A NEW METHOD FOR ASSEMBLY LINE BALANCING HAVING STOCHASTIC WORK ELEMENTS

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Abstract—The main feature of the method suggested in this paper is the assignment of priority to elements and priority elements are preferred to non-priority elements when assigning elements to stations. It accepts element times from known or unknown symmetrical distributions, minimizes the variation within a station and allows assignments of elements to stations such that each station time does not exceed the probability confidence levels set by management.

INTRODUCTION

Assembly line balancing refers to the procedure of assigning tasks to work stations in such a manner as to approxion the assembly work among the stations as evenly and compactly as possible without violating any precedence requirements. The assignment of elements to work stations is subject to the following conditions:

- (1) Each element task is assigned to one and only one work station.
- (2) The sum of the time of all elemental tasks within a work station does not exceed the cycle time.
- (3) The stations thus formed can be ordered so that the partial orderings among elemental tasks are not violated.

Considerable effort has been devoted to the assembly line balancing problem in order to obtain a better balance in terms of minimum number of stations and minimum total idle time. Early work in assembly line balancing by Bryton[8], Salveson[37], Bowman[5], Jackson[18], Held et al.[14], Mitchell[27], Burgeson and Daun[9], Tonge[39, 40], Arcus[2, 3], Kilbridge and Wester [19, 20], Hoffman [16], Helgeson and Birnie [15], Klein [22], Gutjahr and Nemhausher [13] and quite recently work by Bennett et al.[4] and Raouf et al.[34], considered deterministic element times only. However, production lines are manned by human beings who seldom, if ever, maintain exactly the same working pace throughout the work period. Besides, no two individuals have the same working pace. Thus, the human variability complicates the system and converts the assembly line balancing problem from a deterministic into a stochastic problem with which production engineers and shop floor management must cope. Presently, methods developed by Moodie and Young [28], Mansoor [25], Brennecke [7], Ransing and Downing [32], Rao [33], Reeve [34, 35], Mansoor and Tuvia [26], and Dar-El [10, 11] solving the assembly line balancing problem under variable element times assume that element time is normally distributed. Kottas and Lau[23, 24] developed a new heuristic method based on cost consideration for balancing a paced assembly line which exhibits normal element time variations. There is ample evidence in the literature that element time values are not necessarily normally distributed. Sphicas and Silverman[38] showed that for certain classes of distribution of element times, the stochastic formulation is equivalent to the deterministic approach. A review of early work on assembly line balancing problems is given by Ingall [17] and Kilbridge and Wester [21]. From the existing techniques, it is observed that none of the researchers seem to consider minimizing the variations in station times as the elements are assigned to the work stations.

A new heuristic method which is based on Omar's [30] approach, has been developed. The new method is likely to minimize the variations in station times and accept element times which come from any symmetrical distribution.

COEFFICIENT OF VARIATION

The coefficient of variation (CV) of a distribution is defined as the ratio of the standard deviation to the mean. Assuming no correlation between elements, Brady and Drury [6] showed

that "if a new element is added to a group of elements, the coefficient of variation of the new group will be less than that of the old group, provided that the CV^2 of the new element is less than (1+2*r) times the CV^2 of the old group, where "r" is the ratio of the mean of the old group to the mean of the new element".

By incorporating this concept into the assembly line balancing method, it is likely that the variation of station times will be reduced. From a list of available elements for assignment, a set of elements is chosen which can be placed into the current station provided that its inclusion will not cause the station time to exceed the cycle time and that the probability that the station time will exceed the cycle time is within a predetermined value. From this set of elements, a subset of elements is chosen such that its inclusion into the current station will satisfy Brady and Drury's theorem. The one with the lowest CV among the elements in the subset is chosen to be added to the current station. This criterion is bypassed when the subset is empty. In this way, it is assured that the addition of an element to the work station will decrease the variation in station time. Thus, the probability that the station time exceeds the cycle time is reduced. As a result, the overall performance of the assembly line will likely be improved.

CHEBYSHEV'S INEQUALITY

Netter [29] and Dudley [12] showed that the element time values are not necessarily normally distributed. Since there is no evidence that elemental time is precisely normally distributed, the normality assumption on element times and station times can be relaxed by using Chevyshev's inequality:

If X is a random variable with mean μ and variance σ^2 , then for any positive number K the following inequality, known as Chebyshev's inequality holds.

$$P(|x - \mu| \ge K\sigma) \le 1/K^2. \tag{1}$$

By assuming independence between element times and considering station time (ST) as a random variable having a symmetric distribution, with mean C, according to Chebyskev's inequality, we have:

$$P(|ST - C| \ge K\sigma_{ST}) \le 1/K^2 \tag{2}$$

where C is the cycle time and σ_{ST} is the standard deviation of the station time. We are only interested in the case when $(ST - C) \ge 0$. Thus, the last inequality can be written as

$$P[(ST - C) \ge K_{\sigma ST}] \le 1/2K^2.$$
 (3)

The above inequality simply means that the probability of (ST - C) exceeds $K_{\sigma ST}$ is always less than or equal to $1/2K^2$. If the mean and standard deviation of ST are known, it is possible to estimate the probability that each of the operators will be able to accomplish the assigned task within a predetermined C value.

If we are given a certain probability confidence level, say P_c , that represents the probability a ST can exceed the given C time, we then can calculate the value for K from the following expression:

$$K = \sqrt{(1/2P_c)}. (4)$$

Assuming no correlation between element times, we can find the station time for station $j(ST_i)$ at $P_c = 1/2K^2$ from:

$$ST_{i} = \sum_{i \in j} U_{i} + K \sqrt{\left(\sum_{i \in j} \sigma_{i}^{2}\right)}$$
 (5)

where U_i is the mean and σ_i^2 is the variance of element time for element i in station j.

THE HEURISTIC METHOD

Omar's heuristic method [30] is simple to use and provides good results for deterministic element times for almost all problems mentioned in assembly line balancing literature. We shall incorporate the proposed ideas into Omar's method in handling stochastic element times. A brief description of the method for deterministic element time values is given. A complete description of this method and a computer program has been provided in Ref. [34]. A modification of the method in dealing with stochastic time values will then be given in the next section.

It is assumed that a cycle time, uncorrelated element times and a precedence diagram are given. The heuristic method consists of two phases:

Phase I is the determination of the critical path and the assignment or priority to the work elements. The steps employed in phase I are as follows:

- (1) Obtain the critical path of the given problems for each end element that requires at least two stages before its completion.
 - (2) Assign priority to the critical elements which fall in the critical path.
- (3) Assign priority to those elements that have immediate successors and the cumulative time values sum of the immediate successors is greater than or equal to the cycle time.
- (4) Assign priority to those elements which are direct predecessors of a critical element and immediate successors of another element and whose cumulative sum is greater than the cycle time.
- (5) Assign priority to those elements which are direct predecessors of critical elements and have the lowest elemental time value among them.

Phase II is the assignment of elements to the work stations on the assembly line. The assignment of elements is done by the "largest candidate priority rule" which entails considering first the priority elements in declining order of the element time values and then the non-priority elements in the same manner for the purpose of assigning them to the work stations.

For treating the element times as stochastic variables, the coefficient of variation (CV) and Chebyshev's inequality are incorporated into the heuristic method as outlined above. In addition to the cycle times, mean element times and the precedence diagram, elemental time variance and the maximum probability confidence levels are assumed to be given.

Phase I of the new method will be the same as in the deterministic case.

In Phase II, the elements are assigned to consecutive work stations along the assembly line by the "least CV priority rule". This entails considering first the priority elements which cause the least increase in CV of the station and the non-priority elements which follow in the same manner.

The algorithm employed in phase II is as follows:

- (1) From the P-matrix[†], all elements whose rows contain all zeros are noted. These are called "available elements".
- (2) From the available elements, the priority and the non-priority elements are placed in the priority list and the non-priority list respectively.
- (3) From the priority list obtained in step 2, a set of priority elements is formed. Each element in the set satisfied the following two conditions: (a) its inclusion into the station will not cause the station time to exceed the cycle time and, (b) the probability that the resulting station time exceeds the cycle time is less than or equal to a predetermined value.
- (4) A subset of elements from the set obtained in step 3 is formed, consisting of elements that satisfy Brady and Drury's theorem [6].
- (5) If this subset is empty, steps 3 and 4 are repeated for elements in the non-priority list. Otherwise, from this subset the ones which cause the least increase in CV of the station are assigned to the current station. Brady and Drury's theorem is by passed when the subset of non-priority element is also empty.

