

Vv255 Lecture 28

Dr Jing Liu

UM-SJTU Joint Institute

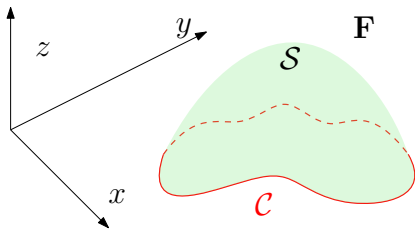
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1. A line integral of \mathbf{F} in \mathbb{R}^2 over a closed **plane** curve \mathcal{C} to an integral of a scalar component of $\text{curl } \mathbf{F}$ over the **region** that is enclosed by \mathcal{C} .

$$\oint_{\mathcal{C}} \mathbf{F} \cdot \mathbf{T} \, ds = \iint_{\mathcal{D}} \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA = \iint_{\mathcal{D}} (\text{curl } \mathbf{F}) \cdot \mathbf{e}_z \, dA$$

- Our next goal is to generalize this result to \mathbb{R}^3 , that is, to relate
- 1. A line integral of \mathbf{F} in \mathbb{R}^3 over a closed **space** curve \mathcal{C} to an integral of a scalar component of $\text{curl } \mathbf{F}$ over the **surface** \mathcal{S} enclosed by \mathcal{C} .

$$\oint_{\mathcal{C}} \mathbf{F} \cdot \mathbf{T} \, ds = \iint_{\mathcal{S}} (\text{curl } \mathbf{F}) \cdot \mathbf{n} \, dS$$

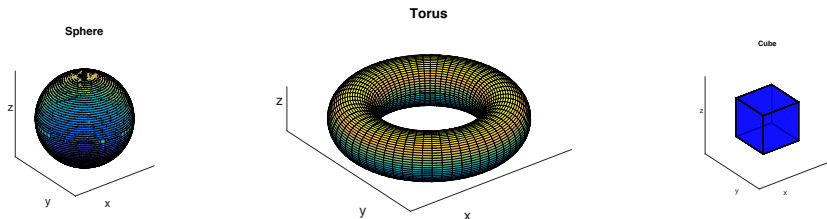


- The surface \mathcal{S} is enclosed by \mathcal{C} in the sense that \mathcal{C} is the only boundary of \mathcal{S} .

2. A line integral of the normal component of \mathbf{F} in \mathbb{R}^2 over a **closed curve** \mathcal{C} to a **double** integral of $\operatorname{div} \mathbf{F}$ over the region that is enclosed by \mathcal{C} .

$$\oint_{\mathcal{C}} \mathbf{F} \cdot \mathbf{n} \, ds = \iint_{\mathcal{D}} \left(\frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} \right) dA = \iint_{\mathcal{D}} \operatorname{div} \mathbf{F} \, dA$$

- We wish to generalize this result as well to \mathbb{R}^3 , that is, to relate
- 2. An integral of the normal component of \mathbf{F} in \mathbb{R}^3 over a **closed surface** \mathcal{S} to a **triple** integral of $\operatorname{div} \mathbf{F}$ over the solid \mathcal{E} that is enclosed by \mathcal{S} .

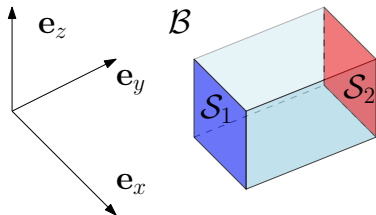
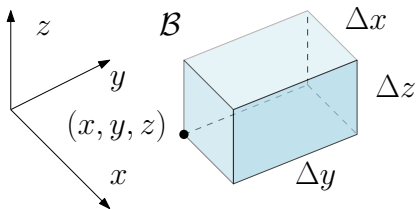


- The solid or the region \mathcal{E} in \mathbb{R}^3 is enclosed by the closed surface \mathcal{S} in the sense that \mathcal{S} has no curve boundary.

