Chapter 1

Example problem: 2D driven cavity flow in a quarter-circle domain with spatial adaptation.

In this example we shall demonstrate

- how easy it is to adapt the code for the solution of the driven cavity problem in a square domain, discussed in a previous example, to a different domain shape,
- · how to apply body forces (e.g. gravity) in a Navier-Stokes problem,
- how to switch between the stress-divergence and the simplified forms of the incompressible Navier-Stokes equations.

1.1 The example problem

In this example we shall illustrate the solution of the steady 2D Navier-Stokes equations in a modified driven cavity problem: The fluid is contained in a quarter-circle domain and is subject to gravity which acts in the vertical direction. We solve the problem in two different formulations, using the stress-divergence and the simplified form of the Navier-Stokes equations, respectively, and by applying the gravitational body force via the gravity vector, \mathbf{G} , and via the body force function, \mathbf{B} , respectively.

Problem 1:

The 2D driven cavity problem in a quarter circle domain with gravity, using the stress-divergence form of the Navier-Stokes equations

Solve

$$Re \ u_j \frac{\partial u_i}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{Re}{Fr} G_i + \frac{\partial}{\partial x_j} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right), \tag{1}$$

and

$$\frac{\partial u_i}{\partial x_i} = 0,$$

in the quarter-circle domain $D=\{x_1\geq 0,\,x_2\geq 0 \text{ and } x_1^2+x_2^2\leq 1\}$, subject to the Dirichlet boundary conditions

$$\mathbf{u}|_{\partial D} = (0,0), \tag{2}$$

on the curved and left boundaries; and

$$\mathbf{u}|_{\partial D} = (1,0), \tag{3}$$

on the bottom boundary, $x_2 = 0$. Gravity acts vertically downwards so that $(G_1, G_2) = (0, -1)$.

When discussing the implementation of the Navier-Stokes equations in an $earlier\ example$, we mentioned that oomph-lib allows the incompressible Navier-Stokes equations to be solved in the simplified, rather than the (default) stress-divergence form. We will demonstrate the use of this feature by solving the following problem:

Problem 2:

The 2D driven cavity problem in a quarter circle domain with gravity, using the simplified form of the Navier-Stokes equations

Solve

$$Re \ u_j \frac{\partial u_i}{\partial x_j} = -\frac{\partial p}{\partial x_i} + B_i + \frac{\partial^2 u_i}{\partial x_j^2}, \tag{1}$$

and

$$\frac{\partial u_i}{\partial x_i} = 0,$$

in the quarter-circle domain $D=\{x_1\geq 0,\, x_2\geq 0 \text{ and } x_1^2+x_2^2\leq 1\}$, subject to the Dirichlet boundary conditions

$$\mathbf{u}|_{\partial D} = (0,0), \tag{2}$$

on the curved and left boundaries; and

$$\mathbf{u}|_{\partial D} = (1,0), \tag{3}$$

on the bottom boundary, $x_2 = 0$. To make this consistent with Problem 1, we define the body force function as $(B_1, B_2) = (0, -Re/Fr)$.

Note that in Problem 2, the gravitational body force is represented by the body force rather than the gravity vector.

1.1.1 Switching between the stress-divergence and the simplified forms of the Navier-Stokes equations

The two forms of the Navier-Stokes equations differ in the implementation of the viscous terms, which may be represented as

$$\frac{\partial^2 u_i}{\partial x_j^2}$$
 or $\frac{\partial}{\partial x_j} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$.

For an incompressible flow, $\partial u_i/\partial x_i=0$, both forms are mathematically equivalent but the stress-divergence form is required for problems with free surfaces , or for problems in which traction boundary conditions are to be applied.

In order to be able do deal with both cases, oomph-lib's Navier-Stokes elements actually implement the viscous term as

$$\frac{\partial}{\partial x_j} \left(\frac{\partial u_i}{\partial x_j} + \Gamma_i \, \frac{\partial u_j}{\partial x_i} \right).$$

By default the components of the vector Γ_i , are set to 1.0, so that the stress-divergence form is used. The components Γ_i are stored in the static data member

static Vector<double> NavierStokesEquations<DIM>::Gamma

of the NavierStokesEquations<DIM> class which forms the basis for all Navier-Stokes elements in oomph-lib. Its entries are initialised to 1.0. The user may over-write these assignments and thus re-define the values of Γ being used for a specific problem. [In principle, it is possible to use stress-divergence form for the first component of the momentum equations, and the simplified form for the second one, say. However, we do not believe that this is a particularly useful/desirable option and have certainly never used such (slightly bizarre) assignments in any of our own computations.]