In this case, the choice of elements assigned to station is based upon the ones which cause the least increases in CV of the station, with preference for the priority elements.

- (6) Elements in the row of the assigned element in the F-matrix \dagger are noted. In the corresponding rows in the P-matrix indicated by the elements just noted, the assigned element is replaced by a zero. If the assignment of a zero causes the row in the P-matrix to become all zeros, the corresponding element becomes an available element.
- (7) The elements are assigned according to steps 2-6 until the priority list and the non-priority list are empty. When this is the case, the problem is solved.

AN ILLUSTRATED PROBLEM

A 14-element problem (1) from industry is chosen to illustrate the new method. Precedence diagram, P-matrix and F-matrix are shown in Fig. 1. Mean element times and element variances are shown in Table 2.

For this problem Omar's method does not seem to produce good results in deterministic element times because there are many starting elements to choose. Conduct phase I in the backward direction (right to left) for the precedence diagram and phase II in the forward direction (left to right), a better result is obtained. A comparison of the results for cycle time 39 sec is shown in Table 3.

Element No.	P-Matrix	F-Matrix
1 2 3 4 5 6 7 8 9 10 11 12 13	0 0 1 0 0 0 0 0 3 4 2 0 0 0 7 0 6 8 9 0 0 0 11 0	0 0 6 0 5 0 5 0 14 0 9 0 8 0 9 0 10 0 13 0 12 0 13 0 14 0

Table 1. Dual precedence matrices for 14-element problem

Table 2. Mean and variance of element time for 14-element problem

Element No.	Elemen	t Time
Lienent no.	Mean	Variance
1 2 3 4 5 6 7 8 9 10 11 12	7 25 12 6 11 13 16 11 6 12 19	0.36 19.36 15.21 2.89 1.69 4.84 5.29 6.25 8.41 1.69 5.29 6.79
14	13	28.09

Table 3. Comparison of proposed backward assignment method with other methods for cycle time 39

(30)	New Method	Moodie & Young(28)	Hoffman (16)
6	5	5	5
61	22	22	22
31.54	9.64	17.32	17.32
74 %	88.7%	88.7%	88.7%
	6 61 31.54	6 5 61 22 31.54 9.64	6 5 5 61 22 22 31.54 9.64 17.32

[†]This shows the immediate followers of each element (see Table 1).

We shall apply the improved method to the 14-element problem for stochastic element time. Further, we assume that the cycle time is fixed at 39 sec abd that management wishes that the maximum probability for each station to exceed the cycle time to be not more than 5%. From eqn (4) we can calculate the value of K.

$$K = \sqrt{(1/0.05)} = 3.162.$$

In phase I, all fourteen elements are priority elements. In phase II, element 1, 3, 4, 7 and 11 are the available elements. To begin with, the one with the least CV^2 is chosen to be assigned to work station 1. From Table 3, element 1 is assigned to station 1 and the station time is increased to 8.14 sec. From the P-matrix, and the F-matrix, element 2 is added to the available element list.

Only elements 3, 4, 7 and 11 are capable of being assigned to station 1 because the inclusion of element 2 in station 1 will cause the station time to exceed the given cycle time. The Brady and Drury theorem is bypassed since none of the elements 3, 4, 7 and 11 satisfied its' hypothesis (Table 4). Element 11 is assigned to station 1 because it causes the least increase in CV of station 1. The station time now is increased to 33.52 sec. Element 12 is added to the available list. No further elements can be added to station 1 since its inclusion will cause the station time to exceed the cycle time of 39 sec. Now a new station is opened for assignment. Continuing the same procedure, the final results of assignment are shown in Table 6.

Element	cv ²
1	0.0073
3	0.1056
4	0.0803
7	0.0207
i	

Table 4. CV² of available elements

Table 5. Resultant station CV^2 with element i included

0.0147

Element i	ement i Element CV ² (1+2r) Station CV	
3	0.0156	0.0160
4	0.0803	0.0245
7	0.0207	0.0138
11	0.0147	0.0128
		l

r = mean of station/mean of new element

Table 6. Balance for the 14-element problem for cycle time 39 sec

E1ements	Station Time (ST)	Idle Time	P(ST > CT)
1,11	33.52	5.48	0.017
7,8	37.74	1.26	0.04
2	38.91	0.09	0.049
6,12	36.91	2.22	0.034
4,3	31.45	7.55	0.021
5,9	27.05	11.95	0.010
10,13	28.28	10.72	0.008
14	29.76	9.24	0.027
	1,11 7,8 2 6,12 4,3 5,9	Time (ST) 1,11 33.52 7,8 37.74 2 38.91 6,12 36.91 4,3 31.45 5,9 27.05 10,13 28.28	Time Time 1,11 33.52 5.48 7,8 37.74 1.26 2 38.91 0.09 6,12 36.91 2.22 4,3 31.45 7.55 5,9 27.05 11.95 10,13 28.28 10.72

Smoothness index = 20.70

output efficiency = 84.5%

ZONING CONSTRAINTS

Besides the precedence requirements imposed upon the grouping of elements into work stations, zoning constraints are common in assembly lines because of the layout of production facilities. An example is the non-assignment of tasks to be done on the front and the back of a product to an operator where those tasks require him to cross the conveyor line.

Modifications are made in the heuristic method to handle zoning constraints as well as deterministic and variable element times values. Instead of placing the available elements into priority and non-priority lists, we now place them in one of the following four lists:

- (1) Priority zone list that contains elements that can only be placed in the current zone.
- (2) Non-priority zone list that contains elements that can only be placed in the current zone.
- (3) Priority list that contains elements that can be placed in the current zone or some other zones.
- (4) Non-priority list that contains elements that can be placed in the current zone or some other zones.

Priority zone list has the highest priority and the non-priority list has the lowest priority. The 21-element problem from Tonge [40] with zoning constraints (Table 7) is solved for varriable element time values and the balance is given in Table 8. Many researchers did mention the zoning constraints but they did not solve the assembly line balancing zone constraints problem using their proposed methods especially for variable element times.

RESULTS

The new heuristic method for assembly line balancing is programmed in FORTRAN language. A flow chart which describes details of the procedure is depicted in Appendix A. The program listing is given in Appendix B. This program can be used for cases where work elements are assumed to be deterministic or stochastic in nature.

Three sample problems are used in testing the new heuristic method. They are:

- (1) 14-element problem from industry[1]
- (2) 21-element problem from Moodie and Young[28]
- (3) 11-element problem from Kottas and Lau[23].

A summary of the solutions under stochastic element times at various probability confidence levels for the three chosen problems and comparisons with other methods are given in Table 8. Further, a summary of the comparisons between the CV^2 of each station obtained by the new heuristic method and the three chosen problems obtained by using other methods are given in Table 9.

Table 7. Zoning constraints for the 21-element from Tonge [40]

Zone	Elements		
1	1, 2, 3, 4, 5, 7, 8, 21		
2	3, 4, 6, 7, 8, 9, 10, 11, 12, 13, 15, 16, 18		
3	13, 14, 15, 16, 17, 18, 19, 20		

Table 8. Balance for the 21-element problem for cycle time 20 under variable element time with zoning constraints with 95% probability confidence level

Work Station	Elements	Station Time(ST)	Idle Time	P (ST>CT)
1	1,2	11.47	8,53	0.006
2	3	13,47	6.53	0.008
3	4,21	18.32	1.68	0.031
4	5	14.48	5.52	0.012
5	7,6	18.32	1.68	0.031
6	8,9	19.07	0.93	0.039
7	11,10,12,15,1	6 20.07	0.00	0.051
8	13,14,18	18.48	1.52	0.031
9	17	20.07	0.00	0.051
10	20,19	9.47	10.53	0.004
	1	1	L	<u> </u>

Smoothness index = 16.27

Output efficiency = 81.55%

Table 9. Comparison of various	methods under variable	element times for	different cycle	times and probability	
confidence levels					

