



*College of Engineering*  
**Swansea University**

# **Dynamics & Earthquake Analysis of Structures**

## **Question Sheet 2 – Solutions**

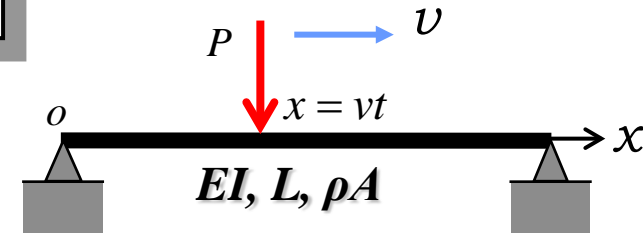
**(Q1, 2 and 3 only)**

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# Question 1

A point load  $P = 1 \text{ kN}$  moves along with constant speed  $v = 10 \text{ m/s}$  on a simply supported beam of length  $L = 10\pi \text{ m}$  as shown in the figure. The beam is made of **concrete**, has a **rectangular section** of height  $1 \text{ m}$  and an average density of  $2,800 \text{ kg/m}^3$ .

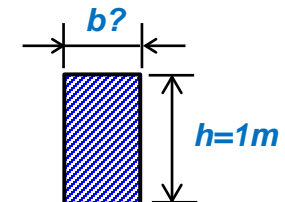
Determine: (a) the **deflection** of the beam as a function of time; (b) the **dynamic magnification factor**; and (c) the **maximum bending moment** at the central section.



The moving force:  $P\delta(x - vt)$

The default shape function:

$$\psi(x) = \sin(\pi x / L)$$



$$A = bh = b$$

$$I = \frac{bh^3}{12} = \frac{b}{12}$$

- From Q2(a) solution 1 in Sheet 1, the natural frequency:

$$\omega^2 = \pi^4 \frac{EI}{\rho AL^4} = \pi^4 \frac{E\cancel{b}/12}{\rho\cancel{b}L^4} = \pi^4 \frac{14 \times 10^9 / 12}{2800(10\pi)^4} = 41.7 \quad \therefore \omega = 6.45 \text{ 1/s}$$

*Independent of the width!*

- The equivalent force:  $F(t) = P \sin(\pi vt / L) = \sin(t) \quad (0 \leq t \leq L / v = \pi)$
- The SDOF equation:  $m\ddot{u}_o + ku_o = \sin(t) \quad (0 \leq t \leq L / v = \pi)$

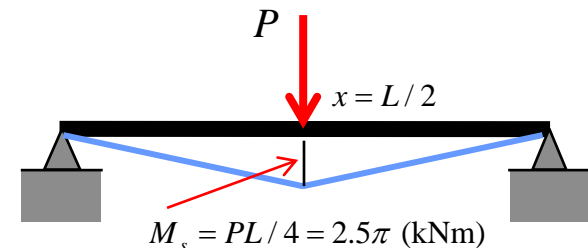
(a) The dynamic solution: See the expression on **Slide No 52**

