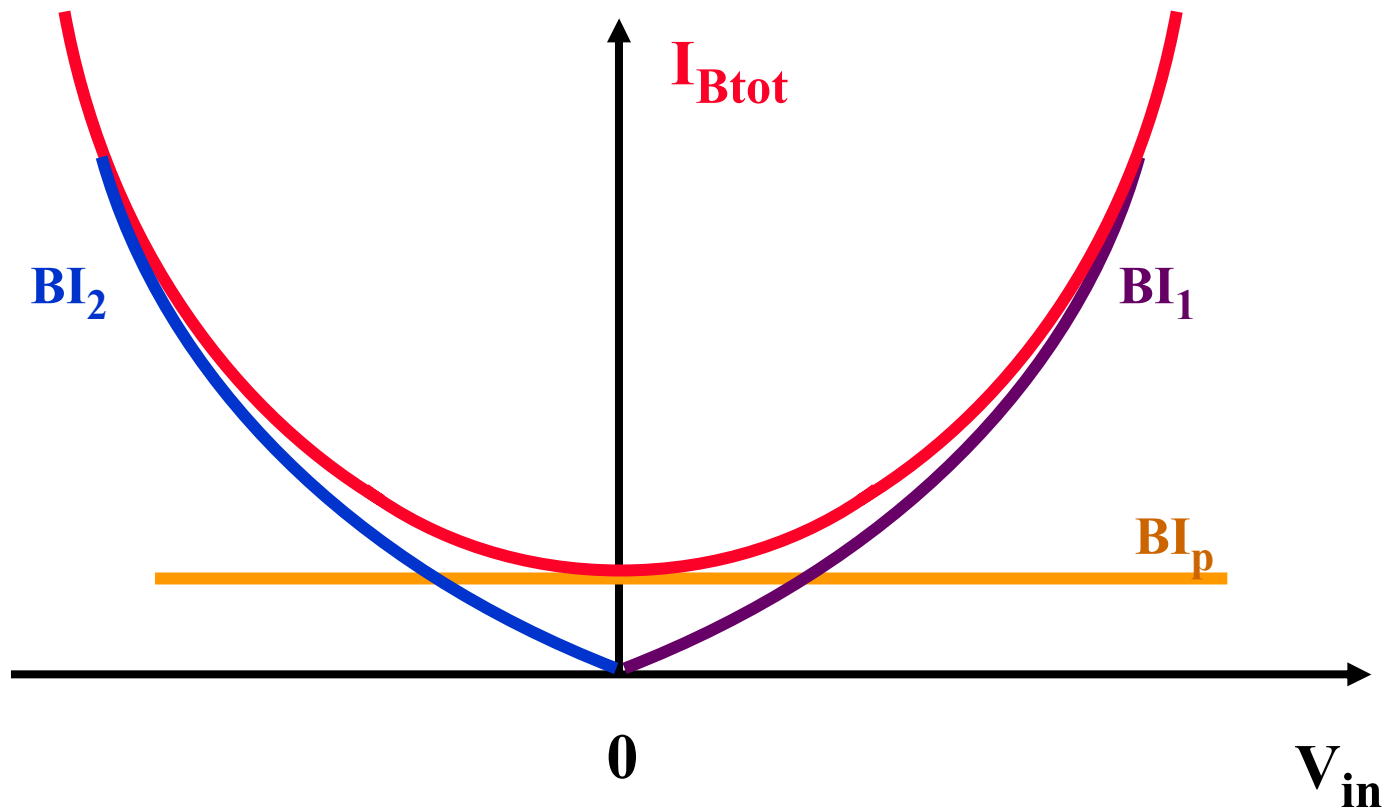
- Problems of class AB drivers
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- Current feedback and other principles
- Low-Voltage realizations

Adaptive Biasing Amplifier



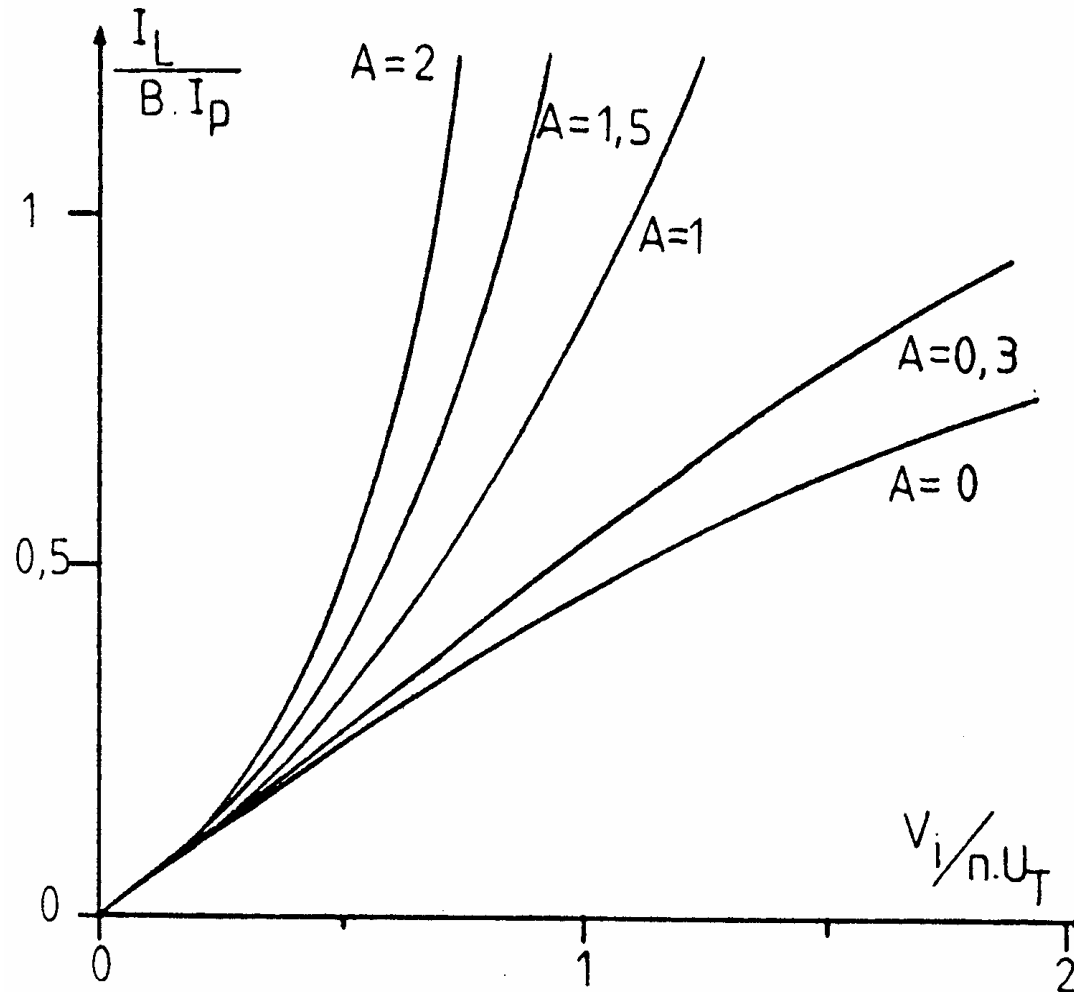
Ref. Degrauwe, JSSC June 82, 522-528

Adaptive Biasing Amplifier : biasing current



Ref. Degrauwe, JSSC June 82, 522-528

Adaptive Bias Amplifier: transfer curve



If $A \cdot \alpha_{\text{mis18-19}} \geq 1$



UN-stable

e.g. if $\alpha_{\text{mismatch}} = 10\%$

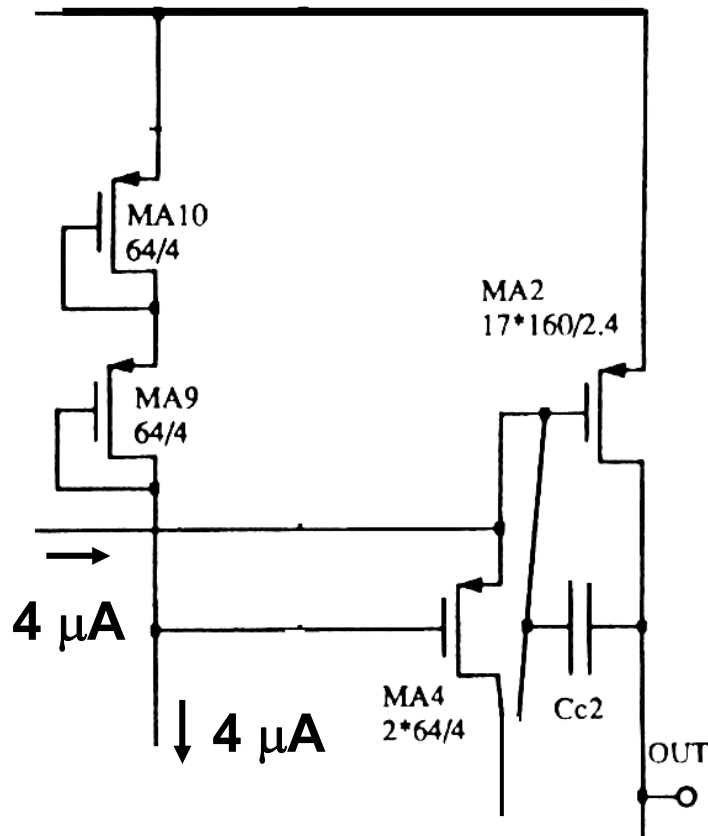


$A \ll 10$

Outline

- Problems of class AB drivers
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Quiescent current control with translinear loop



Translinear loop :

$$V_{GS2} + V_{GS4} = V_{GS9} + V_{GS10}$$

$$V_{GS2} - V_T = \sqrt{\frac{I_{DS2}}{K'_p W/L_2}}$$

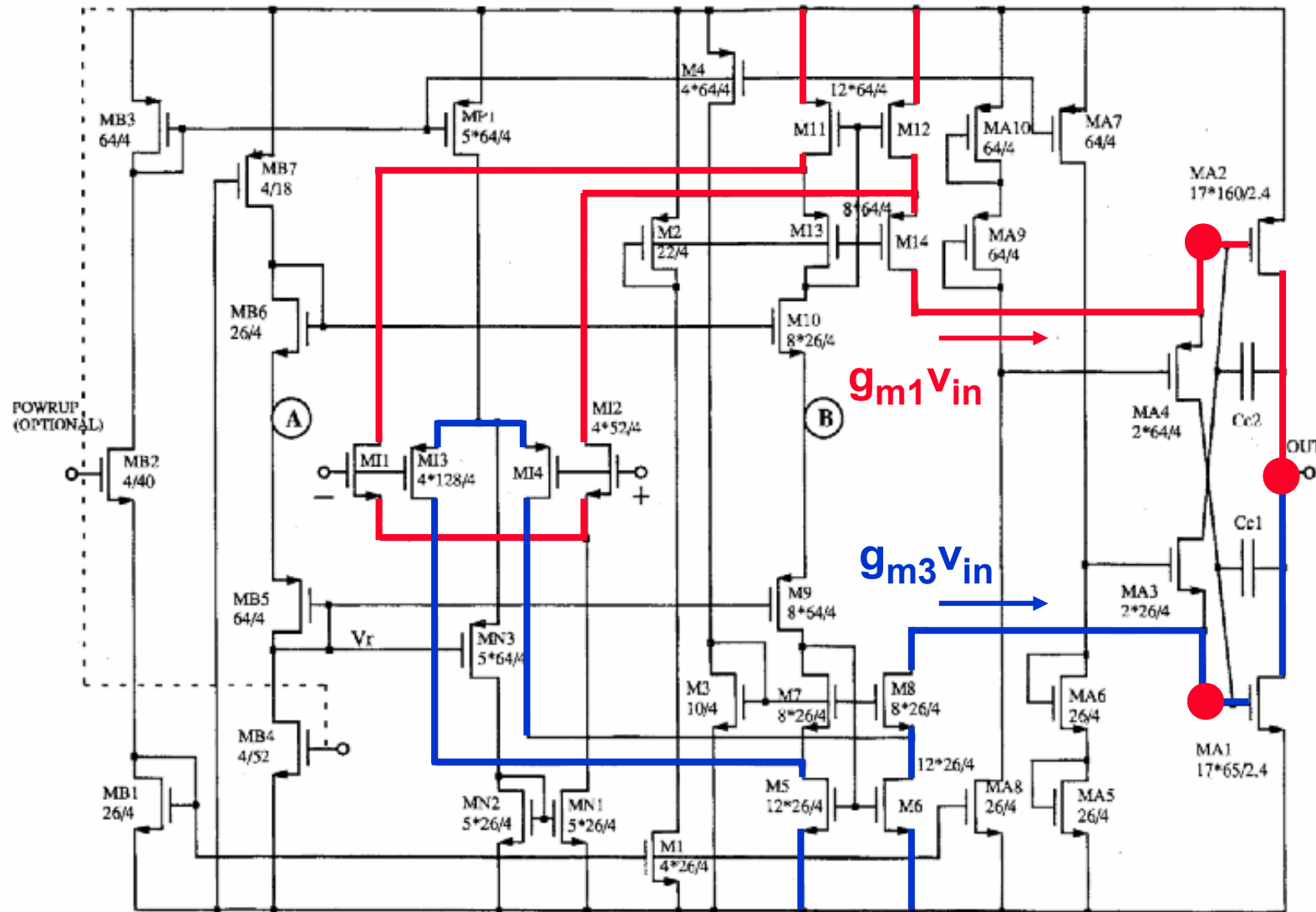
$$\sqrt{\frac{I_{DS2}}{W/L_2}} + \sqrt{\frac{I_{DS4}}{W/L_4}} = 2 \sqrt{\frac{I_{DS9}}{W/L_9}}$$

$$W/L_4 = 2 W/L_9 \text{ \& } W/L_2 = 70.8 W/L_9$$

$$I_{DS2} \approx 473 \mu A \text{ since } I_{DS9} \approx 4 \mu A$$

$$\frac{I_{DS2}}{I_{DS9}} = \frac{W/L_2}{W/L_9} \left(2 - \frac{1}{\sqrt{2}}\right)^2 \approx 118$$