Pc	# of elements	Method	Cycle Time	# of Stat	Idle Time	s.i.	Eff.
95%	14	(1)	39	8	47.51	20.13	84.77
·	1	(2)	1	8	48.52	20.7	84.46
		(3)	ļ	8	49.40	20.0	84.17
95%	14	(1)	40	7	22.03	11.5	92.13
Ì	l '	(2)	Ì	7 7 8	23.3	13.3	91.68
	1	(3)	ļ	8	57.41	20.0	82.0
90%	14	(1)	35	7	12.65	7.0	93.24
		(2)		7 7 8	13.9	8.84	94.32
		(3)	Ì	8	43.68	17.41	84.40
85%	14	(1)	34	7	16.56	7.0	93.04
		(2)	ì	7	17.16	7.86	92.79
]]	(3)		8	49.21	18.3	82.0
95%	21	(1)	21	9	30.0	16.53	84.13
ŀ		(2)	I	9	29.0	16.73	84.64
l		(3)]	10	47.2	20.91	77.52
90%	11	(1)	10	7	14.3	6.17	82.1
i	1	(2)	1	7 7	12.63	6.79	81.96
l		(3)		7	13.48	7.47	80.74

- S.I. Smoothness index
- Output efficiency Eff. {1-Idle time/(Cycle time * Station Time) }*100% Eff =
- Moodie & Young method (28) (1)
- Proposed method
- (3) Helgeson and Birnie method (15)
- (4) (5) Proposed method under normality assumption
 - Kottas & Lau (23) under normality

Table 10. Comparison of CV² of various methods at different probability confidence levels

Work Station	CV1 ²	or ure	14- ment	$\frac{\text{CV}_1^2}{\text{CV}_2^2} \text{ of the 21-} \\ \text{element}$	$\frac{\text{CV}_3^2}{\text{CV}_4^2} \text{ of the 11-} \\ \text{element}$
	95%	90%	85%	95%	90%
1	5.13	1.0	1.0	1.0	1.0
2	1.0	1.0	1.0	1.0	1.0
3	0.82	1.0	1.0	1.0	0.76
4	0.71	1.0	1.0	0.91	1.0
5	0.27	1.58	1.58	0.95	1.40
6	1.45	1.16	1.16	1.33	1.0
7	1.0	1.0	1.0	1.27	1.0
8	1.0			1.0	
9				0.66	

In Table 8, we see that the proposed method is far more superior than the Helgeson and Birdnie RPW method and it gives almost similar results when compared to Moodie and Young's method. From Table 9, the proposed method minimizes the variability of the station for better than any of the methods. Moreover, results from the new heuristic method are more realistic when we take into consideration station variability and all symmetrical distributions of work elements. The new heuristic method provides the maximum allowable balance to the assembly line balancing problem. When the distribution of work element is known, we can simply replace Chebyshev's inequality by the limits imposed by that distribution.

CONCLUSIONS

The incorporation of the coefficient of variation and Chevyshev's inequality into the critical path heuristic method [30] for the assembly line balancing problem do provide good and realistic results. The new heuristic method has the following characteristics:

- (a) It can handle variable element time values.
- (b) It can handle zoning constraints.
- (c) In the case of stochastic assembly line balancing; (1) It accepts element time from known or unknown symmetrical distribution. (2) It minimizes the variation within a station. (3) It allows assignment of elements to station such that each station time does not exceed the probability confidence levels set by management.

REFERENCES

- 1. B. Amin, An Algorithm to Solve Stochastic Line Balancing Problem Using Moodie and Young's and Chevyshev's Inequality, Research paper, Dept. of Industrial Engineering, Rutgers University, New Jersey, 1979.
- A. L. Arcus, Assembly line balancing by computer. Graduate School of Business, University of California, Berkley, June 1962.
- 3. A. L. Arcus, COMOSAL—A computer method of sequencing operations for assembly lines. *Int. J. Production Res.* 4(4), 259-277 (1966).
- 4. G. R. Bennette & Jack Byrd, Jr., A trainable heuriestic procedure for the assembly line balancing problem. *AIIE Trans.* 8(2), 195-201 (1976).
- 5. E. H. Bowman, Assembly line balancing by linear programming. Opers. Res. 8(3), 385-9, (1960).
- 6. W. Brady & C. G. Drury, The dependence of the coefficient of variation of a work time distribution of number of elements in the work task. *Int. J. Production Res.* 7(4), 311, 1 (1969).
- 7. Brennecke, D., Two parameter assembly line balancing model. *Models and Analysis for Production Management* (Edited by M. Hottenstein). International Textbook Company, Scranton, Pennsylvania (1968).
- 8. B. Bryton, Balancing of a continuous production line. Unpublished M.S. Thesis, Northwestern University (1954).
- J. W. Burgeson and T. E. Daum, Production line balancing. File No. 10.3.002, Akron, International Business Machines Corporation, Ohio, 1958.
- E. M. Dar-El, MALB—A heuristic technique for balancing large single-model assembly lines. AIIE Trans 5(5), 343-356 (1973)
- 11. E. M. Dar-El, Solving large single-model assembly line balancing problems—A comparative study. AIIE Trans. 7(3), 302-310 (1975)
- 12. N. A. Dudley, Work Measurement, Some Research Studies, p. 43. MacMillan, London (1968).
- 13. A. Gutjahr & G. Nemhauser, An algorithm for the line balancing problem. Management Sci. 11(2), 308-333 (1964).
- M. Held, P. M. Karp & R. Shareshian, Assembly line balancing—dynamic programming with precedence constraints. Opers Res. 11(3), 442-459 (1963).
- 15. W. P. Helgeson & D. P., Birnie, Assembly line balancing using the ranked positional weight technique. J. Indus. Engng 12(6), 394-398 (1961).
- 16. T. R. Hoffman, Assembly line balancing with a precedence matrix. Management Sci. 9(4), 551-563 (1963).
- 17. E. J. Ingall, A review of assembly line balancing. J. Indus. Engng 16(4), 244-254 (1965).
- 18. J. R. Jackson, A computing procedure for a line balancing problem. Management Sci. 2(3), 261-267 (1956).
- 19. M. D. Kilbridge & L. Wester, A heuristic method of assembly line balancing. J. Indus. Engng 12(4), 292-298 (1961).
- 20. M. D. Kilbridge & L. Wester, Heuristic line balancing—A case. J. Indus. Engng 13(3), 139-149 (1962).
- 21. M. D. Kilbridge & L. Wester, Review of analytical systems of line balancing. Opers Res. 10(5), 626-638, (1962).
- 22. M. Klein, On assembly line balancing. Opers Res. 11(2), 274-281 (1963).
- 23. J. F. Kottas & H. S. Lau, A cost-oriented approach to stochastic line balancing. AIIE Trans. 5(2), 164-171 (1973).
- J. F. Kottas & H. S. Lau, A total operating cost model for paced lines with stochastic tasks times. AIIE Trans. 8(2), 234-240 (1976).
- 25. E. M. Mansoor, Assembly line balancing—An improvement on the ranked positional weight technique. J. Indus. Engng 15(2), 73-77 (1964).
- 26. E. M. Mansoor & B. S. Tuvia, Optimizing balanced assembly lines. J. Indus. Engng 18(3), 1966.
- J. Metchell, A computational procedure for balancing zoned assembly lines. Res. Reps. No. 6-94801-R3, Pittsburgh: Westinghouse Research Laboratories, Feb. 1957.
- 28. C. L. Moodie & H. H. Young, A heuristic method of assembly line balancing for assumptions of constant or variable work element times. J. Indus. Engng 16 (1), 23-29, (1965).
- 29. M. A. Netter, Critical path analysis of repetitive man machine systems operations. Ph.D. Dissertation, University of Michigan, Ann Arbor, Michigan, 1969.
- 30. M. T. Omar, Development of a heuristic method for assembly line balancing, Unpublished M.A.Sc. Thesis, University of Windsor, 1975.
- 31. A. Papoulis, Probability, Random Variables and Stochastic Processes. McGraw-Hill, New York (1965).
- 32. K. Ramsing & R. Downing, Assembly line balancing with variable element time. Indus. Engng 41-43(1970).
- 33. D. Rao, Single and mixed model assembly line balancing methods for both deterministic and normally distributed work element times. Unpublished M.S. Thesis, Oregon State University, June 1971.
- A. Raouf, E. A. El-Sayed & C. L. Tsui, A new heuristic approach to assembly line balancing. Comput. Indus Engng 4, 223-234 (1980).
- 35. N. R. Reeve, A heuristic technique for assembly line balancing, Unpublished M.S. Thesis, State University of New York at Buffalo, 1968.
- N. R. Reeve, Balancing continuous stochastic assembly lines. Unpublished Ph.D. Thesis, State University of New York at Buffalo, 1971.
- 37. N. R. Reeve & W. H. Thomas, Balancing stochastic assembly lines. AIIE Trans. 5(3), 223-229 (1973).
- 38. M. E. Salveson, The assembly line balancing problem. J. Indus. Engng 6(3), 18-25 (1955).

