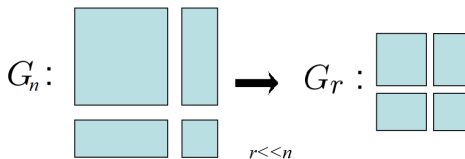


Model Order Reduction For Electrical Circuits

With Focus On Balanced Model Reduction

Shakir Sofi, Razan Debo

Skoltech



1 Problem Statement

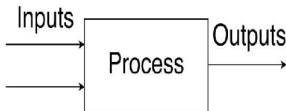
2 Methods

3 Balanced Truncation

4 Results

5 Conclusion

Model order reduction (MOR) is the branch of applied maths, and system theory, in which we study the properties of dynamical systems (i.g; any system) in application for reducing the dimensionality, complexity, while preserving the (to the maximum possible extent) input-output (i.g, cause-effect) behavior



Goals

Replicate input-output behavior of large-scale system by smaller system subject to:

- Good approximation (mimic original system as best as possible)
- Preserve system properties, like stability, passivity, etc.
- Small approximation error and/or global error bound.
- Numerically stable and efficient procedures.

- Reduce computational costs (Overcoming curse of dimensionality)
- Requires less storage
- Fast simulations (we can simulate very large systems in little amount of time)
- Reduced models enable rapid prediction, inversion, design, and uncertainty quantification.
- Extracting the essence of complex problems to make them faster and easier to solve.



- Error should be very small.
- Reduced systems dynamics should converge to dynamics of original system.
- MOR algorithm should preserve system properties like, stability, passivity, etc.

Full model in general: $G : \begin{cases} \dot{x}(t) = f(x(t), u(t)), & x(t) \in \mathbb{R}^n, u \in \mathcal{U} \\ y(t) = g(x(t), u(t)) \end{cases}$

Reduced order model: $G_r : \begin{cases} \dot{z}(t) = f_r(z(t), u(t)), & z(t) \in \mathbb{R}^r, u \in \mathcal{U} \quad r \ll n \\ y_r(t) = g_r(z(t), u(t)) \end{cases}$

Such that $\|y - y_r\|_2 \leq \text{bound}(r) \cdot \|u\|, \quad \forall u \in \mathcal{U}$

Full order system:

$$\Sigma : \begin{cases} \dot{\mathbf{x}} = \mathbf{Ax} + \mathbf{Bu}, & \mathbf{x} \in \mathbb{R}^n \\ \mathbf{y} = \mathbf{Cx} + \mathbf{Du} \end{cases}$$

Reduced order system:

$$\Sigma_r : \begin{cases} \dot{\tilde{\mathbf{x}}} = \mathbf{A}_r \tilde{\mathbf{x}} + \mathbf{B}_r \mathbf{u}, & \mathbf{z} \in \mathbb{R}^r, \quad r \ll n \\ \mathbf{y}_r = \mathbf{C}_r \tilde{\mathbf{x}} + \mathbf{D}_r \mathbf{u} \end{cases}$$

where $\dot{\mathbf{x}}$ is $\frac{d\mathbf{x}}{dt}$, $\dot{\tilde{\mathbf{x}}}$ is $\frac{d\tilde{\mathbf{x}}}{dt}$, \mathbf{x} being full state vector and $\tilde{\mathbf{x}}$ is reduced state vector $\mathbf{A}, \mathbf{B}, \mathbf{C}, \mathbf{D}$ are full system matrices and $\mathbf{A}_r, \mathbf{B}_r, \mathbf{C}_r, \mathbf{D}_r$ are matrices of reduced system, \mathbf{u} is input vector and \mathbf{y} the output vector.

Three broad categories of MOR Methods:

- (a) SVD-based methods
- (b) Krylov-based methods
- (c) Combined SVD and Krylov methods

Table 1. Overview of approximation methods.

Approximation methods for dynamical systems		
SVD		Krylov
Nonlinear Systems	Linear Systems	
<ul style="list-style-type: none"> • POD methods • Empirical grammians 	<div> <ul style="list-style-type: none"> • Balanced truncation • Hankel approximation <p>OUR FOCUS HERE</p> </div>	<ul style="list-style-type: none"> • Realization • Interpolation • Lanczos • Arnoldi
SVD-Krylov		

- *SVD-based approximation methods* have their roots in the Singular Value Decomposition and the resulting solution of the approximation of matrices by means of matrices of lower rank, which are optimal in the 2-norm (or more generally, in unitarily invariant norms)
- *Krylov-subspace based approximation methods* have roots in Moment Matching (of Impulse responses/ transfer function) i.e, $\mathbf{H}(\mathbf{s})$ of the considered system. For LTI systems $\mathbf{H}(\mathbf{s}) = \mathbf{C}(\mathbf{s}\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}$ then approximates this transfer function by $\hat{\mathbf{H}}(\mathbf{s})$ by using Krylov-subspace.

