

An approach for solving industrial robot forward and inverse kinematics

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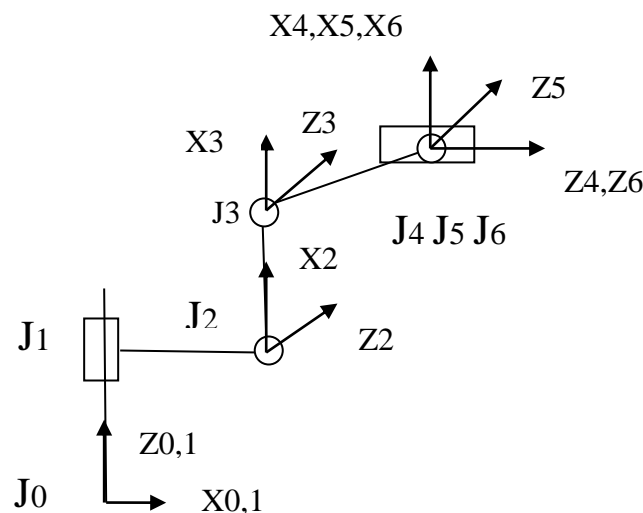
ABSTRACT

Solving the forward/inverse-pose kinematic transformation is the basic problem in the study of mechanical manipulation. In this paper we introduced a widely used approach to working out the forward-pose transformation by using the D-H parameter table, together with a geometric approach to solve the inverse-pose transformation. All the approaches are implemented via MATLAB programs, and the programs are tested by given input data. Results are checked by some functions in the Corke MATLAB robotics Toolbox. The model is established according to the widely used industrial robot, FANUC 2000ib/165EW.

Key word: industrial robot, forward-pose transformation, inverse-pose transformation, kinematic, geometric approach.

Forward-pose kinematics

D-H table. By analyze the drawing of the FANUC Robot, we can built its model as below, which is simplified by some common rules:



Built coordinates on each joint and we can get the D-H parameter table as below

$Link_i$	a_{i-1}	d_i	a_i	θ_i
1	0	0	0	0
2	312	0	-90°	0
3	1075	0	0	0
4	725	1280	-90°	0
5	0	0	90°	0
6	0	0	-90°	0

Homogeneous transformation matrix. the standard process to derive the Homogeneous transformation matrix, which is what we used, is as below:

Rotate about X_{i-1} by α_i

Translate along X_{i-1} by a_{i-1}

Rotate about Z_i by θ_i

Translate along Z_i by d_i

Implement standard process in MATLAB code:

```
A1=rotx(alpha(1))*transl(a(1),0,0)*rotz(theta(1))*transl(0,0,d(1))
A2=rotx(alpha(2))*transl(a(2),0,0)*rotz(theta(2))*transl(0,0,d(2))
A3=rotx(alpha(3))*transl(a(3),0,0)*rotz(theta(3))*transl(0,0,d(3))
A4=rotx(alpha(4))*transl(a(4),0,0)*rotz(theta(4))*transl(0,0,d(4))
A5=rotx(alpha(5))*transl(a(5),0,0)*rotz(theta(5))*transl(0,0,d(5))
A6=rotx(alpha(6))*transl(a(6),0,0)*rotz(theta(6))*transl(0,0,d(6))
```

Multiply the matrix to get transformation matrix 0_3T , 0_6T

```
B1=A1*A2*A3    %T (03)
```

```
B2=A1*A2*A3*A4*A5*A6    %T (06)
```

Check. To check the matrix derived, function link()、robot()、fkine() in robot toolbox are used to build the robot model and derive its forward-pose transformation matrix.

```
sigma=0    %0表示运动关节
L1=link([alpha(1),a(1),theta(1),d(1),sigma],'mod')
L2=link([alpha(2),a(2),theta(2),d(2),sigma],'mod')
L3=link([alpha(3),a(3),theta(3),d(3),sigma],'mod')
L4=link([alpha(4),a(4),theta(4),d(4),sigma],'mod')
L5=link([alpha(5),a(5),theta(5),d(5),sigma],'mod')
L6=link([alpha(6),a(6),theta(6),d(6),sigma],'mod')
R=robot({L1,L2,L3,L4,L5,L6},'Rlan3R')
q=[0 0 0 0 0 0]
%q=theta
IR=fkine(R,q)
```

Input the given data as below:

- a) $[\theta_1 \theta_2 \theta_3 \theta_4 \theta_5 \theta_6]^T = [0 \ 0 \ 0 \ 0 \ 0 \ 0]^T$
- b) $[10^\circ \ 20^\circ \ 30^\circ \ 10^\circ - 30^\circ \ 10^\circ]^T$
- c) $[90^\circ - 35^\circ \ 79^\circ - 80^\circ \ 10^\circ \ 120^\circ]^T$

All of the matrix fit the check result (check 0T only for simplification):

a) $[\theta_1 \ \theta_2 \ \theta_3 \ \theta_4 \ \theta_5 \ \theta_6]^T = [0 \ 0 \ 0 \ 0 \ 0 \ 0]^T$

```
IR =

1.0e+03 *

0.0010         0         0        1.6120
0    -0.0010         0    0.0000    0.0000
0    -0.0000        -0.0010   -1.2800
0         0         0         0.0010

>> B2

B2 =

1.0e+03 *

0.0010         0         0        1.6120
0    -0.0010         0    0.0000    0.0000
0    -0.0000        -0.0010   -1.2800
0         0         0         0.0010
```

b) $[\theta_1 \ \theta_2 \ \theta_3 \ \theta_4 \ \theta_5 \ \theta_6]^T = [10^\circ \ 20^\circ \ 30^\circ \ 10^\circ \ -30^\circ \ 10^\circ]^T$

B2 =

1.0e+03 *

0.0009	-0.0001	-0.0003	0.4789
-0.0002	-0.0010	-0.0001	0.0844
-0.0003	0.0002	-0.0009	-1.3628
0	0	0	0.0010

>> IR

IR =

1.0e+03 *

0.0009	-0.0001	-0.0003	0.4789
-0.0002	-0.0010	-0.0001	0.0844
-0.0003	0.0002	-0.0009	-1.3628
0	0	0	0.0010

c) $[\theta_1 \ \theta_2 \ \theta_3 \ \theta_4 \ \theta_5 \ \theta_6]^T = [90^\circ \ -35^\circ \ 79^\circ \ -80^\circ \ 10^\circ \ 120^\circ]^T$

IR =

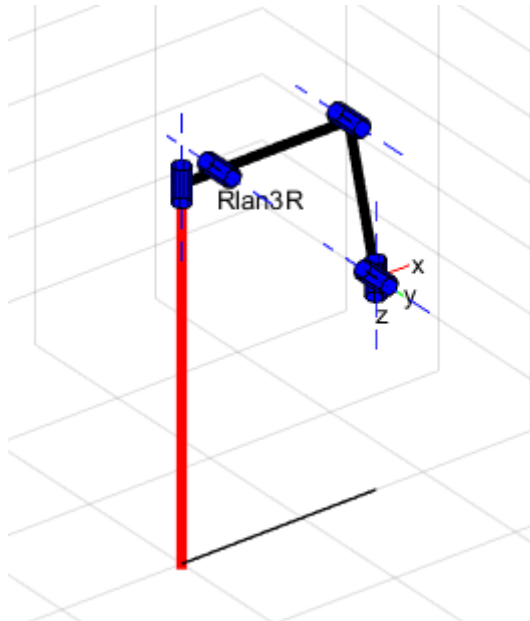
0.6353	0.7531	0.1710	-0.0000
0.6123	-0.3563	-0.7058	465.2772
-0.4706	0.5531	-0.6875	-460.4584
0	0	0	1.0000

>> B2

B2 =

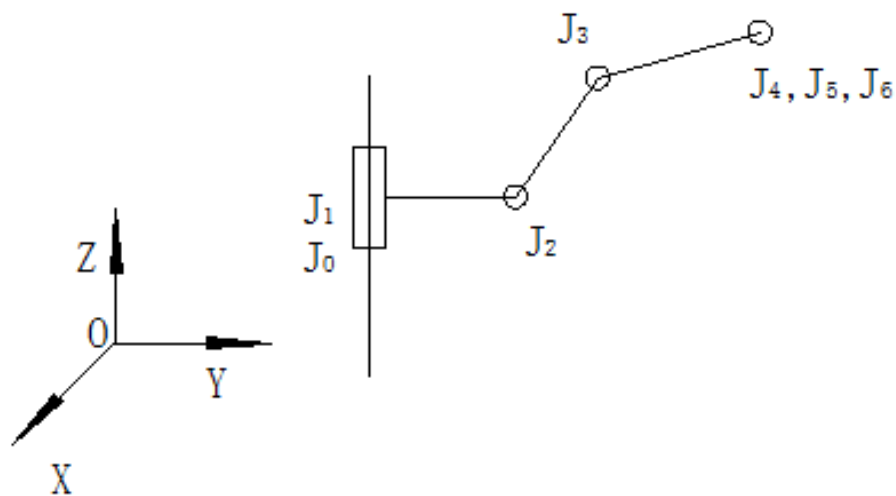
0.6353	0.7531	0.1710	-0.0000
0.6123	-0.3563	-0.7058	465.2772
-0.4706	0.5531	-0.6875	-460.4584
0	0	0	1.0000