- G. P. Sphicas & F. N. Silverman, Deterministic equivalents for stochastic assembly line balancing. AIIE Trans. 8(2), 280-282 (1976).
- 40. F. M. Tonge, Summary of a heuristic line balancing procedure. Management Sci. 7(1), 21-42 (1960).
- 41. F. M. Tonge, A heuristic program for assembly line balancing. Prentice Hall, Englewood Cliffs, New Jersey (1961).
- 42. F. M. Tonge, Using probabilities combinations of heuristics. Management Sci. 11, 727-735 (1965).
- C. L. Tsui, Stochastic assembly line balancing using the coefficient of variation and Chebyshev's inequality, M.A.Sc. Major Paper, Dept. of Industrial Engineering, University of Windsor, Windsor, Ontario, 1980.

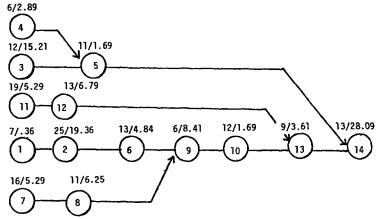
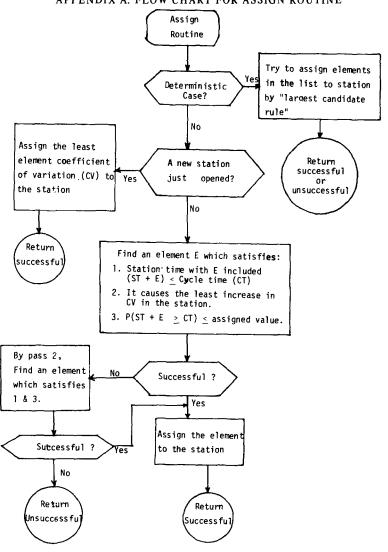
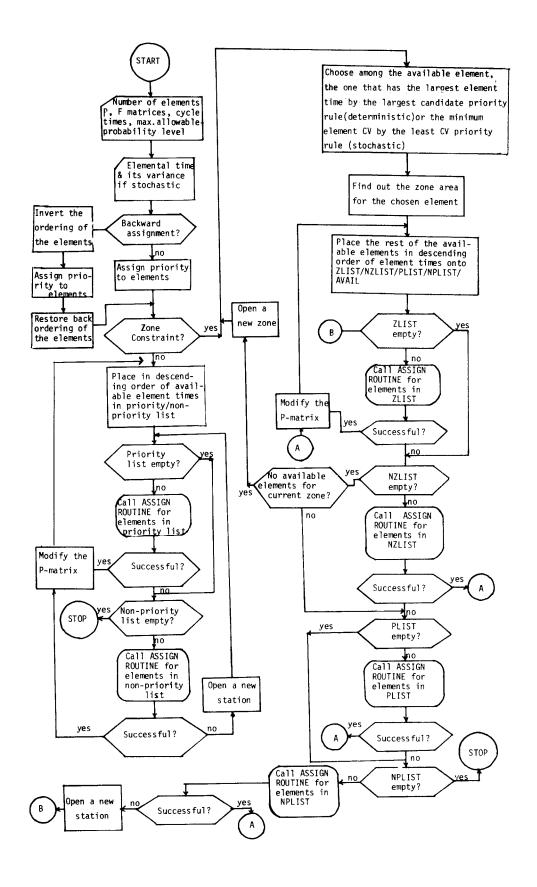


Fig. 1. Precedence diagram for 14 element problem.

APPENDIX A: FLOW CHART FOR ASSIGN ROUTINE





APPENDIX B:

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                     CRITICAL PATH APPROACH TO ASSEMBLY LINE BALANCING ZCNE CONSTRAINTS (IZ = 1)
                      THIS PROGRAM IS WRITTEN IN FORTRAN AND CONSISTS OF TWO PHASES
                               PHASE 1----THE DETERMINATION OF THE CRITICAL PATH FOR EACH ELEMENT WHICH HAS AT LEAST TWO ELEMENTS BEFORE IT ALONG THE PATH & ASSIGNMENT OF PRIORITY TO ELEMENTS

PHASE 2----ASSIGNING THE ELEMENTS TO STATIONS
                    DEFINING THE VARIABLES USED IN THE PROGRAM

CT-----CYCLE TIME

NOE-----NC. OF ELEMENTS IN THE FECBLEM

NOCP----NC. OF CCLUMNS IN F MATRIX

NOCF-----NC. OF CCLUMNS IN F MATRIX

IZ-----INCORPORATES ZONE CONSTRAINTS (VALUE 1)

CR NO CCNSTRAINTS (VALUE 0)

N2------NC. OF ZONE AREA UNDER CONSIDERATION

IB------EACKWARD (VALUE 1) OR FORWARD (VALUE 0) ASSIGNMENT

OF FRIGRITY FOR THE ELEMENTS

ALLOW-----NAXIMUM ALLOWABLE FACBABILITY THAT THE STATION

WILL NOT EXCEED THE CYCLE TIME

TIME (M)-----ELEMENTAL TIME FOR ELEMENT M

VAR(M)-----TIME VARIANCE FOR ELEMENT M

CV2(M)-----SUARE OF COEFFICIENT OF VARIATION FOR ELEMENT M

CDP(M)------CUMULATIVE TIME OF CIRECT PREDECESSIES FOR

ELEMENT M

CIF(M)-----------CUMULATIVE TIME OF IMMEDIATE SUCCESSORS OF

ELEMENT M

CLEMENT M

CLEMENT M

CLEMENT M
                          FLAG-----SUCESS(VALUE 0) OR FAILUFE(VALUE 1) OF A CF AVAILABLE ELEMENTS TO CURRENT STATION
                                                                                                                                                                                                        ASSIGNMENT
                    THIS PROGRAM CAN HANDLE UP TO A SO ELEMENT-PROBLEM. WITH A MAXIMUM OF 15 DIRECT PROBLECTSSERS OR IMMEDIATE SUCCESSURS FOR EACH ELEMENT.
                     DATA INPLT : (FCRMATTED)
                           1. FIRST SET OF DATA CONTAINS:
COLUMN 1-3 NOF
4-6 NGCP
7-9 NOCF
                          1. FIRST SET OF DATA CONTAINS:

CCLUMN 1-3 NOF (12)

4-6 NGCP (13)

7-9 NOCF (13)

10-14 CT (F5.0)

15 12 (11)

16-17 NZ (12)

18 1B (11)

20-23 ALLON (F4.2)

2. SECOND SET OF DATA CONTAINS REAL VALUES OF ELEMENT TIMES

IN F5.0 FCMMAT

3. THIRD SET OF DATA CONTAINS NOE GROUPS UP DATA IN 13 FOR MAT

ITH GROUP CONTAINS DIRECT PREDECESSORS & IMMEDIATE

SUCCESSORS OF ELEMENT 1 (ALL IN INTEGER FURM).

IF THE NUMBER OF DIRECT PREDECESSORS AND ZUR

IMMEDIATE SUCCESSORS < NOCP AND/OR NOCF, FILLED

THE REMAINING WITH ZERCS OR BLANKS.

4. FOURTH SET OF DATA CONTAINS HEAL VALUES OF ELEMENT TIME

VARIANCE IN F6.3 FORMAT.
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```
A. KAOUF and C. L. TSUI

1111 READ(5.555.END=$999)NCE.NDCP.NDCF.CT.12.NZ.IB.ALLOW
555 FDRMAT(313.FE.O.11.12.11.1X.F4.2)
READ(5.555)(TIME(I).I=1.NCE)
FORMAT(116.C)
RVF(2)=CICIT(NCCF)
RVF(4)=DICIT(NCCF)
DO 1 I=1.NCE
READ(5.FY)(F(I,J).J=1.NCCP).(F(I,J).J=1.NUCF)
IF (TIME(I).GT.TLARGE)TLARGE=TIME(I)
TLARGE=TLARGE*NDE
ALPHA=$CRT(I.Y(2*ALLOW))
READ(5.5666)(VAR(I).I=1.NCE)

5666 FURMAT(13FC.3)
IF (IE.EG.O)GC TC 101
CALL INVERT(NCE.NOCP.NLCF.P.F.TIME)

C****** PHASE 1

C****** FIND CUT ELEMENTS THAT DO NOT HAVE FREDECESSORS & ASSIGN THEM
C***** IT THEIR ELEMENTAL TIME AS THEIR LATEST FINISH TIME.

