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Unit 2 - Semiconductor Diode applications – Class 21 - Block diagram of regulated power supply, and Half wave rectifier working Principles

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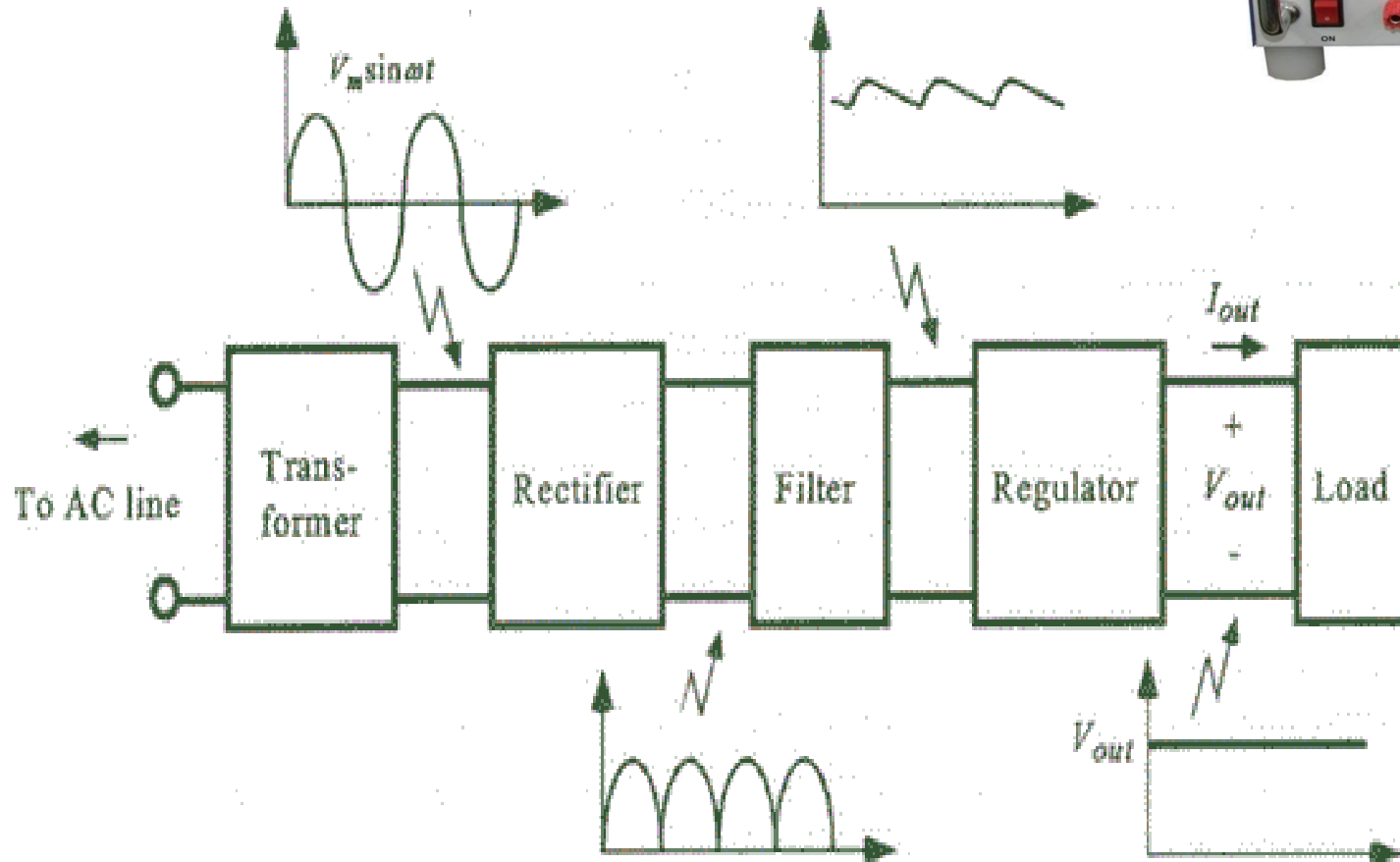
ELECTRONIC PRINCIPLES AND DEVICES

Unit 2 - Class 21 - Block diagram of regulated power supply, and Half wave rectifier working Principles – Text book reference – Section 15.1 – pages 773 to 775