Ref. : Wu etal, JSSC Jan.1994, pp.63-66



14 MHz
/ 11pF

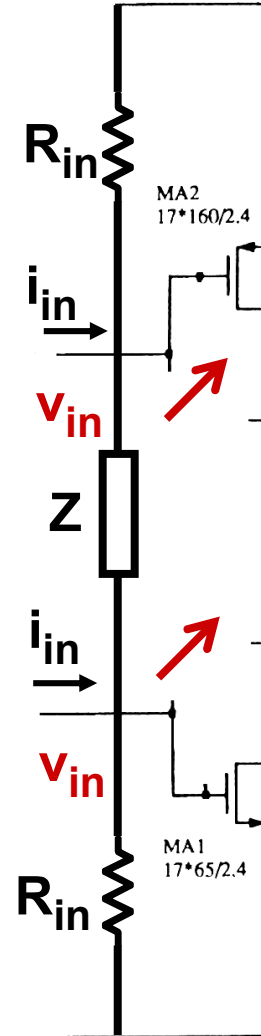
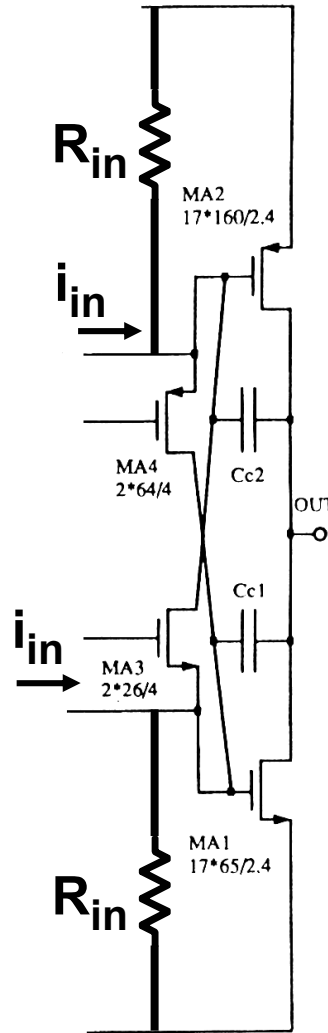
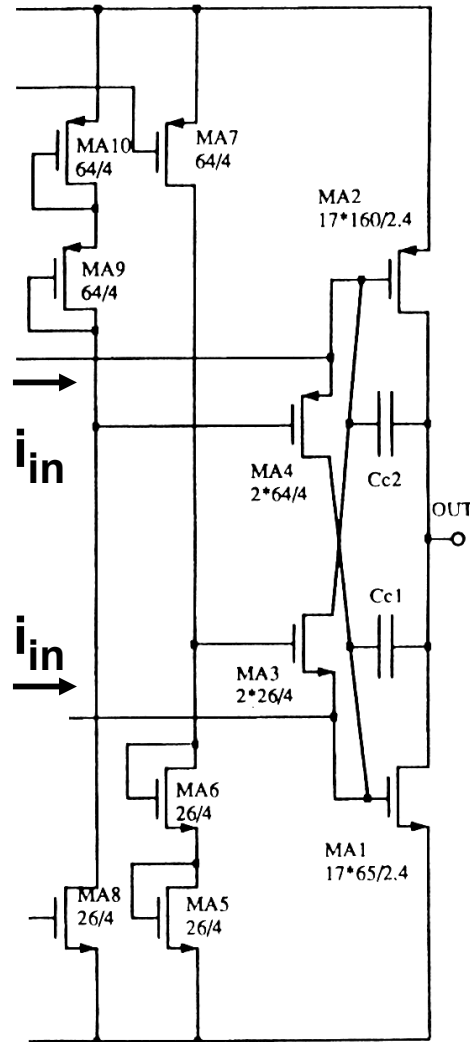
5.6 MHz
/ 100pF

4 V/ μ s

36 nV/ $\sqrt{\text{Hz}}$

5 V
0.4 mA

Output stage : gain



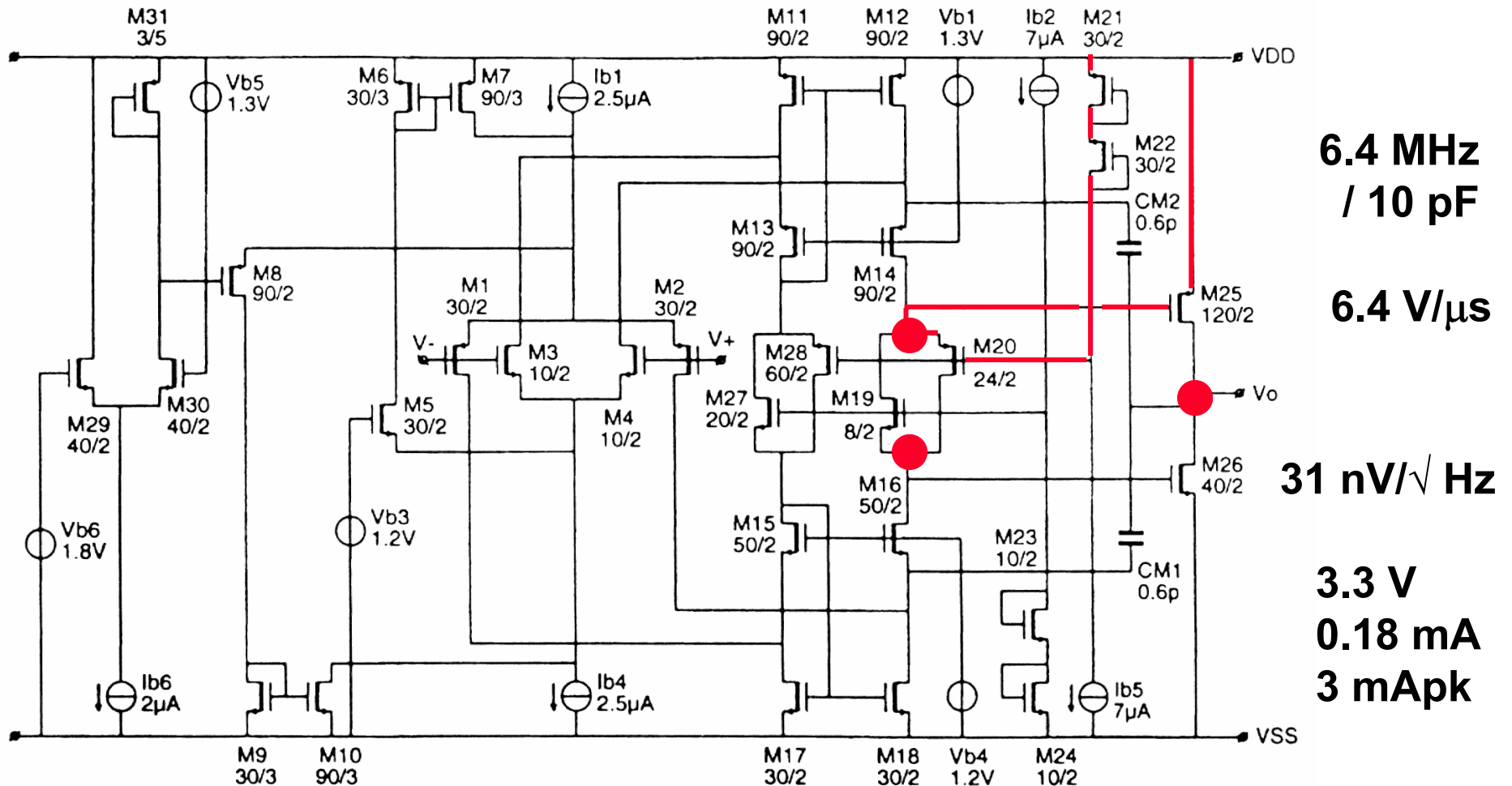
$$i_{in} = g_{m1} v_{+}$$

$$\frac{v_{in}}{i_{in}} = R_{in}$$

$$\frac{v_{out}}{v_{in}} = 2g_{mA1}R_L$$

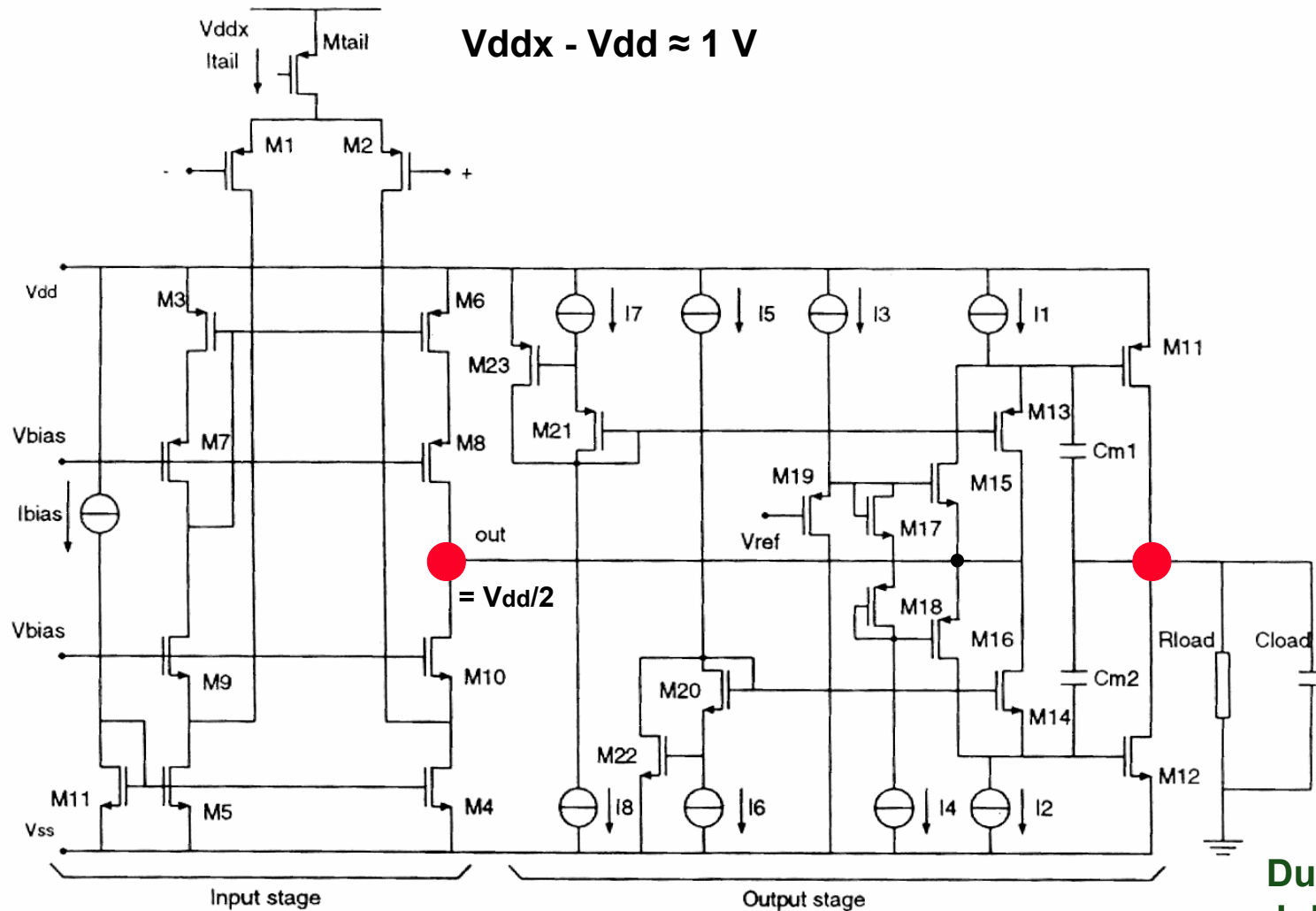
$$A_v = 2g_{m1}R_{in}g_{mA1}R_L$$

Class AB amplifier with translinear loop



Ref. Hogervorst, JSSC Dec 94, 1504-1512

Class-AB Opamp with voltage multiplier



$V_{ddx} - V_{dd} \approx 1 \text{ V}$

1.8 - 3.3 V

0.75 mA

6.5 MHz

On 3 V :