101 DU 10 IS.NOCE
IF (P(I.J).NE.O)GC TC 100
LST(I)=TIME(I)
NIEP-NIEP+1
NF(NIEP)=I

100 IF (F(I,J).NE.O)GC TC 10
DC 12 J=2.NCCF
11 F(F(I,J).NE.O)GC TC 10
NIEP-NIEP+1
NF(NIEP)=I

10 CONTINUE

C****** ASSIGN PRIGRITY IC THOSE END ELEMENTS THAT REQUIRE AT LEAST
                               NF(NIE)=I
CONTINUE

** ASSIGN PRICHITY TO THOSE FND ELEMENTS THAT FEIGHT AT LEAST

** TWO ELEMENTS REFORE IT ALONG THE RATH
DO 120 JF=1.NIE
FF=NF(JF)
DO 122 J=1.NICP
IF(P(FF,J).EG.0)GC TO 122
9P=P(FF,J)
DO 123 JP=1.NIEF
IF(NP(JF).NE.PF)GC TO 123
GU TO 122
 10 CC
C*****
C******
                                GU TO 122
CONTINUE
PRT(FF)=1
        123
PRT(FF)=1
    SLACK(FF)=0.
    GU TC 120

122    CONTINUE
120    CINTINUE
C******    DETERMINE THE LATEST FINISH TIME (LST), COP & C10 FOR LAGGE
C******    ELEMENT
    OU 13    1=1,NCE
    OU 133    J=1,NCCP
    IF(P(I,J),EC.0)GC TU 123
    PP=P(I,J)
    COP(I)=CEP(I)+TIME(PP)

133    CONTINUE
                            CUNTINUE
      133
                             CUNTINUE

DD 14 J=1.NC(F

IF (F(I.J).EC.0)GC TO 14

FF=F(I.J)

CIF(I)=CIF(I)+TIME(FF)

TMAX=LST(I)+TIME(FF)

IF (LST(FF).LT.TMAX)LST(FF)=TMAX

CONTINUE

** ASSI(N PRICRITY TO THOSE ELEMENTS-VHOSE CIF > CT

IF (CIF(I).CE.CT)PRT(I)=1

CONTINUE

DO 171 JF=1.NIE
           13
                               DO 171 JF=1.NTE
FF=NF(JF)
FF=NF(JF)
1777 POINT=C
C***** DETERMINE THE CRITICAL ELEMENT AND ASSIGNED WITH PMIDWITY
DO 172 JJ=1.NGCP
PP=(FF.J)
IF(PP.EC.0)GC TO 172
SLACK(PF)=LST(FF)-LST(PP)-TIME(FF)
IF(SLACK(PF).NE.0.)GO TO 172
PRT(PP)=1
POINT=FF
172 CONTINLE
      172
                              CONTINUE
FF=POINT
                             FF=PGINI

DU 173 JF=1.NIEP

IF (FF.NE.NF(JP)) GU TC 173

PRT(FF)=1

GC TC 171

CONTINUE

GO TO 1777

CONTINUE

TL=TLARGE

DU 14 J-1.NGE
      173
      171
                            CONTINUE
TL=TLARGE
DU 18 I=1.NDE
IF(SLACK(1).NE.O.)GU TO 18

** ELEMENTS WHICH ARE DIRECT PREDECESSORS OF A CRITICAL ELEMENT

** AND HAVE THE LEAST ELEMENTAL TIME AMONG THOSE WHICH ARE

** DIRECT PREDECESSORS OF CRITICAL ELEMENTS ARE ASSIGNED WITH

** PRICRITY
DC 20 J=1.NCCP
PP=P(1,J)
IF(PF.EQ.O)GC TO 20
IF(TL.LT.TIME(PP))GC TO 20
IF(TL.LT.TIME(PP))GC TO 20
IF(TL.LT.TIME(PP))GC TO 21

** NLE=NLE+1
DPCLT(NLE)=PP
C*****
C******
C******
                                                                        DPCLT(NLE)=PP

CC TC 20
TL=TIME(PF)
NLE=1
DPCLT(NLE)=PP
       181
           20
                                             CONTINUE
```

```
21
211
     25
                                                                    CCLNT(K)=0
CD 23 J=1.NDCP
FP=P(I,J)
IF(FF.EC.0)GD TD 23
CD 25 K=1.NDE
IF(SLACK(K).NE.0.)GD TC 29
DD 24 L=1.NDCF
IF(F(K.L).EQ.0)GC TD 24
IF(F(K.L).EQ.0)GC TD 24
IF(F(K.L).EQ.PF)CDUNT(K)=CCUNT(K)+1
CCNTINUE
CCNTINUE
CCNTINUE
CCNTINUE
CCNTINUE
CCNTINUE
CC 6 K=1.NDE
              24
29
23
                                                                      CCNTINLE
DD 26 K=1.NDE
IF(CCUNT(K).LT.1)GD TO 26
M=0
CET=0.
DC 27 J=1.NCCP
DC 27 L=1.NCCP
PP=P(I.J)
IF(PP.EG.C)GD TO 27
IF(PP.NE.F(K,L))GC TC 27
CET=CET-LIME(DD)
                                                                                           CET=CET+TIME(PP)
                                                                                          DEIF(M)=PP
CCNTINUE
IF(CET.LT.CT)GG TC 26
DG 3C J=1.M
MM=DFIF(J)
PRT(NM)=1
            27
    30
                                                                   CENTINUE
                             CONTINUE
                               TF(1B.EG.C)GC TC 8999

CALL INVERT(NCE,NCCP,NCCF,P,F,TIME)

NUMIV=NCE+1
                     CALL INVERTINCE, NCCP, NCCF, P, F, TIME)

NUMIV=NCE+1

DO 44 I=1, NIE

NP(I)=NUMIV-NF(I)

NIEP=NIE

IH=NUMIV/2

DO 43 I=1, IH

IVN=NUMIV-I

PRT(IVN)=PRT(I)

PRT(IVN)=PRT(I)

PRT(IV)=IRRT

WRITE(6, SCCC)NCC

FORMAT('1', T8.'INFUT CATA FOR ', T24, I3, T27, '-CLEMENT PROBLEM',

$////, T5.'ELEMENT NO.', T27, 'PPECEDENCE MATRIX')

DO 2 I=1, NCE

VF(5)=DIGIT(NCCF)

WRITE(6, VF)I, (F(I, J), J=1, NCCP)

WRITE(6, SCC2)

FORMAT(///, T8, 'ELEMENT NC.', T27, 'IMMEDIATE SUCCESSOR MATRIX')

VF(5)=DIGIT(NCCF)

DO 3 I=1, NCE

WRITE(6, VF)I, (F(I, J), J=1, NCCF)

WRITE(6, VF)I, (F(I, J), J=1, NCCF)

WRITE(6, SCC2)

FORMAT(///, I8, 'ELEMENT NC.', T25, 'ELEMENT TIME', T40, 'PRIURITY',

$T33, 'VAFIANCE', T67, 'CV2')

DO 4 I=1, NCE

CV2(I)=VAR(I)/TIME(I), PAT(I), VAR(I), CV2(I)

FORMAT(IX, TII, I3, T27, F7, 2, T43, I1, T54, F6, 3, T66, F6, 4)

*** PHASE 2

IF(IZ, EC, 1)GC TO 7COC

NPTR=0
    44
   43
8999
9000
  2
  9002
  3
  9003
                            PTR=0
NPTR=0
DO 40 J=1.NIEP
PP=NP(J)
IF (PRT(PP).NE.1)CC*TO 401
CALL SCRT(PIR.PLIST.PP)
GU TC 40
CALL SCRT(NPTR.NPLIST.PP)
CONTINLE
      401
                             SN0=1
                             EP=1
CUMST=0
CUMST=0.
CUMVAR=C.
SWP=0.
SWP=0.
SWNP=0.
STMAX=0.