(b) The dynamic amplification factor (**Slide No 52**):  $D_f \approx 1.8$

(c) The maximum static bending moment  $M_s$  when  $P$  at  $x=L/2$

The maximum dynamic bending moment  $M_d$

$$\underline{M_d = D_f M_s} \approx 14.237 \text{ kNm}$$

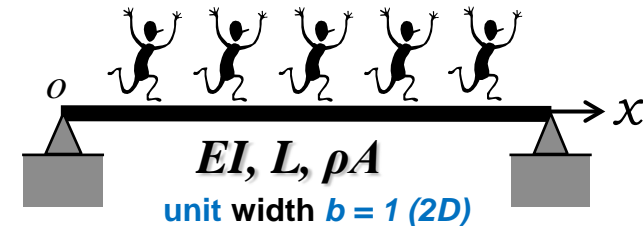


## Question 2

### Rhythmic Activities (BS 6399)

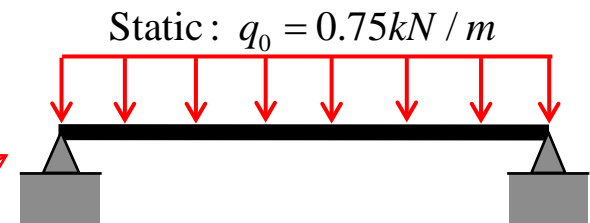
A concrete ribbed slab floor spans **9m** and has an average mass of **500 kg/m<sup>2</sup>**. The floor is simply supported on either side and has a natural frequency of vibration of **6.3 Hz**. The floor is to be used for aerobics and other similar rhythmic activities at frequencies ranging from **1.5 Hz to 2.5 Hz** and with contact ratios  $\alpha$  between **0.5** and **1**. During these activities the average imposed load will remain below **0.75 kN/m<sup>2</sup>** (before applying dynamic magnification) and the damping ratio is taken to be **3%**.

- Determine the **maximum possible resonant displacement** and the resulting **peak acceleration** and **bending moment** per **unit width**;
- If the floor has been designed for a service load of **5kN/m<sup>2</sup>**, determine its **suitability** for the proposed use.



The natural frequency:  
 $f = 6.3\text{Hz}$ ;  $\omega = 2\pi f = 39.58 \text{ 1/s}$   
 $\rho A = 500\text{kg} / \text{m}^2$ ;  $\xi = 3\%$

The force imposed by the activities



- The force imposed by the activities is consider as a UDL.
- The force frequency:  $\Omega_f = 1.5 \sim 2.5\text{Hz}$ ;  $T_f = 2\pi / \Omega_f$
- The contact ratio:  $\alpha = 0.5 \sim 1$
- For a given force frequency  $\Omega_f$ , the frequencies of harmonic forces are:  
 $\Omega_f, 2\Omega_f, 3\Omega_f, \dots, n\Omega_f, \dots$

When **one** of these frequencies is **equal to** the natural frequency  $f$ , a **resonance** happens!

Continued

## Question 2

■ The resonance condition:

$n=1$ :  $\Omega_f = 6.3\text{Hz} > 2.5\text{Hz}$ ; Too large ✗

$n=2$ :  $\Omega_f = 3.15\text{Hz} > 2.5\text{Hz}$ ; Too large ✗

$n \geq 5$ :  $\Omega_f < 1.5\text{Hz}$ ; too small ✗

$$f = n\Omega_f \quad (n=1, 2, 3, \dots)$$

$$f = 6.3\text{Hz}$$

$$\Omega_f = 1.5 \sim 2.5\text{Hz}$$

$n=3$ :  $\Omega_f = 2.1\text{Hz}$ ; valid ✓

$n=4$ :  $\Omega_f = 1.575\text{Hz}$ ; valid ✓

Two possible cases

■ Compute  $D_f$  for Case 1:  $\Omega_f = 2.1\text{Hz}$

Taken a particular contact ratio:  $\alpha = 2/3$

$$D_f = \sqrt{1 + \left(\frac{F_1}{F_0} H_1\right)^2 + \left(\frac{F_2}{F_0} H_2\right)^2 + \dots + \left(\frac{F_n}{F_0} H_n\right)^2 + \dots} = \sqrt{1 + \sum_{n=1}^{\infty} \left(\frac{F_n}{F_0} H_n\right)^2} = \sqrt{1 + \sum_{n=1}^{\infty} D_{f,n}^2} \quad (\text{Slide No. 57})$$

From the 1<sup>st</sup> row of the Table on Slide No. 57:

$$H_n = \frac{1}{\sqrt{(1 - \gamma_n^2)^2 + 4\xi^2 \gamma_n^2}}; \quad \gamma_n = \frac{n\Omega}{\omega} = \frac{n\Omega_f}{f}$$

$$\frac{F_1}{F_0} = 1.29; \quad \frac{F_2}{F_0} = 0.16; \quad \frac{F_3}{F_0} = 0.13; \quad \frac{F_4}{F_0} = 0.04$$

$$\gamma_1 = \frac{\Omega_f}{f} = \frac{1}{3}; \quad \gamma_2 = \frac{2\Omega_f}{f} = \frac{2}{3}; \quad \gamma_3 = \frac{3\Omega_f}{f} = 1; \quad \gamma_4 = \frac{4\Omega_f}{f} = \frac{4}{3}$$