- Recall for a **sufficiently smooth** velocity field of a type of fluid,

$$\mathbf{V}(x, y, z) = v_x(x, y, z)\mathbf{e}_x + v_y(x, y, z)\mathbf{e}_y + v_z(x, y, z)\mathbf{e}_z$$

we consider the flux of \mathbf{V} out of a tiny box in the xyz -coordinate system,



- Consider the flux out of such a similar box in terms of **surface integrals**,

$$\mathcal{B}: \quad a \leq x \leq b, \quad c \leq y \leq d, \quad e \leq z \leq f$$

- For \mathcal{S}_1 and \mathcal{S}_2 , both oriented outward, the net flux across \mathcal{S}_1 and \mathcal{S}_2

$$\iint_{\mathcal{S}_1} \mathbf{V} \cdot d\mathbf{S} + \iint_{\mathcal{S}_2} \mathbf{V} \cdot d\mathbf{S} = \iint_{\mathcal{D}_1} \mathbf{V} \cdot (-\mathbf{e}_y) dA + \iint_{\mathcal{D}_2} \mathbf{V} \cdot \mathbf{e}_y dA$$

Q: What is the region \mathcal{D}_1 and \mathcal{D}_2 ?

- The region \mathcal{D}_1 and \mathcal{D}_2 are the same by construction,

$$\mathcal{D}_1 = \mathcal{D}_2: \quad a \leq x \leq b, \quad e \leq z \leq f$$

- If we simply use x and y to be the variable of integrations,

$$\begin{aligned} \iint_{S_1} \mathbf{V} \cdot d\mathbf{S} + \iint_{S_2} \mathbf{V} \cdot d\mathbf{S} &= \iint_{\mathcal{D}_1} \mathbf{V} \cdot (-\mathbf{e}_y) dA + \iint_{\mathcal{D}_2} \mathbf{V} \cdot \mathbf{e}_y dA \\ &= \int_e^f \int_a^b -v_y(x, c, z) dx dz + \int_e^f \int_a^b v_y(x, d, z) dx dz \\ &= \int_e^f \int_a^b \left(v_y(x, d, z) - v_y(x, c, z) \right) dx dz \end{aligned}$$

- By the fundamental theorem of Calculus,

$$v_y(x, d, z) - v_y(x, c, z) = \int_c^d \frac{\partial v_y}{\partial y} dy$$

- Making the substitution, and converting the iterated integral to a triple

$$\begin{aligned}
 v_y(x, d, z) - v_y(x, c, z) &= \int_c^d \frac{\partial v_y}{\partial y} dy \\
 \implies \iint_{S_1} \mathbf{V} \cdot d\mathbf{S} + \iint_{S_2} \mathbf{V} \cdot d\mathbf{S} &= \int_e^f \int_a^b \left(v_y(x, d, z) - v_y(x, c, z) \right) dx dz \\
 &= \int_e^f \int_c^d \int_a^b \frac{\partial v_y}{\partial y} dx dy dz \\
 &= \iiint_B \frac{\partial v_y}{\partial y} dV
 \end{aligned}$$

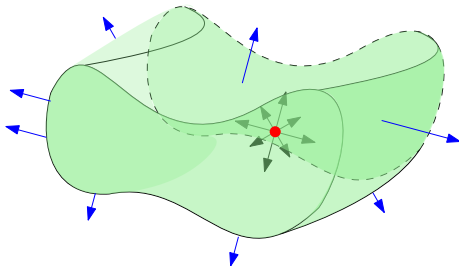
- Similarly, we can obtain the flux across the remaining four faces

$$\begin{aligned}
 \iint_{S_3} \mathbf{V} \cdot d\mathbf{S} + \iint_{S_4} \mathbf{V} \cdot d\mathbf{S} &= \iiint_B \frac{\partial v_x}{\partial x} dV \\
 \iint_{S_5} \mathbf{V} \cdot d\mathbf{S} + \iint_{S_6} \mathbf{V} \cdot d\mathbf{S} &= \iiint_B \frac{\partial v_z}{\partial z} dV
 \end{aligned}$$

- Hence the net **outward** flux across the surface \mathcal{S} of the box \mathcal{B} is given by

$$\iint_{\mathcal{S}} \mathbf{V} \cdot d\mathbf{S} = \iiint_{\mathcal{B}} \left(\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} \right) dV = \iiint_{\mathcal{B}} \operatorname{div} \mathbf{V} dV$$

- This result is also true for any sufficiently smooth vector field \mathbf{F} acting on any region \mathcal{E} enclosed by a piecewise smooth oriented closed surface.



