

Homework 1: representation and simulation of Inverted Pendulum

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11 de abril de 2018

Outline

Modeling

- Introduction

- Physical modeling

- Mathematical Analysis

Representation

- Linearization

- State space and Transfer Functions

- Stability

Introduction

This presentation wants to cover the topics of Homework 1, of the discipline of advanced control, namely,

- ▶ Mathematical Modeling of the system,
- ▶ Linearization and system representation,
- ▶ Stability analysis.

The physical system which we will analyze is called "Inverted Pendulum".

- ▶ Codes and further explanation are available in <https://github.com/eddardd/Control-Theory/tree/master/Advanced-Control>

Intuition

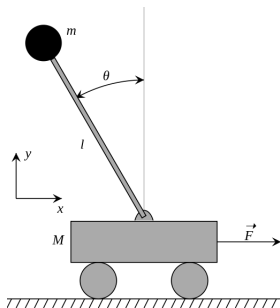


Figura: The physical schematic of our system

The system we have chosen is composed by a cart, with mass M , with a pole of length ℓ attached to it, with a ball of mass m at its extrema.

Intuition

The study of such system encounters applications, for example, in the development of devices called "Segways",



Figura: An example of a segway

Physical modeling

In order to describe the motion of our system, we shall adopt the Lagrangian formalism. To that effort, we need to define

$$\mathcal{L} = T - V$$

which accomplishes for the total energy in the system. Once we have it, we know it satisfies, for each degree of freedom, the **Euler-Lagrange** equation,

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{q}} - \frac{\partial \mathcal{L}}{\partial q} = 0$$

Physical Modeling

Analyzing the system, we recognize two degrees of freedom:

- ▶ The cart's position, x ,
- ▶ The pole's angle, θ

Being so,

- ▶ $T = \frac{1}{2}(M + m)\dot{x}^2 - m\dot{x}\dot{\theta}\ell\cos(\theta) + \frac{1}{2}(m\ell^2 + I)\dot{\theta}^2$
- ▶ $V = mg\ell\cos(\theta)$

Physical Modeling

With the last equations, and taking derivatives, we can write the Euler-Lagrange equations twice,

$$\begin{aligned}\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{x}} - \frac{\partial \mathcal{L}}{\partial x} &= F - b_x \dot{x} \\ \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\theta}} - \frac{\partial \mathcal{L}}{\partial \theta} &= -b_\theta \dot{\theta}\end{aligned}$$

These expressions leads to a system of (non-linear) equations,

$$\begin{aligned}(M + m)\ddot{x} - m\ell\cos(\theta)\ddot{\theta} &= F + m\ell\sin(\theta)\dot{\theta} - b_x\dot{x} \\ (m\ell^2 + I)\ddot{\theta} - m\ell\cos(\theta)\ddot{x} &= mg\ell\sin(\theta) - b_\theta\dot{\theta}\end{aligned}$$

Physical Modeling

Those equations can be solved by using Cramer's Rule, yielding the following,

$$\ddot{x} = \frac{(m\ell^2 + I)(F + m\ell\dot{\theta}\sin(\theta) - b_x\dot{x}) + m\ell\cos(\theta)(mg\ell\sin(\theta) - b_\theta\dot{\theta})}{(M + m)(m\ell^2 + I) - m^2\ell^2\cos^2(\theta)}$$
$$\ddot{\theta} = \frac{(M + m)(mg\ell\sin(\theta) - b_\theta\dot{\theta}) + m\ell\cos(\theta)(F + m\ell\dot{\theta}\sin(\theta) - b_x\dot{x})}{(M + m)(m\ell^2 + I) - m^2\ell^2\cos^2(\theta)}$$

which are the non-linear equations that govern the system dynamics.

Mathematical Analysis

Since we have equations for \ddot{x} and $\ddot{\theta}$, we notice that,

$$\dot{x} = f_1(t, x, \dot{x}, \theta, \dot{\theta}, u)$$

$$\ddot{x} = f_2(t, x, \dot{x}, \theta, \dot{\theta}, u)$$

$$\dot{\theta} = f_3(t, x, \dot{x}, \theta, \dot{\theta}, u)$$

$$\ddot{\theta} = f_4(t, x, \dot{x}, \theta, \dot{\theta}, u)$$

That is, by defining $\mathbf{x} = (x, \dot{x}, \theta, \dot{\theta})$, $\mathbf{f} = (f_1, f_2, f_3, f_4)$, we have,

$$\dot{\mathbf{x}} = \mathbf{f}(t, \mathbf{x}, u)$$

Mathematical Analysis

Indeed, we have defined a (non-linear) vectorial field over \mathbf{R}^4 .
A quick simulation using numerical integration gives us the following results,