1.1.2 Solution to problem 1

The figure below shows "carpet plots" of the velocity and pressure fields as well as a contour plot of the pressure distribution with superimposed streamlines for Problem 1 at a Reynolds number of Re=100 and a ratio of Reynolds and Froude numbers (a measure of gravity on the viscous scale) of Re/Fr=100. The velocity vanishes along the entire domain boundary, apart from the bottom boundary ($x_2=0$) where the moving "lid" imposes a unit tangential velocity which drives a large vortex, centred at $(x_1,x_2)\approx (0.59,0.22)$. The pressure singularities created by the velocity discontinuities at $(x_1,x_2)=(0,0)$ and $(x_1,x_2)=(1,0)$ are well resolved. The pressure plot shows that away from the singularities, the pressure decreases linearly with x_2 , reflecting the effect of the gravitational body forces which acts in the negative x_2- direction.

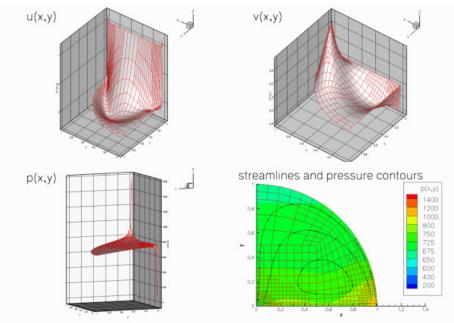


Figure 1.1 Plot of the velocity and pressure fields for problem 1 with Re=100 and Re/Fr=100, computed with adaptive Taylor-Hood elements.

1.1.3 Solution to problem 2

The next figure shows the computational results for Problem 2, obtained from a computation with adaptive Crouzeix-Raviart elements.

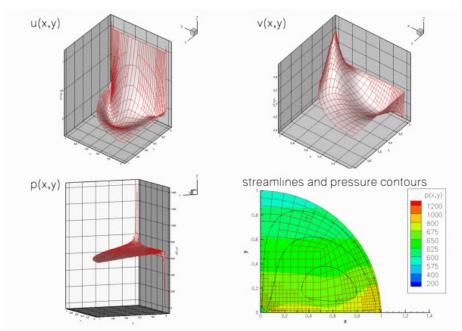


Figure 1.2 Plot of the velocity and pressure fields for problem 2 with Re=100 and Re/Fr=100, computed with adaptive Crouzeix-Raviart elements.

1.2 The code

We use a namespace Global_Physical_Variables to define the various parameters: The Reynolds number.

the gravity vector \mathbf{G} , and the ratio of Reynolds and Froude number, Re/Fr, which represents the ratio of gravitational and viscous forces,

```
/// Reynolds/Froude number
double Re_invFr=100;
/// Gravity vector
Vector<double> Gravity(2);
```

In Problem 2, gravity is introduced via the body force function ${\bf B}$ which we define such that Problems 1 and 2 are equivalent. (We use the gravity vector ${\bf G}=(0,-1)$ to specify the direction of gravity, while indicating it magnitude by Re/Fr.)

Finally we define a body force function, which returns zero values, for use when solving Problem 1.

1.3 The driver code 5

```
} // end of namespace
```

1.3 The driver code

First we create a <code>DocInfo</code> object to control the output, and set the maximum number of spatial adaptations to three

To solve problem 1 we define the direction of gravity, $\mathbf{G}=(0,-1)$, and set the entries in the NavierStokes \leftarrow Equations<2>::Gamma vector to (1,1), so that the stress-divergence form of the equation is used [In fact, this step is not strictly necessary as it simply re-assigns the default values.]

```
// Solve problem 1 with Taylor-Hood elements
//------
{
   // Set up downwards-Gravity vector
   Global_Physical_Variables::Gravity[0] = 0.0;
   Global_Physical_Variables::Gravity[1] = -1.0;

// Set up Gamma vector for stress-divergence form
NavierStokesEquations<2>::Gamma[0]=1;
NavierStokesEquations<2>::Gamma[1]=1;
```