$$H_1 = 1.5; \quad H_2 = 3.0; \quad H_3 = 16.67; \quad H_4 = 0.34$$

$$D_f = 3.1 \quad \checkmark$$

■ Compute  $D_f$  for Case 2:  $\Omega_f = 1.575\text{Hz}$

$$D_f = ? \quad \times$$

So Case 1 is the worse case:  $D_f = 3.1$

Continued

## Question 2

(a) The maximum displacement:  $u_{\max} = D_f u_s$

$$u_s = \frac{5q_0 L^4}{384EI} \quad EI = ?$$

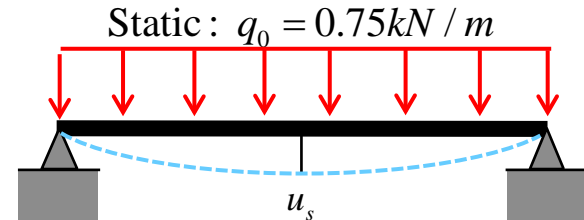
From Q2(a) solution 1 in Sheet 1, the natural frequency

$$\omega^2 = \pi^4 \frac{EI}{\rho A L^4} \longrightarrow \frac{L^4}{EI} = \frac{\pi^4}{\rho A \omega^2} \longrightarrow$$

The maximum displacement:  $u_{\max} = D_f u_s = \underline{3.72mm}$

The maximum acceleration:  $a_{\max} = \omega^2 u_{\max} = \underline{5.826m/s^2}$

The maximum bending moment:  $M_{\max} = D_f M_s = \underline{23.54kNm}$



The maximum static displacement

$$u_s = \frac{5\pi^4 q_0}{384\rho A \omega^2} = \underline{1.2mm}$$

The maximum static bending moment

$$M_s = \frac{q_0 L^2}{8} = 7.59kNm$$

(b) The **suitability** of the structure – **Safety** check

The dynamic UDL load:

$$q_d = D_f q_0 = 3.1 \times 0.75 = 2.33kN/m < q_{\max} = \underline{5kN/m}$$

Safe!



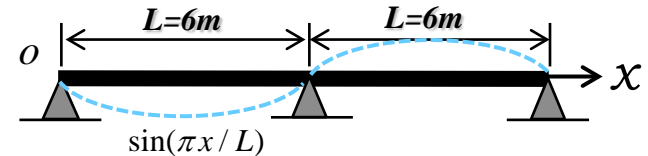
Alternatively, compute the maximum bending moment under the designed service load  $q_{\max}$  and compare it with  $M_{\max}$

A **12m** long rail bridge has the continuous beam configuration shown in the figure, an average flexural stiffness  **$EI=5GNm^2$** , a mass per unit length of  **$100,000\text{ kg/m}$**  and a damping ratio of **2%**.

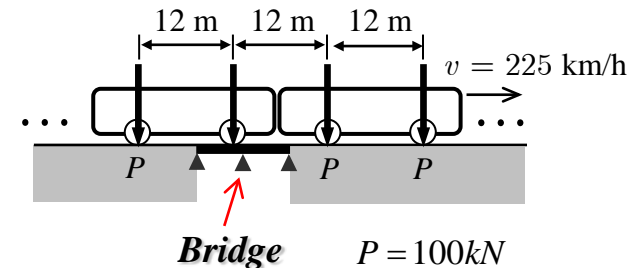
a) Using Rayleigh's method with an appropriate sinusoidal function, obtain its fundamental **frequency** of vibration.

b) Determine the **equivalent modal force** that results from the motion of a train consisting of an '**infinite**' number of  **$100kN$**  point loads separated by equal distances of **12m** and travelling at a constant speed of  **$225\text{ km/h}$** .

c) Obtain the **dynamic amplification factor** for the above train of loads.



$$EI = 5GNm^2; \rho A = 10^5 \text{ kg / m}; \xi = 2\%$$



a) The shape function:  $\psi(x) = \sin(\pi x / L)$  (Check it satisfies the boundary conditions)

$$m = \int_0^{2L} \rho [\psi(x)]^2 A dx = \rho A \int_0^{2L} \sin^2\left(\frac{\pi x}{L}\right) dx \quad k = \int_0^{2L} EI [\psi''(x)]^2 dx$$

$$\omega^2 = \pi^4 \frac{EI}{\rho AL^4} \quad \longrightarrow \quad \omega = \underline{61.3 \text{ 1/s}}$$