For details refer to : Approximation of Large-Scale Dynamical Systems, SIAM, Athanasios C. Antoulas,
<https://doi.org/10.1137/1.9780898718713>

Controllability and Observability :

A system is said to be **controllable** at time t_o if it is possible by means of an unconstrained control/input vector to transfer the system from any initial state $\mathbf{x}(t_o)$ to any other state in a finite interval of time.

A system is said to be **observable** at time t_o if, with the system in state $\mathbf{x}(t_o)$, it is possible to determine this state from the observation of the output over a finite time interval.

Controllable LTI system if :

The $n \times n$

$$\mathbf{W}_c(t) = \int_0^t e^{\mathbf{A}\tau} \mathbf{B} \mathbf{B}^* e^{\mathbf{A}^* \tau} d\tau, \quad \text{is not singular for any } t \geq 0$$

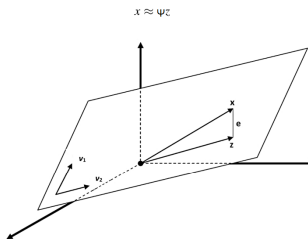
Observable LTI system if :

The $n \times n$

$$\mathbf{W}_o(t) = \int_0^t e^{\mathbf{A}^* \tau} \mathbf{C}^* \mathbf{C} e^{\mathbf{A} \tau} d\tau, \quad \text{is not singular for any } t \geq 0$$

They are the solutions of **Lyapunov equations** for LTI system defined above

- Fact is, large scale dynamical systems are poorly controllable and observable, that means the cancelation of some variables is possible.
- Important dynamics of underlying system is often restricted to a smaller subspace.
- MOR methods are designed to find the dominant subspaces, so we Project the original system onto it.



These MOR methods will give different strategies to find matrix Ψ

Can only singular values or eigen value decide the truncation? lets us check the example, consider the following simplified model:

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 10^{-10} \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 10^{-10} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

So, the choice the state $z = x_2$, is intuitive (as it is more lightly damped) but this is bad. But choice $z = x_1$ is better, since it is better controlable and observable.

So, we cannot decide simply by looking at matrix A , we must take account of matrix B and C .

Hint: What if we balance the controllability and observability Gramians of a state(aka *Balancing*) then simply truncate the system at r .

Let $\mathbf{x} = \mathbf{T}\mathbf{z}$, such that this transformation that makes the controllability and observability Gramians equal and diagonal:

$$\hat{\mathbf{W}}_c = \hat{\mathbf{W}}_o = \Sigma$$

The transformed (in z coordinates) product of Gramian's will be given by:

$$\hat{\mathbf{W}}_c \hat{\mathbf{W}}_o = \mathbf{T}^{-1} \mathbf{W}_c \mathbf{W}_o \mathbf{T}$$

Plugging in the desired $\hat{\mathbf{W}}_c = \hat{\mathbf{W}}_o = \Sigma$ yields

$$\mathbf{T}^{-1} \mathbf{W}_c \mathbf{W}_o \mathbf{T} = \Sigma^2 \implies \mathbf{W}_c \mathbf{W}_o \mathbf{T} = \mathbf{T} \Sigma^2 \quad (\text{spectral decomposition})$$

But, there can be many such transformation that makes $\hat{\mathbf{W}}_c \hat{\mathbf{W}}_o = \Sigma^2$, so we need to scale them, let \mathbf{T}_u have unscaled eigenvectors, and the scaled version \mathbf{T} have unit normed columns

$$\begin{aligned} \mathbf{T}_u^{-1} \mathbf{W}_c \mathbf{T}_u^{-*} &= \Sigma_c \\ \mathbf{T}_u^* \mathbf{W}_o \mathbf{T}_u &= \Sigma_o \end{aligned}$$

The scaling that exactly balances these Gramians is then given by $\Sigma_s = \Sigma_c^{1/4} \Sigma_o^{-1/4}$ the exact balancing transformation is given by $\mathbf{T} = \mathbf{T}_u \Sigma_s$

Given the new coordinates $\mathbf{z} = \mathbf{T}^{-1}\mathbf{x} \in \mathbb{R}^n$, it is possible to define a reduced-order state

$$\tilde{\mathbf{x}} \in \mathbb{R}^r, \text{ as } \mathbf{z} = \begin{bmatrix} z_1 \\ \vdots \\ z_r \\ z_{r+1} \\ \vdots \\ z_n \end{bmatrix}, \quad \tilde{\mathbf{x}}$$

in terms of the first r most controllable and observable directions. If we partition the balancing transformation \mathbf{T} and inverse transformation $\mathbf{S} = \mathbf{T}^{-1}$ into the first r modes to be retained and the last $n - r$ modes to be truncated,

$$\mathbf{T} = \begin{bmatrix} \Psi & \mathbf{T}_t \end{bmatrix}, \quad \mathbf{S} = \begin{bmatrix} \Phi^* \\ \mathbf{S}_t \end{bmatrix}$$