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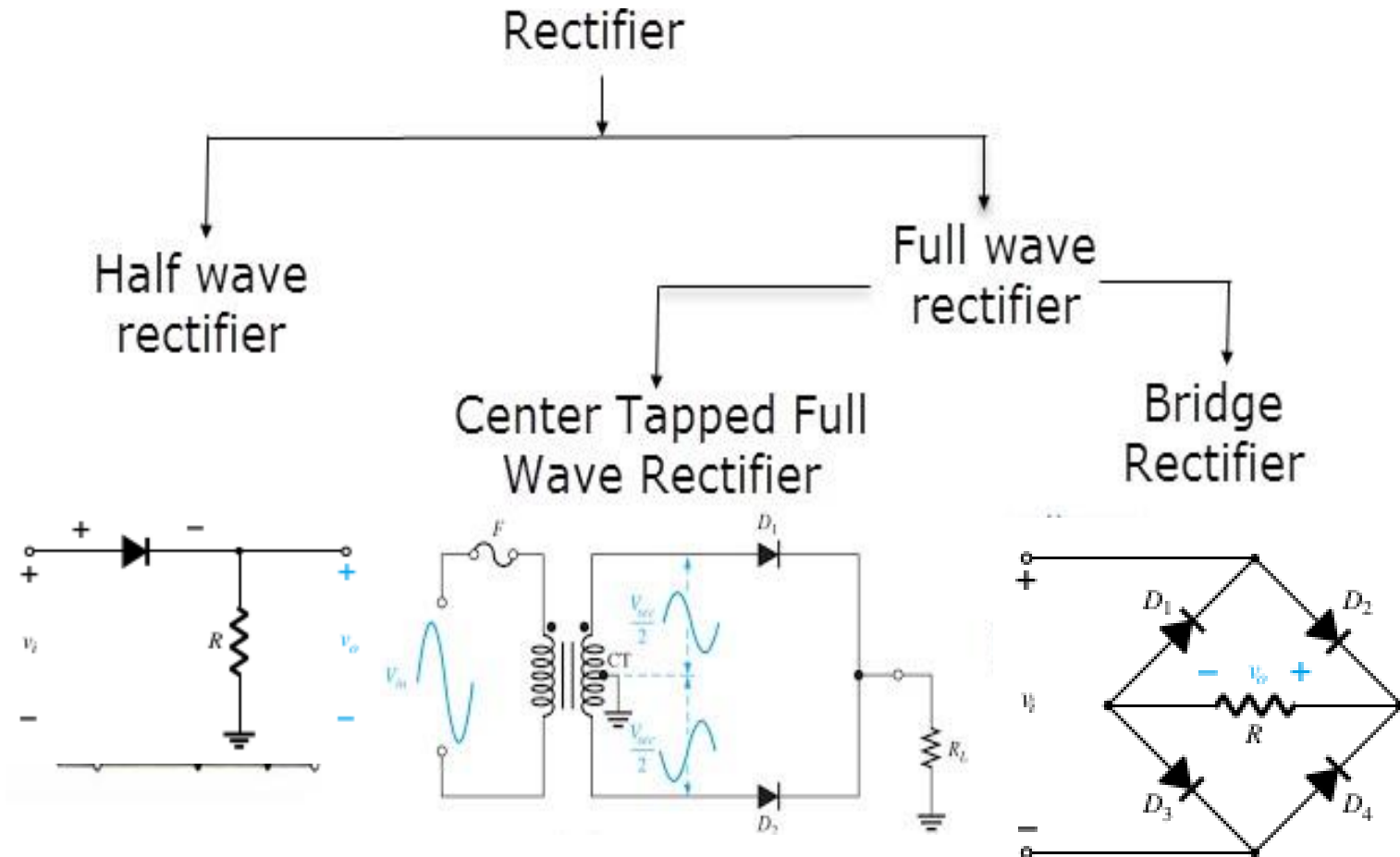
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Unit 2 – Class 21 - Regulated Power Supply



