



# JOINT INSTITUTE

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## 交大密西根学院

## **BJT and BJT Circuit**

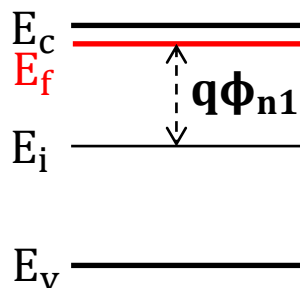
Ve311 Electronic Circuits (Summer 2019)

Dr. Chang-Ching Tu

# BJT (Before Contact)

## Emitter

n-type

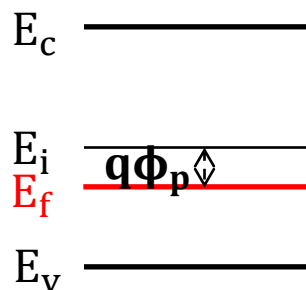


$$n \cong N_{d1} = n_i e^{\frac{q\phi_{n1}}{kT}}$$

$$p \cong \frac{n_i^2}{N_{d1}} = n_i e^{\frac{-q\phi_{n1}}{kT}}$$

## Base

p-type

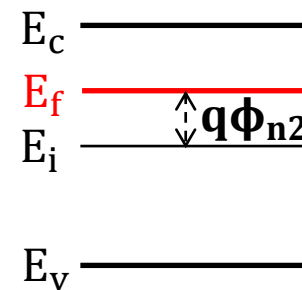


$$p \cong N_a = n_i e^{\frac{q\phi_p}{kT}}$$

$$n \cong \frac{n_i^2}{N_a} = n_i e^{\frac{-q\phi_p}{kT}}$$

## Collector

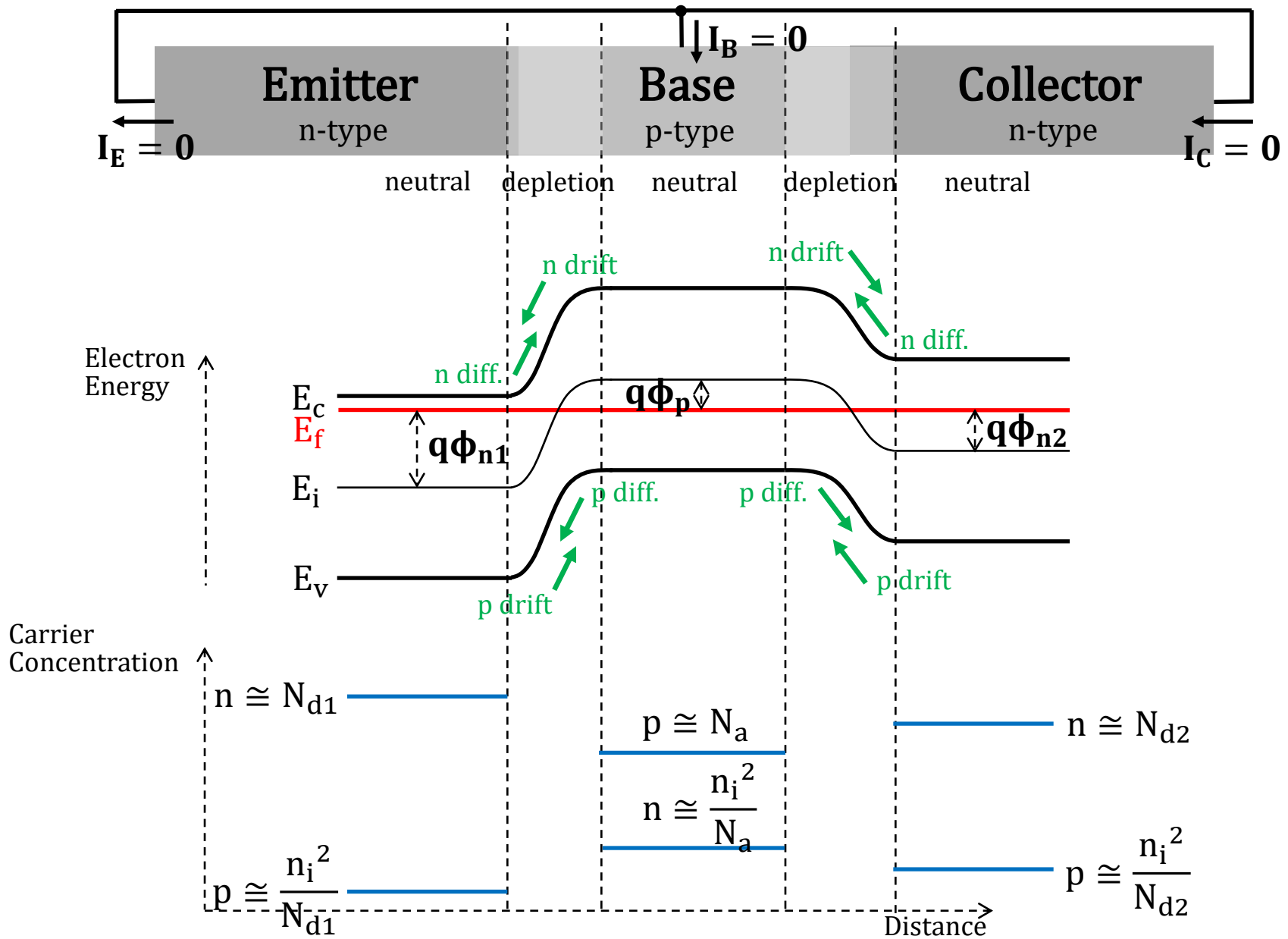