Next we build problem 1 using Taylor-Hood elements and passing a function pointer to the zero_body_← force(...) function (defined in the namespace Global_Physical_Variables) as the argument.

```
// Build problem with Gravity vector in stress divergence form,
// using zero body force function
QuarterCircleDrivenCavityProblem<RefineableQTaylorHoodElement<2> >
problem(&Global_Physical_Variables::zero_body_force);
```

Now problem 1 can be solved as in the previous example.

```
// Solve the problem with automatic adaptation
problem.newton_solve(max_adapt);

// Step number
doc_info.number() = 0;

// Output solution
problem.doc_solution(doc_info);
```

To solve problem 2 we set the entries in the <code>NavierStokesEquations<2>::Gamma vector to zero</code> (thus choosing the simplified version of the <code>Navier-Stokes equations</code>), define $\mathbf{G}=(0,0)$, and pass a function pointer to the <code>body_force(...)</code> function to the problem constructor.

```
// Solve the problem with automatic adaptation
problem.newton_solve(max_adapt);
// Step number
```

```
doc_info.number()=1;

// Output solution
problem.doc_solution(doc_info);
} // end of problem 2
```

1.4 The problem class

The problem class is very similar to that used in the previous example, with two exceptions:

- ullet We pass a function pointer to the body force function ${f B}$ to the constructor and
- store the function pointer to the body force function in the problem's private member data.

```
/// Driven cavity problem in quarter circle domain, templated
/// by element type.
template<class ELEMENT>
class QuarterCircleDrivenCavityProblem : public Problem
public:
 /// Constructor
 QuarterCircleDrivenCavityProblem(
 NavierStokesEquations<2>::NavierStokesBodyForceFctPt body_force_fct_pt);
 /// Destructor: Empty
 ~QuarterCircleDrivenCavityProblem() {}
 /// Update the after solve (empty)
 void actions_after_newton_solve() {}
 /// Update the problem specs before solve.
 /// (Re-)set velocity boundary conditions just to be on the safe side...
 void actions_before_newton_solve()
  // Setup tangential flow along boundary 0:
  unsigned ibound=0;
  unsigned num_nod= mesh_pt()->nboundary_node(ibound);
  for (unsigned inod=0;inod<num_nod;inod++)</pre>
    // Tangential flow
    unsigned i=0;
    mesh_pt()->boundary_node_pt(ibound,inod)->set_value(i,1.0);
    // No penetration
    i=1;
   mesh_pt()->boundary_node_pt(ibound,inod)->set_value(i,0.0);
  \ensuremath{//} Overwrite with no flow along all other boundaries
  unsigned num_bound = mesh_pt()->nboundary();
  for(unsigned ibound=1;ibound<num_bound;ibound++)</pre>
    unsigned num_nod= mesh_pt()->nboundary_node(ibound);
    for (unsigned inod=0;inod<num_nod;inod++)</pre>
      for (unsigned i=0;i<2;i++)</pre>
        mesh_pt()->boundary_node_pt(ibound,inod)->set_value(i,0.0);
       }
     }
  } // end_of_actions_before_newton_solve
 /// After adaptation: Unpin pressure and pin redudant pressure dofs.
 void actions_after_adapt()
  {
// Unpin all pressure dofs
   RefineableNavierStokesEquations<2>::
   unpin_all_pressure_dofs(mesh_pt()->element_pt());
   // Pin redundant pressure dofs
   RefineableNavierStokesEquations<2>::
   pin_redundant_nodal_pressures(mesh_pt()->element_pt());
   // Now pin the first pressure dof in the first element and set it to 0.0
   fix_pressure(0,0,0.0);
  } // end_of_actions_after_adapt
```

1.5 The problem constructor

We store the function pointer to the body force function in the private data member Body_force_fct_pt.

As usual the first task is to create the mesh. We now use the RefineableQuarterCircleSectorMesh< \leftarrow ELEMENT>, which requires the creation of a GeomObject to describe geometry of the curved wall: We choose an ellipse with unit half axes (i.e. a unit circle).

```
// Build geometric object that parametrises the curved boundary
// of the domain

// Half axes for ellipse
double a_ellipse=1.0;
double b_ellipse=1.0;

// Setup elliptical ring
GeomObject* Wall_pt=new Ellipse(a_ellipse,b_ellipse);

// End points for wall
double xi_lo=0.0;
double xi_hi=2.0*atan(1.0);

//Now create the mesh
double fract_mid=0.5;
Problem::mesh_pt() = new
RefineableQuarterCircleSectorMesh<ELEMENT>(
Wall_pt,xi_lo,fract_mid,xi_hi);
```