Then it is possible to rewrite the transformed dynamics in transformed system as:

$$\frac{d}{dt} \begin{bmatrix} \tilde{\mathbf{x}} \\ \mathbf{z}_t \end{bmatrix} = \begin{bmatrix} \Phi^* \mathbf{A} \Psi & \Phi^* \mathbf{A} \mathbf{T}_t \\ \mathbf{S}_t \mathbf{A} \Psi & \mathbf{S}_t \mathbf{A} \mathbf{T}_t \end{bmatrix} \begin{bmatrix} \tilde{\mathbf{x}} \\ \mathbf{z}_t \end{bmatrix} + \begin{bmatrix} \Phi^* \mathbf{B} \\ \mathbf{S}_t \mathbf{B} \end{bmatrix} \mathbf{u}$$

$$\mathbf{y} = \begin{bmatrix} \mathbf{C} \Psi & \mathbf{C} \mathbf{T}_t \end{bmatrix} \begin{bmatrix} \tilde{\mathbf{x}} \\ \mathbf{z}_t \end{bmatrix} + \mathbf{D} \mathbf{u}.$$

In balanced truncation, the state \mathbf{z}_t is simply truncated (i.e., discarded and set equal to zero), and only the $\tilde{\mathbf{x}}$ equations remain:

$$\frac{d}{dt} \tilde{\mathbf{x}} = \Phi^* \mathbf{A} \Psi \tilde{\mathbf{x}} + \Phi^* \mathbf{B} \mathbf{u}$$

Computational cost is reduced from $\mathbf{O}(n^3)$ to $\mathbf{O}(n.r^2)$

$$\mathbf{y} = \mathbf{C} \Psi \tilde{\mathbf{x}} + \mathbf{D} \mathbf{u}$$

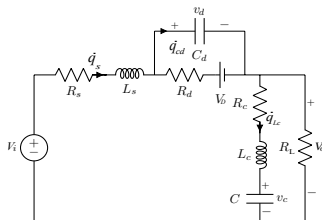
The upper and lower bounds on the error of a given order truncation:

$$\text{Upper bound: } \|\mathbf{G} - \mathbf{G}_r\|_{\infty} \leq 2 \sum_{j=r+1}^n \sigma_j$$

$$\text{Lower bound: } \|\mathbf{G} - \mathbf{G}_r\|_{\infty} > \sigma_{r+1}$$

where σ_j is the j th diagonal entry of the balanced Gramians.

Let us consider a circuit as shown below



Using Euler-Lagrangian equations to model this circuit, that is:

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}(z, \dot{z}, t)}{\partial \dot{z}} \right) = \frac{\partial \mathcal{L}(z, \dot{z}, t)}{\partial z} - \frac{\partial \mathcal{D}(\dot{z})}{\partial \dot{z}}$$

$$\mathcal{L}(z, \dot{z}, t) = \mathcal{T}(z, \dot{z}, t) - \mathcal{V}(z, \dot{z}, t)$$

Lagrangian (\mathcal{L}) is the difference between the kinetic energy (\mathcal{T}) and potential energy (\mathcal{V}) of the system. Rayleigh dissipation (\mathcal{D}) = $\frac{1}{2}$ power dissipation.

$$\mathcal{T} = \frac{1}{2}L_s\dot{q}_s^2 + \frac{1}{2}L_c\dot{q}_{Lc}^2$$

$$\mathcal{V} = \frac{1}{2C_d}q_{cd}^2 + \frac{1}{2C}q_{Lc}^2 - V_i \times q_s + V_D(q_s - q_{cd})$$

$$\mathcal{L} = \frac{1}{2}L_s\dot{q}_s^2 + \frac{1}{2}L_c\dot{q}_{Lc}^2 - \frac{1}{2C_d}q_{cd}^2 - \frac{1}{2C}q_{Lc}^2 \\ + V_i \times q_s - V_D(q_s - q_{cd})$$

$$\mathcal{D} = \frac{1}{2}R_s(\dot{q}_s)^2 + \frac{1}{2}R_c(\dot{q}_{Lc})^2 + \frac{1}{2}R_d(\dot{q}_s - \dot{q}_{cd})^2 \\ + \frac{1}{2}R_L(\dot{q}_s - \dot{q}_{Lc})^2$$

Putting these equations in Euler-lagrangian equations, and let:

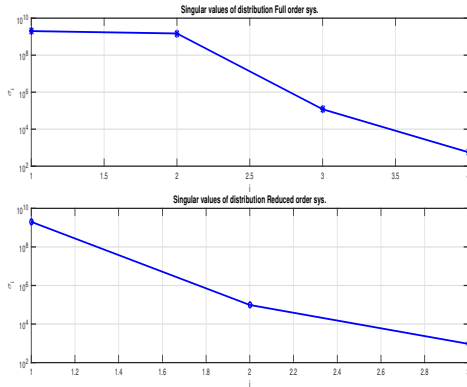
$$\mathbf{x} = (i, v_d, i_{Lc}, v_c)^T = \left(\dot{q}_s, \frac{q_{cd}}{C_d}, \dot{q}_{Lc}, \frac{q_{Lc}}{C} \right)^T$$

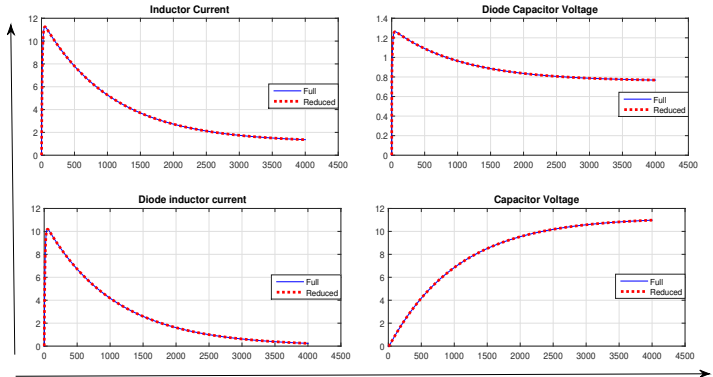
The final state-space LTI model is

$$\mathbf{A} = \begin{bmatrix} \frac{(-R_s - R_L)}{L_s} & \frac{-1}{L_s} & \frac{R_c}{L_s} & 0 \\ \frac{1}{C_d} & \frac{1}{R_d C_d} & 0 & 0 \\ \frac{R_L}{L_c} & 0 & \frac{(-R_L - R_c)}{L_c} & \frac{-1}{L_c} \\ 0 & 0 & \frac{1}{C} & 0 \end{bmatrix}; \mathbf{x} = \begin{bmatrix} i \\ v_d \\ i_{Lc} \\ v_c \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} \frac{1}{L_s} & 0 \\ 0 & \frac{1}{R_d C_d} \\ 0 & 0 \\ 0 & 0 \end{bmatrix}; u = \begin{bmatrix} V_i \\ V_D \end{bmatrix}; \mathbf{C} = [I]_{4 \times 4}; \mathbf{D} = [0]_{4 \times 2}$$

With the parameters $R_s = 0.01\Omega$, $C = 1e^{-3}F$, $L_c = 10e^{-6}H$, $R_L = 10\Omega$; $L_s = 10e^{-6}H$, $R_d = 0.05\Omega$, $C_d = 10e^{-9}F$, $R_c = 1\Omega$, $R_L = 10\Omega$, $L_c = 10e^{-9}H$
 After doing the *Balanced Model Truncation* this system reduced to third order ($r = 3$). The singular value of full and reduced order is shown below





And for Full order system simulation took **4.47165 sec**, while Reduced order took only **3.931263 sec**

Norm Error of approximation is: $\|y - y_r\|_2 \approx 0.067$ (..seems good..)

- MOR for stiff electrical systems suits best to achieve computationally efficient simulation and perform analysis.
- MOR for electrical circuits allow us to design accurate controllers as most of them are based on average behaviour of underlying system.
- Further directions are to use MOR for Non linear electrical circuits, also to reduce circuitry in MEMS systems.
- And many more...

Nowdays, we are sucessfully applying MOR for switched-electrical systems, in which the dynamics are completely dependent on the switches in the electrical systems like; switched power electronic converters, etc,

- APPROXIMATION OF LARGE-SCALE DYNAMICAL SYSTEMS: AN OVERVIEW, Athanasios C. ANTOULAS, Dan C. SORENSEN
- Model Reduction for Circuit Simulation, Peter Benner Michael Hinze.
- Numerical Linear Algebra and Applications, Biswa Nath Datta
- Model Reduction Based on Spectral Projection Methods, Peter Benner and Enrique S. Quintana-Ort
- Model Order Reduction in Power Electronics: Issues and Perspectives, S.A Nahvi, Mohammad Abid Bazaz, Hadhiq Khan
- Model Reduction and Approximation Theory and Algorithms, PETER BENNER, KAREN WILLCOX
- MORLAB-Model Order Reduction LABoratory, Max-Planck Institute
- Organization of the SLICOT Library, Benchmarks and examples Model Reduction.

Thank You