n-type



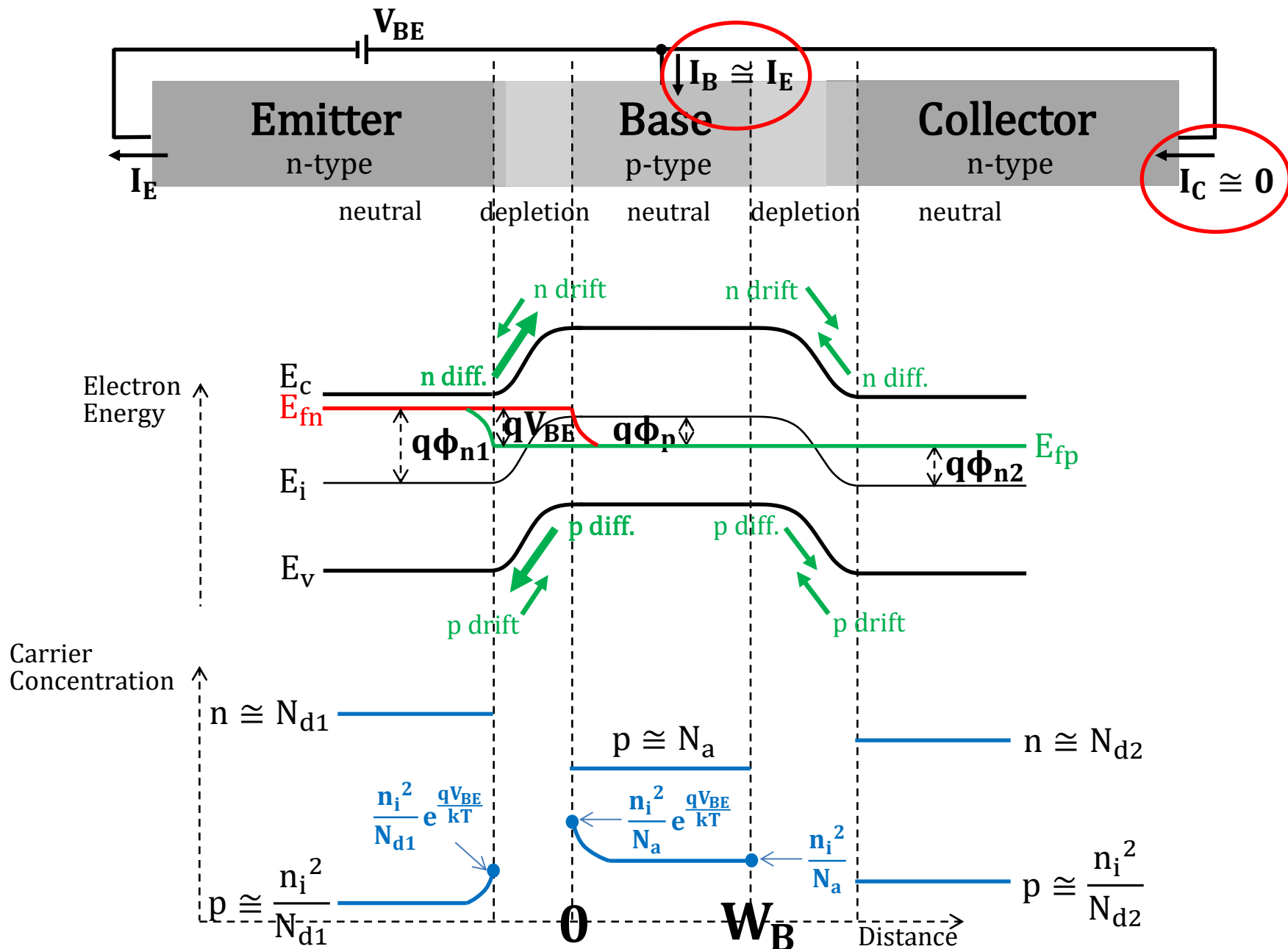
$$n \cong N_{d2} = n_i e^{\frac{q\phi_{n2}}{kT}}$$

$$p \cong \frac{n_i^2}{N_{d2}} = n_i e^{\frac{-q\phi_{n2}}{kT}}$$

$$V_{BE} = 0 \text{ and } V_{CB} = 0$$

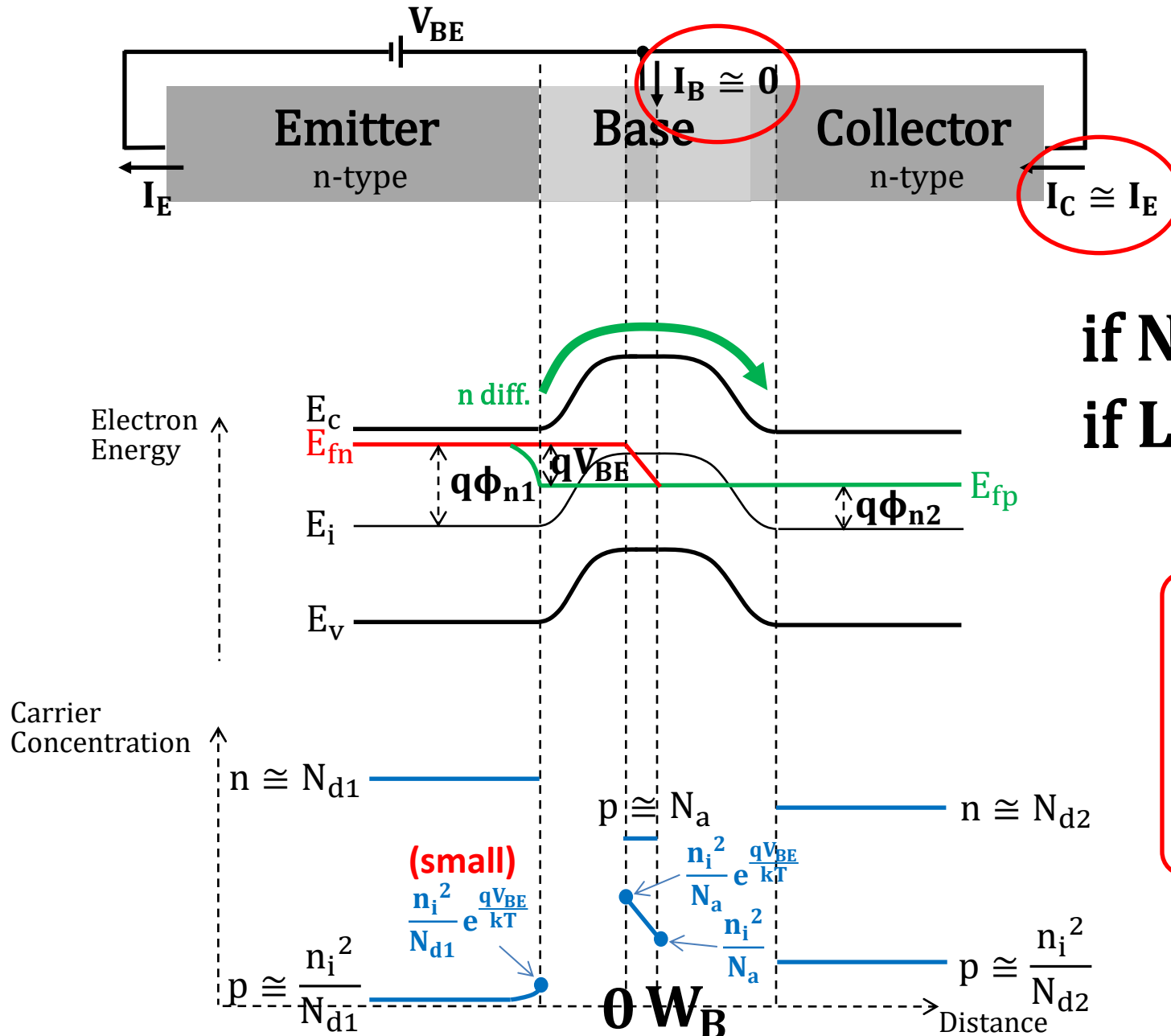


$$V_{BE} > 0 \text{ and } V_{CB} = 0$$



$V_{BE} > 0$  and  $V_{CB} = 0$  ( $W_B$  Short and  $N_{d1}$  Large)

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$$I_E = I_C + I_B$$

$$\frac{I_C}{I_E} = \alpha$$

$$\frac{I_C}{I_B} = \beta$$

# I-V Characteristic

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# I-V Characteristic (I)