C****** TRY TO ASSIGN ELEMENTS IN PRICEITY LIST AND THEN ELEMENTS IN C******** NCN-PRICEITY LIST TO CUPRENT STATION
200 IF(PIR.LE.0)GO TO 300
201 F(AG=0
                          FLAG=0

CALL ASSIGN(PTR.PLIST.SNC,EP,FLAG,LELE,SWP)

IF(FLAG.EC.0)GC TC 21C

IF(NPTR.LE.0.AND.SWP.EC.1.)GO TO 2C3

IF(NPTR.LE.0)GC TC 202
                         IF(NPTR.LE.0)GC TC 202
FLAG=0
CALL ASSIGN(NPTR.NPLIST.SND.EP.FLAG.LELE.SWNP)
IF(FLAG.EG.C)GC TO 210
IF(SMP.EG.1..OF.SWNP.EG.1.)GD TC 200

** ELEMENTS IN EDTH LISTS CANNOT BE ASSIGNED TC CURRENT STATION
NWS(SNC)=EP-1
STCV2(SNC)=CLWVAR/CUMST**2
PROB(SNC)=CUWVAR/(2.*(CT-CUMST)**2)
ST(SNO)=CUWVAR/(2.*SGFT(CUMVAR)
     201
     202
```

```
CUMVAR=(.

IF(ST(SNC).LE.CT)GG TC 2222

STMAX=CT
IDLE(SNC)=0.

GU TO 2CCC

IF(ST(SNC).GT.STMAX)STMAX=ST(SNC)
IDLE(SNC)=CT-ST(SNC)
  2222
  2000
                       FP = 1
                        EP=1
SNO=SNC+1
CUMST=C.
IF(IZ.EC.1)GC TG 7299
GD TO 200
                        SU 1U 200

1* MCDIFYING F-MATRIX

DO 50 L=1.NCCF

FF=F(LELE.L)

1F(FF.EG.0) CC TC 50

CZ=0
  C*****
      210
                        DO 41 J=1,NCCP

IF(P(FF+J).NE.C)GC TO 40C0

CZ=CZ+1

GD TC 41
                    IF(P(FF.J).NE.LELE)GC TC
P(FF.J)=0
CZ=C2+1
CONTINUE
IF(CZ.NE.NCCF)GC TC 50
IF(PRI(FF).NE.I)GC TC 50
CALL SCFT(PTR.PLIST.FF)
GU TC 50
CALL SCFT(NFTR.NPLIST.FF)
CUNTINUE
SMP=0.
SMNP=0.
GD TC 260
  4000
                                     IF (P(FF.J).NE.LELE) GC TC 41
      500
                  SWP=0.
SWNP=0.
GO TO 2GO

*** TRY TC ASSICN ELEMENTS IN NCN-FRICKITY LIST WHEN THE PRIDRITY

*** LIST IS EMPTY. IF FOTH LISTS ARE EMPTY STOP.

IF(NPIR.GI.O.GR.SWNP.EC.I.)GO TC 201
    ST(SNC)=CLMS1+ALPHA*SCRT(CUMVAF)
    PRDE(SNC)=CUMVAR/CUMSI**2)

STCV2(SNC)=CLMVAR/CUMSI**2

IF(ST(SNO).GI.STMAX)SIMAX=ST(SNO)

IDLE(SNC)=CT-ST(SNC)

NWS(SNO)=EP-1

TIDL=0.

TIDL=0.

TIDL=0.

##ITE(6.9CG6)NCE

FORMAT('!'.//*T8.'CRITICAL PATH APPREACH TO ASSEMBLY LINE',

$T49.'BALANCING FCF'.TE3.I3.TGG.'-FLEWENT PROBLEM')

#GRAT(120.'WITH'.T27.A20)

WRITE(6.9IC1)C2.ALLOW

FORMAT(T20.'WITH'.T27.A20.TSO.' & FFCHABILITY = ',

$T72.FS.3)

IF(IB.EG.0)GC TC 652

WRITE(6.9ICC)C3

WRITE(6.9ICC)C3

IF(IZ.EG.0)GL TG 653

WRITE(6.9ICC)C4

WRITE(6.9ICC)C4

WRITE(6.9ICC)C5

FGRMAT('C'.//.T8.'STATICN NO.', F30.'ELEMENT IN THE STATIUN'./)

DO 60 I=1.5NC

NWSE=NKS(I)

TIDL=TIDL+TDLE(I)

IF(STMAX.NEW.ECT)GC TO 600
 C******
C*****
      300
 7100
 9006
 9100
 650
9101
    €52
               9001
    600
605
601
     602
       60
9200
80
 9201
 9009
 9012
7000
5000
7005
9105
```

```
DO 7008 J=1,NZ
IZC=0
DO 7099 I=1.NCE
IF(ZGNE(I,J).EG.0)GO TC 7099
IZC=IZC+1
NF(IZC)=I
 NF(IZC)=I

7099 CONTINUE

yF(5)=DIGIT(IZC)

7008 WRITE(6.VF)J,(NF(IJ),IJ=1.IZC)

DO 7007 KK=1,24

7007 AVAIL(KK,2)=KK+1

AVAIL(KK,2)=C

C******* CHECSE AMONG THE AVAILABLE ELEMENTS THE ONE THAT HAS THE

C****** CHOSEN ELEMENT CV2. FIND CUT THE ZONE AREA FOR THIS

C****** CHOSEN ELEMENT & FLACE THE REST OF THE AVAILABLE ELEMENTS

C****** CNTO THE ZLIST, NZLIST, PLIST, NPLIST & AVAIL

7PTR=0
                              ZP TR=0
                              NZPTR=0
PTR=0
NPTR=0
                            FIND=0.
APTR=0
PPTR=1
SWZ=0.
SWP=0.
SWN=0.
                            SWNP=0.
SWD=0.
TCV2=10C.
DO 7001 J=1.NIEF
PP=NP(J)
IF (PRT(PP).NE.1)GC TG 7010
IF (CV2(FP).GE.TCV2)GC TC 7010
TC V2=CV2(PP)
IF (SWZ.EQ.C.)GG TC 7005
CALL INSERT(MPE)
MPE=PP
SWZ=1.
  7009
                            MPE=PP

SWZ=1.

GO TO 7CC1

CALL INSERT(FP)

CONTINUE

CALL SEF(NZCNE,MPE,ZLIST,ZPTR,NZLIST,NZFTP,PLIST,PTR,NPLIST,NPTR)

SNU=1

EP=1

EP=1
  7010
7001
CUMST=0.
    STMAX=0.
7299    IEMPTY=PTR+NPTR+ZPTR+NZPTR

C******    IF NC AVAILABLE ELEMENTS CAN BE PLACED INTO THE CURRENT

C******    ZONE AREA. FIND A NEW ZUNE AREA
    IF(IEMPTY-EG.0.AND.APTF-EG.3)GC TO 7100
    IF(IEMPTY-EG.0.GC TO 7200
    DU 7301    I=1.NGE
    IF(ZCNE(I,NZCNE).EG.1.AND.SZ(I).EG.1)GC TO 7332

7301    IF(ZCNE(I,NZCNE).EG.1.AND.SZ(I).GT.1.AND.EP.GT.1)GG TO 7332

C******    ASSIGNMENT OF ELEMENTS TO CURRENT STATION.
7302    IF(ZPTR-LE.C)GC TO 7300
7304    FLAG=0
                              CUMST=0.
                            TELEGO CALL ASSIGN(ZPTR, ZLIST, SNO, EP, FLAG, LELE, SWP)

IF (FLAG, EG, C) GC TC 731C

IF (NZPTR, LE. C. AND. SWP. EQ. 1.) GO TC 7304
                              IF(NZPTR.LE.0)GC TC 7320
  7300
7305
                              FLAG=0
                             FLAG=0
CALL ASSIGN(NZPTR,NZLIST.SNO.EP.FLAG.LELE.SWNP)
IF(FLAG.EQ.0)GO TO 7310
IF(SWNP.EG.1..AND.SWP.EQ.1.)GO TC 7304
IF(SWNP.EG.1.)GC TO 7305
IF(SWNP.EG.1.)GC TO 7305
IF(FTR.LE.0)GO TC 7330
  7320
                            IF(PTR.LE.0)GU IL 7330
FLAG=0
CALL ASSIGN(FTR.PLIST.SNC,EP.FLAG,LELE.SWD)
IF(FLAG.EG.0)GC TO 7310
IF(NPTR.LE.C)GC TC 202
FLAG=0
CALL ASSIGN(NPTR.NPLIST.SNO.EP.FLAG.LELE.SWD)
IF(FLAG.EQ.0)GC TC 7310
CD TD 202
  7330
IF(FLAG.EQ.0)GL IL /J.U
GD TO 202