Step response summary

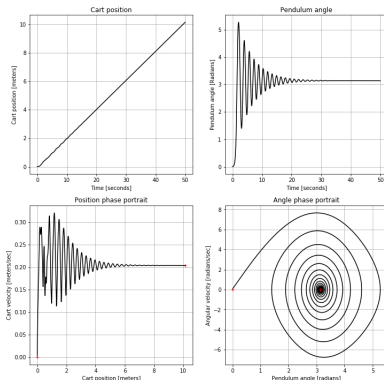


Figura: Step-response of the system

Mathematical Analysis

Indeed, two points are of our interest,

- ▶ The upward point, $\mathbf{x}_{sp} = (0, 0, 0, 0)$, which yields, by inspection, $\mathbf{f}(t, \mathbf{x}) = 0$.
- ▶ The downward point, $\mathbf{x}_{sp} = (0, 0, \pi, 0)$, which yields, by inspection, $\mathbf{f}(t, \mathbf{x}) = 0$.

These points gives rise of what we call **singular trajectories**, since for every t , with those initial conditions, $\mathbf{f}(\mathbf{x}) = 0$.

Stability

Assuming \mathbf{x}_{sp} being a stationary point, we informally define stability as,

- ▶ Stable stationary points are those whose, after applied a disturbance, tends to get back to the original point.
- ▶ Unstable points are those whose, after applied a disturbance, tends to go away from the original point.

Under those definitions, we notice that $(0, 0, 0, 0)$ is a unstable point, while $(0, 0, \pi, 0)$ is a stable one, matching our common sense.

Linearization

- ▶ Linearization is a local technique analysis, which permits us to transform the nonlinear equation $\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, u)$ into a linear one,
- ▶ By Taylor's Expansion,

$$\mathbf{f}(\mathbf{x}_{sp}, u) = \frac{\partial \mathbf{f}}{\partial \mathbf{x}}(\mathbf{x} - \mathbf{x}_{sp}) + \frac{\partial \mathbf{f}}{\partial u}u$$

in which we identify $\frac{\partial \mathbf{f}}{\partial \mathbf{x}}$ as the Jacobian matrix of \mathbf{f} . This gives us the following state-space representation,

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u$$

State Space equations

For $\mathbf{x}_{sp} = (0, 0, 0, 0)$, we calculate the partial derivatives of f , to achieve:

$$\mathbf{A} = \begin{bmatrix} 0 & \frac{1}{(m\ell^2 + I)b_x} & \frac{0}{(m\ell)^2 g} & \frac{0}{-m\ell b_\theta} \\ 0 & \frac{\alpha}{0} & \frac{\alpha}{0} & \frac{\alpha}{1} \\ 0 & \frac{m\ell b_x}{\alpha} & \frac{(M+m)mg\ell}{\alpha} & \frac{-(M+m)b_\theta}{\alpha} \\ 0 & \frac{m\ell b_x}{\alpha} & \frac{(M+m)mg\ell}{\alpha} & \frac{-(M+m)b_\theta}{\alpha} \end{bmatrix}$$

with $\alpha = (M+m)(m\ell^2 + I) - (m\ell)^2$.

State Space equations

For $\mathbf{x}_{sp} = (0, 0, \pi, 0)$, we calculate the partial derivatives of f , to achieve:

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & -\frac{(m\ell^2 + I)b_x}{\alpha} & -\frac{(m\ell)^2 g}{\alpha} & \frac{m\ell b_\theta}{\alpha} \\ 0 & 0 & 0 & 1 \\ 0 & \frac{m\ell b_x}{\alpha} & -\frac{(M+m)mg\ell}{\alpha} & -\frac{(M+m)b_\theta}{\alpha} \end{bmatrix}$$

with $\alpha = (M+m)(m\ell^2 + I) - (m\ell)^2$.

State Space equations

For \mathbf{B} , we have:

$$\mathbf{B}_0 = \begin{bmatrix} 0 \\ \frac{m\ell^2 + I}{\alpha} \\ 0 \\ \frac{m\ell}{\alpha} \end{bmatrix}$$

$$\mathbf{B}_\pi = \begin{bmatrix} 0 \\ \frac{m\ell^2 + I}{\alpha} \\ 0 \\ \frac{-m\ell}{\alpha} \end{bmatrix}$$

Transfer Function

The transfer functions of the system can be encountered by transforming the State-Space equation to frequency, and solving for $\frac{\mathbf{Y}}{U}$,

$$s\mathbf{X}(s) = \mathbf{A}\mathbf{X}(s) + \mathbf{B}u(s)$$

$$(s\mathbf{I} - \mathbf{A})\mathbf{X} = \mathbf{B}u$$

$$\mathbf{X}(s) = (s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}u$$

And, being $\mathbf{Y} = \mathbf{I}\mathbf{X}$, we have:

$$\frac{Y(s)}{U(s)} = (s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}$$

Transfer Function

Calculating and solving for each variable yields, for $\mathbf{x}_{sp} = (0, 0, 0, 0)$.