- Assume  $E_x = 0$

$$(n = n_o + \Delta n)$$

$$J_n(\text{electron current in the base neutral region}) = q\mu_n n E_x + qD_n \frac{dn}{dx} = qD_n \frac{dn}{dx} = qD_n \frac{d\Delta n}{dx}$$

$$\text{In steady - state} \Rightarrow \frac{\partial n}{\partial t} = \frac{1}{q} \frac{dJ_n}{dx} + G - R = 0$$

$$\Rightarrow \frac{d^2 \Delta n}{dx^2} = \frac{\Delta n}{D_n \tau_n} = \frac{\Delta n}{L_n^2}$$

Put  $\Delta n$  back into here



$$\Rightarrow \Delta n(x) = K_1 e^{\frac{-x}{L_n}} + K_2 e^{\frac{x}{L_n}}$$

$$\text{B.C.} \begin{cases} \Delta n(0) = \frac{n_i^2}{N_a} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \\ \Delta n(W_B) = 0 \end{cases}$$

$$\Rightarrow \Delta n(x) = \frac{n_i^2}{N_a} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \frac{\sinh\left(\frac{W_B - x}{L_n}\right)}{\sinh\left(\frac{W_B}{L_n}\right)}$$

$$\sinh(x) = \frac{e^x - e^{-x}}{2}$$

# I-V Characteristic (II)

$$I_n(x=0) = I_E = \frac{AqD_n n_i^2}{L_n N_a} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \coth\left(\frac{W_B}{L_n}\right) = \frac{AqD_n n_i^2}{W_B N_a} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \text{ if } L_n \gg W_B$$

$$I_n(x=W_B) = I_C = \frac{AqD_n n_i^2}{L_n N_a} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \operatorname{csch}\left(\frac{W_B}{L_n}\right) = \frac{AqD_n n_i^2}{W_B N_a} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \text{ if } L_n \gg W_B$$

$$\alpha = \frac{I_C}{I_E} = \operatorname{sech}\left(\frac{W_B}{L_n}\right) \cong 1 - \frac{W_B^2}{2L_n^2} \text{ if } L_n \gg W_B$$

$$\beta = \frac{I_C}{I_B} = \frac{\alpha I_E}{I_E - \alpha I_E} = \frac{\alpha}{1 - \alpha}$$

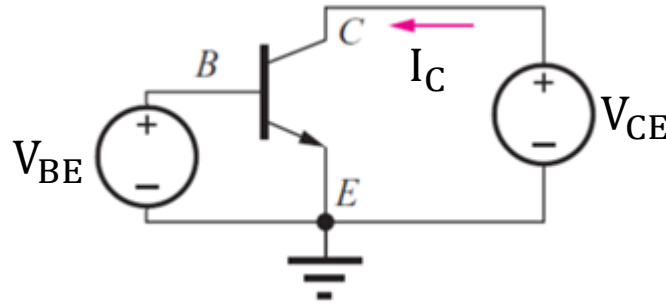
$$\coth(x) = \frac{e^x + e^{-x}}{e^x - e^{-x}} \cong \frac{1}{x} \text{ if } x \text{ small}$$

$$\operatorname{csch}(x) = \frac{2}{e^x - e^{-x}} \cong \frac{1}{x} \text{ if } x \text{ small}$$

$$\operatorname{sech}(x) = \frac{2}{e^x + e^{-x}}$$



# Summary



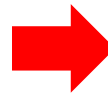
$V_{CE} \geq V_{BE}$   
 $\Rightarrow$  Forward – Active

For  $L_n \gg W_B$

$$I_C \cong \frac{AqD_n n_i^2}{N_a W_B} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right)$$

$$\alpha = \frac{I_C}{I_E} \cong 1 - \frac{W_B^2}{2L_n^2}$$

$$\beta = \frac{I_C}{I_B} = \frac{\alpha}{1 - \alpha}$$



Ideal

$$I_C = \frac{AqD_n n_i^2}{N_a W_B} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right)$$