2.8 V_{ptpt}

THD :

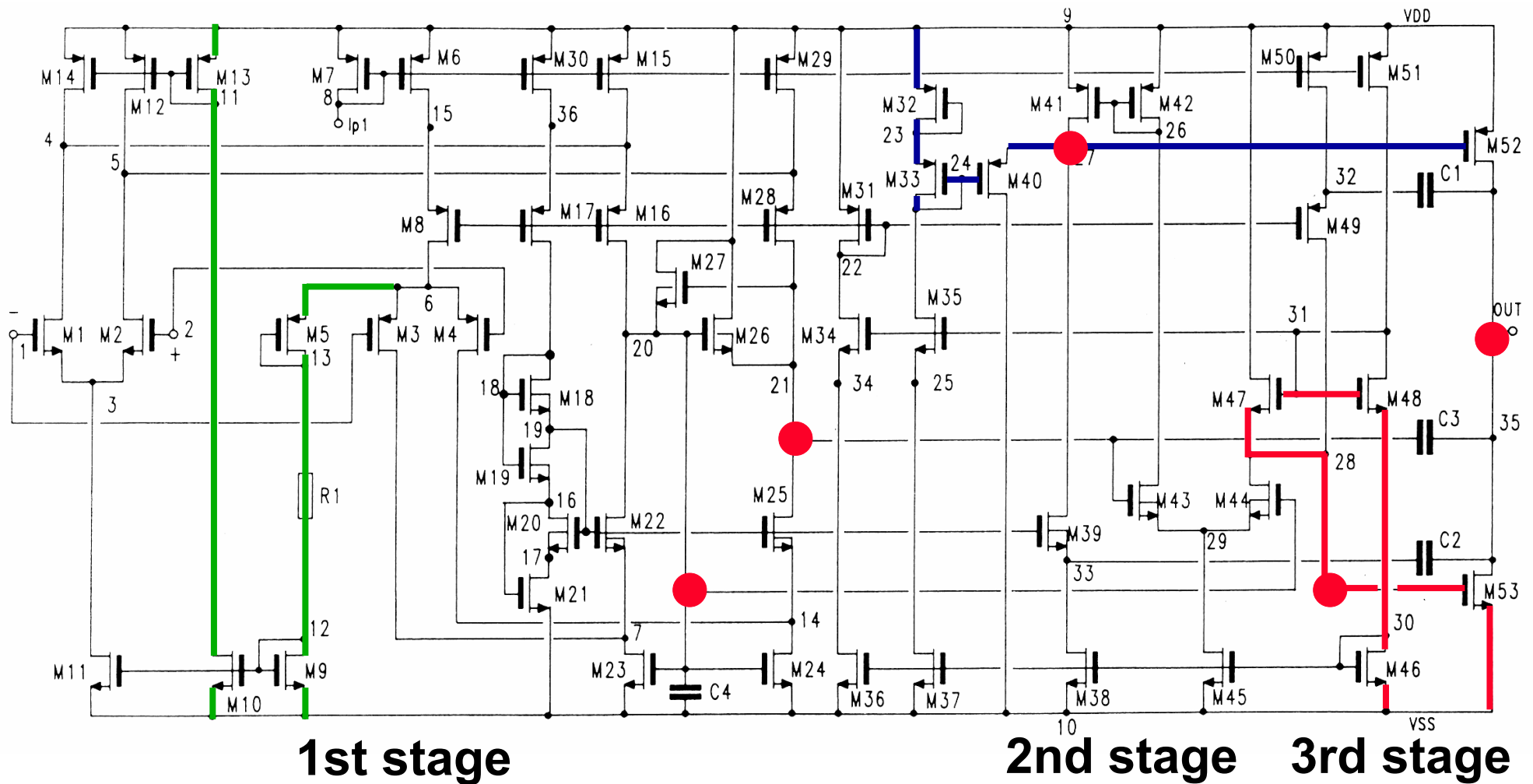
-90 dB / 10kΩ

-81 dB / 32 Ω

0.5 μm CMOS

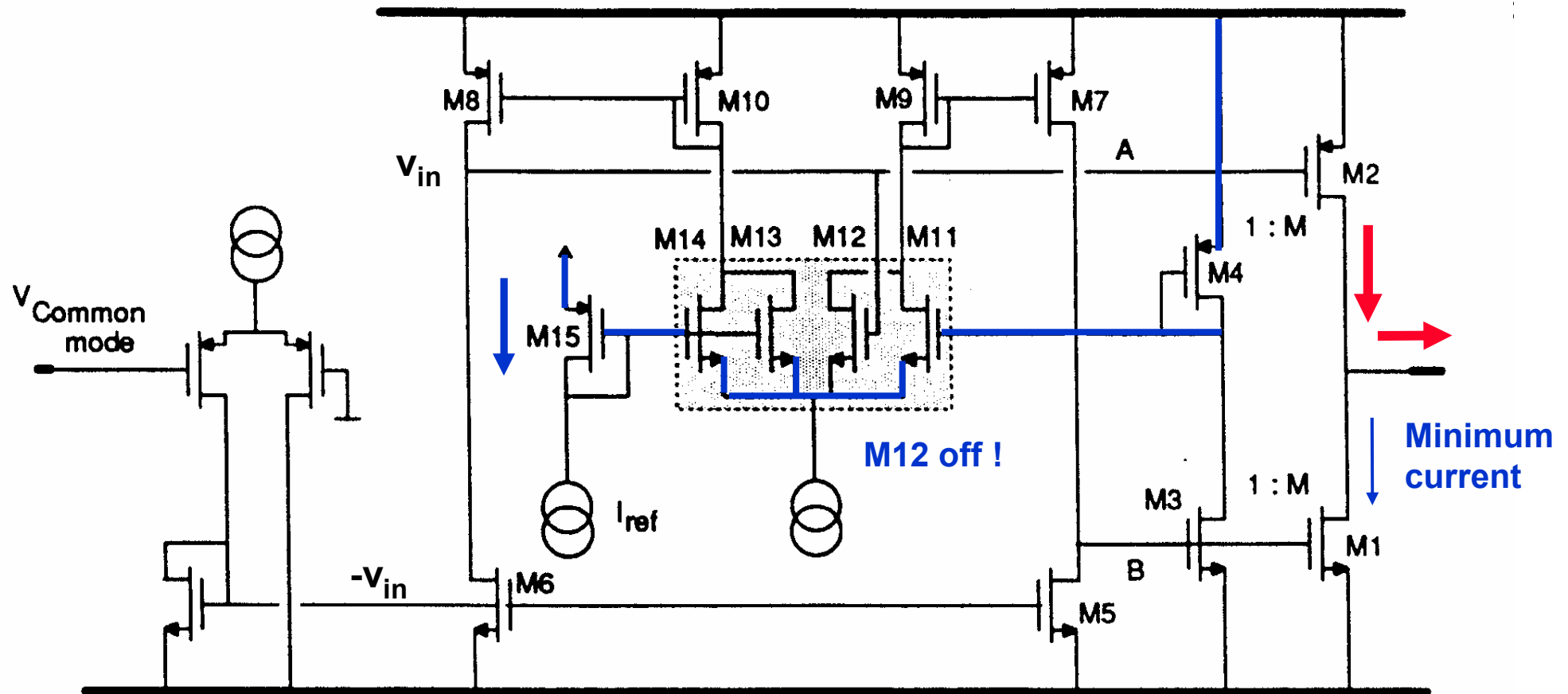
Duisters, .., JSSC
July 98, pp.947-955

Three-stage Modified Current Mirror



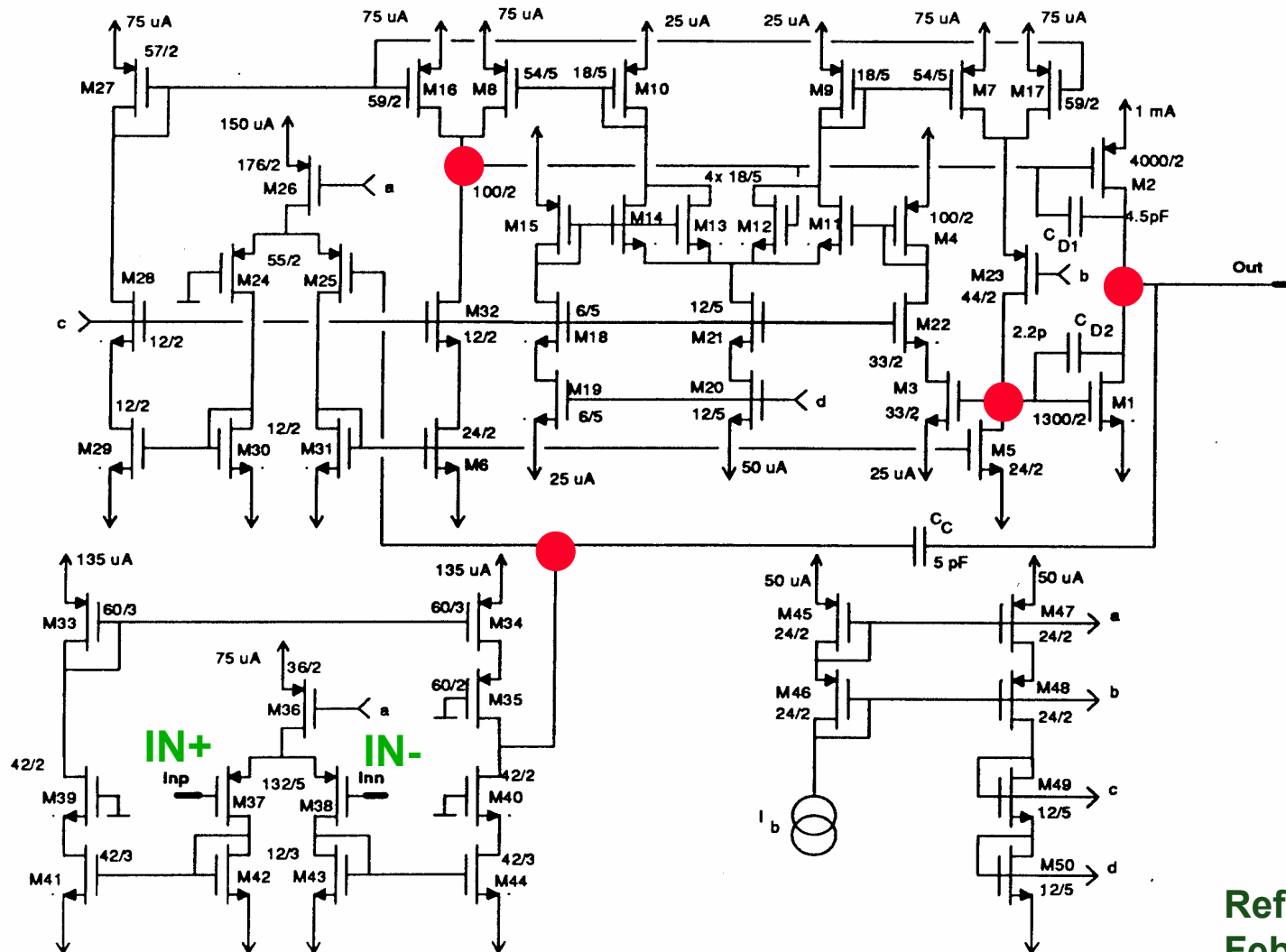
Pardoen, ..., JSSC April 90, 501-504

Translinear I_Q Control



Ref. Op 't Eynde, JSSC Febr.90, 265-273

