# Вывод ур-я относ. массового расхода горючего, отнесенного к массовому расходу на входе в I контур, через относ. массовый расход горючего, отнесенного к массовому расходу на входе в КС.

$$\mathbf{g}_{\text{OXJI\_KC3}} = \frac{\mathbf{G}_{\text{OXJI}}}{\mathbf{G}_{\text{KC3}}} = \frac{\mathbf{G}_{\text{OXJI}}}{\mathbf{G}_{\text{I}} - \mathbf{G}_{\text{OXJI}} - \mathbf{G}_{\text{YT}} + \mathbf{G}_{\text{Pop}}}$$

$$g_{\text{OXJ\_KC3}} = \frac{G_{\text{OXJ}}}{G_{\text{I}} - G_{\text{OXJ}} - G_{\text{VT}} + G_{\text{FOD}}} \text{ solve, } G_{\text{OXJ}} = \frac{g_{\text{OXJ\_KC3}} \cdot \left(G_{\text{I}} - G_{\text{VT}} + G_{\text{FOD}}\right)}{g_{\text{OXJ} \text{ KC3}} + 1}$$
 (Тихонов)

$$\mathbf{g}_{\text{гор\_KC1}} = \frac{\mathbf{G}_{\text{гор}}}{\mathbf{G}_{\text{KC1}}} = \frac{\mathbf{G}_{\text{гор}}}{\mathbf{G}_{\text{I}} - \mathbf{G}_{\text{охл}} - \mathbf{G}_{\text{ут}}}$$

$$\mathbf{g}_{\text{rop\_KC1}} = \frac{\mathbf{G}_{\text{rop}}}{\mathbf{G}_{\text{I}} - \mathbf{G}_{\text{OXJ}} - \mathbf{G}_{\text{YT}}} \text{ solve, } \mathbf{G}_{\text{rop}} = -\mathbf{g}_{\text{rop\_KC1}} \cdot \left(\mathbf{G}_{\text{YT}} - \mathbf{G}_{\text{I}} + \mathbf{G}_{\text{OXJ}}\right)$$

$$g_{\text{rop\_KC1}} = \frac{G_{\text{rop}}}{G_{\text{I}} - G_{\text{OXJ}} - G_{\text{YT}}} \text{ substitute, } G_{\text{OXJ}} = \frac{g_{\text{OXJ\_KC3}} \cdot \left(G_{\text{I}} - G_{\text{YT}} + G_{\text{rop}}\right)}{g_{\text{OXJ\_KC3}} + 1} \\ = g_{\text{rop\_KC1}} = -\frac{G_{\text{rop}} \cdot \left(g_{\text{OXJ\_KC3}} + 1\right)}{G_{\text{YT}} - G_{\text{I}} + G_{\text{rop}} \cdot g_{\text{OXJ\_KC3}}}$$

$$\mathbf{g}_{\text{rop\_KC1}} = -\frac{\mathbf{G}_{\text{rop}} \cdot \left(\mathbf{g}_{\text{OX}\pi\_\text{KC3}} + 1\right)}{\mathbf{G}_{\text{yT}} - \mathbf{G}_{\text{I}} + \mathbf{G}_{\text{rop}} \cdot \mathbf{g}_{\text{OX}\pi\_\text{KC3}}} \text{ solve}, \mathbf{G}_{\text{rop}} = \frac{\mathbf{G}_{\text{I}} \cdot \mathbf{g}_{\text{rop\_\text{KC1}}} - \mathbf{G}_{\text{yT}} \cdot \mathbf{g}_{\text{rop\_\text{KC1}}}}{\mathbf{g}_{\text{OX}\pi\_\text{KC3}} + \mathbf{g}_{\text{rop\_\text{KC1}}} \cdot \mathbf{g}_{\text{OX}\pi\_\text{KC3}} + 1}$$

$$G_{\text{rop}} = \frac{G_{\text{I}} g_{\text{rop\_KC1}} - G_{\text{yT}} g_{\text{rop\_KC1}}}{g_{\text{OXJ} \text{ KC3}} + g_{\text{rop} \text{ KC1}} g_{\text{OXJ} \text{ KC3}} + 1} = G_{\text{I}} \cdot \frac{g_{\text{rop\_KC1}} - g_{\text{yT}} g_{\text{rop\_KC1}}}{g_{\text{OXJ} \text{ KC3}} + g_{\text{rop} \text{ KC1}} g_{\text{OXJ} \text{ KC3}} + 1}$$

$$\mathbf{g}_{\text{rop}} = \frac{\mathbf{G}_{\text{rop}}}{\mathbf{G}_{\text{I}}} = \frac{\mathbf{G}_{\text{I}} \frac{\mathbf{g}_{\text{rop\_KC1}} - \mathbf{g}_{\text{yT}} \cdot \mathbf{g}_{\text{rop\_KC1}}}{\mathbf{g}_{\text{OXJ\_KC3}} + \mathbf{g}_{\text{rop\_KC1}} \cdot \mathbf{g}_{\text{OXJ\_KC3}} + 1}}{\mathbf{G}_{\text{I}}} = \frac{\mathbf{g}_{\text{rop\_KC1}} - \mathbf{g}_{\text{yT}} \cdot \mathbf{g}_{\text{rop\_KC1}}}{\mathbf{g}_{\text{OXJ}} \cdot \mathbf{g}_{\text{COS}} \cdot \mathbf{g}_{\text{COS}}} + 1}$$

## Вывод ур-я Тихонова относ. массового расхода на охлаждение, отнесенного к массовому расходу на входе в I контур, через относ. массовый расход на охлаждение, онесенного к массовому расходу на выходе из КС.

$$g_{\text{OXJ}} = \frac{G_{\text{OXJ}}}{G_{\text{I}}} = \frac{\frac{g_{\text{OXJ}} \text{_KC3}} \cdot \left(G_{\text{I}} - G_{\text{yT}} + G_{\text{POP}}\right)}{g_{\text{OXJ}} \text{_KC3} + 1}}{G_{\text{I}}} = \frac{G_{\text{I}} \cdot \frac{g_{\text{OXJ}} \text{_KC3}} \cdot \left(1 - g_{\text{yT}} + g_{\text{POP}}\right)}{g_{\text{OXJ}} \text{_KC3} + 1}}{G_{\text{I}}} = \frac{g_{\text{OXJ}} \text{_KC3} \cdot \left(1 - g_{\text{yT}} + g_{\text{POP}}\right)}{g_{\text{OXJ}} \text{_KC3} + 1}}{g_{\text{OXJ}} \text{_KC3} + 1}$$