$$\alpha = \frac{I_C}{I_E} = 1$$

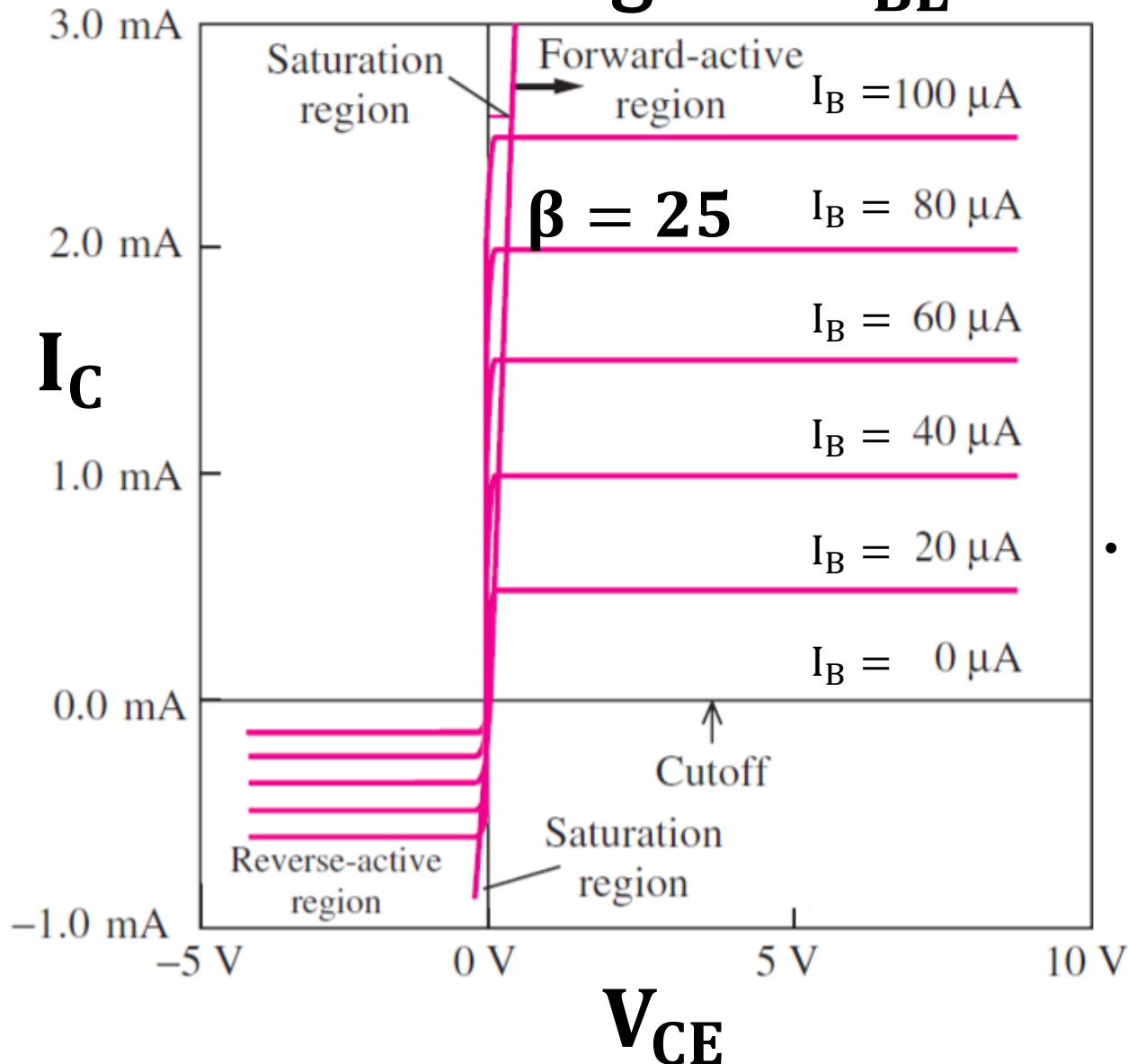
$$\beta = \frac{I_C}{I_B} = \infty$$

$I_C$  vs  $V_{CE}$  and  $I_C$  vs  $V_{BE}$   
in Forward-Active Region

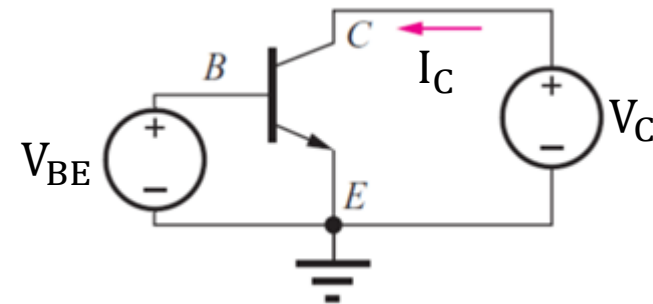
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# $I_C$ vs $V_{CE}$

For each given  $V_{BE}$



$$V_{CE} \geq V_{BE} \Rightarrow \text{Forward - Active}$$

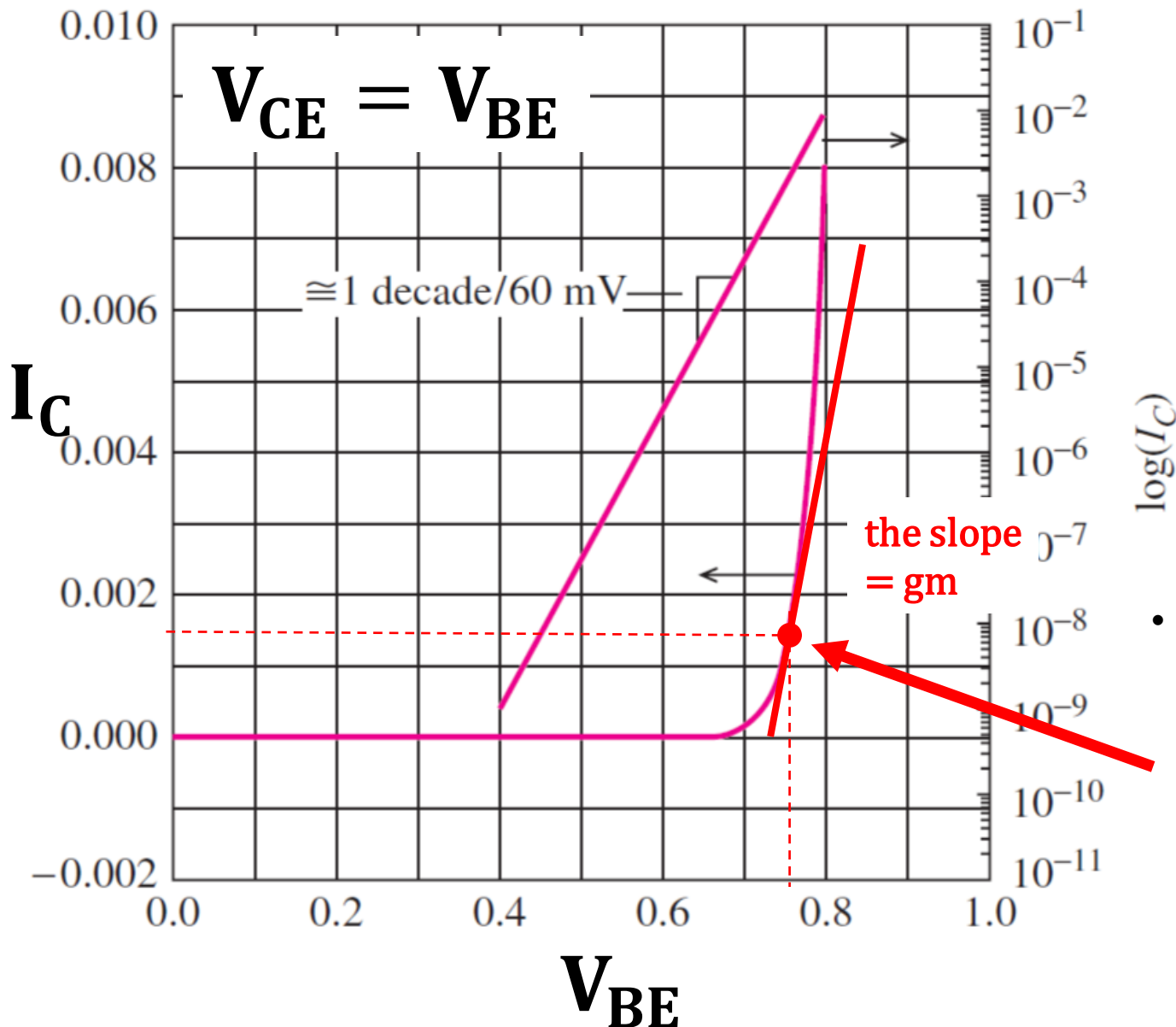


- At certain  $V_{BE}$  and  $V_{CE}$  biasing condition, small-signal output impedance ( $r_o$ ):

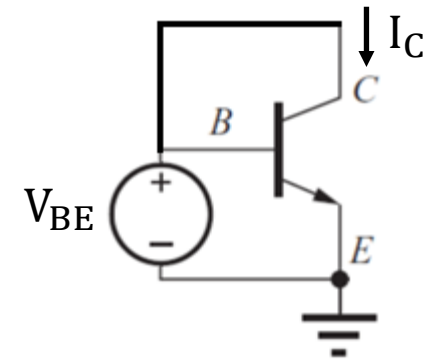
$$\frac{1}{r_o} = \frac{dI_C}{dV_{CE}} = 0$$

$$r_o = \infty$$

# $I_C$ vs $V_{BE}$



$V_{CE} \geq V_{BE}$   
 $\Rightarrow$  Forward – Active



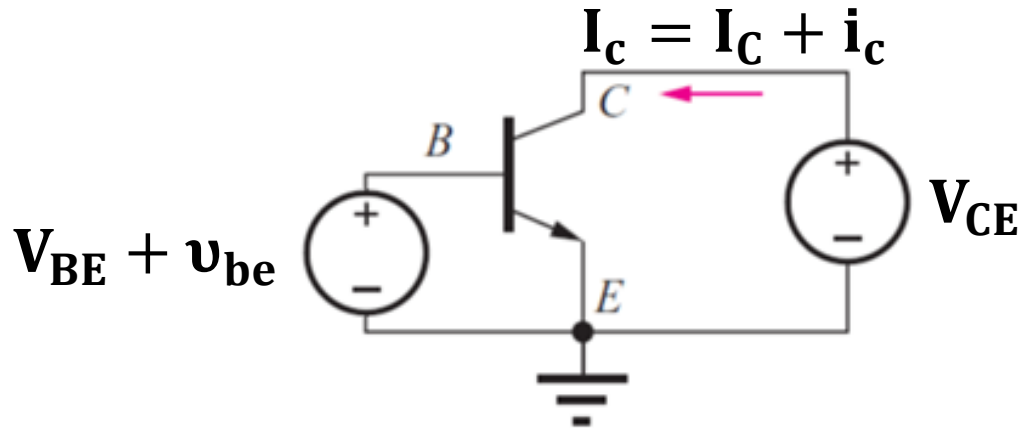
- At certain  $V_{BE}$  and  $V_{CE}$  biasing condition, small-signal transconductance gain ( $g_m$ ):

$$g_m = \frac{dI_C}{dV_{BE}} \cong \frac{I_C}{kT/q}$$

# Small-Signal Model

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# Hybrid- $\pi$ Model (without Early Effect)