Function `drivebot(R, q)` can be used to draw the figure of the robot model, which is coincident with the model we built before.

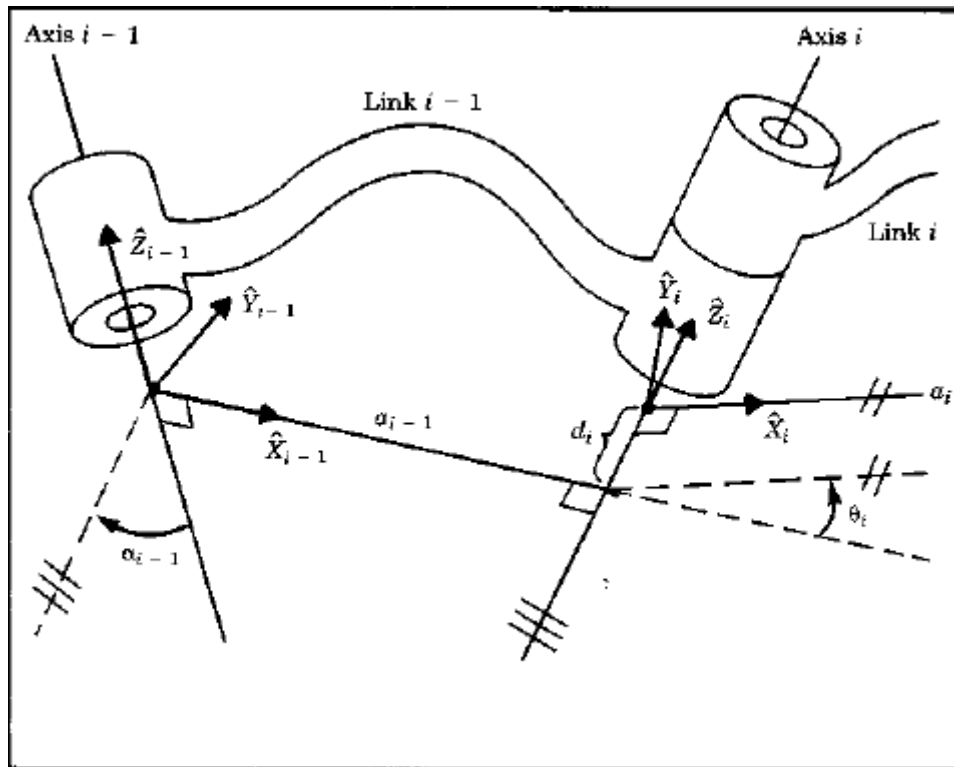


Inverse-pose kinematics

Inverse-pose solution. To derive the solution of a given ${}^0_H T$, we decided to use a partially geometric and partially algebraic method. Build a coordinate as below:

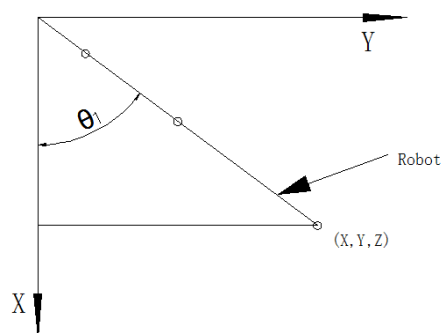


As we know, derive the inverse-pose solution means find the equation of $\theta_i (i=1, \dots, 6)$, θ_i is the intersection angle of the two common normal line between axis(i-1)、axis(i) and axis(i)、axis(i+1)