### Вывод термодинамических парамтеров смешения

Ур-е теплового баланса:

$$Q + Q_{add} = Q_{CM}$$

или

$$G \cdot Cp \cdot T + G_{add} \cdot Cp_{add} \cdot T_{add} = G_{CM} \cdot Cp_{CM} \cdot T_{CM} = \left(G + G_{add}\right) \cdot Cp_{CM} \cdot T_{CM}$$

Температура СМ [К]:

$$G \cdot Cp \cdot T + G_{add} \cdot Cp_{add} \cdot T_{add} = \left(G + G_{add}\right) \cdot Cp_{CM} \cdot T_{CM} \text{ solve, } T_{CM} = \frac{Cp \cdot G \cdot T + Cp_{add} \cdot G_{add} \cdot T_{add}}{Cp_{CM} \cdot \left(G + G_{add}\right)}$$

$$T_{CM} = \frac{Cp \cdot g \cdot T + Cp_{add} \cdot g_{add} \cdot T_{add}}{Cp_{CM} \cdot (g + g_{add})}$$

Давление СМ [Па] как среднемассовое:

$$P_{CM} = \frac{G \cdot P + G_{add} \cdot P_{add}}{G + G_{add}} = \frac{g \cdot P + g_{add} \cdot P_{add}}{g + g_{add}}$$

Коэф. избытка окислителся СМ []:

$$\alpha_{CM} = \frac{G_{oK\Sigma}}{G_{rop\Sigma}} = \frac{G_{oK} + G_{add}}{G_{rop} \cdot l_0(Fuel)} = \frac{g_{oK} + g_{add}}{g_{rop} \cdot l_0(Fuel)}$$

#### Вывод оптимальной скорости выхода из С І контура

$$L_{e} = \frac{L_{B}}{\eta_{PB} \cdot \eta_{MeX}} + \frac{c_{CI}^{2} - \upsilon^{2}}{2} + \frac{c_{CII}^{2} - \upsilon^{2}}{2} \text{ solve, } L_{B} \rightarrow \eta_{PB} \cdot \eta_{MeX} \cdot \left(\upsilon^{2} - \frac{c_{CI}^{2}}{2} - \frac{c_{CII}^{2}}{2} + L_{e}\right)$$

$$L_{\text{TMT}}\!\!\left(\upsilon,c_{CI},c_{CII},L_{e},\eta_{\text{Mex}},\eta_{PB},\eta_{B},L_{B}\right) = L_{B}\cdot\eta_{B} + \left(c_{CI}-\upsilon\right)\cdot\upsilon + \left(c_{CII}-\upsilon\right)\cdot\upsilon + \left(c_{CII}-\upsilon\right)\cdot\upsilon$$

$$\frac{\mathrm{d}}{\mathrm{d}\mathfrak{c}_{CI}} L_{\mathsf{TMI}} \! \left( \upsilon, \mathfrak{c}_{CI}, \mathfrak{c}_{CII}, L_e, \eta_{\mathsf{MeX}}, \eta_{PB}, \eta_B, L_B \right) \rightarrow \upsilon - \mathfrak{c}_{CI} \cdot \eta_B \cdot \eta_{PB} \cdot \eta_{\mathsf{MeX}}$$

$$\frac{\text{d}}{\text{dc}_{CI}} L_{\text{TMI}} \! \left( \upsilon, c_{CI}, c_{CII}, L_e, \eta_{\text{MeX}}, \eta_{PB}, \eta_{B}, L_B \right) = 0 \text{ solve}, c_{CI} = \frac{\upsilon}{\eta_{B} \cdot \eta_{PB} \cdot \eta_{\text{MeX}}}$$

$$L_{e}\!\!\left(\upsilon,c_{CI},c_{CII},m2,L_{B\pi II}\right) = m2\cdot L_{B\pi II} + \frac{c_{CI}\!\!\left(L_{B\pi II}\right)^{2} - \upsilon^{2}}{2}$$

$$\frac{d}{dL_{B\pi II}}L_{e}\!\!\left(\upsilon,c_{CI},c_{CII},m2,L_{B\pi II}\right) = m2 + c_{CI}\!\!\left(L_{B\pi II}\right) \cdot \frac{d}{dL_{B\pi II}}c_{CI}\!\!\left(L_{B\pi II}\right) \\ \text{ solve}, \\ \frac{d}{dL_{B\pi II}}c_{CI}\!\!\left(L_{B\pi II}\right) = -\frac{m2}{c_{CI}\!\!\left(L_{B\pi II}\right)} \cdot \frac{d}{dL_{B\pi II}}c_{CI}\!\!\left(L_{B\pi II}\right) \\ = -\frac{m2}{c_{CI}\!\!\left(L_{B\pi II}\right)}c_{CI}\!\!\left(L_{B\pi II}\right) \\ = -\frac{m2}{c_{CI}\!\!\left(L_{B\pi II}\right)}c_{CI}\!\!\left(L_{B\pi II}\right) \\ = -\frac{m2}{c_{CI}\!\!\left(L_{B\pi II}\right)}c_{CI}\!\!\left(L_{B\pi II}\right)$$

Баланс энергии II контура: 
$$L_{B\pi II} \cdot \eta_{II} = \frac{c_{CII} \left(\upsilon, \eta_{II}, L_{B\pi II}\right)^2 - \upsilon^2}{2} \text{ solve, } c_{CII} \left(\upsilon, \eta_{II}, L_{B\pi II}\right) \\ = \begin{pmatrix} \sqrt{\upsilon^2 + 2 \cdot \eta_{II} \cdot L_{B\pi II}} \\ -\sqrt{\upsilon^2 + 2 \cdot \eta_{II} \cdot L_{B\pi II}} \end{pmatrix}$$

$$c_{\text{CII}}(\upsilon, \eta_{\text{II}}, L_{\text{B}\pi\text{II}}) = \sqrt{\upsilon^2 + 2 \cdot \eta_{\text{II}} \cdot L_{\text{B}\pi\text{II}}}$$

$$\frac{\text{d}}{\text{d}L_{B\pi II}}c_{CII}\!\!\left(\upsilon,\eta_{II},L_{B\pi II}\right) \,=\, \frac{\eta_{II}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}}$$

$$\text{Удельная тяга двигателя:} \quad R_{\text{уд}}\!\!\left(\upsilon,c_{\text{CI}},c_{\text{CII}},m2,L_{\text{ВлІІ}},\eta_{\text{II}}\right) = \frac{R_{\text{удI}}+m2\cdot R_{\text{удII}}}{1+m2} \quad \begin{vmatrix} \text{substitute},R_{\text{удI}}=c_{\text{CI}}\!\left(L_{\text{ВлІІ}},m2\right)-\upsilon\\ \text{substitute},R_{\text{удII}}=c_{\text{CII}}\!\left(\upsilon,\eta_{\text{II}},L_{\text{ВлІІ}}\right)-\upsilon \end{vmatrix} = -\frac{\upsilon-m2\cdot c_{\text{CII}}\!\left(\upsilon,\eta_{\text{II}},L_{\text{ВлІІ}}\right)+\upsilon\cdot m2-c_{\text{CI}}\!\left(L_{\text{ВлІІ}},m2\right)}{m2+1}$$