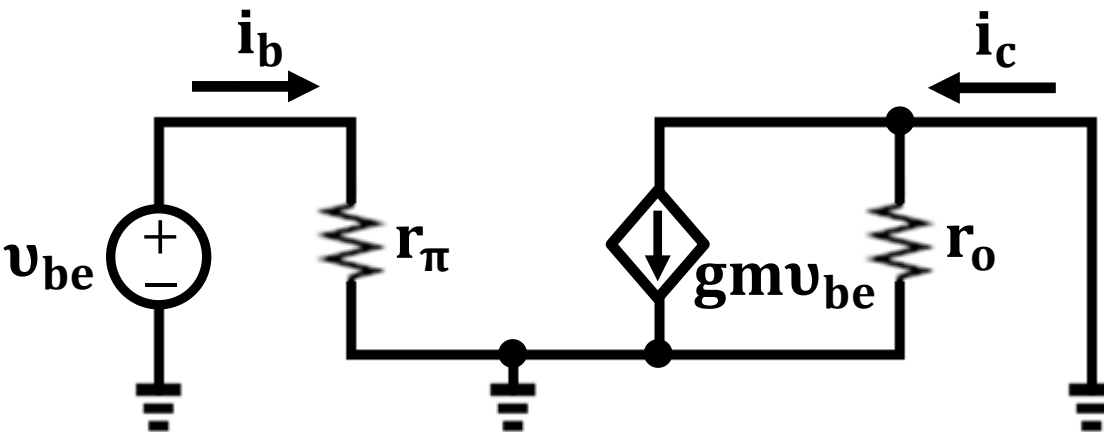
$$V_{CE} \geq V_{BE}$$

$\Rightarrow$  Forward – Active

$$I_C \cong \frac{AqD_n n_i^2}{N_a W_B} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right)$$



In small-signal analysis:

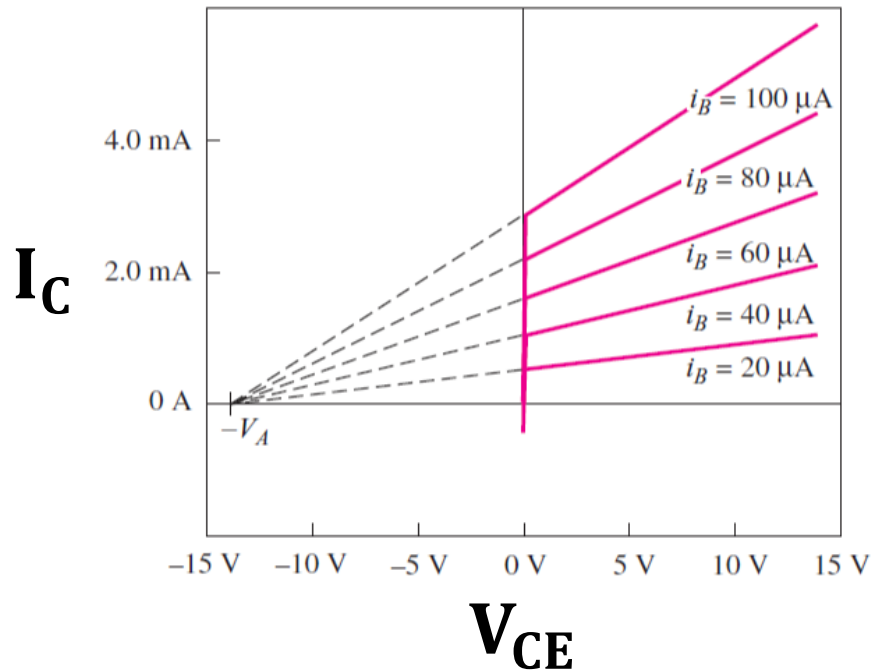


$$r_\pi = \frac{1}{\frac{dI_B}{dV_{BE}}} = \frac{1}{\beta \frac{dI_C}{dV_{BE}}} = \frac{1}{\frac{gm}{\beta}} = \frac{\beta}{gm}$$

$$gm = \frac{dI_C}{dV_{BE}} \cong \frac{I_C}{kT/q}$$

$$r_o = \frac{1}{\frac{dI_C}{dV_{CE}}} = \infty$$

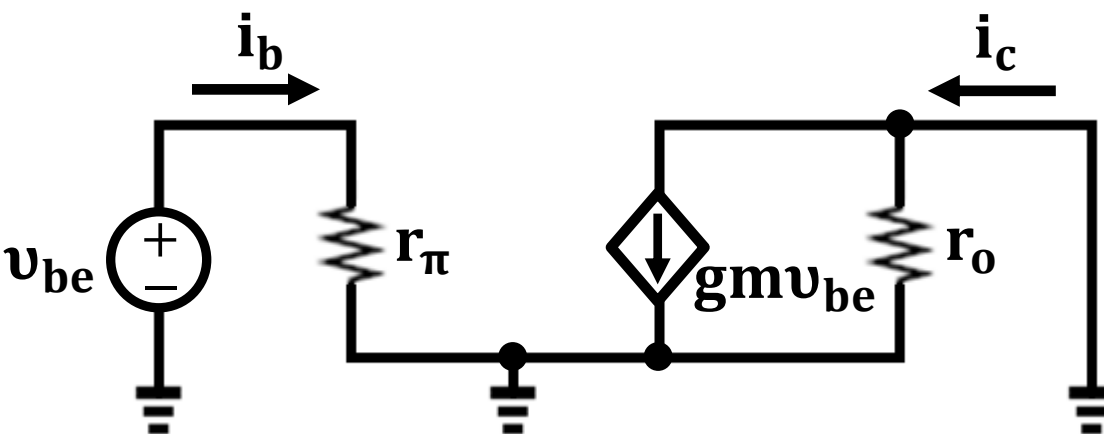
# Hybrid- $\pi$ Model (with Early Effect)



$$V_{CE} \geq V_{BE}$$

$\Rightarrow$  Forward – Active

$$I_C \cong \frac{AqD_n n_i^2}{N_a W_B} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \left( 1 + \frac{V_{CE}}{V_A} \right)$$