① θ_1

Express θ_1 in X-Y plane



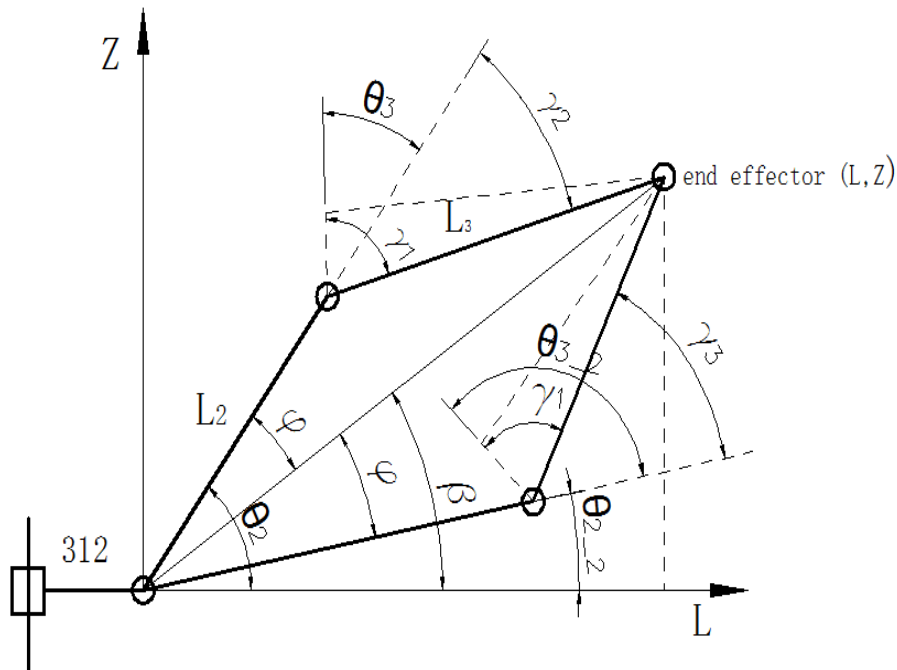
Form the H_0T we can easily get the coordinates (x, y, z) of the end effector,

in which $x = {}^6_H T(1,4)$, $y = {}^6_H T(2,4)$, $z = {}^6_H T(3,4)$

Then $\theta_1 = \text{Atan2}(y, x)$

② θ_2, θ_3

To derive the equation of θ_2, θ_3 , the robot is analyzed in vertical plane.



Relationships among angles are as above .

In this case, we can usually find a solutions of a ${}^0_H T$, but when the manipulator is at its singularity, only one solution will be found.

We can apply the “law of cosines” to solve θ_3 .

$$Z^2 + L^2 = L_2^2 + L_3^2 - 2L_2L_3\cos(180^\circ - r_2)$$

Introduce

$$L = \sqrt{x^2 + y^2} - 312$$

$$\cos(180^\circ - r_2) = -\cos(r_2)$$

We get

$$\cos r_2 = \frac{L^2 + Z^2 - L_2^2 - L_3^2}{2L_2L_3}$$

$$r_2 = a \cos\left(\frac{L^2 + Z^2 - L_2^2 - L_3^2}{2L_2L_3}\right)$$

Also we know

$$r_1 = a \tan 2(1280, 225)$$

So

$$\theta_3 = -(r_1 - r_2) = r_2 - r_1$$

θ_3 in another solution has a different equation

$$\theta_{3-2} = -(r_1 + r_3)$$

In which

$$Z^2 + L^2 = L_2^2 + L_3^2 - 2L_2L_3 \cos(180^\circ - r_3)$$

$$\text{Apply } L = \sqrt{X^2 + Y^2} - 312$$

$$\cos(180^\circ - r_3) = -\cos(r_3)$$

we get

$$r_3 = a \cos\left(\frac{L^2 + Z^2 - L_2^2 - L_3^2}{2L_2L_3}\right)$$

And

$$r_1 = a \tan 2(1280, 225)$$

For θ_2 , we know

$$\theta_2 = \beta + \varphi$$

$$\theta_{2-2} = \beta - \varphi$$

In which

$$\beta = \text{atan2}(Z, L)$$

And

$$Z^2 + L^2 + L_2^2 - L_3^2 = 2L_2\sqrt{Z^2 + L^2} \bullet \cos \varphi$$

$$\varphi = \arccos\left(\frac{L^2 + Z^2 + L_2^2 - L_3^2}{2L_2\sqrt{Z^2 + L^2}}\right) \quad , \quad \varphi \in [0^\circ \sim 180^\circ]$$