Условие получения max тяги: 
$$\frac{\mathrm{d}}{\mathrm{d}L_{\mathrm{B\pi II}}}\mathrm{R}_{\mathrm{y}\mathrm{J}}\!\!\left(\upsilon,c_{\mathrm{CI}},c_{\mathrm{CII}},m2,L_{\mathrm{B\pi II}},\eta_{\mathrm{II}}\right)=0$$

$$\frac{d}{dL_{B\pi II}}R_{y\mu}(\upsilon,c_{CI},c_{CII},m2,L_{B\pi II},\eta_{II}) = \frac{\frac{d}{dL_{B\pi II}}c_{CI}(L_{B\pi II},m2) + \frac{m2\cdot\eta_{II}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}}}{m2 + 1} \\ = \frac{\frac{d}{dL_{B\pi II}}c_{CI}(L_{B\pi II},m2) + \frac{m2\cdot\eta_{II}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}}}{m2 + 1} \\ = \frac{\frac{d}{dL_{B\pi II}}c_{CI}(L_{B\pi II},m2) + \frac{m2\cdot\eta_{II}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} - \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot c_{CI}(L_{B\pi II},m2))}}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}} \\ = \frac{m2\cdot(\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}} - \eta_{II}\cdot L_{B\pi II})}{\sqrt{\upsilon^2 + 2\cdot\eta_{II}\cdot L_{B\pi II}}}$$

#### Вывод общего ур-я профилирования Л цилиндрической ступени К

Вывод:

$$\frac{d}{dr}H_T = \frac{d}{dr}\left(\frac{c_a^2}{2}\right) + c_u\cdot\left(\frac{d}{dr}c_u\right) + \frac{c_u^2}{r} = 0$$
  $\Rightarrow$   $\frac{d}{dr}\left(\frac{c_a^2}{2}\right) = -c_u\cdot\left(\frac{d}{dr}c_u\right) - \frac{c_u^2}{r}$  (00) Домножим на  $2 \Rightarrow$   $\frac{d}{dr}\left(c_a^2\right) = -2 \cdot c_u\cdot\left(\frac{d}{dr}c_u\right) - \frac{2 \cdot c_u^2}{r}$ 

$$\Rightarrow \frac{d}{dr} \left( \frac{c_a^2}{2} \right) = -c_u \cdot \left( \frac{d}{dr} c_u \right) - \frac{c_u}{r}$$

$$\frac{d}{dr}\left(c_a^2\right) = -2 \cdot c_u \cdot \left(\frac{d}{dr}c_u\right) - \frac{2 \cdot c_u^2}{r}$$

$$\frac{c_{1u} + c_{2u}}{2} \cdot r^{m} = const$$

(2) 
$$H_T = (c_{2u} \cdot u_2 - c_{1u} \cdot u_1) = (c_{2u} - c_{1u})u$$

 $R = 1 - \frac{c_{1u} + c_{2u}}{u_1 + u_2} = 1 - \frac{c_{1u} + c_{2u}}{2 \cdot u}$ 

$$u = \omega \cdot r$$

$$\omega = \text{const} \qquad \frac{u_1}{r_1} = \frac{u_2}{r_2}$$

$$1 - \frac{c_{1u} + c_{2u}}{2 \cdot u} - \frac{c_{a2}^2 - c_{a1}^2}{2 \cdot H_T}$$

(000)

$$c_{1u} = (1 - R) \cdot \omega \cdot r + \frac{H_T}{2 \cdot \omega \cdot r}$$

$$c_{2u} = -(1 - R) \cdot \omega \cdot r + \frac{H_T}{2 \cdot \omega \cdot r}$$

$$\omega \cdot \mathbf{r} + \frac{\mathbf{H}_{\mathrm{T}}}{2 \cdot \omega \cdot \mathbf{r}}$$
 (c2)

$$\frac{c_{1u} + c_{2u}}{2} = (1 - R) \cdot \omega \cdot r$$

(1): 
$$const = \frac{c_{1u} + c_{2u}}{2} \cdot r^{m} = (2) = (1 - R)\omega \cdot r \cdot r^{m} = (1 - R)\omega \cdot r^{m+1} = (1 - R_{cp})\omega \cdot r_{cp}^{m+1}$$

$$\Rightarrow (1 - R)\omega = \frac{\left[\left(1 - R_{cp}\right) \cdot \omega \cdot r_{cp}^{m+1}\right]}{r^{m+1}}$$

$$(\&) \rightarrow (c1u)$$

$$c_{1u} = (1 - R) \cdot \omega \cdot r - \frac{H_T}{2 \cdot \omega \cdot r} = \frac{\left[ \left( 1 - R_{cp} \right) \cdot \omega \cdot r_{cp}^{-m+1} \right]}{r^{m+1}} \cdot r - \frac{H_T}{2 \cdot \omega \cdot r} = \frac{\left[ \left( 1 - R_{cp} \right) \cdot \omega \cdot r_{cp}^{-m+1} \right]}{r^{m+1}} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot \omega \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot r_{cp}^{-m+1}}{r} \cdot r - \frac{\left( \frac{H_T}{2 \cdot \omega} \right) \cdot r_{cp$$

(AB1) 
$$A = \left[ \left( 1 - R_{cp} \right) \cdot \omega \cdot r_{cp} \right]^{m+1}$$

$$A = \left[ \left( 1 - R_{cp} \right) \cdot \omega \cdot r_{cp}^{m+1} \right]$$

$$c_{1u}(r, m, A, B) = \frac{(A)}{r} - \frac{(B)}{r}$$

$$(\&) \rightarrow (c2u)$$

$$c_{2u} = (1 - R) \cdot \omega \cdot r + \frac{H_T}{2 \cdot \omega \cdot r} = \frac{\left[ (1 - R_{cp}) \cdot \omega \cdot r_{cp}^{-m+1} \right]}{r^{m+1}} \cdot r + \frac{H_T}{2 \cdot \omega \cdot r} = \frac{\left[ (1 - R_{cp}) \cdot \omega \cdot r_{cp}^{-m+1} \right]}{r^{m+1}} \cdot r + \frac{\left[ \frac{H_T}{2 \cdot \omega} \right]}{r} \cdot r + \frac{\left[ \frac{H_T}{2 \cdot \omega} \right]}{r^{m+1}} \cdot r + \frac{\left[ \frac{H_T}{2 \cdot \omega} \right]}{r} \cdot r + \frac{\left[ \frac{H_T}{2 \cdot \omega}$$