Next the error estimator is set, the boundary nodes are pinned and the Reynolds number is assigned, as before

```
// Set error estimator
Z2ErrorEstimator* error_estimator_pt=new Z2ErrorEstimator;
dynamic_cast<RefineableQuarterCircleSectorMesh<ELEMENT>*>(
mesh_pt())->spatial_error_estimator_pt()=error_estimator_pt;
// Set the boundary conditions for this problem: All nodes are
// free by default -- just pin the ones that have Dirichlet conditions
// here: All boundaries are Dirichlet boundaries.
unsigned num_bound = mesh_pt()->nboundary();
for(unsigned ibound=0;ibound<num_bound;ibound++)</pre>
  unsigned num_nod= mesh_pt()->nboundary_node(ibound);
  for (unsigned inod=0;inod<num_nod;inod++)</pre>
     // Loop over values (u and v velocities)
    for (unsigned i=0;i<2;i++)</pre>
       mesh_pt()->boundary_node_pt(ibound,inod)->pin(i);
 } // end loop over boundaries
//Find number of elements in mesh
unsigned n_element = mesh_pt()->nelement();
// Loop over the elements to set up element-specific
// things that cannot be handled by constructor: Pass pointer to Reynolds
// number
```

```
for (unsigned e=0;e<n_element;e++)
{
    // Upcast from GeneralisedElement to the present element
    ELEMENT* el_pt = dynamic_cast<ELEMENT*>(mesh_pt()->element_pt(e));

    //Set the Reynolds number, etc
    el_pt->re_pt() = &Global_Physical_Variables::Re;

Within this loop we also pass the pointers to Re/Fr, the gravity vector and the body-force function to the elements.
    //Set the Re/Fr
    el_pt->re_invfr_pt() = &Global_Physical_Variables::Re_invFr;
    //Set Gravity vector
    el_pt->g_pt() = &Global_Physical_Variables::Gravity;
```

The RefineableQuarterCircleSectorMesh<ELEMENT> contains only three elements and therefore provides a very coarse discretisation of the domain. We refine the mesh uniformly twice before pinning the redundant pressure degrees of freedom, pinning a single pressure degree of freedom, and assigning the equation

```
numbers, as before.
// Initial refinement level
refine_uniformly();
refine_uniformly();

// Pin redudant pressure dofs
RefineableNavierStokesEquations<2>::
pin_redundant_nodal_pressures(mesh_pt()->element_pt());
// Now pin the first pressure dof in the first element and set it to 0.0
fix_pressure(0,0,0.0);
// Setup equation numbering scheme
cout «"Number of equations: " « assign_eqn_numbers() « std::endl;
} // end of constructor
```

1.6 Post processing

-start_of_doc_solution==

// Output solution

some_file.close();
} // end_of_doc_solution

some_file.open(filename);

//set body force function

} // end loop over elements

el_pt->body_force_fct_pt() = Body_force_fct_pt;

sprintf(filename, "%s/soln%i.dat", doc_info.directory().c_str(),

The post processing function remains the same as in the previous examples .

1.7 Comments and Exercises

doc_info.number());

mesh_pt()->output(some_file,npts);

1. Try making the curved boundary the driving wall [Hint: this requires a change in the wall velocities prescribed in Problem::actions_before_newton_solve(). The figure below shows what you should expect.]

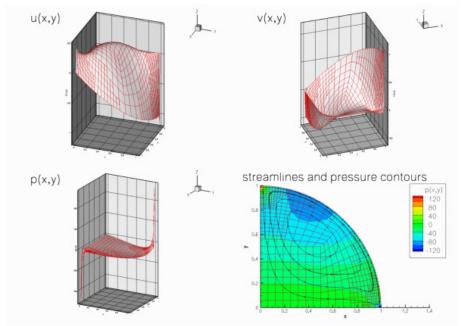


Figure 1.3 Plot of the velocity and pressure distribution for a circular driven cavity in which the flow is driven by the tangential motion of the curvilinear boundary.

1.8 Source files for this tutorial

• The source files for this tutorial are located in the directory:

demo_drivers/navier_stokes/circular_driven_cavity/

• The driver code is:

 $\label{lem:cavity} {\tt demo_drivers/navier_stokes/circular_driven_cavity/circular_driven_} \leftarrow {\tt cavity.cc}$

1.9 PDF file

A pdf version of this document is available.