## b) The equivalent force

The  $n^{\text{th}}$  point force  $P_n(t) = P\delta(x - x_n(t))$

The *equivalent* force  $F_n(t) = P \sin(\pi x_n / L)$

The *total equivalent* force  $F(t) = \sum_n F_n(t) = P \sum_n \sin(\pi x_n / L)$

- 1<sup>st</sup> Force: Starts at the left end at  $t = 0$

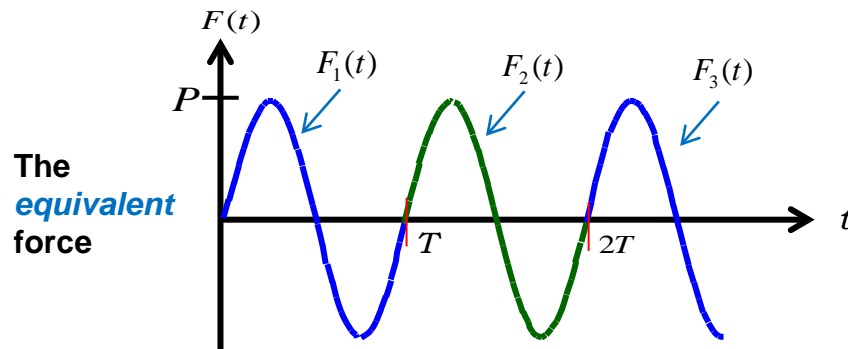
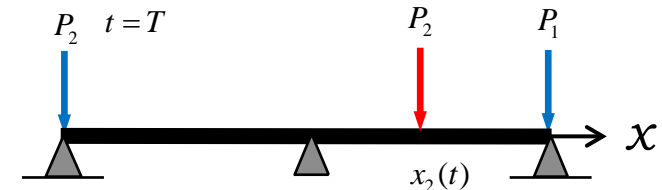
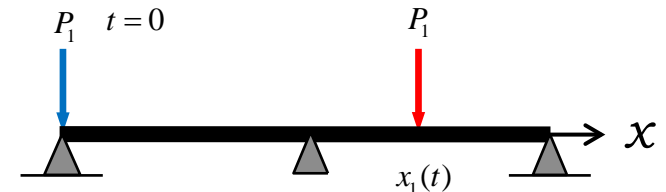
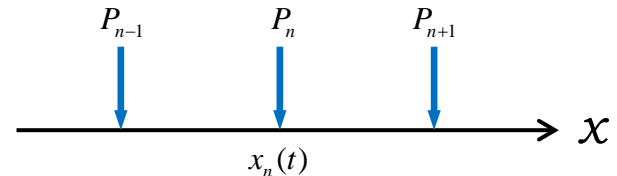
$$x_1(t) = vt \quad 0 \leq t \leq T = 2L/v$$

- 2<sup>nd</sup> Force: Enters the bridge at  $t = T$   
while 1<sup>st</sup> force is about to leave

$$x_2(t) = v(t - T) \quad T \leq t \leq 2T$$

- $n^{\text{th}}$  Force

$$x_n(t) = v[t - (n-1)T] \quad (n-1)T \leq t \leq nT$$



## A Harmonic Force

$$F(t) = \sum_n F_n(t) = P \sin(\pi vt / L)$$

$$\Omega = \pi v / L = 32.72 \text{ 1/s}$$

## c) The dynamic amplification factor

$$D_f = H = \frac{1}{\sqrt{(1-\gamma^2)^2 + 4\xi^2\gamma^2}}$$

$$\gamma = \frac{\Omega}{\omega} = \frac{32.72}{61.3} = 0.5338$$

$$\underline{D_f = 1.3978}$$

## The Harmonic Force

$$F(t) = \sum_n F_n(t) = P \sin(\pi vt / L)$$

$$\Omega = \pi v / L = 32.72 \text{ 1/s}$$