(AB2) 
$$B = \left(\frac{H_T}{2 \cdot \omega}\right)$$

$$c_{2u}(r,m,A,B) = \frac{(A)}{r} + \frac{(B)}{r}$$

(0000)

(000) 
$$\int_{r_{cp}}^{r} \frac{d}{dr} \left(c_{a}^{2}\right) dr = c_{a}^{2} - c_{a.cp}^{2} = \int_{r_{cp}}^{r} -2 \cdot c_{u} \cdot \left(\frac{d}{dr}c_{u}\right) - \frac{2 \cdot c_{u}^{2}}{r} dr$$

$$c_{a1}^{2} - c_{a1.cp}^{2} = \int_{r_{cp}}^{r} -2 \cdot c_{u1} \cdot \left(\frac{d}{dr}c_{u1}\right) - \frac{2 \cdot c_{u1}^{2}}{r} dr$$

$$c_{a2}^{2} - c_{a2.cp}^{2} = \int_{r_{cp}}^{r} -2 \cdot c_{u2} \cdot \left(\frac{d}{dr}c_{u2}\right) - \frac{2 \cdot c_{u2}^{2}}{r}$$

$$c_{a1}^{2} - c_{a1.cp}^{2} = \int_{r_{cp}}^{r} -2 \cdot c_{u1} \cdot \left(\frac{d}{dr}c_{u1}\right) - \frac{2 \cdot c_{u1}^{2}}{r} dr$$

$$= > c_{a1} = \int_{r_{cp}}^{r} -2 \cdot c_{u1} \cdot \left(\frac{d}{dr}c_{u1}\right) - \frac{2 \cdot c_{u1}^{2}}{r} dr$$

$$= > c_{a2}^{2} - c_{a2.cp}^{2} = \int_{r_{cp}}^{r} -2 \cdot c_{u2} \cdot \left(\frac{d}{dr}c_{u2}\right) - \frac{2 \cdot c_{u2}^{2}}{r} dr$$

$$= > c_{a2} = \int_{r_{cp}}^{r} -2 \cdot c_{u2} \cdot \left(\frac{d}{dr}c_{u2}\right) - \frac{2 \cdot c_{u2}^{2}}{r} dr$$

$$c_{a2} = \sqrt{c_{a2.cp}^2 + \int_{r_{cp}}^{r} -2 \cdot c_{u2} \cdot \left(\frac{d}{dr} c_{u2}\right) - \frac{2 \cdot c_{u2}^2}{r} dr}$$

$$\sqrt{c_{a1.cp}^{2} + \int_{r_{cp}}^{r} -2 \, c_{1u}(r, m, A, B) \cdot \left(\frac{d}{dr} c_{1u}(r, m, A, B)\right) - \frac{2 \, c_{1u}(r, m, A, B)^{2}}{r} \, dr \, assume, \\ r_{cp} > 0, \\ r \ge 0, \\ m = 0 = \sqrt{2 \cdot A^{2} \cdot ln \left(r_{cp}\right) - 2 \cdot A^{2} \cdot ln \left(r\right) + c_{a1.cp}^{2} - \frac{2 \cdot A \cdot B}{r} + \frac{2 \cdot A \cdot B}{r_{cp}} }$$

$$\sqrt{c_{a2.cp}^{2} + \int_{r_{cp}}^{r} -2 \, c_{2u}(r, m, A, B) \cdot \left(\frac{d}{dr} c_{2u}(r, m, A, B)\right) - \frac{2 \, c_{2u}(r, m, A, B)^{2}}{r} \, dr \, assume, \\ r_{cp} > 0, \\ r \ge 0, \\ m = 0 = \sqrt{2 \cdot A^{2} \cdot ln \left(r_{cp}\right) - 2 \cdot A^{2} \cdot ln \left(r\right) + c_{a2.cp}^{2} + \frac{2 \cdot A \cdot B}{r} - \frac{2 \cdot A \cdot B}{r_{cp}} }$$

$$\sqrt{c_{a1.cp}^{2} + \int_{r_{cp}}^{r} -2 c_{1u}(r, m, A, B) \cdot \left(\frac{d}{dr} c_{1u}(r, m, A, B)\right) - \frac{2 c_{1u}(r, m, A, B)^{2}}{r}} dr \ assume, r_{cp} > 0, r \ge 0, -1 < m \le 1, m \ne 0$$

$$= \sqrt{c_{a1.cp}^{2} + \frac{A \cdot (m-1) \cdot \left(A \cdot r_{1}^{2 \cdot m} \cdot r_{cp} - A \cdot r_{cp} \cdot r_{cp}^{2 \cdot m} - 2 \cdot B \cdot m \cdot r_{1}^{2 \cdot m} \cdot r_{cp}^{m} + 2 \cdot B \cdot m \cdot r_{1}^{m} \cdot r_{cp}^{m} + 2 \cdot B \cdot m \cdot r_{1}^{m} \cdot r_{cp}^{m} - A \cdot m \cdot r_{1}^{2 \cdot m} \cdot r_{cp}^{m} - A \cdot m \cdot r_{1}^{2 \cdot m} \cdot r_{1}^{2 \cdot m} \cdot r_{1}^{m} \cdot r_{1}^{2 \cdot m} \cdot r_{1}^{2 \cdot m} + A \cdot m \cdot r_{1}^{2 \cdot m} \cdot r_{1}^{$$