Before calculate θ_2, θ_3 , we have to make sure that the position of end effector

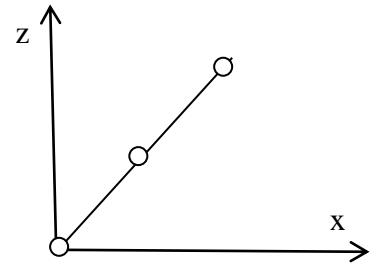
expressed by ${}^0_H T$ is in the reach of the manipulator, which means ${}^0_H T$ has a solution.

So

$$L_2 + L_3 \geq \sqrt{Z^2 + L^2}$$

When $L_2 + L_3 = \sqrt{Z^2 + L^2}$

The manipulator is at the singularity point.



After getting the values of $\theta_1, \theta_2, \theta_3$ by geometric approach, we used algebraic

approach to derive the values of $\theta_4, \theta_5, \theta_6$.

Introduce the values of $\theta_1, \theta_2, \theta_3$ in the equation

$${}^0_1 T {}^1_2 T {}^2_3 T {}^3_4 T {}^4_5 T {}^5_6 T = {}^0_H T$$

$${}^3_4 T {}^4_5 T {}^5_6 T = ({}^0_1 T {}^1_2 T {}^2_3 T)^{-1} {}^0_H T$$

Assume

$$X_1 = ({}^0_1 T {}^1_2 T {}^2_3 T)^{-1} {}^0_H T$$

$$X_2 = {}^3_4 T {}^4_5 T {}^5_6 T$$

The results are below:

```
>> X2=A4*A5*A6
```

X2 =

```
[ cos(theta4)*cos(theta5)*cos(theta6) - sin(theta4)*sin(theta6), -cos(theta6)*sin(theta4) - cos(theta4)*cos(theta5)*sin(theta6), -cos(theta4)*sin(theta5), 225]
[ cos(theta6)*sin(theta5), -sin(theta5)*sin(theta6), cos(theta5), 1280]
[ -cos(theta4)*sin(theta6) - cos(theta5)*cos(theta6)*sin(theta4), cos(theta5)*sin(theta4)*sin(theta6) - cos(theta4)*cos(theta6), sin(theta4)*sin(theta5), 0]
[ 0, 0, 0, 1]
```

Chose 3 equations to derive $\theta_4, \theta_5, \theta_6$.

$$\begin{cases} X_2(2,3) = X_1(2,3) \\ X_2(3,3) = X_1(3,3) \\ X_2(2,1) = X_1(2,1) \end{cases}$$

$$\Rightarrow \begin{cases} \theta_4 = a \cos\left(\frac{X_1(3,3)}{\sin \theta_5}\right) \\ \theta_5 = -a \cos(X_1(2,3)) \\ \theta_6 = a \cos\left(\frac{X_1(2,1)}{\sin \theta_5}\right) \end{cases}$$

Up to now, we have derived the solution of the given translation matrix

$$\theta_i = (\theta_1, \theta_2, \theta_3, \theta_4, \theta_5)$$

Check. Function ikine(), drivebot() can be used to check the result.

Test the program by given ${}^0_H T$:

T1:

$${}^0_H T = {}^0_6 T = \begin{bmatrix} -0.11013 & 0.52562 & 0.84356 & 1604.7 \\ -0.96534 & -0.1455 & 0.21668 & 926.49 \\ 0.23663 & -0.83819 & 0.49138 & 1569.1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

T2:

$${}^0_H T = {}^0_6 T = \begin{bmatrix} -0.73794 & 0.57972 & 0.34551 & 1499.3 \\ -0.63372 & -0.77128 & -0.059391 & 0 \\ 0.23205 & -0.26278 & 0.93654 & 2056.5 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

T3:

$${}^0_H T = {}^0_6 T = \begin{bmatrix} 0.1658 & -0.1736 & -0.9708 & 2655 \\ 0.0292 & 0.9848 & -0.1712 & 866.5 \\ 0.9857 & 0 & 0.1683 & 806.3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

It is also necessary to check if each joint angle result is in the working range as below table.