$$r_\pi = \frac{1}{\frac{dI_B}{dV_{BE}}} = \frac{1}{\beta \frac{dI_C}{dV_{BE}}} = \frac{1}{\frac{gm}{\beta}} = \frac{\beta}{gm}$$

$$gm = \frac{dI_C}{dV_{BE}} \cong \frac{I_C}{kT/q}$$

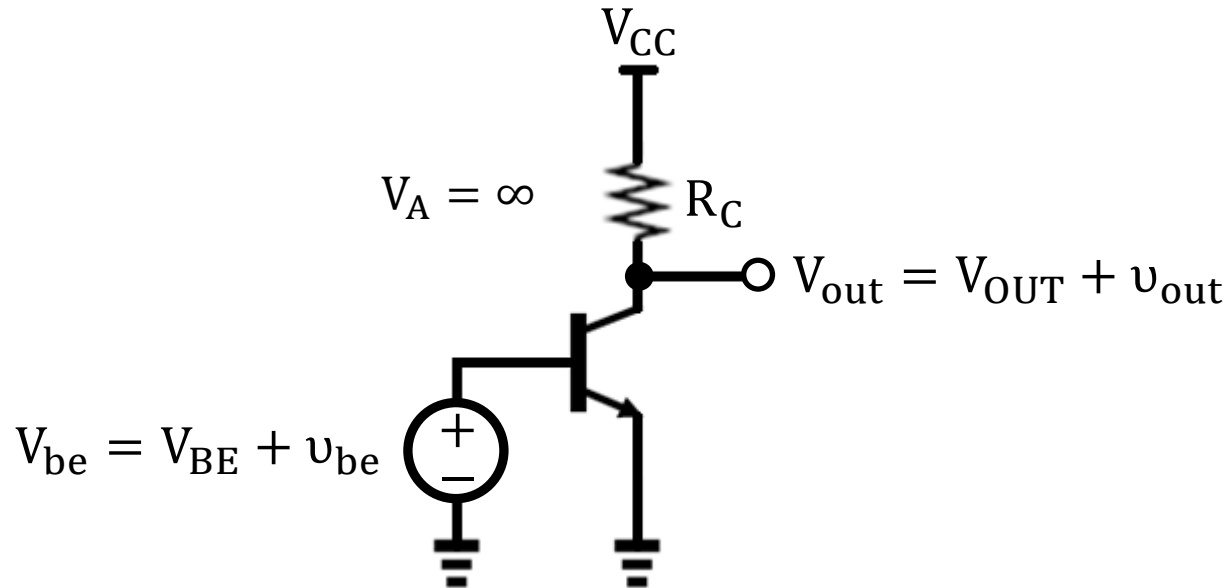
$$r_o = \frac{1}{\frac{dI_C}{dV_{CE}}} \cong \frac{V_A}{I_C}$$

# Common-Emitter Amplifier

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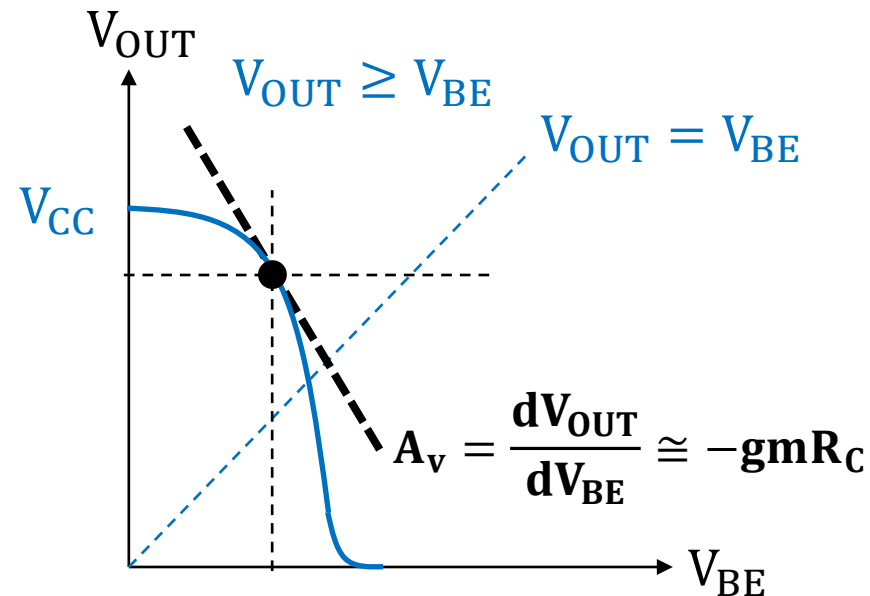
# Common-Emitter Amplifier ( $V_A = \infty$ )



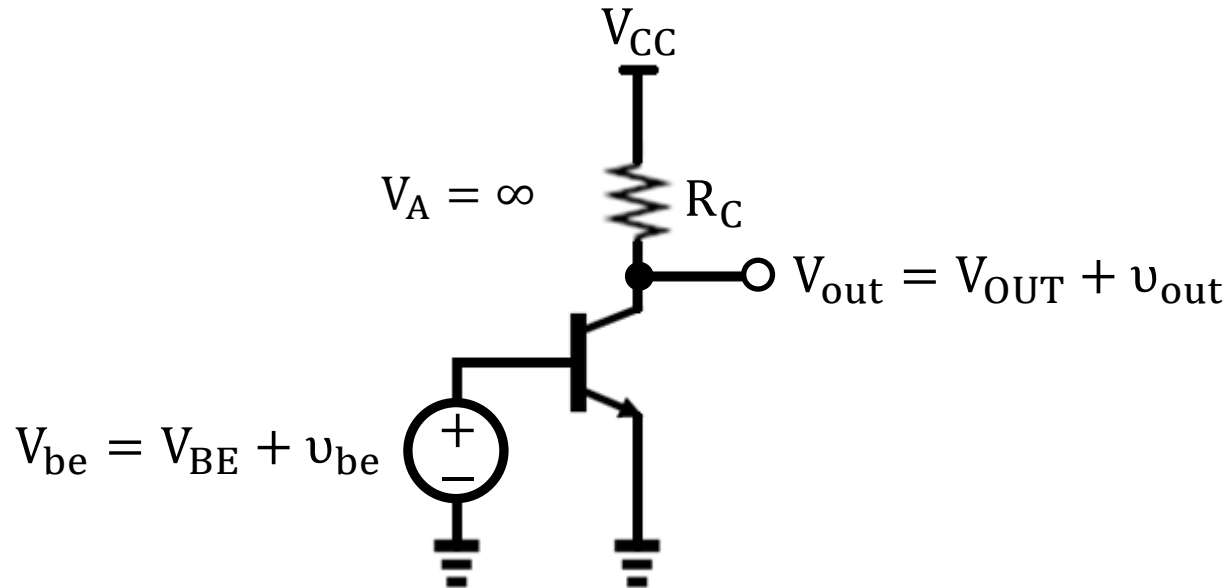
## • DC Analysis

$$\begin{aligned} V_{OUT} &= V_{CC} - I_C R_C \\ &= V_{CC} - \frac{A_q D_n n_i^2}{N_a W_B} \left( e^{\frac{q V_{BE}}{kT}} - 1 \right) R_C \end{aligned}$$