C****** MCDIFYING THE P-MATRIX UNDER ZCNING CONSTRAINTS
7310 DO 7342 J=1.NZ
7342 ZONE(LEL.J)=0
DO 7350 L=1.NGCF
FF=F(LELE.L)
IF(FF.EG.0)GC TO 7350
                            CZ=0
DO 7341 J=1,NCCF
IF(P(FF,J).NE.0)GC TU 7345
                          IF(P(FF, J) .NE.0)GC TO 7345

CZ=CZ+1
GO TC 7341

IF(P(FF, J) .NE.LELE)GO TC 7341

P(FF, J)=0

CZ=CZ+1

CONTINUE

IF(CZ.NE.NCCP)GO TO 7350

IF(ZONE(FF, NZCNE).EG.1)GC TO 7800

CALL INSERT(FF)
GO TO 7350

IF(PRT(FF).EG.0)GO TC 7825

IF(SZ(FF).EG.0)GO TC 7825

IF(SZ(FF).EG.0)GO TC 7825

CALL SCRT(ZPTR, ZLIST, FF)
GO TO 7350

CALL SCRT(PTR, FLIST, FF)
GO TO 7350

IF(SZ(FF).EG.0)GC TO 7826

CALL SCRT(PTR, FLIST, FF)
GO TO 7350

CALL SCRT(NZFTR, NZLIST, FF)
  7345
  7341
 7800
  7820
  7825
 7826
```

```
7350 CONTINUE
                                   CUNTAL
SWP=0.
SWNP=0.
CO TO 7299
  GO TO 7299

C****** START A NEW 2CNE AFEA. PUT ALL ELEMENTS IN THE PLIST & C****** NPLIST CNIC THE LINKEC LIST AVAIL.

7200 IF (PIR.EG.C)CO IC 7210
DO 7201 J=1.PTR
PP=PLIST(J)
ZONE(PP.NZENE)=0
SZ(PP)=SZ(FP)=1

7201 CALL INSERT(FP)
PIR=0
7210 IF (NPIR.EG.A)SC IC 72220
TALL INSERTIFE

7210 IF (NPTR.EG.0) GC TC 7220

00 7202 J=1.NPTR

PP=NPLIST(J)

ZONE(PP.NZCNE)=0

SZ(PP)=SZ(FF)=1

7202 CALL INSERT(FP)

NPTR=0

C****** ERCM THE LINKED LIST AVAIL. FIND THE UNE THAT HAS THE LAPSEST

C****** ELEMENT TIME WITH FREFERENCE GIVEN TO PRIORITY ELEMENTS

7220 IP=AVAIL(AFIR.2)

IF (IP.NE.0) GC TC 7221

MPE=AVAIL(AFIR.1)

CALL DELETE(0.APTR)

GO TO 7262

7221 MPE=0.
                                   SNPE = 0 .
                                  S# TH=0.
   7222
                             UPTR=0
CPTR=APTK
FIND=0.
TCV2=100.
MVAIL=AVAIL(CPTR.1)
IF(SNPE.EC.1.)GD TO 7252
IF(PRT(MVAIL).EG.C)GC TC 7250
IF(CV2(MVAIL).GE.TCV2)GC TO 7250
TCV2=CV2(MVAIL)
IF(SNTH.EG.C).GC TC 7265
CALL INSERT(MPE)
IF(UPTR.EG.C)UPTK=APTR
GO TO 7266
SWTH=1.
MPE=MVAIL
CALL DELETE(UPTR.CPTR)
GU TO 7261
UPTR=CPTK
CPTR=AVAIL(UFTR.2)
IF(CFTR.NE.0)CC TC 7261
IF(MPE.NE.C)GC TC 7262
SNPE=1.
GD TO 7222
                                    CPTR=APTH
   7251
  7252
  7265
   7266
IF (MPE.NE.0)CC TC 7251
IF (MPE.NE.0)GC TC 7262
SNPES1.
GO TO 7222
C****** FIND CUT THE NEW ZENE AREA FROM THE CHOSEN ELEMENT & PLACED
C****** THE REST OF THE FLEMENT IN AVAIL TO ZUIST, NZUIST, DUIST
C****** 6 NPLIST
7262 CALL SEP(NZENE, MFE.ZUIST, ZPTR.NZUIST, NZETR, DUIST, PTE.NPLIST, NDTE)
GO TO 7259
STUP
END
SUBROUTINE SERVEST
SIND
END
SUBRECTINE SCRI(LFTR.LIST.LELL)

C****** THIS FCUTINE SORT THE AVAILABLE FLEMENTS IN PHICKITY OF

C****** NON-FRICRITY LIST USING LARGEST CANCIDATE RULE
INTEGER WS(25.20).AVAIL(25.2).ZGNE(50.7).5Z(50).APTR.PPTR
INTEGER PRI(50)
DIMENSICN TIME(50).LIST(50).VAR(50).CV2(50)
COMMON TIME.WS.CT.CUMST.AVAIL.ZDNE.SZ.AFTR.PPTR.NZ.PRI
COMMON CMEAN.QVAR.CVC2.VAR.ALPHA.CUMVAR.STIME.CV2
IF(LPTR.NE.0)GC TO 5
LIST(1)=LELE
GO TO 15

DO 1 I=1.LFTR
L=LIST(1)
IF(TIME(LELE).LE.TIME(L))GC TO 1
J=LPTR

7 IF(J.LT.I)GC TO 10
                                IF (J.LT.1) @C TC LO
LIST(J+1)=LIST(J)
                              LIST(J+1)=LI
J=J-1
GO TO 7
CONTINUE
LIST(I)=LELE
LPTR=LPTR+1
RETURN
 END
SUBROUTINE ASSIGN(LPTR.LIST.SNC.EP.FLAC.LELF.SWV)

C****** THIS RCUTINE ASSIGNS THE AVAILABLE ELEMENTS TO THE CURRENT

C***** STATICN & DELETES THAT ASSIGNED FLEMENT FROM THE PRIURITY |

C****** NCN-PFICFITY LIST

INTEGER SNC.EP.FLAG.WS(25.20)
[NTEGER AVAIL(25.2).ZCNE(50.7).SZ(50).APTR.PPTR.PRT(50)

DIMENSIGN TIME(50).LIST(50).VAR(50).CV2(50)

COMMEN TIME.WS.CT.CUMST.AVAIL.ZCNE.SZ.AFTR.PPTR.NZ.PRT

COMMEN (MEAN.OVAF.CVC2.VAR.ALPFA.CUMVAF.STIME,CV2

SW=0.
                                 END
                                 COMMCN (MEAN, OVAF, CVL2, VAR, ALPF

SW=0.

UL=-.05*ALFHA

IF(EP.GT.1)GC TO 3

DO 1 K=1.*LPTR

LELE=LIST(K)

[F(K.*EG.1)GC TC 2

IF(CV2(LELE).GT.CVC2)GC TO 1

CVD2=CV2(LELE)
                   2
                                                  CONTINUE
LELE=LIST(II)
                   1
```

```
CUMST=TIME(LELE)
CUMVAR=VAR(LELE)
OMEAN=CUMST
OVAR=CUNVAR
GD TG 20
SW1=0.