Translinear I_Q Control

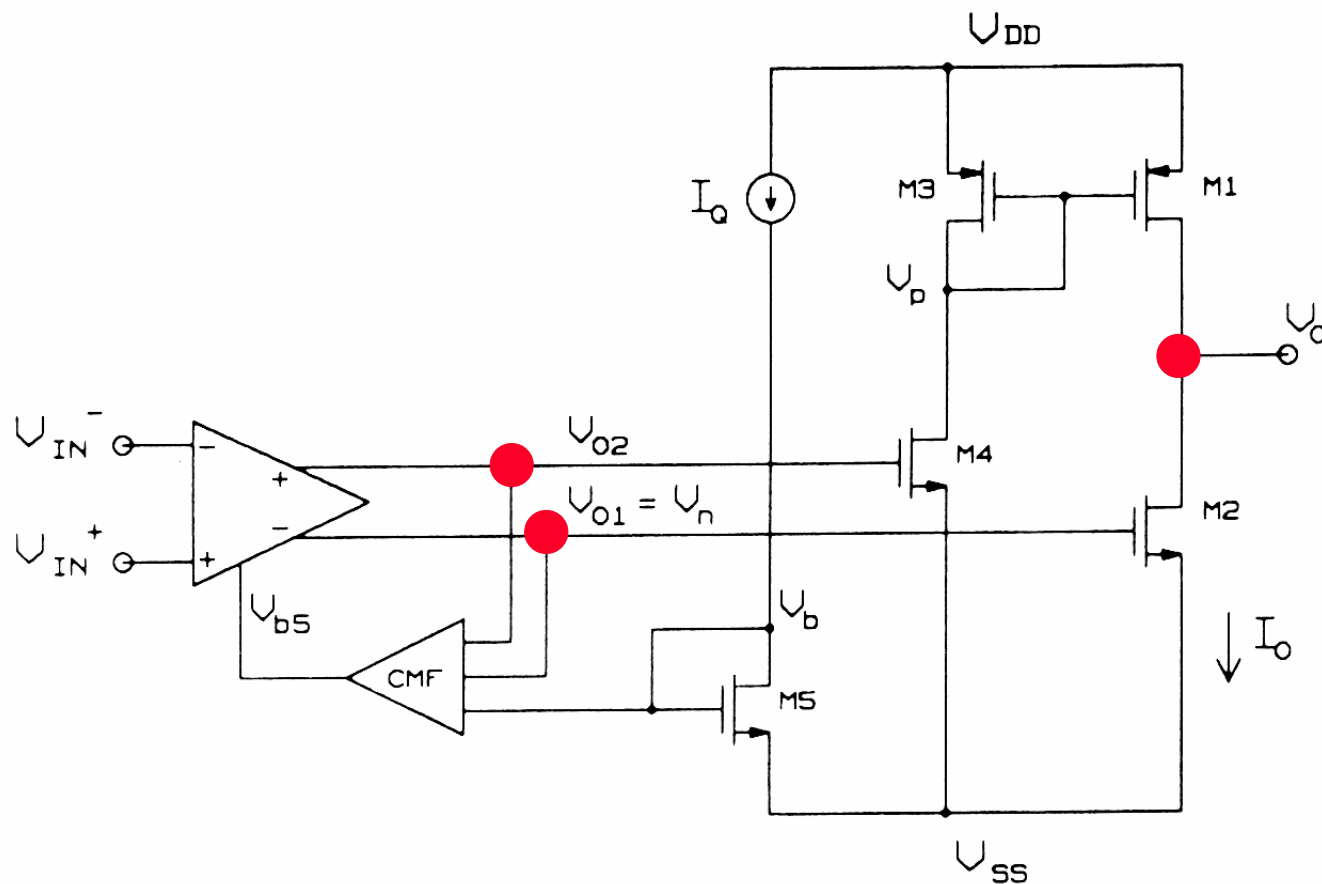


**3 stage
Class-AB
Amplifier**

I_Q control

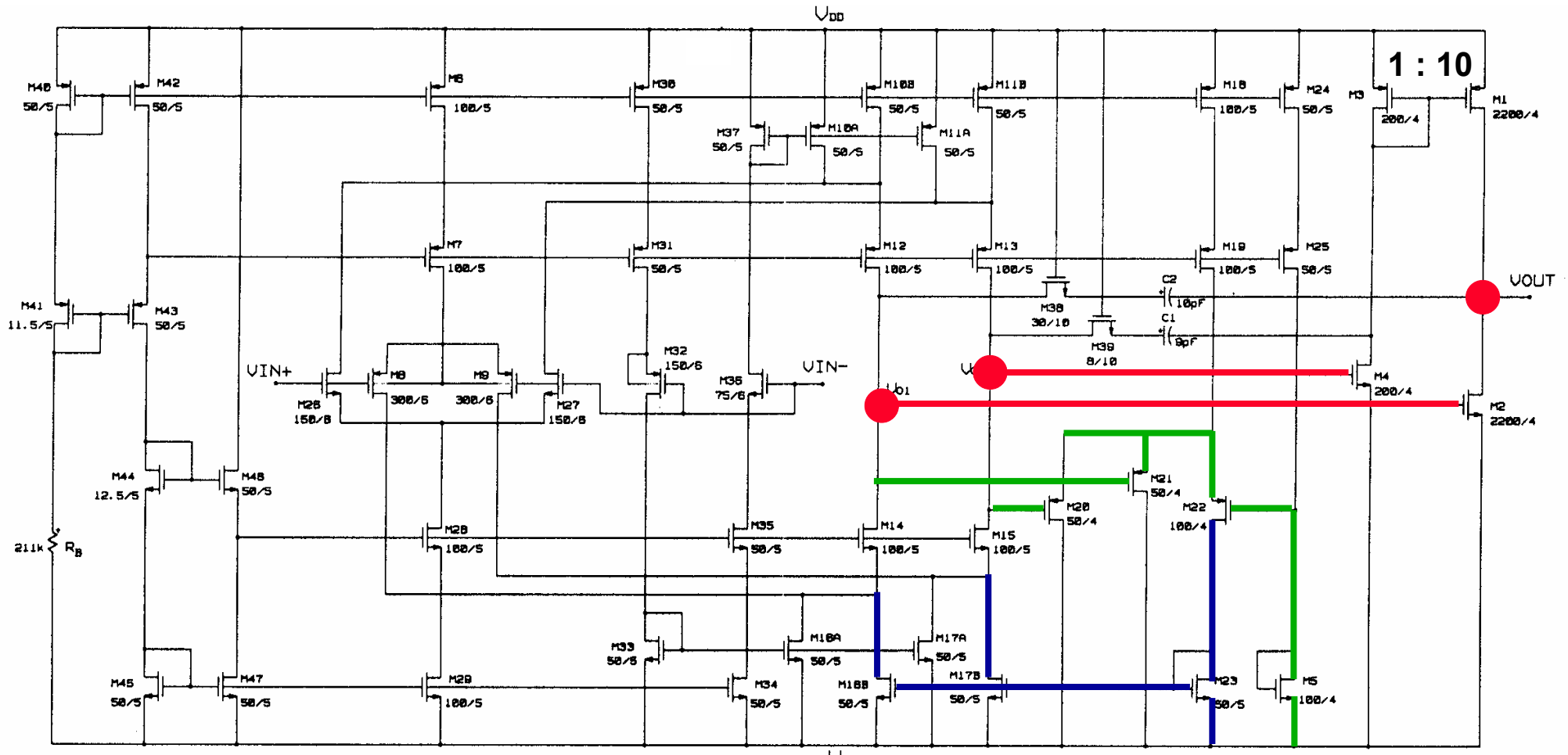
Ref. Op 't Eynde, JSSC
Febr.90, 265-273

Class-AB amplifier with differential drive



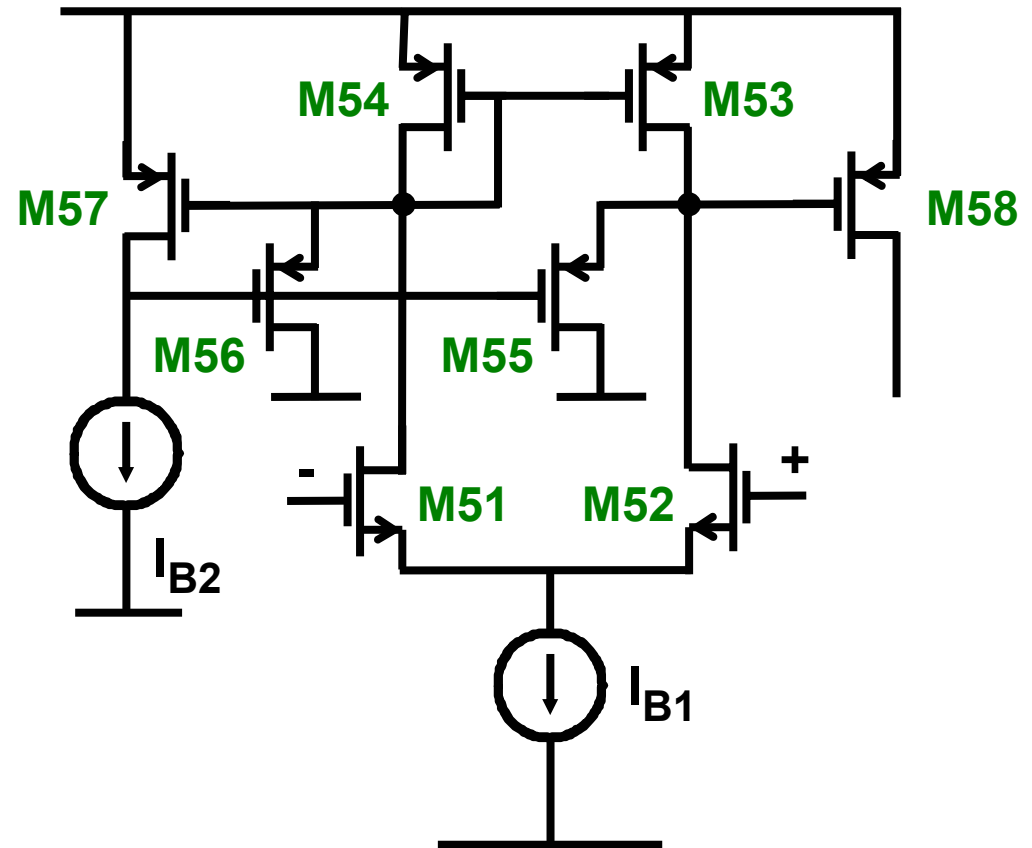
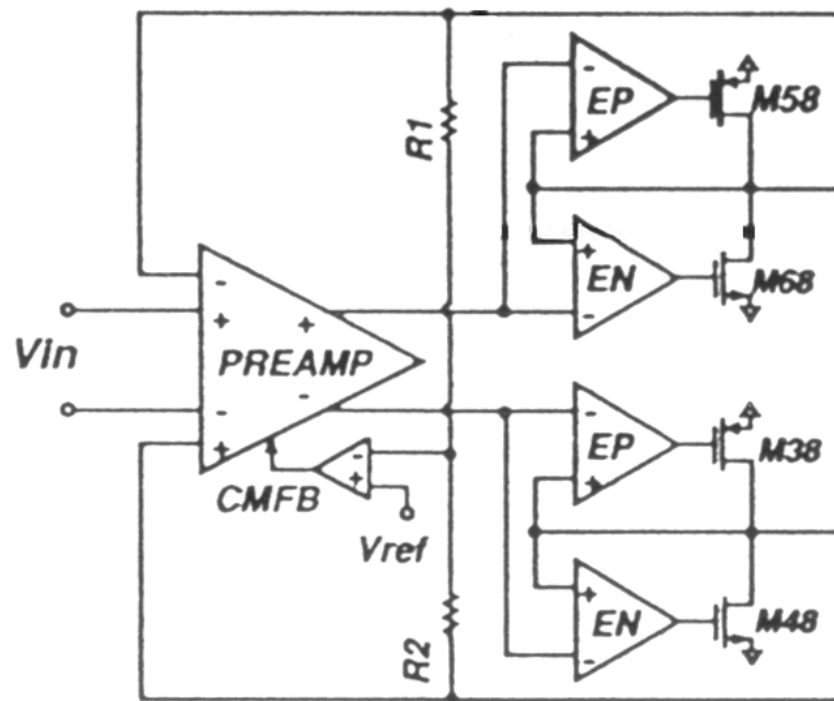
Ref. Babanezhad, JSSC Dec.88, 1414-1417