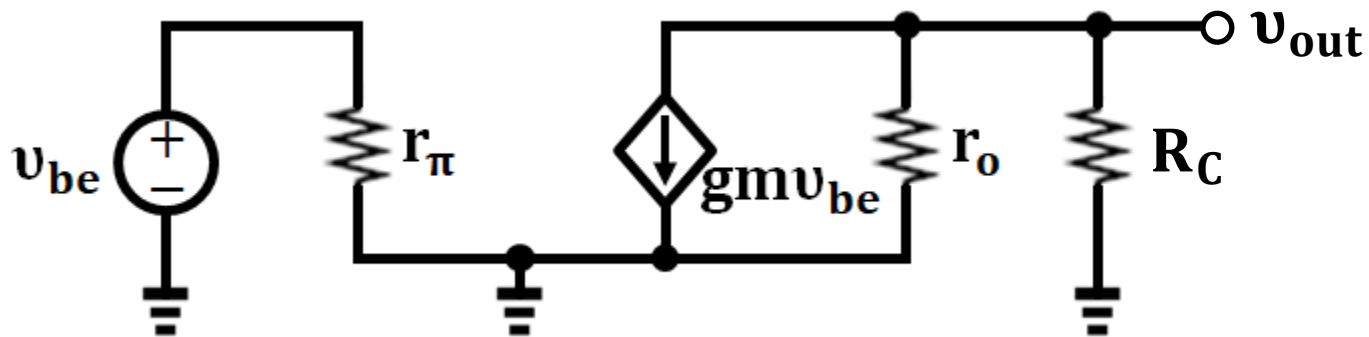
$$A_v = \frac{dV_{OUT}}{dV_{BE}} \cong -\frac{I_C}{kT/q} R_C = -g_m R_C$$



# Common-Emitter Amplifier ( $V_A = \infty$ )

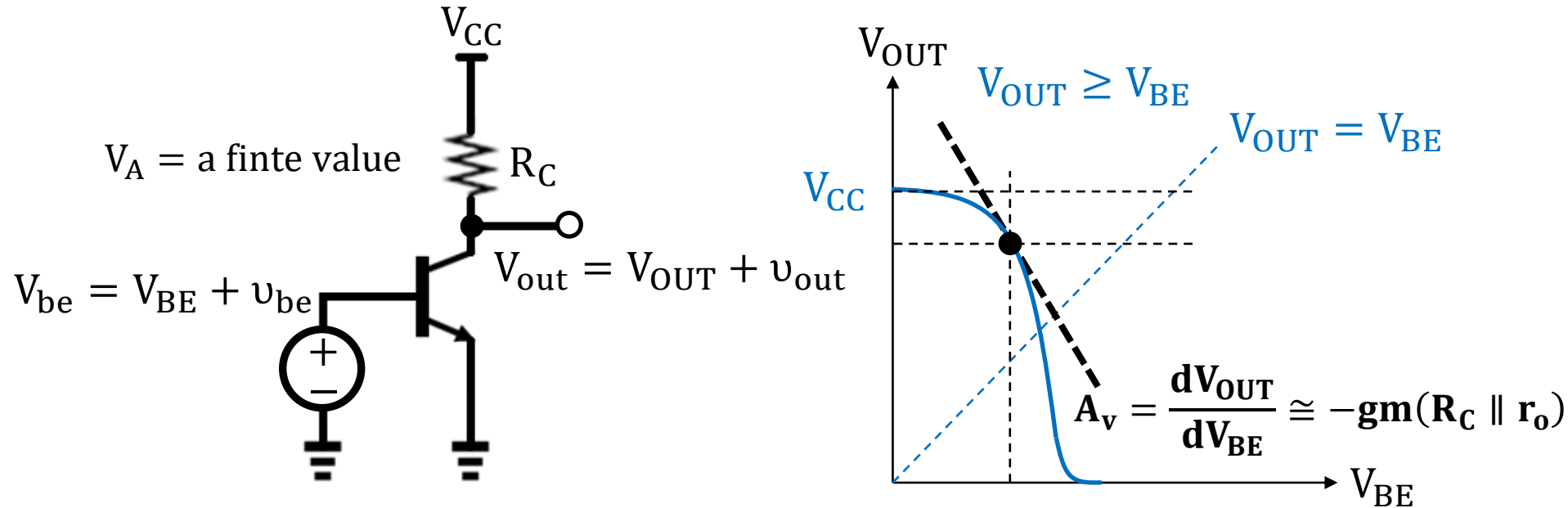


- Small-Signal Analysis



$$A_v = \frac{v_{out}}{v_{be}} = -gm(R_C \parallel r_o) = -gmR_C \quad (\text{since } r_o = \infty)$$

# Common-Emitter Amplifier ( $V_A = \text{a finite value}$ )<sup>19</sup>



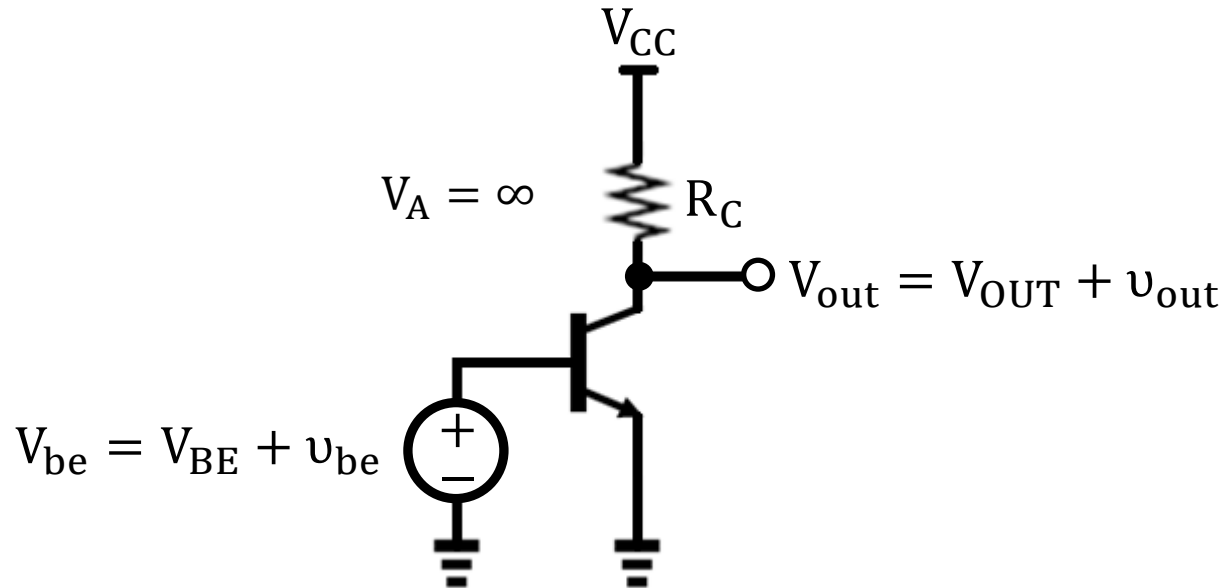
- DC Analysis

$$V_{OUT} = V_{CC} - I_C R_C = V_{CC} - I_S \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \left( 1 + \frac{V_{OUT}}{V_A} \right) R_C$$

