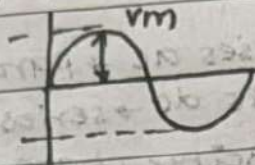


RECTIFIERS

AC → pulsating DC

$$v_{in} = v_m \sin \omega t$$



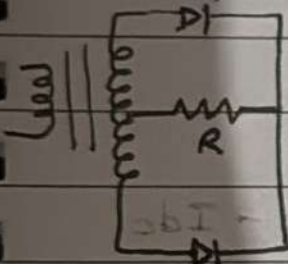
HALFWAVE
 $v_{avg} = \frac{\text{Area of curve}}{\text{base}}$

$$= \frac{\int_0^{2\pi} v_m \sin \omega t d\omega t}{2\pi}$$

$$V_a = \frac{V_{avg}}{V_{dc}} \frac{V_m}{\pi} \quad \text{also } I_o = \frac{I_m}{\pi}$$

FULL WAVE

centre-tap



$$PIV \geq 2V_m$$

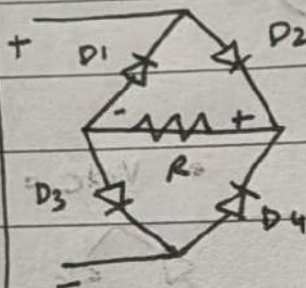
$$V_o = V_m$$

non-ideal

$$PIV \geq 2V_m - V_K$$

$$V_o = V_m - V_K$$

bridge wave



ideal

$$V_o = V_m$$

$$PIV \geq V_m$$

Non-ideal

$$V_o = V_m - 2V_K$$

$$PIV \geq V_m - V_K$$

$$V_{rms} = \left[\frac{1}{2\pi} \int_0^{2\pi} (v_m \sin \omega t)^2 d\omega t \right]^{1/2}$$

$$= \left[\frac{V_m^2}{2\pi} \int_0^{2\pi} \frac{1 - \cos 2\omega t}{2} d\omega t \right]^{1/2}$$

$$= \frac{V_m}{\sqrt{2}} = V_{rms} \text{ [HWR]}$$

non-ideal

$$v_{avg} = \frac{V_m - V_K}{\pi}$$

$$V_{rms} = \frac{V_m - V_K}{\sqrt{2}}$$

ripple factor

$$r = \frac{V_{rms \text{ of ac}}}{V_{avg}} = \frac{\sqrt{V_{rms}^2 - V_{dc}^2}}{V_{dc}}$$

$$= 1.21$$

$$(V_{rms})_{ac} = [V_{rms}^2 - V_{dc}^2]^{1/2}$$

FWR

$$V_{dc} = \frac{1}{\pi} \int_0^{\pi} v_m \sin \omega t d\omega t = \frac{2V_m}{\pi}$$

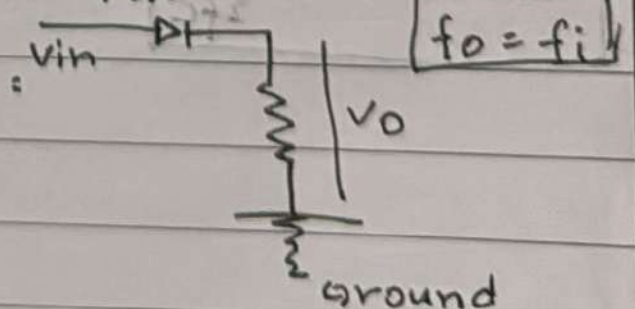
$$V_{rms} = \left[\frac{1}{\pi} \int_0^{\pi} (v_m \sin \omega t)^2 d\omega t \right]^{1/2}$$

$$V_{rms} = \frac{V_m}{\sqrt{2}}$$

$$\sigma = 0.48$$

$$f_o = 2f_i$$

$$\eta = \frac{P_{dc}}{P_{ac}} = \frac{\text{load deliver}}{\text{input}}$$



SEMICONDUCTORS

DATE

• **Intrinsic conductors.**
pure semiconducting materials without any significant impurities.

→ e^- gain energy as $T \uparrow$, E_T jump from valence to conduction band leaving behind holes.

thermal generation of e^- -h pair

At thermal equilibrium $n_i = n_e = n_h$

PLN joined

Diode → conducts current in

only one way $p \rightarrow n$.

No-bias → minority charge carriers combine, resulting in lack of free carriers near junction forming a depletion layer.

net flow of charge = 0A.

V_{oc}

Reverse → $+ve \rightarrow n$, $+ve \rightarrow p$ results in widening of depletion layer as e^- in n and h^+ in p are drawn to their terminals.

this establishes a barrier to great for a carrier to overcome.

• the **minority charge carriers** result in **reverse saturation current** I_s

forward → $+ve \rightarrow p$ $-ve \rightarrow n$

the application of voltage will pressure the e^- in n type and h^+ in p type to recombine with ions near the layer causing the layer to reduce. This results in heavy majority carrier flow while I_s remains unaffected

avalanche → high V_R across RB region, velocity of minority carriers responsible for I_s increases. The energy gain will result in minority carriers colliding with the lattice. Ionisation takes place

ve^- of atoms absorb energy to leave parent atom, causing multiplication of carriers. Avalanche multiplication occurs and avalanche current is produced.

zener → quantum mechanical tunnelling. e^- pulled into CB. due to strong electrical fields that generate carriers.