各轴工作范围	
	角度 (度)
J1 轴	-180-0/0-180
J2 轴	-60-0/0-75
J3 轴	-128-0/0-80
J4 轴	-360-0/0-360 (软件限位)
J5 轴	-125-0/0-125
J6 轴	-220-0/0-220

Due to the degree of accuracy of iteration , the ikine() function can only derived one solution of T1, as below :

$q = [0.5236 \ -1.2217 \ -0.6196 \ 0.7541 \ -0.3490 \ 0.4362]$

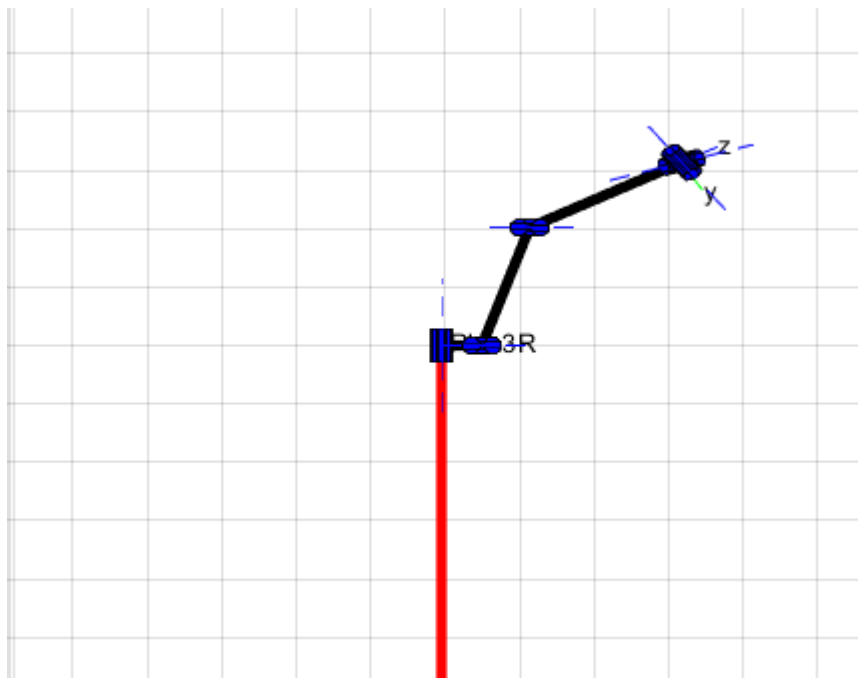
Following are the result derived by the partially geometric and partially algebraic algorithm:

One solution of the T1

```
theta =  
  
    0.5236   -1.2217   -0.6196    0.8167   -0.3491    0.4363
```

Most values in the solution are coherent to the result of ikine.

Pose of the manipulator derived from the solution above:



Convert to angle system:

```
q =  
  
    30.0004   -70.0008   -35.5014    46.7962   -19.9991    24.9986
```

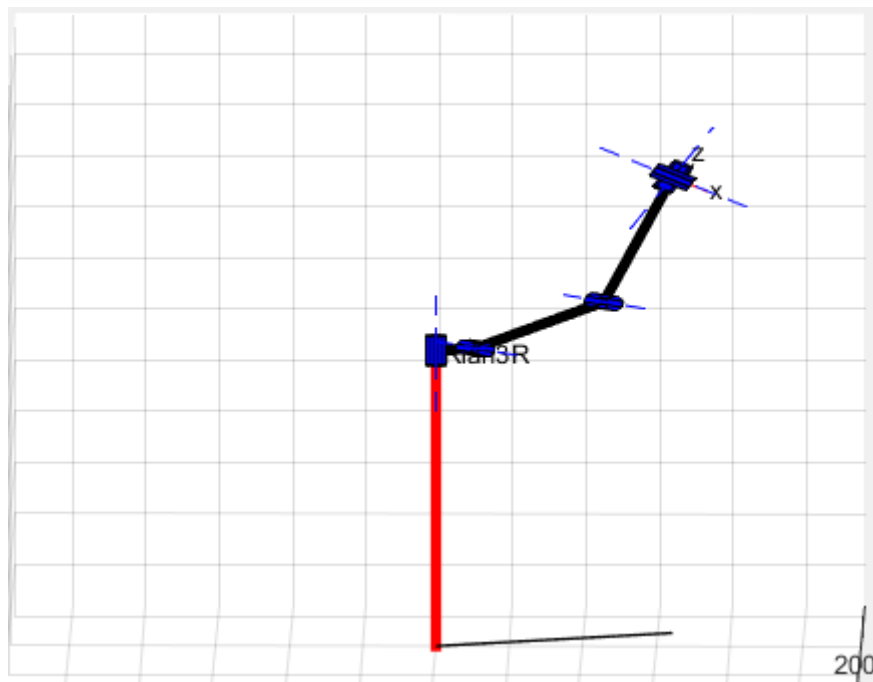
We find theta2 is out of range, so it is an invalid pose for the manipulator.