#### Вывод общего ур-я профилирования Л цилиндрической ступени Т

$$\frac{c_{1u} + c_{2u}}{2} \cdot r^{m} = const$$

$$const = \frac{c_1 u + c_2 u}{2} \cdot r^m = (3) = (1 - R)\omega \cdot r \cdot r^m = (1 - R)\omega \cdot r^{m+1} = \left(1 - R_{cp}\right)\omega \cdot r_{cp}^{m+1} \qquad \Rightarrow \qquad (1 - R)\omega \cdot r = \frac{\left[\left(1 - R_{cp}\right)\cdot\omega \cdot r_{cp}^{m+1}\right]}{m}$$

$$A = \left[\left(1 - R_{cp}\right)\cdot\omega \cdot r_{cp}^{m+1}\right]$$

$$(1 - R)\omega \cdot r = \frac{\left[\left(1 - R_{cp}\right) \cdot \omega \cdot r_{cp}\right]^{m+1}}{m}$$

$$A = \left[ \left( 1 - R_{cp} \right) \cdot \omega \cdot r_{cp}^{m+1} \right]$$

$$c_{1u}(r, m, A, B) = \frac{(A)}{r} + \frac{(B)}{r}$$

(2) 
$$L_u = c_{2u} \cdot u_2 + c_{1u} \cdot u_1 = (c_{2u} + c_{1u})u_1$$

$$u = \omega \cdot r$$

$$\mathbf{L}_u = \mathbf{c}_{2u} \cdot \boldsymbol{\omega} \cdot \mathbf{r}_2 + \mathbf{c}_{1u} \cdot \boldsymbol{\omega} \cdot \mathbf{r}_1 = \left(\mathbf{c}_{2u} + \mathbf{c}_{1u}\right) \boldsymbol{\omega} \cdot \mathbf{r}_1$$

$$c_{2u} = c_{1u} + \frac{L_u}{L_{u}}$$

$$c_{2u} = c_{1u} + \frac{L_u}{\omega \cdot r}$$

$$c_{1u} = (1 - R) \cdot \omega \cdot r + \frac{L_u}{2 \cdot \omega \cdot r} = (1 - R) \cdot \omega \cdot r + \frac{\left(\frac{L_u}{2 \cdot \omega}\right)}{r}$$

$$=\left(\frac{L_{u}}{2}\right)$$

(3) 
$$R = 1 - \frac{c_{1u} - c_{2u}}{2 \cdot u}$$

$$u = \omega \cdot r$$

$$R = 1 - \frac{c_{1u} - c_{2u}}{2 \cdot \omega \cdot r}$$

$$c_{2u} = -(1 - R) \cdot 2 \cdot \omega \cdot r - c_{1u}$$

$$c_{2u} = -(1 - R) \cdot \omega \cdot r + \frac{L_u}{2 \cdot \omega \cdot r} = -(1 - R) \cdot \omega \cdot r + \frac{\left(\frac{L_u}{2 \cdot \omega}\right)}{r}$$

Работа сил трения: 
$$L_{Tp} = \left(\frac{1}{\omega^2} - 1\right) \cdot \frac{c_1^2}{2} = \frac{c_1^2}{2 \cdot \omega^2} - \frac{c_1^2}{2}$$

Работа гидравлических сил сопротивления:

$$L_{\text{\tiny $\Gamma$MJ$}} = \left(\frac{1}{\phi^2} - 1\right) \cdot \frac{{c_1}^2}{2} + \left(\frac{1}{\psi^2} - 1\right) \cdot \frac{{w_2}^2}{2} = \left(\frac{1}{\phi^2} - 1\right) \cdot \frac{{c_a}_1^2 + {c_u}_1^2}{2} + \left(\frac{1}{\psi^2} - 1\right) \cdot \frac{\left({c_2}_u + {u_2}\right)^2 + {c_2}_a^2}{2}$$

Ур-е радиадьного равновесия:  $\frac{1}{0} \cdot \frac{d}{dr} P = \frac{c_u}{r}$ 

$$\frac{1}{\rho} \cdot \frac{d}{dr} P = \frac{c_u^2}{r}$$

$$\frac{1}{\rho} \cdot dP + d\left(\frac{1}{2}\right) + d\left(L_{Tp}\right) = d\left(H_{T}\right)$$

$$0 = \frac{c_1^2}{2} + \int_0^1 \frac{1}{\rho} dP + L_{Tp}$$

$$0 = \frac{c_2^2}{2} + \int_0^2 \frac{1}{\rho} dP + L_{\text{ГИД}} + L_{\text{СТ}}$$

Допущения: 
$$H_T(r) = const$$
  $\frac{d}{dr}H_T(r) = 0$ 

$$\varphi(\mathbf{r}) = \text{const}$$

$$\frac{\mathrm{d}}{\mathrm{d}r}\varphi(r)=0$$

$$\psi(\mathbf{r}) = \text{const}$$

$$\frac{\mathrm{d}}{\mathrm{d}\mathbf{r}}\psi(\mathbf{r})=0$$

$$0 = \frac{c_1^2}{2} + \int_0^1 \frac{1}{\rho} dP + L_{Tp} = \frac{c_1^2}{2} + \int_0^1 \frac{1}{\rho} dP + \frac{c_1^2}{2 \cdot \phi^2} - \frac{c_1^2}{2} = \frac{c_1^2}{2 \cdot \phi^2} + \int_0^1 \frac{1}{\rho} dP = \frac{c_{a1}^2 + c_{u1}^2}{2 \cdot \phi^2} + \int_0^1 \frac{1}{\rho} dP = \frac{1}{\phi^2} \cdot \left(\frac{c_{a1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2}{2}\right) + \int_0^1 \frac{1}{\rho} dP = \frac{1}{\phi^2} \cdot \left(\frac{c_{a1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2}{2}\right) + \int_0^1 \frac{1}{\rho} dP = \frac{1}{\phi^2} \cdot \left(\frac{c_{a1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2}{2}\right) + \int_0^1 \frac{1}{\rho} dP = \frac{1}{\phi^2} \cdot \left(\frac{c_{u1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2}{2} + \frac{c_{u1}^2}{2}\right) + \int_0^1 \frac{1}{\rho} dP = \frac{1}{\phi^2} \cdot \left(\frac{c_{u1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2}{2} + \frac{c_{u1}^2}{2} + \frac{c_{u1}^2}{2} + \frac{c_{u1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2 + c_{u1}^2 + c_{u1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2 + c_{u1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2 + c_{u1}^2 + c_{u1}^2 + c_{u1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2 + c_{u1}^2 + c_{u1}^2 + c_{u1}^2 + c_{u1}^2}{2} + \frac{c_{u1}^2 + c_{u1}^2 + c_{u1}^$$

$$0 = \frac{d}{dr} \left[ \frac{1}{\phi^2} \cdot \left( \frac{c_{a1}^2}{2} + \frac{c_{u1}^2}{2} \right) + \int_0^1 \frac{1}{\rho} \, dP \right] = \frac{1}{\phi^2} \cdot \left( c_{a1} \cdot \frac{d}{dr} c_{a1} + c_{u1} \cdot \frac{d}{dr} c_{u1} \right) + \frac{1}{\rho} \cdot \frac{d}{dr} P = \frac{1}{\phi^2} \cdot \left( c_{a1} \cdot \frac{d}{dr} c_{a1} + c_{u1} \cdot \frac{d}{dr} c_{u1} \right) + \frac{c_{u1}^2}{r} + \frac{c_{u1}^2}{r} \cdot \frac{d}{dr} C_{u1} + \frac{d}{$$