P_{IV} → maximum reverse bias potential that can be applied before entering breakdown region. **Peak Inverse.**

I_s doubles for every $10^\circ C \uparrow$.

• **Voltage V_B decreases by 2.5mV by every $1^\circ C$ increase**

Avalanche		Zener		V_T at $25^\circ C$ 25.7mV
$T \uparrow$	$V \uparrow$	$T \uparrow$	$V \downarrow$	

• **Intrinsic conductors.**
semiconductor materials in which impurities are added to alter electrical properties.
Doping: process of adding impurities to pure semiconductor to increase conductivity.

DOPANTS

pentavalent	trivalent
n type	p type
sc with e^- as majority charge carriers as they are doped with pentavalent imp. (antimony, phosphorus, arsenic)	sc with holes as majority charge carriers as they are doped with trivalent imp. (boron, gallium, indium).
• donor atom gains $+ve$ charge	• Acceptor ion $+ve$ charge

Shockley's Eq.

$$I_D = I_s \left[e^{\frac{qV_D}{kT}} - 1 \right]$$

where $\frac{kT}{q} = V_T$ thermal voltage

$$I_D = I_s \left[e^{\frac{V_D}{nV_T}} - 1 \right]$$

where n = ideality factor

$$k = 1.38 \times 10^{-23} \text{ J/K}$$

Boltzmann

$$k = \text{Kelvin } q = 1.6 \times 10^{-19}$$

$$I_2 = I_1 \times 2^{\frac{(T_2 - T_1)}{10}}$$

→ I saturation current

forward current rating → max current that can flow without damaging diode.

As $T \uparrow$, $V_K \downarrow$ → voltage required to conduct current
→ min voltage required to break depletion layer
→ V at which current starts flowing rapidly.

T_s for $1^\circ C$

$$T_s = 1.0718$$

RESISTANCE

DC

application of dc voltage to s.c diode → results in an operating point that remains unaffected with time.

AC

$$R_D = \frac{V_D}{I_D}$$

resistance at and below V_K will be greater than the R from vertical graph.

application of sinusoidal input causes a operating pt to vary up and down.

$$R_{ac} = \frac{\Delta V_{ac}}{\Delta I_{ac}}$$

$$r_d = \frac{26mV}{I_d}$$

only for vertical rise

Average Resistance

If input produces a broad swing (large variation).

$$r_{avg} = \frac{\Delta V_d}{\Delta I_d} \bigg|_{pt - pt} = \frac{V_2 - V_1}{I_2 - I_1}$$

Diode Approx

- 1) open switch | close (ideal diode)
- 2) $R_B \rightarrow$ open | $FB \rightarrow$ cell (simplified)
- 3) piece-wise → consider resistance after diode.

diode → results
 forward current + max current
 voltage required to break down rapidly
 conduct to break down rapidly
 current that can flow without damaging
 saturation current I_s
 $I_2 = I_1 \times 2$
 $\frac{Q_1}{(I_1 - I_s)}$

CLIPPERS

DATE

SERIES

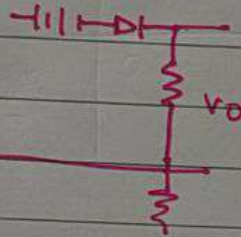
unbiased

- FB → nsc
- RB → psc



biased

- (voltage applied)
- FB → nsc



nsc

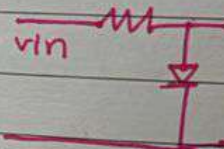
(negative series clipper)

psc

PARALLEL

unbiased

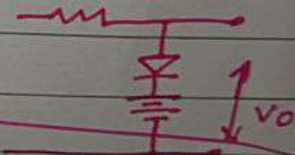
- FB → psc
- RB → nsc



biased

voltage applied

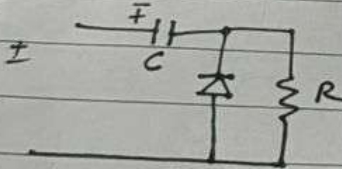
- clips
- ps → V
- and ns → Ven



CLAMPERS

AC → DC

$T = RC$ → how fast capacitor charges or discharges.



FILTERS

shunt capacitor
capacitor blocks dc and passes ac → parallel

inductor blocks ac and passes dc → series

T = time required for capacitor charge & discharge.

$$T = RC$$

EXP

FWR

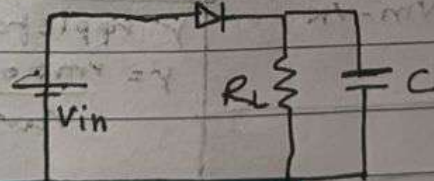
$$\gamma = \frac{1}{4\sqrt{3} f C R_L}$$

$C \uparrow \quad \gamma \downarrow$

$$V_{r(rms)} = \frac{I_{dc}}{4\sqrt{3} f C}$$

HW R

$$\gamma = \frac{V_{r(rms)}}{V_{dc}}$$



$$\gamma = \frac{1}{2\sqrt{3} f C R_L}$$

$$V_{rms} = \frac{I_{dc}}{2\sqrt{3} f C}$$

$$V_{dc} = V_m - \frac{I_{dc}}{2 f C}$$

$$V_{dc} = V_m - \frac{I_{dc}}{4 f C}$$