Differentially driven stage



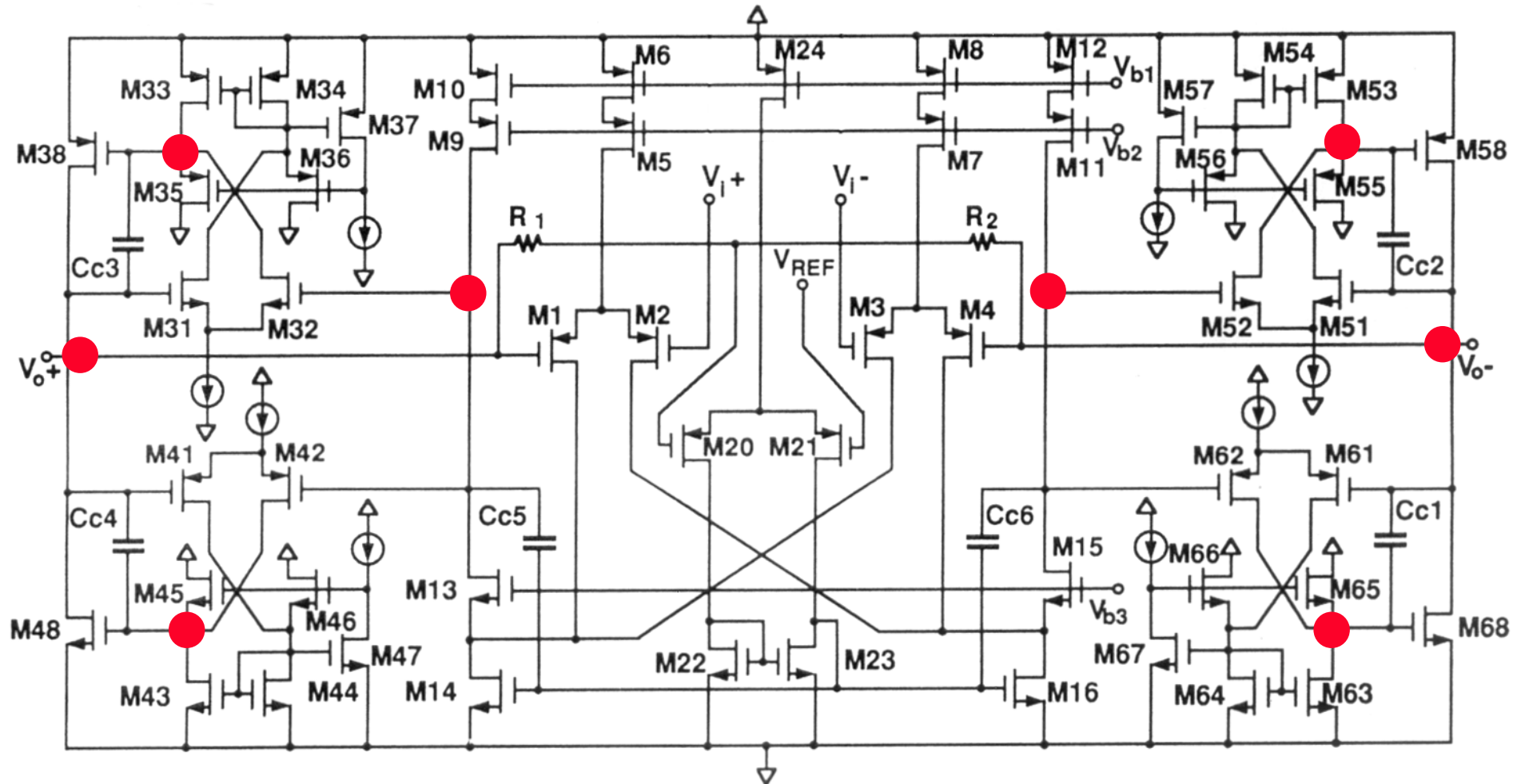
Rail-to-rail input **CMFB** + **I_Q**

Class-AB amplifier with high linearity



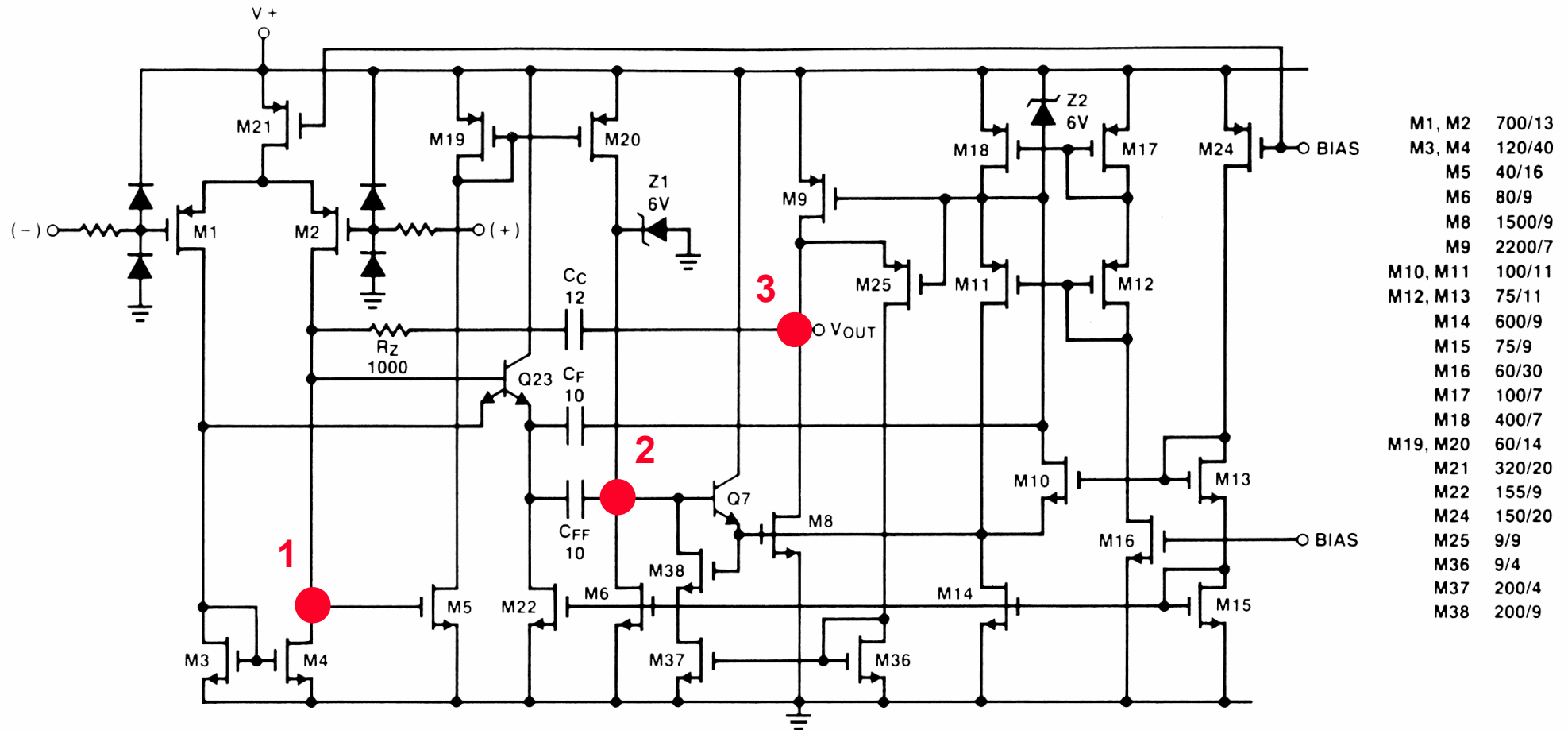
Ref. Khorramabadi, JSSC April 92, 539-544

Class-AB amplifier with high linearity



Ref. Khorramabadi, JSSC April 92, 539-544

Three-stage class AB amplifier with FF

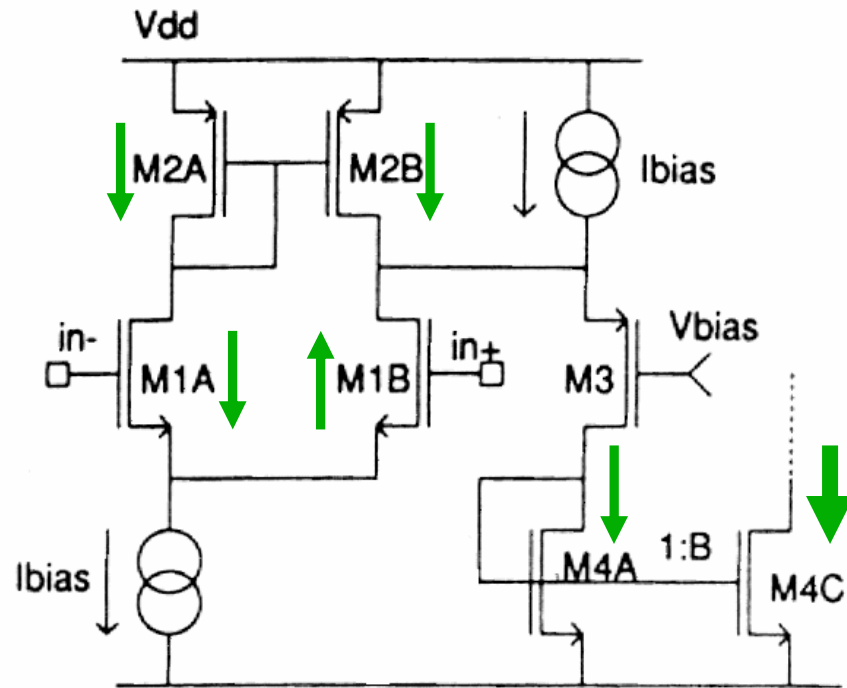


Ref. Monticelli JSSC Dec.86, 1026-1034

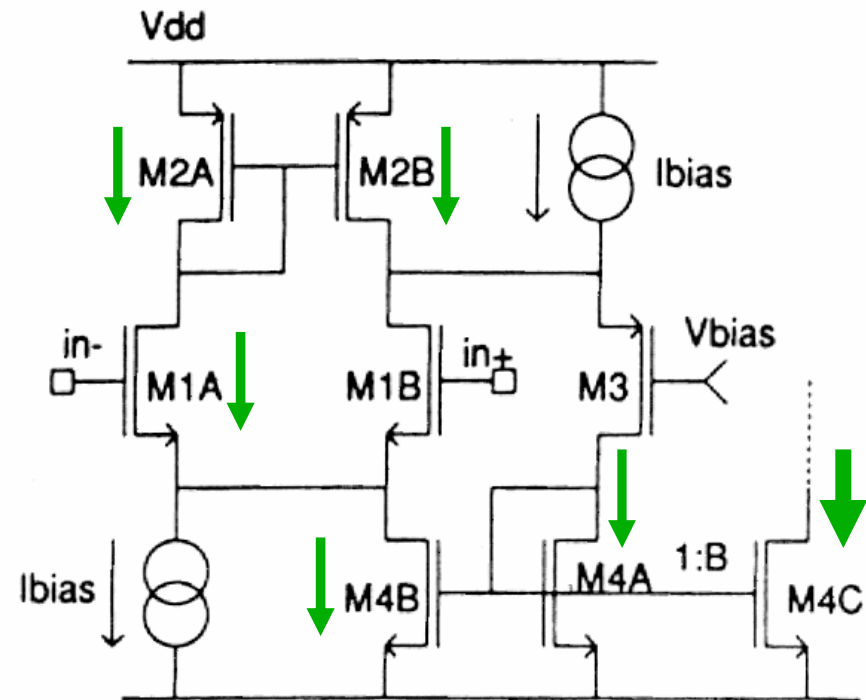
Outline

- Problems of class AB drivers
- Cross-coupled quads
- Adaptive biasing
- I_Q control with translinear circuits, etc.
- Current feedback and other principles
- Low-Voltage realizations