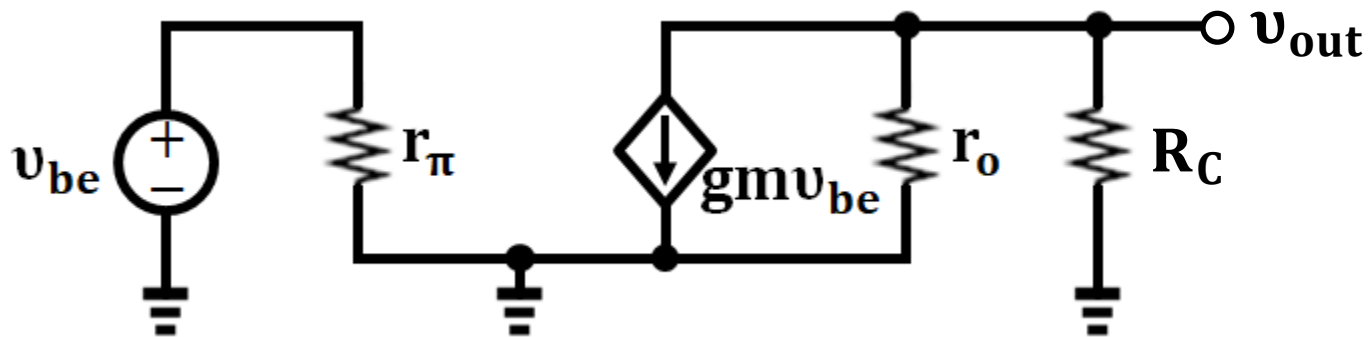
$$\frac{dV_{OUT}}{dV_{BE}} = -\frac{q}{kT} I_S e^{\frac{qV_{BE}}{kT}} \left( 1 + \frac{V_{OUT}}{V_A} \right) R_C - I_S \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \frac{1}{V_A} \frac{dV_{OUT}}{dV_{BE}} R_C \cong -gm R_C - \frac{1}{r_o} \frac{dV_{OUT}}{dV_{BE}} R_C$$

$$A_v = \frac{dV_{OUT}}{dV_{BE}} \cong -gm(R_C \parallel r_o)$$

# Common-Emitter Amplifier ( $V_A = \text{a finite value}$ )<sup>20</sup>



- Small-Signal Analysis

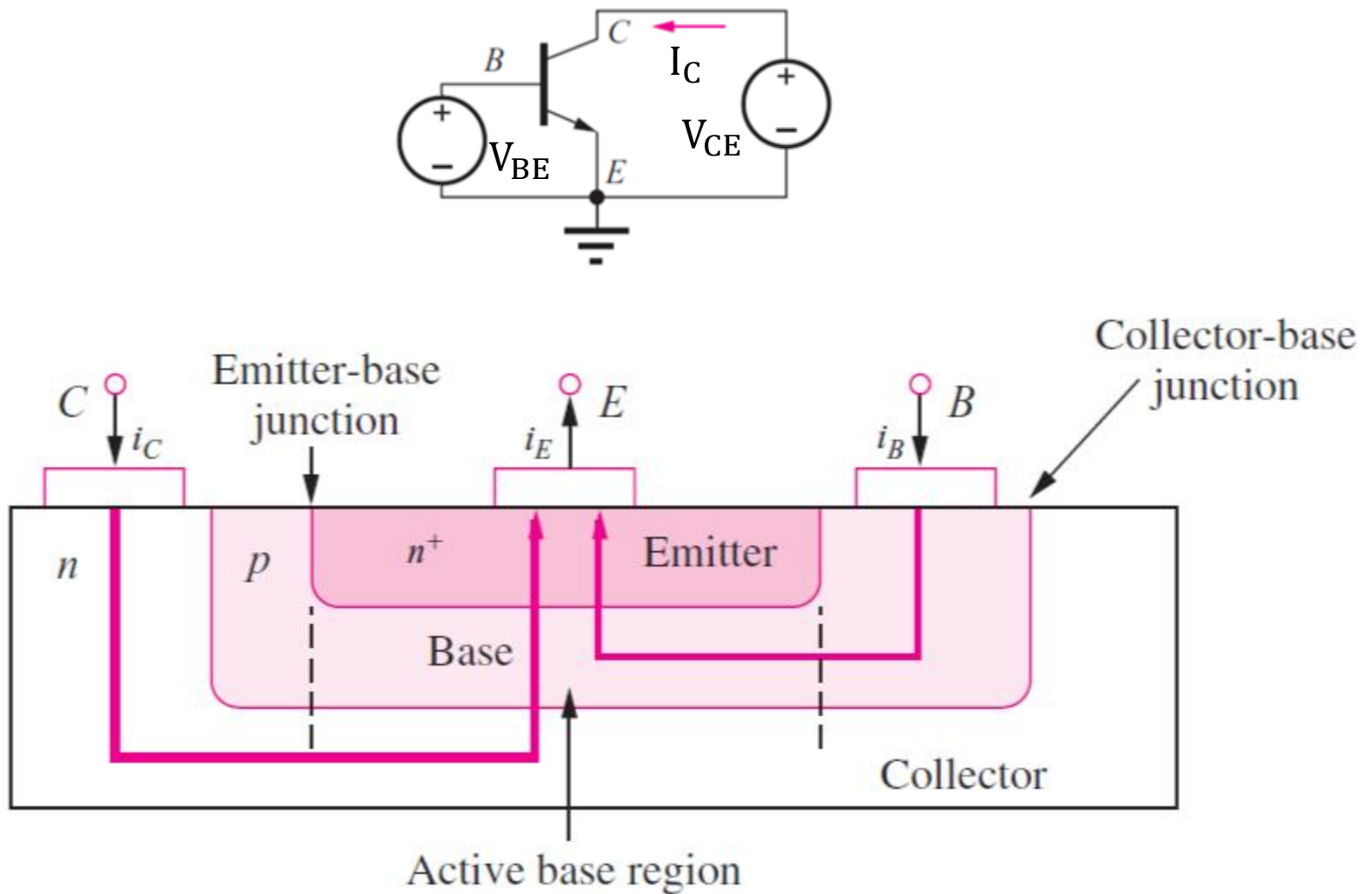


$$A_v = \frac{v_{out}}{v_{be}} = -gm(R_C \parallel r_o)$$

# BJT Structure and Pspice Model

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# npn BJT Cross Section



# npn BJT Pspice Model

.model Qbreakn NPN IS=1e-18 BF=100 VAF=100

$$I_C = \textcolor{blue}{IS} \left( e^{\frac{qV_{BE}}{kT}} - 1 \right) \left( 1 + \frac{V_{CE}}{\textcolor{blue}{VAF}} \right)$$

$$\textcolor{blue}{BF} = \frac{I_C}{I_B} \quad I_E = I_C + I_B$$

$$g_m \cong \frac{I_C}{kT/q} \quad r_\pi = \frac{\textcolor{blue}{BF}}{g_m} \quad r_o \cong \frac{\textcolor{blue}{VAF}}{I_C}$$