- The proof can be extended to non-rectangular region \mathcal{E} by considering

$$x = x(u, v, w), \quad y = y(u, v, w), \quad z = z(u, v, w)$$

The Divergence Theorem

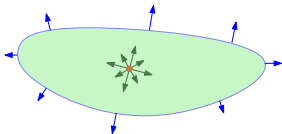
Let \mathcal{S} be a piecewise smooth closed surface with outward orientation and \mathcal{E} be a region in \mathbb{R}^3 that is enclosed by \mathcal{S} . Suppose \mathbf{F} is a vector field with a continuous partial derivatives in an open region containing \mathcal{E} , then

$$\iint_{\mathcal{S}} \mathbf{F} \cdot \mathbf{n} \, dS = \iiint_{\mathcal{E}} \operatorname{div} \mathbf{F} \, dV$$

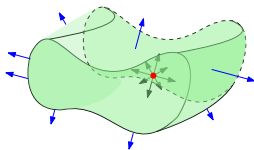
where \mathbf{n} is the outward unit normal vector of \mathcal{S} .

- Roughly speaking, it relates the flux integral of a vector field across a closed surface \mathcal{S} to an integral of its divergence in the enclosed region $\partial\mathcal{S}$

The normal form of Green's theorem



The divergence theorem



- The theorem can serve as a bridge between surface and triple integral.

Exercise

- (a) Use the divergence theorem to calculate the surface integral

$$\iint_S \mathbf{F} \cdot d\mathbf{S},$$

where S is the surface of the box with vertices $(\pm 1, \pm 2, \pm 3)$ and

$$\mathbf{F}(x, y, z) = x^2 z^3 \mathbf{e}_x + 2xyz^3 \mathbf{e}_y + xz^4 \mathbf{e}_z$$

- (b) Use the divergence theorem to evaluate

$$\iint_S \mathbf{F} \cdot d\mathbf{S},$$

where S is the top half of the sphere $x^2 + y^2 + z^2 = 1$, and

$$\mathbf{F}(x, y, z) = z^2 x \mathbf{e}_x + (y^3/3 + \tan z) \mathbf{e}_y + (x^2 z + y^2) \mathbf{e}_z$$

- If we bring the density at t and position (x, y, z) into consideration,

$$\rho(x, y, z, t)$$

- Applying the divergence theorem to the vector field,

$$\mathbf{F} = \rho \mathbf{V}$$

- The total mass flux out of the region \mathcal{E} at t is given by the triple integral

$$\iint_{\mathcal{S}} \mathbf{F} \cdot \mathbf{n} \, dS = \iiint_{\mathcal{E}} \operatorname{div} \mathbf{F} \, dV$$

- However, this flux must equal the rate of change of mass in the region \mathcal{E} , i.e.

$$\iint_{\mathcal{S}} \mathbf{F} \cdot \mathbf{n} \, dS = -\frac{\partial}{\partial t} \iiint_{\mathcal{E}} \rho \, dV = -\iiint_{\mathcal{E}} \frac{\partial \rho}{\partial t} \, dV$$

the minus sign is for the fact we are measuring net mass loss due to outflow.

- Thus equating the two expressions of the total mass flux,

$$\iiint_{\mathcal{E}} \operatorname{div} \mathbf{F} \, dV = - \iiint_{\mathcal{E}} \frac{\partial \rho}{\partial t} \, dV \implies \iiint_{\mathcal{E}} \left(\operatorname{div} \mathbf{F} + \frac{\partial \rho}{\partial t} \right) \, dV$$

- The domain is arbitrary, so this can only happen if the integrand vanishes,

$$\operatorname{div} \mathbf{F} + \frac{\partial \rho}{\partial t} = 0$$

- For a steady state fluid flow,

$$\operatorname{div}(\rho \mathbf{V}) + \frac{\partial \rho}{\partial t} = 0 \implies \rho \operatorname{div} \mathbf{V} = 0 \implies \operatorname{div} \mathbf{V} = 0 \implies \text{Incompressible}$$

and the net fluid flux through \mathcal{S} must be zero,

$$\iint_{\mathcal{S}} \mathbf{V} \cdot d\mathbf{S} = \iiint_{\mathcal{E}} \operatorname{div} \mathbf{V} \, dV = 0$$