Current feedback



Folded Cascode OTA



Current Feedback

Ref. Callewaert, JSSC June 90, 684-691

Two-stage Miller Amplifier with current FB

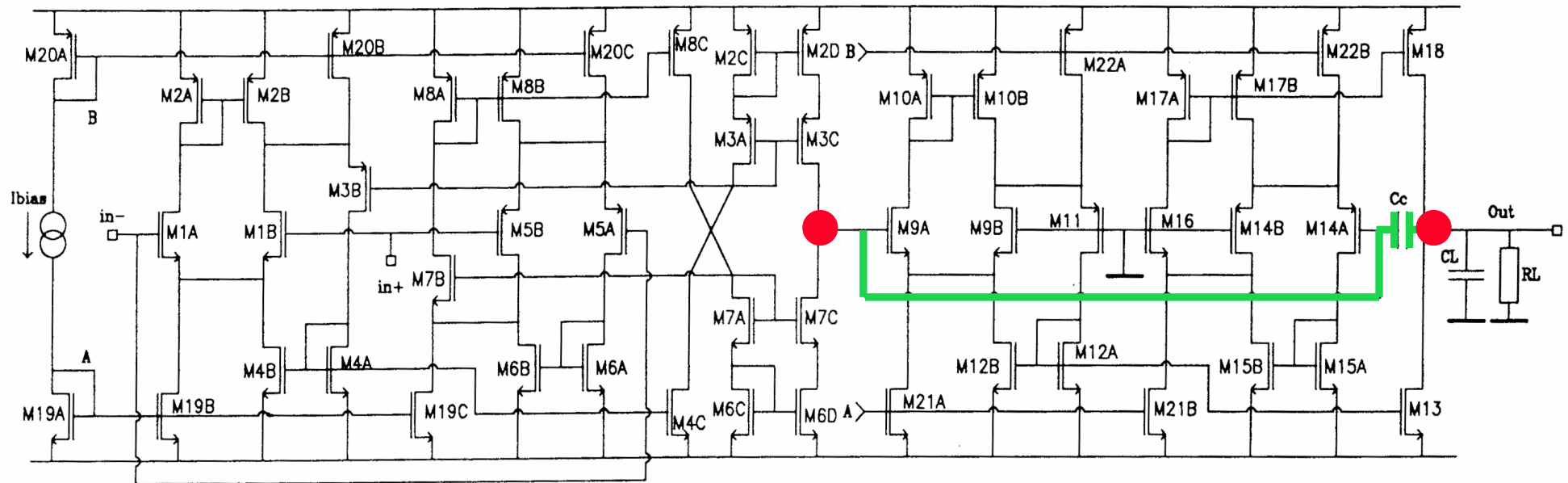
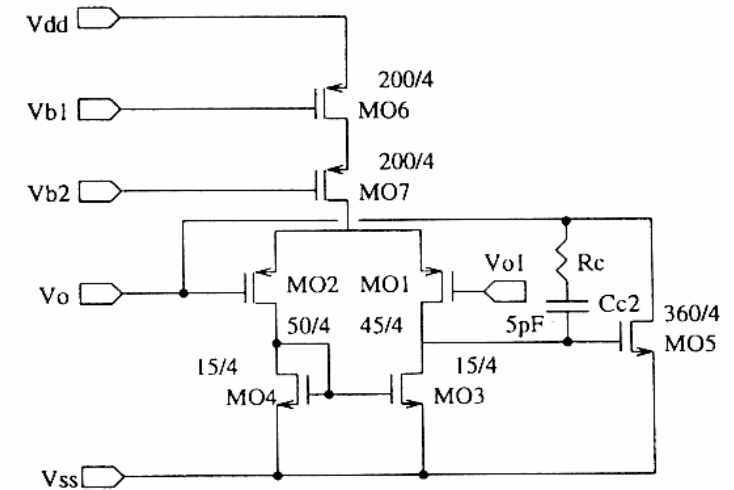
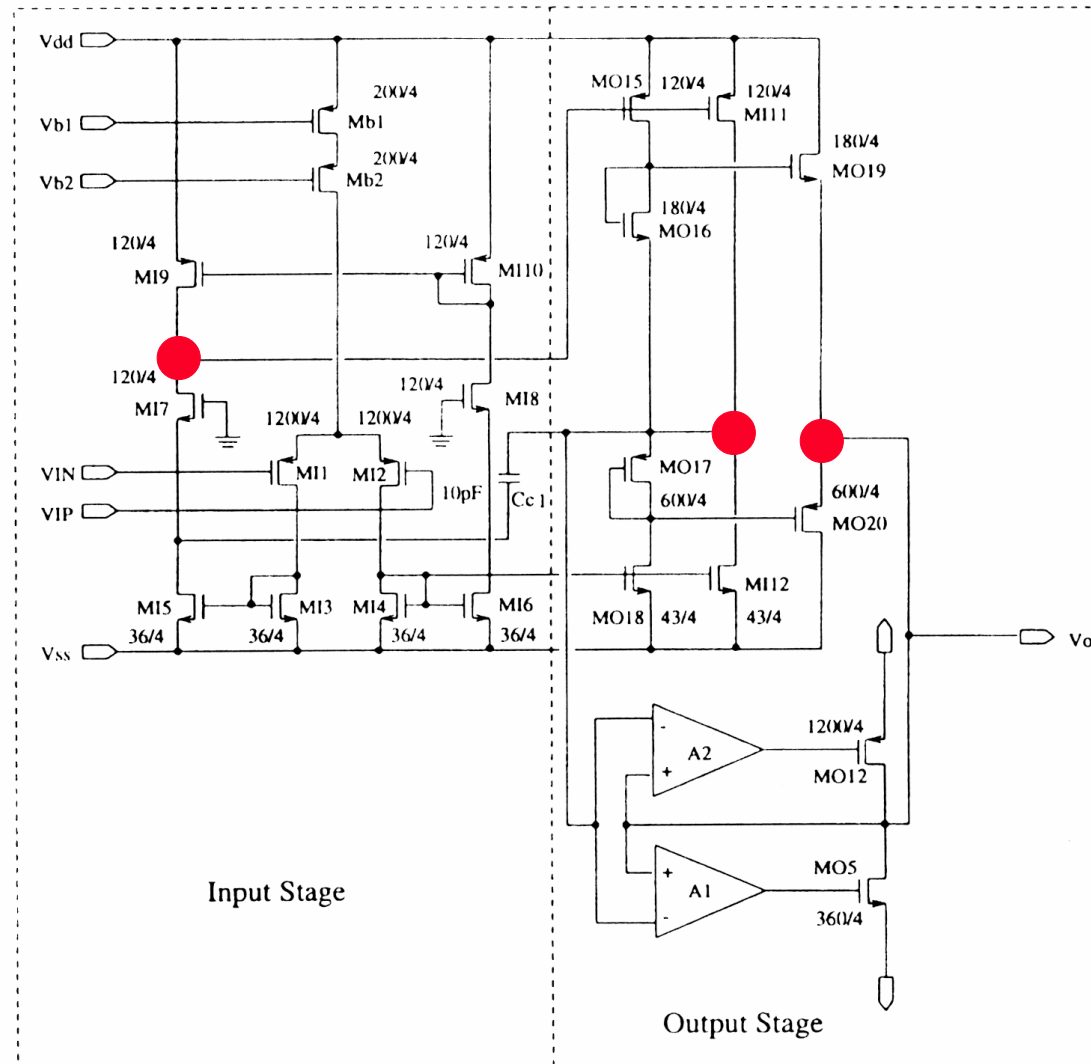


Fig. 11. Circuit diagram of the amplifier with both input and output stages based on the new class AB principle.

4 current feedback stages
2 stage Miller amplifier

Ref. Callewaert, JSSC June 90, 684-691

Low-distortion symmetrical class-AB amplifier



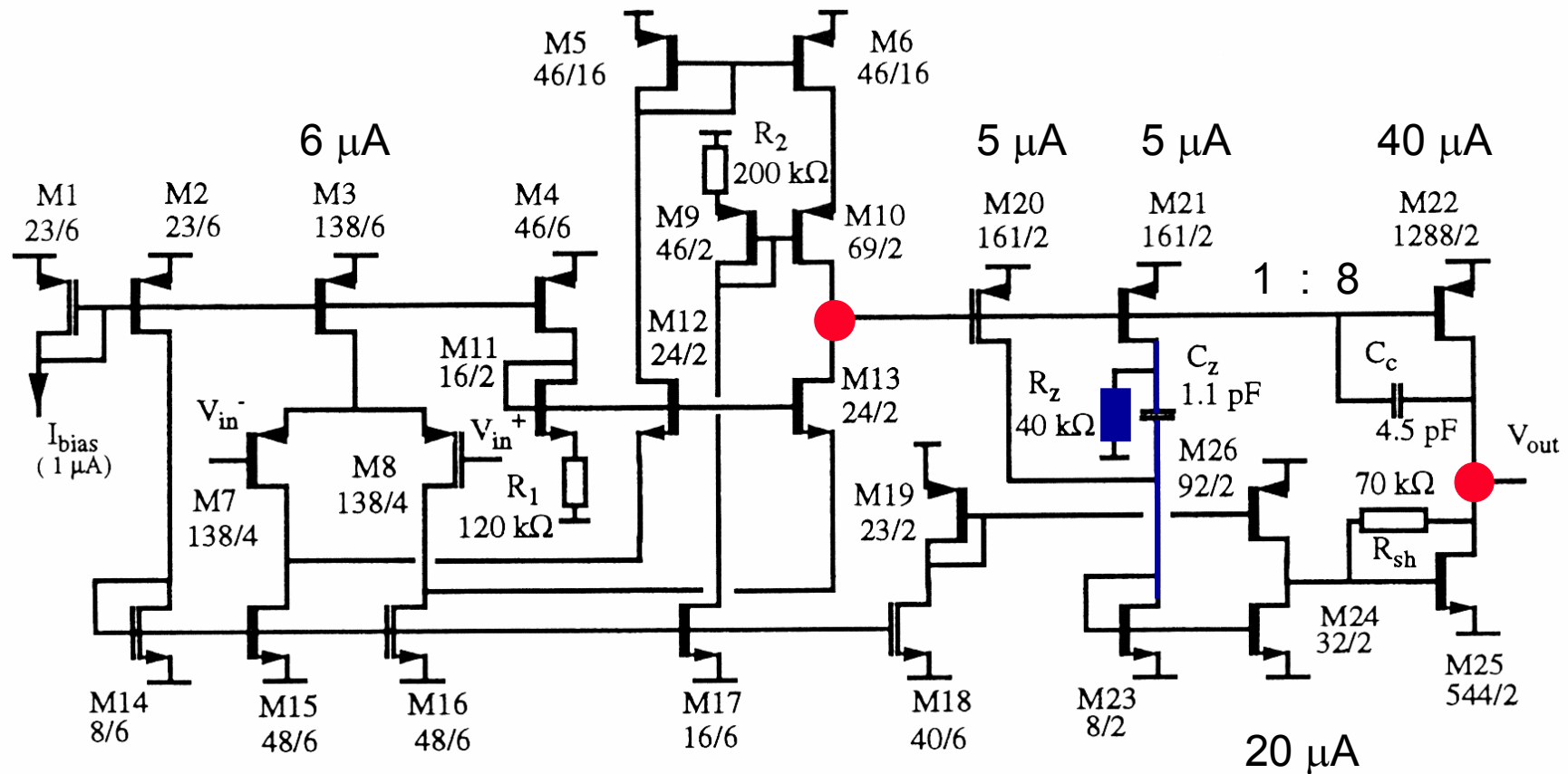
**Class-AB source foll.
In parallel with
Class-AB power amp.**

Ref. Saether, JSSC
Febr.96, 255-258

Outline

- **Problems of class AB drivers**
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- **Current feedback and other principles**
- **Low-Voltage realizations**