$$\frac{1}{\varphi^2} \cdot \left( c_{a1} \cdot \frac{d}{dr} c_{a1} + c_{u1} \cdot \frac{d}{dr} c_{u1} \right) + \frac{c_{u1}^2}{r} = 0 \qquad \qquad \frac{d}{dr} \left( \frac{c_{a1}^2}{2} \right) = -c_{u1} \cdot \left( \frac{d}{dr} c_{u1} \right) - \varphi^2 \cdot \frac{c_{u1}^2}{r} \qquad \qquad \frac{d}{dr} c_{a1}^2 = -2 \cdot c_{u1} \cdot \left( \frac{d}{dr} c_{u1} \right) - 2 \cdot \varphi^2 \cdot \frac{c_{u1}^2}{r}$$

$$\frac{d}{dr}\left(\frac{c_{a1}^{2}}{2}\right) = -c_{u1}\cdot\left(\frac{d}{dr}c_{u1}\right) - \varphi^{2}\cdot\frac{c_{u1}^{2}}{r}$$

$$\frac{d}{dr}{c_{a1}}^2 = -2 \cdot c_{u1} \cdot \left(\frac{d}{dr}c_{u1}\right) - 2 \cdot \phi^2 \cdot \frac{c_{u1}^2}{r}$$

$$\int_{r_{cp}}^{r} \frac{d}{dr} c_{a1}^{2} dr = c_{a1}^{2} - c_{a1.cp}^{2} = \int_{r_{cp}}^{r} -2 \cdot c_{u1} \cdot \left(\frac{d}{dr} c_{u1}\right) - 2 \cdot \phi^{2} \cdot \frac{c_{u1}^{2}}{r} dr$$

$$c_{a1} = \int_{r_{cp}}^{r} -2 \cdot c_{u1} \cdot \left(\frac{d}{dr} c_{u1}\right) - 2 \cdot \phi^{2} \cdot \frac{c_{u1}^{2}}{r} dr$$

$$c_{a1} = \sqrt{c_{a1.cp}^2 + \int_{r_{cp}}^{r} -2 \cdot c_{u1} \cdot \left(\frac{d}{dr}c_{u1}\right) - 2 \cdot \phi^2 \cdot \frac{c_{u1}^2}{r} dr}$$

$$\begin{aligned} & -\frac{a}{a} c_{a}^{2} - \frac{c}{a} c_{a}^{2} - \left(\frac{1}{c^{2}} - 1\right) \sqrt{\left(\frac{a}{a} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right)} + \sqrt{\frac{2c_{a}^{2}}{c^{2}}} + \left(1 - \sqrt{\frac{a}{a}} \left(2 c_{a} c_{a}^{2} + 2\right) - \frac{a}{a} c_{a}^{2} - \frac{d}{a} c_{a}^{2} - \left(\frac{1}{c^{2}} - 1\right) \sqrt{\left(\frac{a}{a} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right)} - \sqrt{\frac{2c_{a}^{2}}{c^{2}}} + \left(1 - \sqrt{\frac{a}{a}} c_{a}^{2} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right)} - \sqrt{\frac{2c_{a}^{2}}{c^{2}}} - \left(1 - \sqrt{\frac{a}{a}} c_{a}^{2} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right) - \sqrt{\frac{2c_{a}^{2}}{c^{2}}} - \left(1 - \sqrt{\frac{a}{a}} c_{a}^{2} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right)} - \sqrt{\frac{2c_{a}^{2}}{c^{2}}} - \left(1 - \sqrt{\frac{a}{a}} c_{a}^{2} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right) - \sqrt{\frac{2c_{a}^{2}}{c^{2}}} - \left(1 - \sqrt{\frac{a}{a}} c_{a}^{2} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right) - \sqrt{\frac{2c_{a}^{2}}{c^{2}}} - \left(1 - \sqrt{\frac{a}{a}} c_{a}^{2} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right) - \sqrt{\frac{2c_{a}^{2}}{c^{2}}} - \left(1 - \sqrt{\frac{a}{a}} c_{a}^{2} c_{a}^{2} - \frac{c}{a} c_{a}^{2}\right) - \sqrt{\frac{2c_{a}^{2}}{c^{2}}} - \left(1 - \sqrt{\frac{a}{a}} c_{a}^{2} c_{a}^{2}} - \frac{c}{a} c_{a}^{2}\right) - \sqrt{\frac{a}{a}} c_{a}^{2}} - \frac{c}{a} c_{a}^{2} c_{a}^{2}} - \frac{c}{a} c_{a}^{2} c_{a}^{2} - \frac{c}{a} c_{a}^{2}} - \sqrt{\frac{a}{a}} c_{a}^{2}} - \sqrt{\frac{a}{a}} c_{a}^{2} - \frac{c}{a} c_{a}^{2}} - \frac{c}{a} c_{a}^{2} c_{a}^{2}} - \sqrt{\frac{a}{a}} c_{a}^{2}} - \frac{c}{a} c_{a}^{2} c_{a}^{2} c_{a}^{2} c_{a}^{2}} - \frac{c}{a} c_{a}^{2} c_{a}^{2} c_{a}^{2} c_{a}^{2} c_{a}^{2} c_{a}^{2} c_{a}^{2} c_{a}^{2}} - \frac{c}{a} c_{a}^{2} c_{a}^{2} c_{a}^{2} c_{a}^{2} c_{a}^{$$

$$c_{a1.cp} = 160$$

 $c_{a1.cp} = 160$  r = 0.8  $r_{cp} = 0.4$   $L_u = 250000$   $\omega = 3200$   $R_{cp} = 0.3$  m = -1

 $c_{a2.cp} = 150$ 

 $\mathbf{B} = \left(\frac{\mathbf{L}_{\mathbf{u}}}{2 \cdot \mathbf{\omega}}\right) \qquad \mathbf{A} = \left[\left(1 - \mathbf{R}_{\mathbf{cp}}\right) \cdot \mathbf{\omega} \cdot \mathbf{r}_{\mathbf{cp}}^{\mathbf{m}+1}\right]$ 

$$\sqrt{c_{a1.cp}^2 - \frac{2 \cdot \varphi^2 \cdot (\ln(r) - \ln(r_{cp})) \cdot (A \cdot r^2 + B)^2}{r^2}} = 2161.496i$$

$$\frac{\sqrt{B^2 \cdot r^2 - B^2 \cdot r_{cp}^2 - B^2 \cdot \phi^2 \cdot r^2 + B^2 \cdot \phi^2 \cdot r_{cp}^2 + A^2 \cdot r^2 \cdot r_{cp}^4 - A^2 \cdot r^4 \cdot r_{cp}^2 + r^2 \cdot r_{cp}^2 \cdot r_{cp}^2 + A^2 \cdot \phi^2 \cdot r^2 \cdot r_{cp}^4 - A^2 \cdot \phi^2 \cdot r^2 \cdot r_{cp}^4 - A^2 \cdot \phi^2 \cdot r^2 \cdot r_{cp}^2 - 4 \cdot A \cdot B \cdot \phi^2 \cdot r^2 \cdot r_{cp}^2 \cdot \ln(r) + 4 \cdot A \cdot B \cdot \phi^2 \cdot r^2 \cdot r_{cp}^2 \cdot \ln(r)}{r \cdot r_{cp}}} = 2243.635i$$