$$\frac{X(s)}{U(s)} = \frac{-((m\ell^2 + I)s^2 + b_\theta s - \frac{((m\ell^2 + I) - (m\ell)^2)mg\ell}{\alpha})}{\alpha s^4 + ((M + m)b_\theta + (m\ell^2 + I)b_x)s^3 + (b_\theta b_x - (M + m)mg\ell)s^2 - (mg\ell b_x)s}$$

$$\frac{\Theta(s)}{U(s)} = \frac{\frac{(m\ell^2 + I)m\ell}{\alpha}s^2 + \frac{(m\ell^2 + I)m\ell(b_x - 1)}{\alpha}s}{\alpha s^4 + ((M + m)b_\theta + (m\ell^2 + I)b_x)s^3 + (b_\theta b_x - (M + m)mg\ell)s^2 - (mg\ell b_x)s}$$

similar results can be done for $\mathbf{x}_{sp} = (0, 0, \pi, 0)$

Stability analysis in linear systems

The following theorem states the equivalence between stability of stationary points in non-linear and linear systems,

Lyapunov-Perron Theorem

Let \mathbf{x}_{sp} be a stationary point of a field $\mathbf{f} : \mathbb{R}^n \rightarrow \mathbb{R}^n$. Thus, \mathbf{x}_{sp} is a stable stationary point of \mathbf{f} if, and only if $\mathbf{J}|_{\mathbf{x}=\mathbf{x}_{sp}}$ has only eigenvalues with negative real part.

- ▶ This indeed allows us to substitute the analysis of stability of $\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x})$ by $\dot{\mathbf{x}} = \mathbf{J}\mathbf{x}$

Linear stable systems

We begin by noticing that the solution of $\dot{\mathbf{x}} = \mathbf{J}\mathbf{x}$ relies on the spectra of \mathbf{J} ,

- ▶ If \mathbf{J} is diagonalizable, then the solution is

$$\mathbf{x}(t) = \sum_{i=1}^n \xi_i e^{\lambda_i t}$$

for eigenvalues λ_i and eigenvectors ξ_i .

- ▶ If any λ_i has positive real part, then the solution diverges on at least one of its coordinates.
- ▶ The system is thus, unstable.

This is the criteria for Linear Stability.

Responses

Unstable linearized step response summary

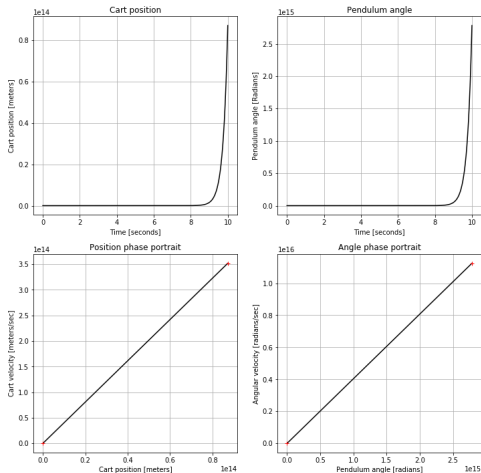


Figura: Linearized step response for $\theta_{sp} = 0$. Observe how it is unstable.

Responses

Stable linearized step response summary

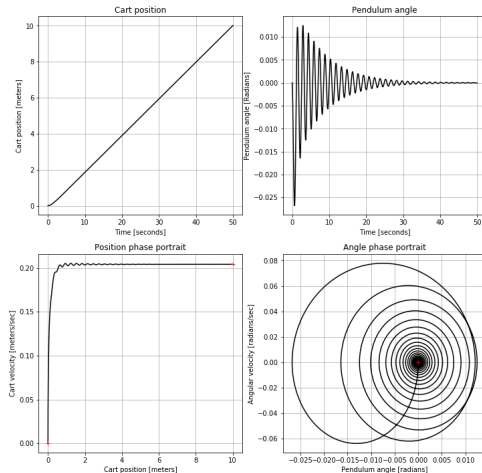


Figura: Linearized step response for $\theta_{sp} = \pi$. Confirming our claim that π is a stable stationary point.

Poles of linearizations

The later responses can be understood by looking at the eigenvalues of each linearized matrix, A :

Eigenvalue	A_0	A_π
λ_1	0	0
λ_2	-4.423	-1.0819
λ_3	-0.9469	$-0.126 + 4.218i$
λ_4	4.0349	$-0.126 - 4.218i$

Tabela: System's Eigenvalues

Since A_0 has a pole (or eigenvalue) with positive real part, we conclude that it is an unstable stationary point.