1.5 V supply voltage class-AB amp.

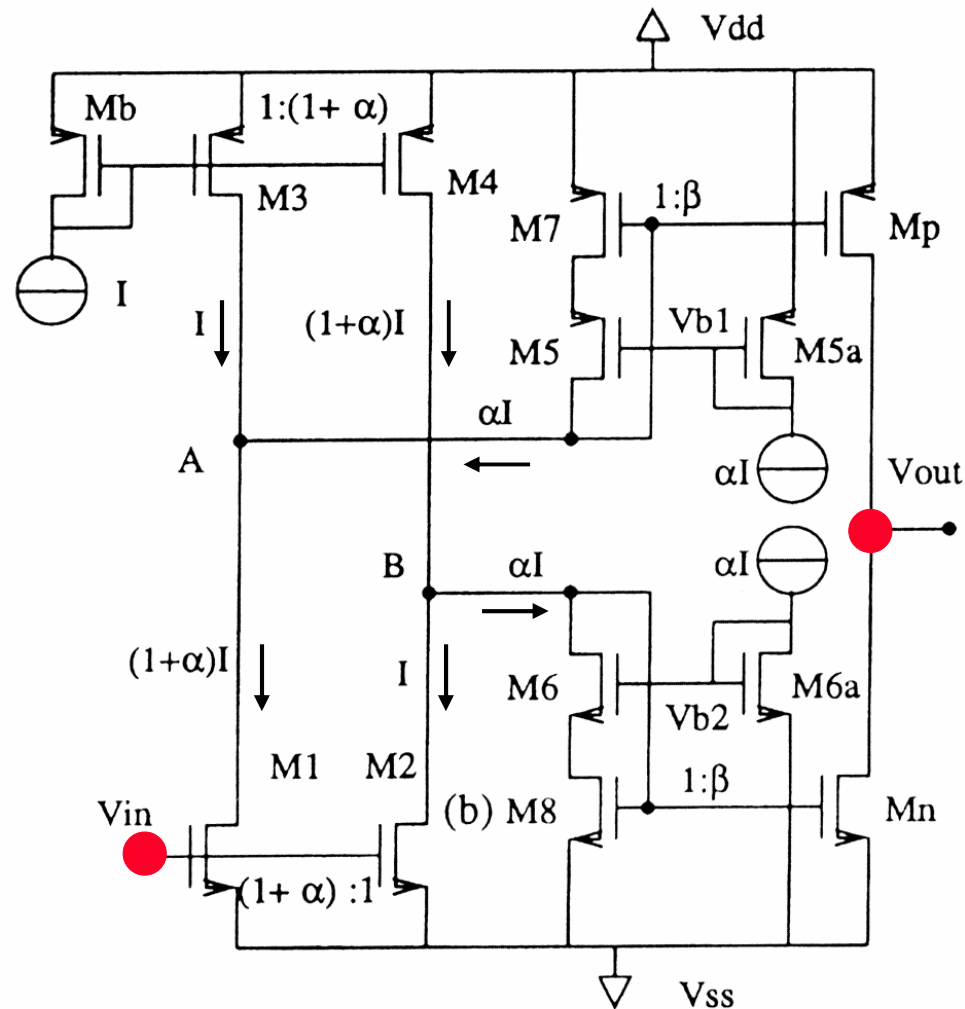


Zero

1.5 V 90 μA 1 MHz/150 pF

Ref. Van Dongen, JSSC Dec.95, 1333-1337

1.5 V class AB driver principle



**Maximum voltage swing
on A & B:**

$$\alpha \approx 0.2$$

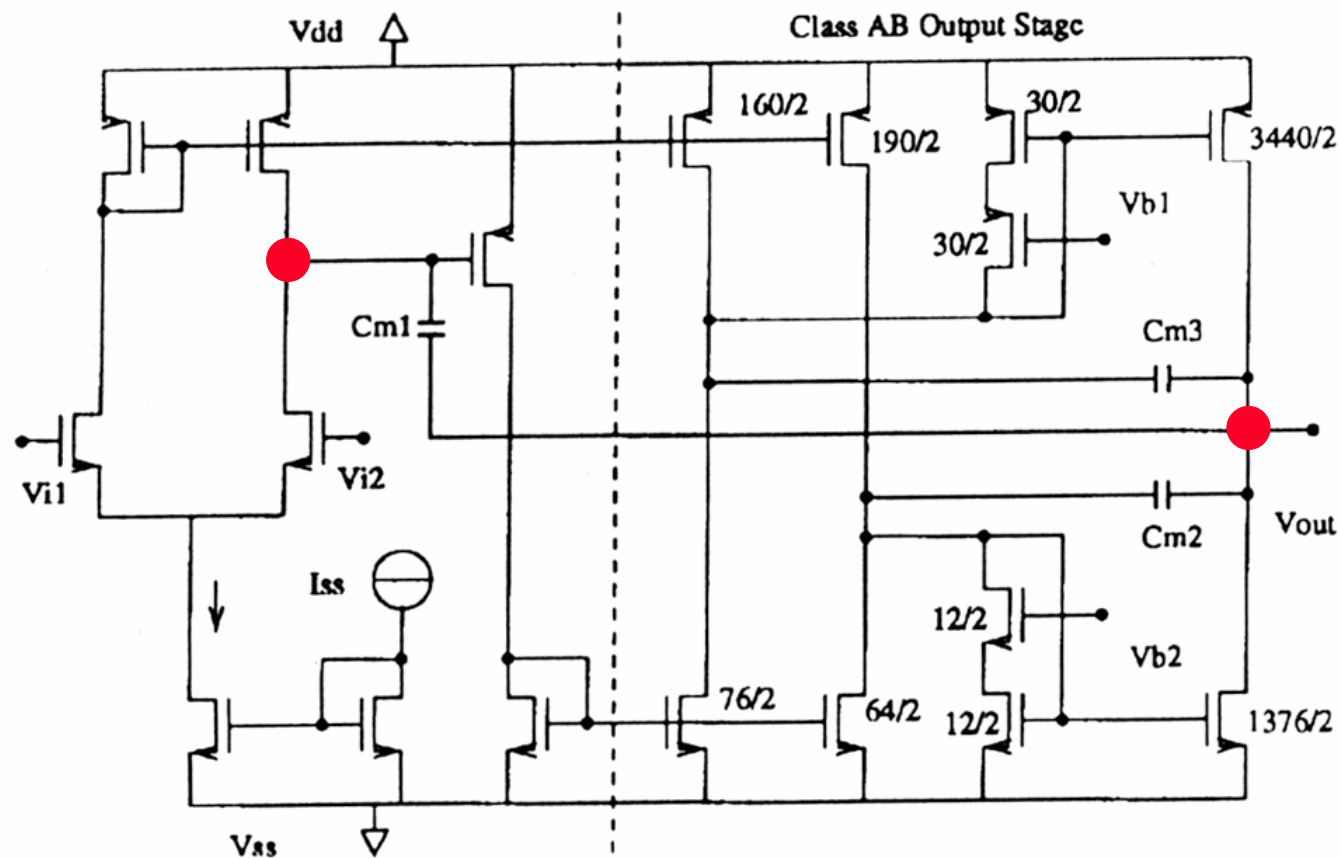
For larger α :