### Вывод общего ур-я профилирования Л Т по радиусу с потерями

$$\frac{1}{\rho} \cdot \left( \frac{\mathrm{d}}{\mathrm{dr}} \mathbf{p} \right) = \frac{c_{\mathrm{u}}^2}{\mathrm{r}}$$

$$\frac{1}{\rho} \cdot \left(\frac{d}{dr}p\right) = \frac{c_u^2}{r}$$

Ур-е Бернулли: 
$$\frac{c^2}{2} = -\int_0^1 \frac{1}{\rho} d\rho - L_{Tp}$$

Работа трения: 
$$L_{\text{тp}} = \left(\frac{1}{\varphi^2} - 1\right) \cdot \frac{c^2}{2}$$

$$c_{11} \cdot r^{m} = const$$

$$c_u \cdot r^m = c_{u.cp} \cdot r_{cp}^m$$
 следовательно

$$c_{u}(r) = c_{u.cp} \cdot \left(\frac{r_{cp}}{r}\right)^{m}$$

$$\frac{d}{dr}c_{u}(r) = \begin{vmatrix} x0 = 0.8 & \text{simplify} = \\ \frac{d}{dx0}c_{u}(x0) & \frac{d}{dx0}c_{u}(x0) \end{vmatrix}$$

$$\varphi(r) = const$$

следовательно

$$\frac{\mathrm{d}}{\mathrm{d}r}\varphi = 0$$

(B) 
$$\frac{c^2}{2} = -\int_0^1 \frac{1}{\rho} dp - L_{Tp}$$

$$\frac{c^2}{2} = -\int_0^1 \frac{1}{\rho} d\rho - \left(\frac{1}{\varphi^2} - 1\right) \cdot \frac{c^2}{2}$$

$$\frac{c^2}{2} + \left(\frac{1}{\varphi^2} - 1\right) \cdot \frac{c^2}{2} + \int_0^1 \frac{1}{\rho} dp =$$

$$\frac{1}{\varphi^2} \cdot \frac{c^2}{2} + \int_0^1 \frac{1}{\rho} dp = 0$$

+C

$$\frac{1}{\varphi^2} \cdot \frac{c_a^2 + c_u^2}{2} + \int_0^1 \frac{1}{\rho} dp = 0$$

(B) 
$$\frac{c^2}{2} = -\int_0^1 \frac{1}{\rho} dp - L_{Tp}$$
  $\frac{c^2}{2} = -\int_0^1 \frac{1}{\rho} dp - \left(\frac{1}{\varphi^2} - 1\right) \cdot \frac{c^2}{2}$   $\frac{c^2}{2} + \left(\frac{1}{\varphi^2} - 1\right) \cdot \frac{c^2}{2} + \int_0^1 \frac{1}{\rho} dp = 0$   $\frac{1}{\varphi^2} \cdot \frac{c^2}{2} + \int_0^1 \frac{1}{\rho} dp = 0$  (PP)  $\frac{1}{\varphi^2} \cdot \frac{c^2 + c_u^2}{2} + \int_0^1 \frac{1}{\rho} dp = 0$ 

$$\frac{d}{dr} \left( \frac{1}{\varphi^2} \cdot \frac{c_a^2 + c_u^2}{2} + \int_0^1 \frac{c_u^2}{r} dr \right) =$$

$$\frac{d}{dr}\left(\frac{1}{\varphi^2}\cdot\frac{c_a^2+c_u^2}{2}+\int_0^1\frac{c_u^2}{r}dr\right)=0 \qquad \qquad \frac{d}{dr}\left(\frac{1}{\varphi^2}\cdot\frac{c_a^2+c_u^2}{2}\right)+\frac{d}{dr}\left(\int_0^1\frac{c_u^2}{r}dr\right)=0 \qquad \qquad \frac{1}{2\cdot\varphi^2}\cdot\frac{d}{dr}\left(c_a^2+c_u^2\right)+\frac{d}{r}\left(c_a^2+c_u^2\right)+\frac{d$$

$$\frac{1}{2 \cdot \varphi^2} \cdot \frac{d}{dr} \left( c_a^2 + c_u^2 \right) + \frac{c_u^2}{r} = 0$$

$$\frac{1}{2 \cdot \varphi^2} \cdot \left[ \frac{\mathrm{d}}{\mathrm{dr}} \left( c_a^2 \right) + \frac{\mathrm{d}}{\mathrm{dr}} \left( c_u^2 \right) \right] + \frac{c_u^2}{r} = 0$$

$$\frac{1}{\varphi^2} \cdot \left[ c_a \cdot \frac{d}{dr} (c_a) + c_u \cdot \frac{d}{dr} (c_u) \right] + \frac{c_u^2}{r} = 0$$

$$c_a \cdot \frac{d}{dr} (c_a) + c_u \cdot \frac{d}{dr} (c_u) + \phi^2 \cdot \frac{c_u^2}{r} = 0$$

$$c_{a} \cdot \frac{d}{dr} \left(c_{a}\right) + \left[c_{u.cp} \cdot \left(\frac{r_{cp}}{r}\right)^{m}\right] \cdot \left[-\frac{m \cdot c_{u.cp} \cdot \left(\frac{r_{cp}}{r}\right)^{m}}{r}\right] + \varphi^{2} \cdot \frac{\left[c_{u.cp} \cdot \left(\frac{r_{cp}}{r}\right)^{m}\right]^{2}}{r} = 0$$

$$c_{a} \cdot \frac{d}{dr} \left( c_{a} \right) + \left[ c_{u.cp} \cdot \left( \frac{r_{cp}}{r} \right)^{m} \right] \cdot \left[ - \frac{m \cdot c_{u.cp} \cdot \left( \frac{r_{cp}}{r} \right)^{m}}{r} \right] + \varphi^{2} \cdot \frac{\left[ c_{u.cp} \cdot \left( \frac{r_{cp}}{r} \right)^{m} \right]^{2}}{r} = 0$$

