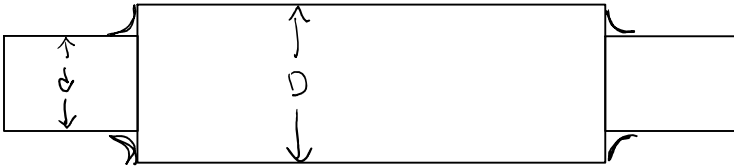


# Shaft Design

Parker Knopf

A15830016

## Problem Statement



FOS: 1.5

Reliability: 99.9%

$S_y = 60 \text{ ksi}$

Surface: Machined

$S_{ut} = 80 \text{ ksi}$

Forces:

Min/Max Bending Moment: 800 - 5000 lb·in

Min/Max Torque: 0 - 2000 lb·in

Geometry:

$D = (1.2)d$

$r = d(0.1)$

## Static / Dynamic Loads

$$M_a = M_{\max} - M_m = 5000 - 2900 = 2100 \text{ lb·in}$$

$$M_m = \frac{M_{\max} + M_{\min}}{2} = \frac{5000 + 800}{2} = 2900 \text{ lb·in}$$

$$T_a = T_{\max} - T_m = 2000 - 1000 = 1000 \text{ lb·in}$$

$$T_m = \frac{T_{\max} + T_{\min}}{2} = \frac{2000 + 0}{2} = 1000 \text{ lb·in}$$

$$M_a = 2100$$

$$M_m = 2900$$

$$T_a = 1000 \text{ lb·in}$$

$$T_m = 1000$$

## Initial Diameter Guess

Idea: Use Static Failure theory to form initial guess

$$M_{\max} = 5000 \text{ lb·in}$$

$$\sigma = \frac{Mc}{I}$$

$$\tau = \frac{Tc}{J}$$

$$I = \frac{\pi}{4} (r)^4$$

$$T_{\max} = 2000 \text{ lb·in}$$

$$\sigma' = \frac{1}{\sqrt{2}} [2(\sigma)^2 + 6(\tau)^2]^{1/2} \quad n = \frac{S_y}{\sigma'} \quad \Rightarrow \quad \frac{S_y}{n} = \frac{1}{\sqrt{2}} [2(\sigma)^2 + 6(\tau)^2]^{1/2}$$

solve for  $r$

$$d_0 = 1.104 \text{ in Initial Guess}$$

$$r = \left[ \frac{32}{\pi^2 \left( \frac{S_y \sqrt{2}}{n} \right)^2} (32 M^2 + 24 T^2) \right]^{1/6}$$

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$S_e$

$$S_e' = S_{ut}/2 = (80 \text{ ksi})/2 = 40 \text{ ksi}$$

$$S_e = k_a k_b k_c k_d k_e S_e'$$

$$k_a = a (S_{ut})^b$$

$$a = 2.00$$

$$k_b = 0.91 d^{(-0.157)}$$

$$k_c = 1$$

$$b = -0.217$$

$$S_e = (2)(80)^{-0.217} (0.91 d)^{-0.157} (0.753)$$

$$k_d = 1$$

$$k_e = 0.753$$

$$S_e = (0.5245) d^{-0.157} S_{ut}/2 = 20.854 \text{ ksi}$$

Stress Concentrations

Estimates	Bending	Torsional	Axial
Shoulder fillet—sharp ( $r/d = 0.02$ )	2.7	2.2	3.0
Shoulder fillet—well rounded ( $r/d = 0.1$ )	1.7	1.5	1.9

$$K_t = 1.7$$

$$K_{ts} = 1.5$$

$\Rightarrow$  Initial Guesses

Bending:

Table A-15-9

	$0.1 \leq t/r \leq 2.0$	$2.0 \leq t/r \leq 20.0$
$K_t = C_1 + C_2 \left(\frac{2t}{D}\right) + C_3 \left(\frac{2t}{D}\right)^2 + C_4 \left(\frac{2t}{D}\right)^3$		
$C_1$	$0.947 + 1.206\sqrt{t/r} - 0.131t/r$	$1.232 + 0.832\sqrt{t/r} - 0.008t/r$
$C_2$	$0.022 - 3.405\sqrt{t/r} + 0.915t/r$	$-3.813 + 0.968\sqrt{t/r} - 0.260t/r$
$C_3$	$0.869 + 1.777\sqrt{t/r} - 0.555t/r$	$7.423 - 4.868\sqrt{t/r} + 0.869t/r$
$C_4$	$-0.810 + 0.422\sqrt{t/r} - 0.260t/r$	$-3.839 + 3.070\sqrt{t/r} - 0.600t/r$

Torsional:

Table A-15-8

	$0.25 \leq t/r \leq 4.0$
$K_{ts} = C_1 + C_2 \left(\frac{2t}{D}\right) + C_3 \left(\frac{2t}{D}\right)^2 + C_4 \left(\frac{2t}{D}\right)^3$	
$C_1$	$0.905 + 0.783\sqrt{t/r} - 0.075t/r$
$C_2$	$-0.437 - 1.969\sqrt{t/r} + 0.553t/r$
$C_3$	$1.557 + 1.073\sqrt{t/r} - 0.578t/r$
$C_4$	$-1.061 + 0.171\sqrt{t/r} + 0.086t/r$

$$K_f = 1 + \frac{K_t - 1}{1 + \sqrt{a}/\sqrt{r}}$$

Bending or axial:

$$\sqrt{a} = 0.246 - 3.08(10^{-3})S_{ut} + 1.51(10^{-5})S_{ut}^2 - 2.67(10^{-8})S_{ut}^3 \quad 50 \leq S_{ut} \leq 250 \text{ kpsi}$$

$$\sqrt{a} = 1.24 - 2.25(10^{-3})S_{ut} + 1.60(10^{-6})S_{ut}^2 - 4.11(10^{-10})S_{ut}^3 \quad 340 \leq S_{ut} \leq 1700 \text{ MPa} \quad (6-35)$$

Torsion:

$$\sqrt{a} = 0.190 - 2.51(10^{-3})S_{ut} + 1.35(10^{-5})S_{ut}^2 - 2.67(10^{-8})S_{ut}^3 \quad 50 \leq S_{ut} \leq 220 \text{ kpsi}$$

$$\sqrt{a} = 0.958 - 1.83(10^{-3})S_{ut} + 1.43(10^{-6})S_{ut}^2 - 4.11(10^{-10})S_{ut}^3 \quad 340 \leq S_{ut} \leq 1500 \text{ MPa} \quad (6-36)$$

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$K_f :$

$$\sqrt{a'} = 0.0826$$

$$K_f = 1.63$$

$K_{fs} :$

$$\sqrt{a'} = -0.0234$$

$$K_{fs} = 1.5163$$

Solve

$$d = \left\{ \frac{16n}{\pi} \left[ 4 \left( \frac{K_f M_a}{S_e} \right)^2 + 3 \left( \frac{K_{fs} T_a}{S_e} \right)^2 + 4 \left( \frac{K_f M_m}{S_y} \right)^2 + 3 \left( \frac{K_{fs} T_m}{S_y} \right)^2 \right]^{1/2} \right\}^{1/3}$$

$$d_1 = 1.732 \text{ in}$$