- less gain (more current)
- more mismatch and distortion

$$\beta \approx 120$$

You, etal, JSSC June 98, pp. 915-920

1.5 V class AB driver opamp



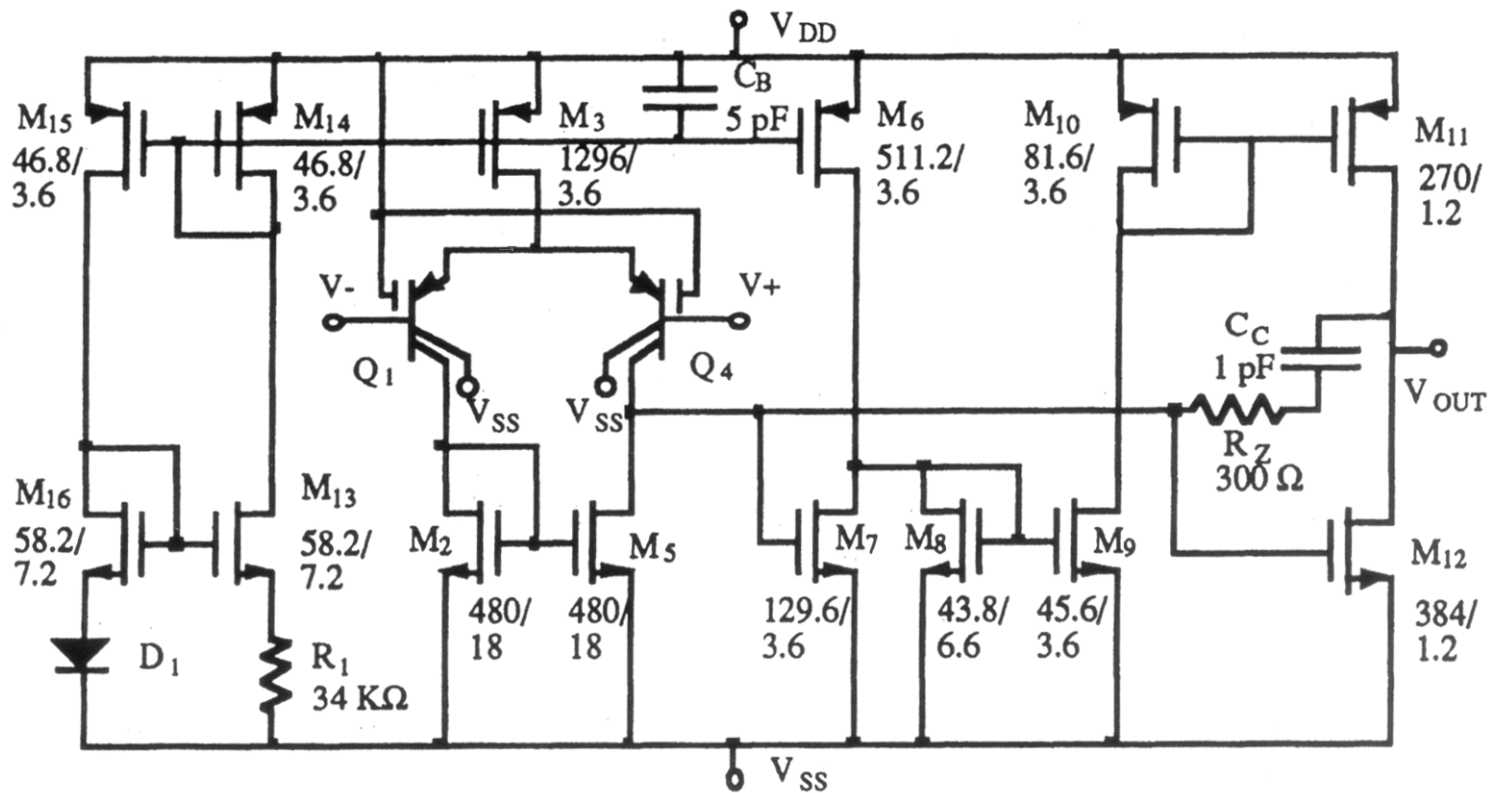
$$I_Q = 300 \mu A$$

$$100 \text{ pF} // 200 \Omega$$

Two stage Miller compensation

You, etal, JSSC June 98, pp. 915-920

BiCMOS low-voltage opamp

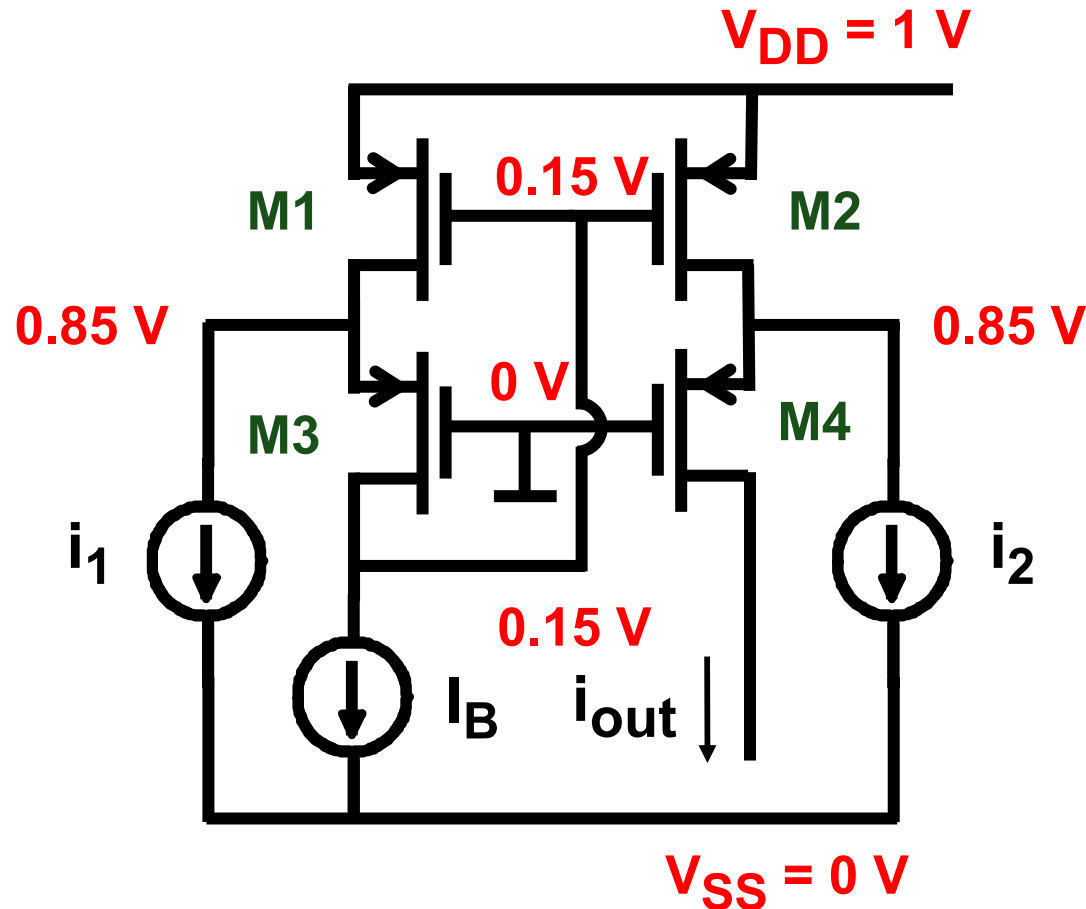


12 MHz 2.1 mA 3.2 nV_{RMS}/√Hz

Vittoz, JSSC June 83, pp. 273-279

Holman, JSSC June 95, pp. 710-714

Current differential amplifier for $< 1\text{V}$



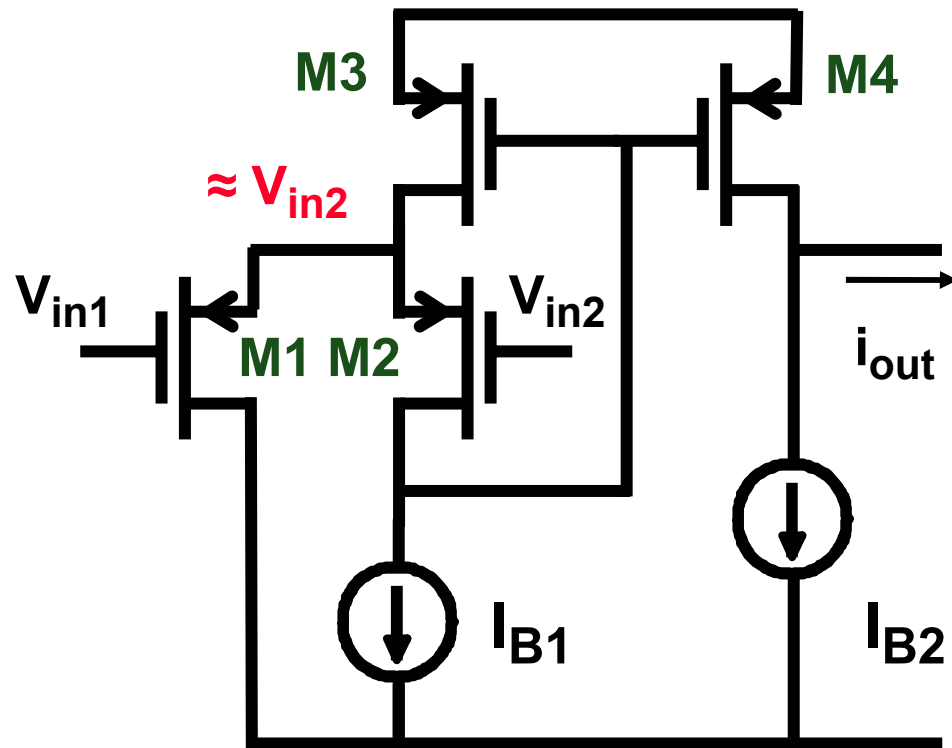
$$i_{out} = I_B + i_1 - i_2$$

$$V_{GS} = 0.85\text{ V}$$

$$V_{DSsat} = 0.15\text{ V}$$

$$V_{outmax} = 0.7\text{ V}$$

Class AB differential Voltage amplifier



M2 is source follower

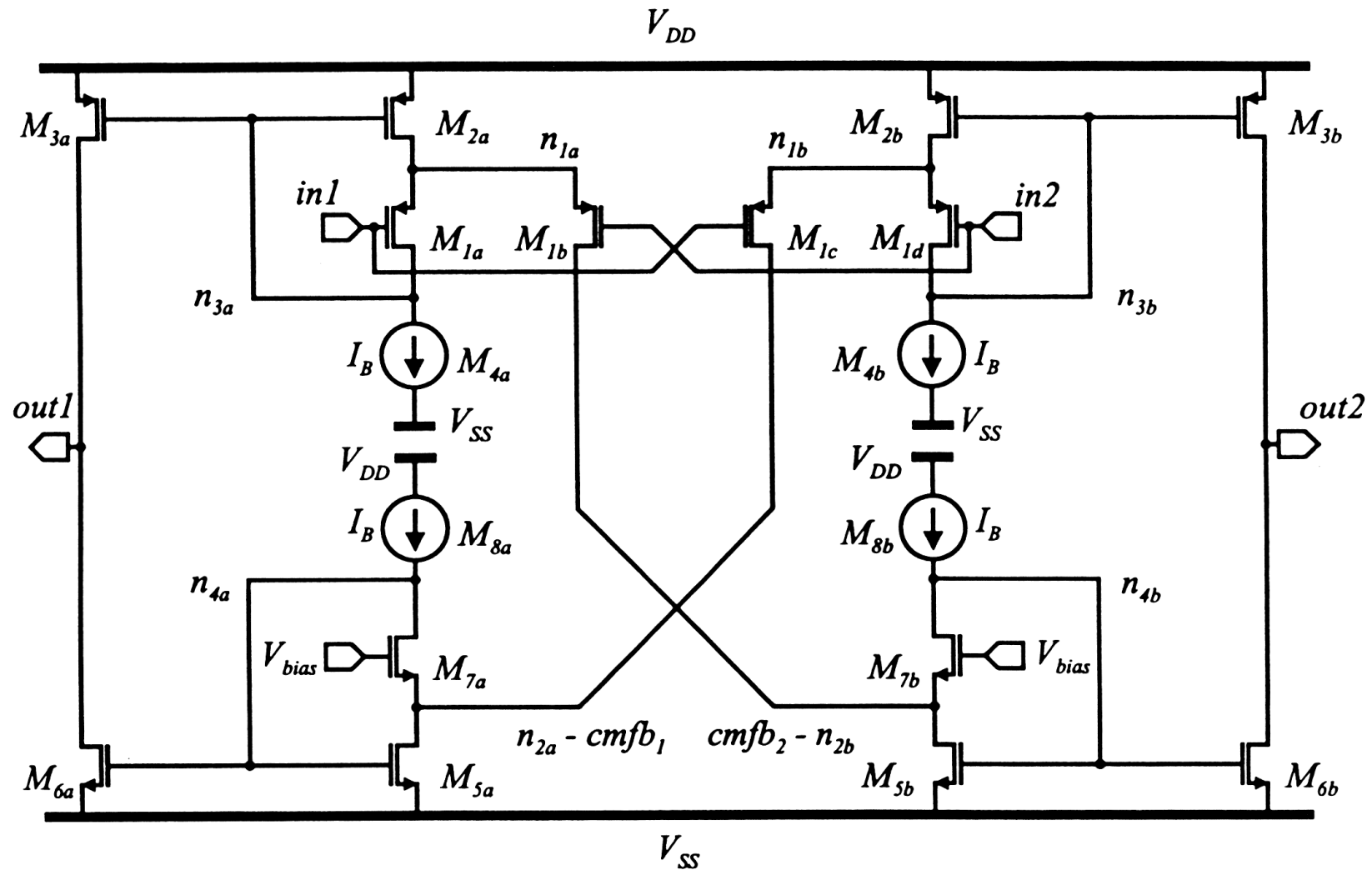
$$V_{GS1} = V_{in1} - V_{in2}$$

$$i_{out} \sim (V_{in1} - V_{in2})^2$$

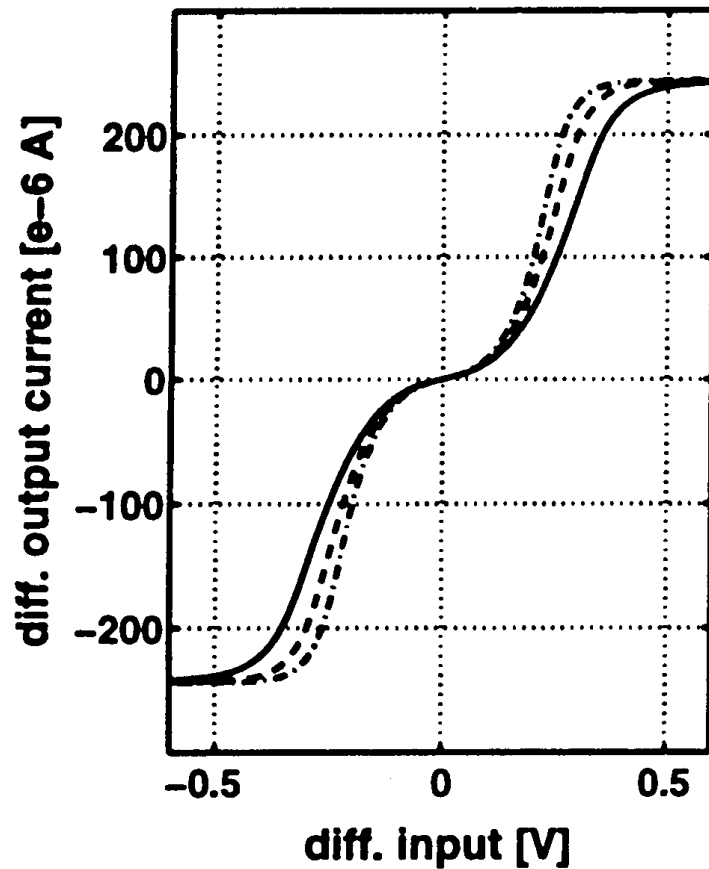
>>> Class AB

Ref. Peluso, JSSC Dec.98, 1887-1897

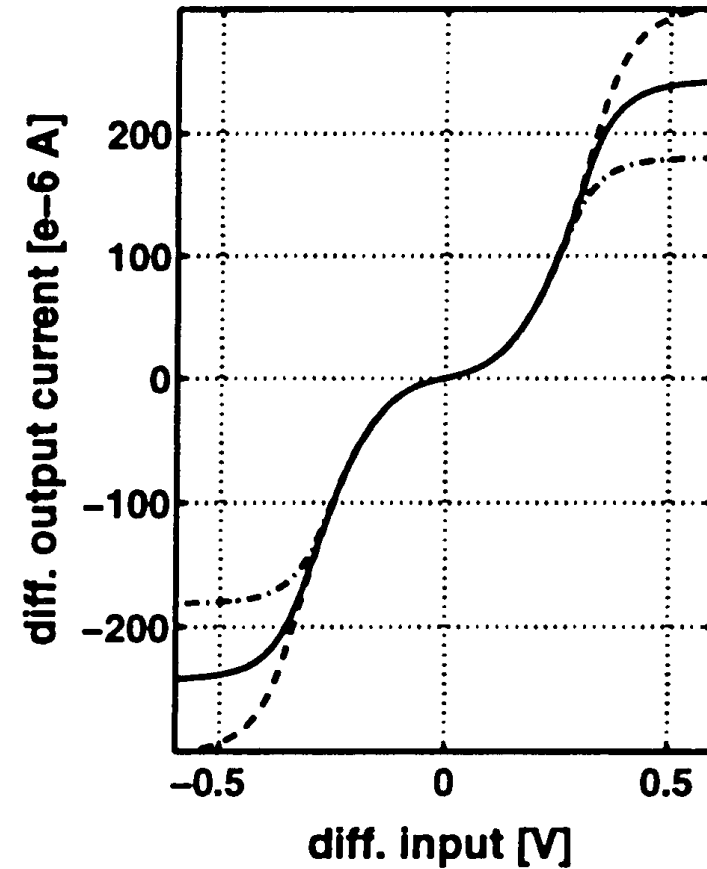
Differential class-AB OTA on 1 V supply voltage



Class-AB characteristic

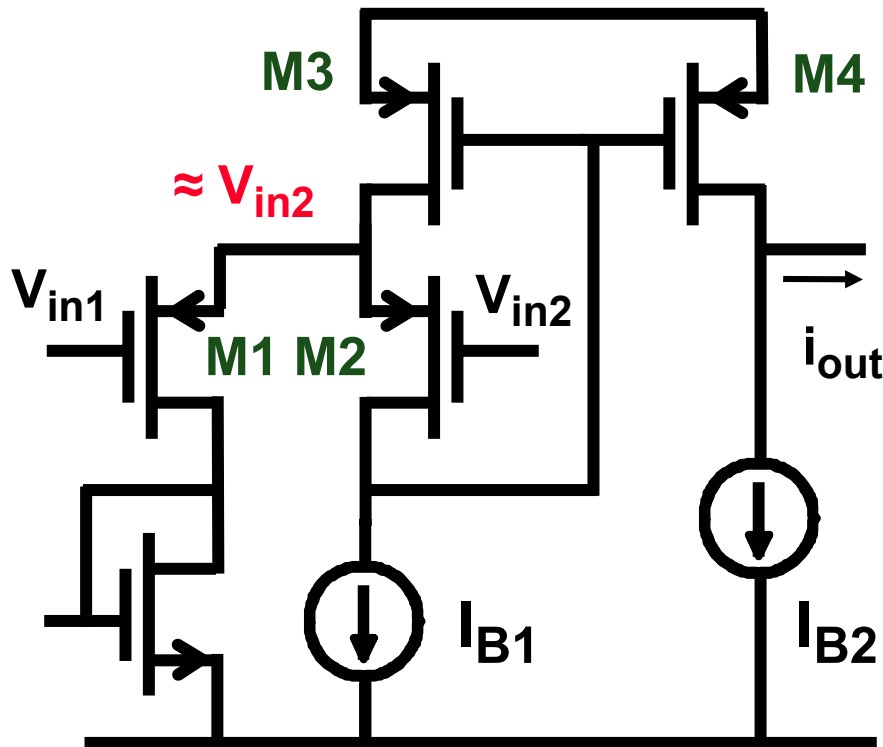


Larger input W/L



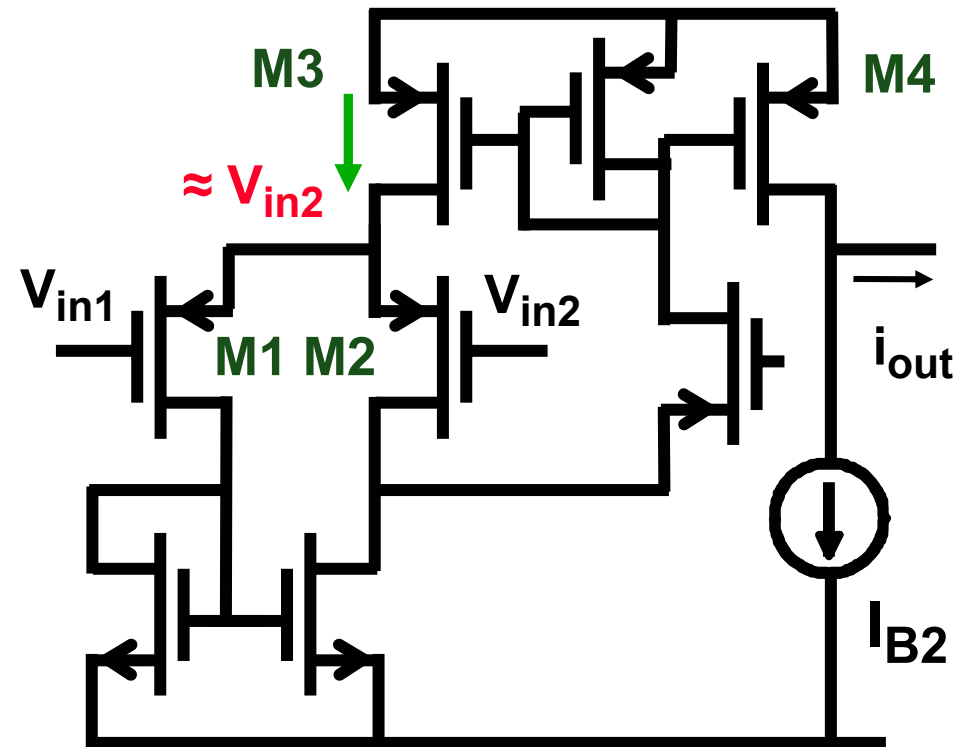
Larger current source W/L

Low-voltage Class AB amplifiers



M2 is source follower
3 trans. carry current
 $V_{GS} + V_{DSsat}$

Ref. Peluso, JSSC Dec.98, 1887-1897



M2 is source follower
7 trans. carry current
 $V_{GS} + 2V_{DSsat}$

Ref. Callewaert, JSSC June 90, 684-691

Conclusions

- **Problems of class AB drivers**
- **Cross-coupled quads**
- **Adaptive biasing**
- **I_Q control with translinear circuits, etc.**
- **Current feedback and other principles**
- **Low-Voltage realizations**

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