*** BY FASS THE CCEFFICIENT OF VARIATION CRITERION
IF(SWV.EQ.0.)GC TO 12
CO 16 K=1.LPTK
LELE=LIST(K)
CUMVAR=CUMVAR+VAR(LELE)
3
C*****
                                                                      CUMST=CLMST+TIME(LELE)
CLMVAR=CLMVAR+VAR(LELE)
Z=(CT-CLMST)/SGRT(CUMVAR)
IF((Z-ALFHA).LT.UL)GC TC 19
CVC2=(CV4F+VAR(LELE))/(CMEAN+TIME(LELL))**2
IF(SM1.EC.L.)GC TO 60
CV2MIN=CVC2
II=K
SW1=1.
GC TC 19
IF((VC2.GE.CV2VIN)GC TC 19
CV2MIN=CVC2
II=K
CUMST=CLMST-TIME(LELE)
          60
                                                 CV2MIN=CVC2

II=K

CLMSI=CLMST-TIME(LELE)

CUMVAR=CLMVAR-VAR(LELE)

LELE=LIST(II)

CLMSI=CLMST+TIME(LELE)

CLMVAR=CUMVAR+VAR(LELE)

CVAR=GVAR+VAR(LELE)

CVAR=GVAR+VAR(LELE)

CVO2=CV2MIN

SNV=C*

GC TC 20

FIND CLI FLEWENTS THAT CAN HE ASSIGNED TO THE PRESENT STATION

DC 15 K=1*LPTE

LLLE=LIST(K)

CLMVAR=CLMVAR+VAR(LELE)

CUNVAR=CLMVAR+VAR(LELE)

Z=(CI-CLMSI)/SGRT(CUMVAR)

IF ((2-ALPHA)*LI*UL)GO TC 13

R=CMEAN/TIME(LELE)

C=(1+2*R)*CVO2

CVN2=CV2(LELE)

FROM THOSE CHOSEN ELEMENTS* THE LNE THAT GIVES THE MINIMUM

STATICN CV2 IS ASSIGNED

IF (CVX*LE*C)GC TC 70

SNV=I*

GC TO 13
19
18
C******
C*****
                                                                                                 GC TO 13
                                                                         5 * V=C.
          70
                                                                         Sw=0.
1F(Sw1.EG.1.)GC TO 80
                                                                       80
                                                                        GC TL 14
SN=1.
CLMST=CLMST-TIME(LELE)
CLMVAR=CLMVAR-VAR(LELE)
IF(SN.EG.O.)GC TC 90
FLAG=1
FETUEN
FFIE=LIST([I])
          13
 15
                                                                                                 HETIEN
LELE=LIST(II)
CLMST=CUMST+TIME(LELE)
CLMVAR=CUNVAR+VAR(LELE)
OMEAN=OMEAN+TIME(LELE)
CVAR=CVAR+VAR(LELE)
CVC2=CVAR/GMEAN**2
           90
                              WS(SNO.EF)=LELE
EP=EP+1
LPTR=LPTR-1
IF(II.LE.LPTF)GC TO 100
           20
                               LIST(II)=C
RETURN
                                               100
10
                               RETURN
                             RETURN
END
SUBROUTINE SEF(NZE, MPE, ZL, ZPTR, NZL, NZFTR, PL, PTR, NPL, NPTR)

** THIS RCUTINE FINDS THE NEW ZCNE AREA FROM THE CHOSEN ELEMENT

** (MPE) AND CALLS THE SCRT RCUTINE TO SORT ELEMENTS IN THE

** LIKED LIST AVAIL TO ZLIST, NZLIST, PLIST, NPLIST,

INTEGER AVAIL(25,2), ZCNE(50,7), SZ(50), ZL(50), ZPTF, PTR, APTR

INTEGER PL(50), PRT(50), UPTR, CPTR, PPTR, NS(25,2))

DIMENSICN NZL(5C), NPL(5C), TIME(50), VAR(5C), CV2(5C)

COMMON TIME, NS, CT, CUMST, AVAIL, ZCNE, SZ, AFTR, PPTR, NZ, PRT

COMMON TIME, NS, CT, CUMST, AVAIL, ZCNE, SZ, AFTR, PPTR, NZ, PRT

COMMON TIME, NS, CT, CUMST, AVAIL, ZCNE, SZ, AFTR, PTR, NZ, PRT

COMMON TIME, NS, CT, CUMST, AVAIL, ZCNE, SZ, AFTR, PTR, NZ, PRT

COMMON TIME, NS, CT, CUMST, AVAIL, ZCNE, SZ, AFTR, PTR, NZ, PRT

COMMON TIME, NS, CT, CUMST, ALPHA, CUMVAF, STIME, CV2

IF(ZCNE(NFE, J), EQ, 1)GC TC 11

NZE=J
C * * * * *
C*****
C *****
                            IF(ZCNE(NFE,J).EQ.1)GC IC II
NZE=J
IF(PRT(MPE).EQ.0)GC TC I3
CALL SCRT(ZFTR.ZL,MPE)
GO TO 14
CALL SORT(NZFTR.NZL,MFE)
IF(APTR.EG.0)RETURN
UPTR=0
CPTR=APTR
MVAIL=AVAIL(CPTF.1)
IF(ZGNE(MVAIL.NZE).EQ.C)GC TO 33
IF(PRT(MVAIL).EG.0)GO TO 25
```

END

```
IF (SZ(MVAIL).GT.1)GO TC 20
CALL SCRT(ZPTR,ZL,MVAIL)
GO TO 31
CALL SCRT(PTF.PL.MVAIL)
GO TC 31
IF (SZ(MVAIL).GT.1)GO TC 26
CALL SCRT(NZFTR.NZL,MVAIL)
GO TO 31
UP TR=CPTR
CPTR=AVAIL(UFTF.2)
GO TO 32
CALL SCRT(NPIR.NPL.MVAIL)
CALL DELETE(UPTR.CPTR)
IF (CPTR.GT.C)GC TC 12
RETURN
           25
           26
                         RETURN
                           RETURN
PRINT, 'EMPTY PCCL'
RETURN
END
END
SUBROUTINE CELETE(IPTR.JPTF)

C***** THIS RCUTINE DELETES AN ELEMENT FROM THE LINKED LIST AVAIL
INTEGER %S(25.20).AVAIL(25.2).ZCNE(50.7).SZ(50)
INTEGER PRI(50).FFTR.AFTF
DIMENSICN TIME(50).VAR(50).CV2(50)
COMMCN TIME.%S.CT.CUMST.AVAIL.ZONE.SZ.AFTR.PPTR.NZ.PPT
COMMCN CMEAN.JVAF.CV02.VAR.ALPHA.CUMVAF.STIME.CV2
IF(IPTR.NE.C)GC TC 1
IEMP=APTR
APTR=AVAIL(IEMP.2)
JPTR=APTR
AVAIL(IEMP.2)=PPTR
PPTR=IEMP
RETURN
1 AVAIL(IFTR.2)=AVAIL(JPTF.2)
                            RETURN
AVAIL(JPTR,2)=AVAIL(JPTR,2)
AVAIL(JPTP,2)=PPTR
PPTR=JPTR
JPTR=AVAIL(IFTR,2)
RETURN
 RETURN
END
SUBROUTINE INVERT(NCE,NCCP,NCCF,F,F,TIME)

C****** THIS RCUTINE INVERTS THE ELEMENT NUMBER IN PHMATRIX, F-MATRIX

C****** & TIME LIST FOR BACKWARD ASSIGNMENT
INTEGER P(SC.15),F(50.15)
DIMENSION TIME(EC)
IF(NCCF-NCCF)10,11,12

10 JJ=NCCP+1
DI LITTLE
                           JJ=NGCP+1
DD 1 I=1,NCE
DU 1 J=JJ,NCCF
P(I,J)=0
GO TC 11
JJ=NCCF+1
DU 2 I=1,NCE
DD 2 J=JJ,NCCP
F(I,J)=0
NCOL=(NCCP+NCCF+1)/2
NUM=NCE+1
DD 3 I=1,NCE
IVN=NUM-1
DD 3 J=1,NCCL
ITEMP=0
IF(F(IVN,J).EG.0)GC
   ı
           12
           11
                           UI 3 J=1, NCLL
ITEMP=0

IF(F(IVN,J).EG.0)GC TC 2C

ITEMP=NUM-F(IVN,J)

IF(P(I,J).EC.0)GC TO 21

F(IVN,J)=NUM-F(I,J)

GO TC 22

F(IVN,J)=0

P(I,J)=ITEMF

CONTINUE

IHALF=NUM-Z

DO 5 I=1.IHALF

IVN=NUM-I

TEMP=TIME(IVN)

TIME(IVN)=TIME(I)

TIME(I)≈TEMP

ITEMP=NOCP

NOCF=NOCF

NOCF=ITEMP
            20
           22
   5
                               NOCE-LIENE
                               RETURN
```