$$\left[ c_a(r) \cdot \frac{d}{dr} \left( c_a(r) \right) + \left[ c_{u.cp} \cdot \left( \frac{r_{cp}}{r} \right)^m \right] \cdot \left[ - \frac{m \cdot c_{u.cp} \cdot \left( \frac{r_{cp}}{r} \right)^m}{r} \right] + \phi^2 \cdot \frac{\left[ c_{u.cp} \cdot \left( \frac{r_{cp}}{r} \right)^m \right]^2}{r} \right] dr = \frac{c_a(0.8)^2}{2} + 4 \cdot c_{u.cp}^2$$

$$\frac{c_a(r)^2}{2} + \frac{c_{u.cp}^2 \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}}{2} - \frac{\varphi^2 \cdot c_{u.cp}^2 \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}}{2 \cdot m} + C = 0 \quad \begin{vmatrix} \text{substitute}, r = r_{cp} \\ \text{substitute}, c_a(r_{cp}) = c_{a.cp} \end{vmatrix} = 4 \cdot c_{u.cp}^2 + C + 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \text{ simplify} \quad = 4 \cdot c_{u.cp}^2 + C + 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \text{ solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^2 - 0.5 \cdot c_a\left(\frac{2}{5}\right)^2 = 0 \quad \text{solve}, C \quad = -4 \cdot c_{u.cp}^$$

$$\frac{c_{a}(r)^{2}}{2} + \frac{c_{u.cp}^{2} \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}}{2} - \frac{\varphi^{2} \cdot c_{u.cp}^{2} \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}}{2 \cdot m} + C = 0 \text{ substitute}, C = -\frac{m \cdot c_{a.cp}^{2} - \varphi^{2} \cdot c_{u.cp}^{2} + m \cdot c_{u.cp}^{2}}{2 \cdot m} = 3 \cdot c_{u.cp}^{2} - 0.5 \cdot c_{a.cp}^{2} + 0.5 \cdot c_{a}^{2} \cdot \left(\frac{4}{5}\right)^{2} = 0$$

$$-\frac{m \cdot c_{a.cp}^{2} + m \cdot c_{u.cp}^{2} - m \cdot c_{a}(r)^{2} - \phi^{2} \cdot c_{u.cp}^{2} - m \cdot c_{u.cp}^{2} \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m} + \phi^{2} \cdot c_{u.cp}^{2} \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}}{2 \cdot m} = 0 \text{ simplify } = 3 \cdot c_{u.cp}^{2} - 0.5 \cdot c_{a.cp}^{2} + 0.5 \cdot c_{a}^{2} \left(\frac{4}{5}\right)^{2} = 0$$

$$\frac{c_{a}(r)^{2}}{2} - \frac{c_{u.cp}^{2}}{2} - \frac{c_{a.cp}^{2}}{2} + \frac{c_{u.cp}^{2} \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}}{2} + \frac{\varphi^{2} \cdot c_{u.cp}^{2}}{2 \cdot m} - \frac{\varphi^{2} \cdot c_{u.cp}^{2} \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}}{2 \cdot m} = 0 \text{ solve, } c_{a}(r) = 0$$

Проверка

m = 0.6

 $\varphi = 0.98$ 

$$\begin{pmatrix} r \\ r_{cp} \end{pmatrix} = \begin{pmatrix} 0.45 \\ 0.5 \end{pmatrix}$$

$$\begin{pmatrix} c_{a.cp} \\ c_{u.cp} \end{pmatrix} = \begin{pmatrix} 12 \\ 120 \end{pmatrix}$$

$$\frac{\sqrt{m \cdot c_{a.cp}^{2} + m \cdot c_{u.cp}^{2} - \phi^{2} \cdot c_{u.cp}^{2} - m \cdot c_{u.cp}^{2} \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m} + \phi^{2} \cdot c_{u.cp}^{2} \cdot \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}}{\sqrt{m}} = 36.19$$

$$\sqrt{c_{a.cp}^2 + c_{u.cp}^2 \cdot \left(1 - \frac{\varphi^2}{m}\right) \cdot \left[1 - \left(\frac{r_{cp}}{r}\right)^{2 \cdot m}\right]} = 36.19$$

(c.a2

 $(r_{cp})$ 

 $(r_{c_l})$ 

 $\frac{1}{p^2 \cdot \ln(r_{c_1})}$ 

 $p^2 \cdot \ln(r_{cp})$ 

$$\frac{A^{2} \cdot \varphi^{2} \cdot m \cdot r_{cp}^{2-2 \cdot m} + A^{2} \cdot \varphi^{2} \cdot r_{cp}^{2} \cdot \left(\frac{1}{2}\right)^{m} - A^{2} \cdot m^{2} \cdot r_{cp}^{2} \cdot \left(\frac{1}{2}\right)^{m} - \frac{B^{2} \cdot m^{2} \cdot r_{cp}^{2}}{r^{2}} + 2 \cdot A \cdot B \cdot m^{2} \cdot r_{cp}^{1-m} - A^{2} \cdot m \cdot r_{cp}^{2} \cdot \left(\frac{1}{2}\right)^{m} - \frac{B^{2} \cdot m \cdot r_{cp}^{2}}{r^{2}} - \frac{2 \cdot A \cdot B \cdot m \cdot r_{cp}^{2}}{r^{2}} - \frac{2 \cdot A \cdot B \cdot m^{2} \cdot r_{cp}^{2}}{r^{2}}$$

r<sub>cp</sub>

$$\frac{A^{2} \varphi^{2} \cdot m \cdot r_{cp}^{2-2 \cdot m} + A^{2} \cdot \varphi^{2} \cdot r_{cp}^{2} \cdot \left(\frac{1}{r}\right)^{m} - A^{2} \cdot m^{2} \cdot r_{cp}^{2} \cdot \left(\frac{1}{r}\right)^{m} - \frac{B^{2} \cdot m^{2} \cdot r_{cp}^{2}}{r^{2}} - 2 \cdot A \cdot B \cdot m^{2} \cdot r_{cp}^{1-m} - A^{2} \cdot m \cdot r_{cp}^{2} \cdot \left(\frac{1}{r}\right)^{m} - \frac{B^{2} \cdot m \cdot r_{cp}^{2}}{r^{2}} + \frac{2 \cdot A \cdot B \cdot m \cdot r_{cp}^{2}}{r^{2}} + \frac{2 \cdot A \cdot B \cdot m^{2} \cdot r_{cp}^{2}}{r^{2}} +$$

r<sub>cp</sub>