Another solution of T1

$\theta =$

0.5236 -0.3672 -2.1740 1.0566 -0.4962 1.5212

Pose of the manipulator derived from the solution above:



It is easy to find that two solutions have the same position of the end effector and are in the pose as we expected.

Convert to angle system:

$q =$

30.0004 -21.0362 -124.5593 60.5391 -28.4278 87.1582

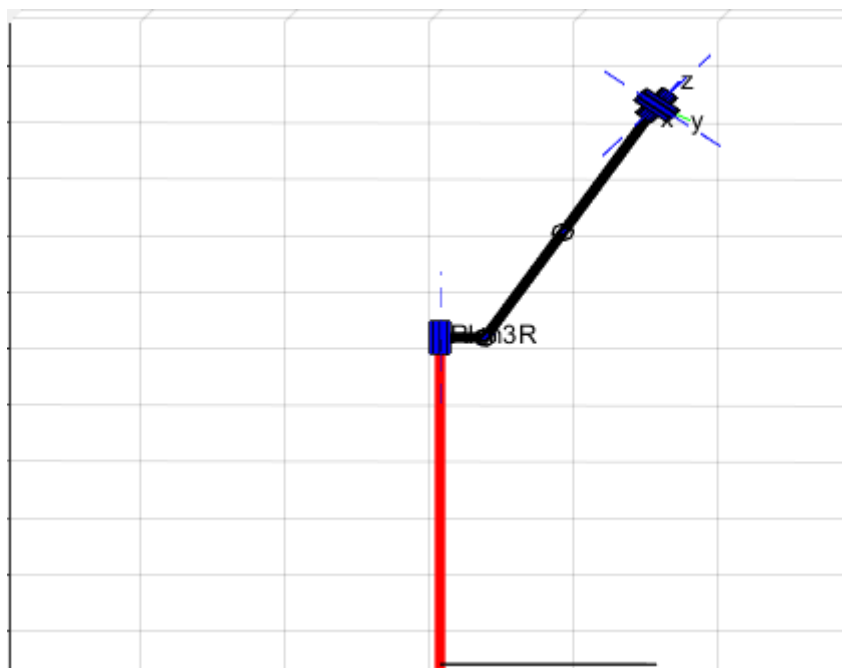
All the angles are in working range.

solution of the T2 (T2 has only one solution because the end effector is at singularity point)

$q =$

0 -1.0472 -1.3968 1.3962 -0.3490 0.5235

Figure derive by “drivebot()” function:



Convert to angle system:

$q =$

0 -60.0001 -80.0307 79.9964 -19.9962 29.9943

All the angles are in working range.

T3 has no solution, because it doesn't satisfy the condition $L_2 + L_3 \geq \sqrt{Z^2 + L^2}$, which means the pose presented by the transformation matrix is out of the reach of the manipulator.

```
>> sqrt(z^2+Len^2)

ans =

    2.6086e+03

>> Len2+Len3

ans =

    2.3746e+03

>> if(cmp1>cmp2)

    fprintf('out of reach');
else
    theta3=acos((z^2+Len^2-Len2^2-Len3^2)/(2*Len2*Len3))-atan2(1280,225)
    fprintf('theta3=%d\n',theta3)
end
out of reach>>
```

With all the results we get, it is safe to say that our algorithms work well.

CONCLUSION

In this paper, focusing on the kinematics of the industrial robot, we discussed a standard way to get the forward transformation matrix based on a 6 DOF manipulator. Also, we introduced a partially geometric and partially algebraic method to derive the inverse solution of the robot. All the algorithms are implemented via MATLAB programs, and are proved correct by the results. The method has the two following distinguishing features: (1) simple and easy to understand. (2) small amount of calculation. (3) able to derive multiple solutions.

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