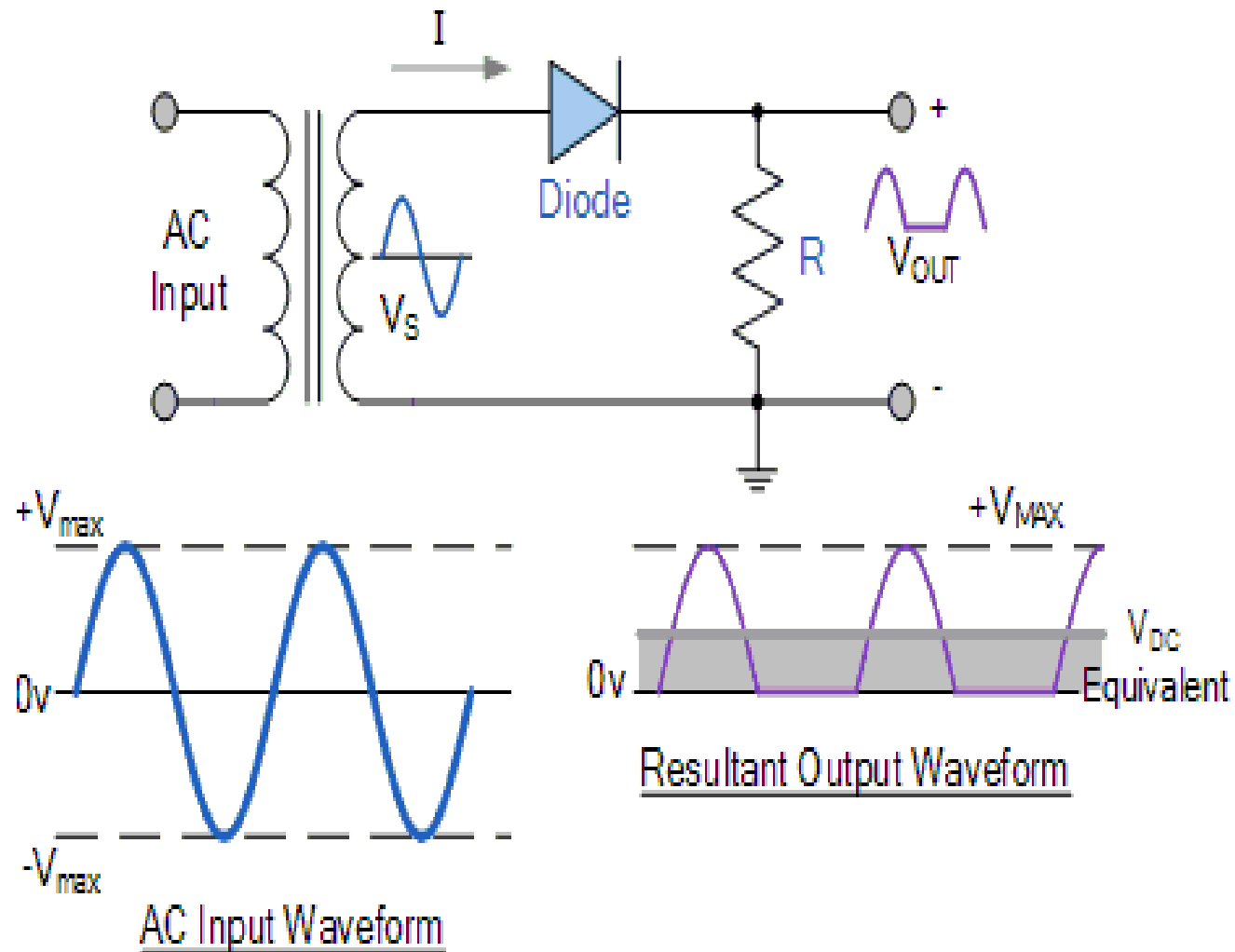
Regulated power supply converts an alternating signal into a constant DC signal.

- **Transformer** : The output sinusoid voltage is either step-up or step-down from the input sinusoid voltage value
- **Rectifier** : Converts an alternating current into a direct one by allowing a current to flow through it in one direction only.
- **Filter** : Removes the AC ripples from the DC signal obtained from the rectifier.
- **Regulator** : Converts DC voltage into a lower constant voltage



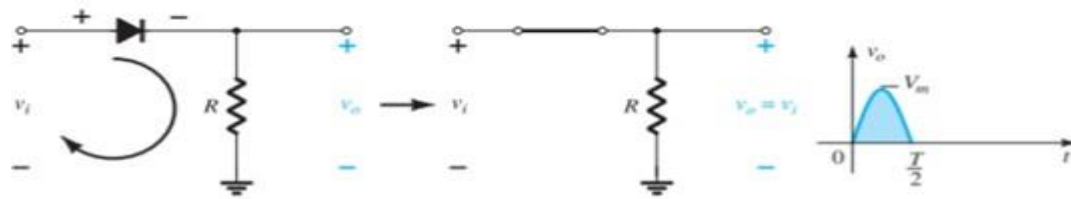
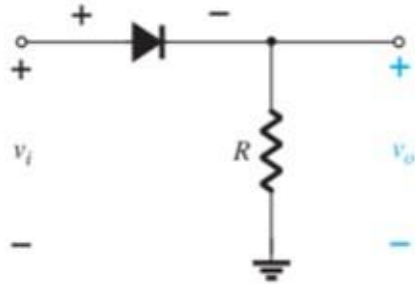
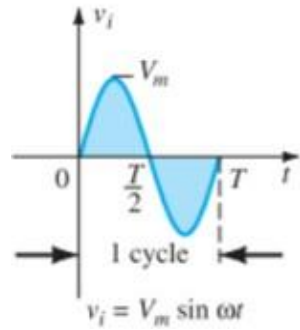
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Half Wave Rectifier

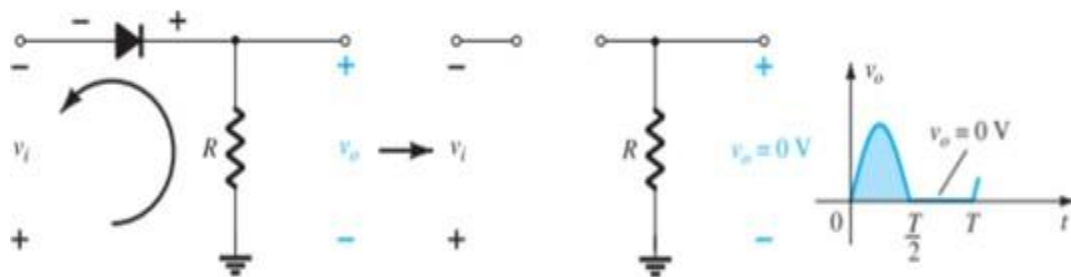


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Half Wave Rectifier contd.



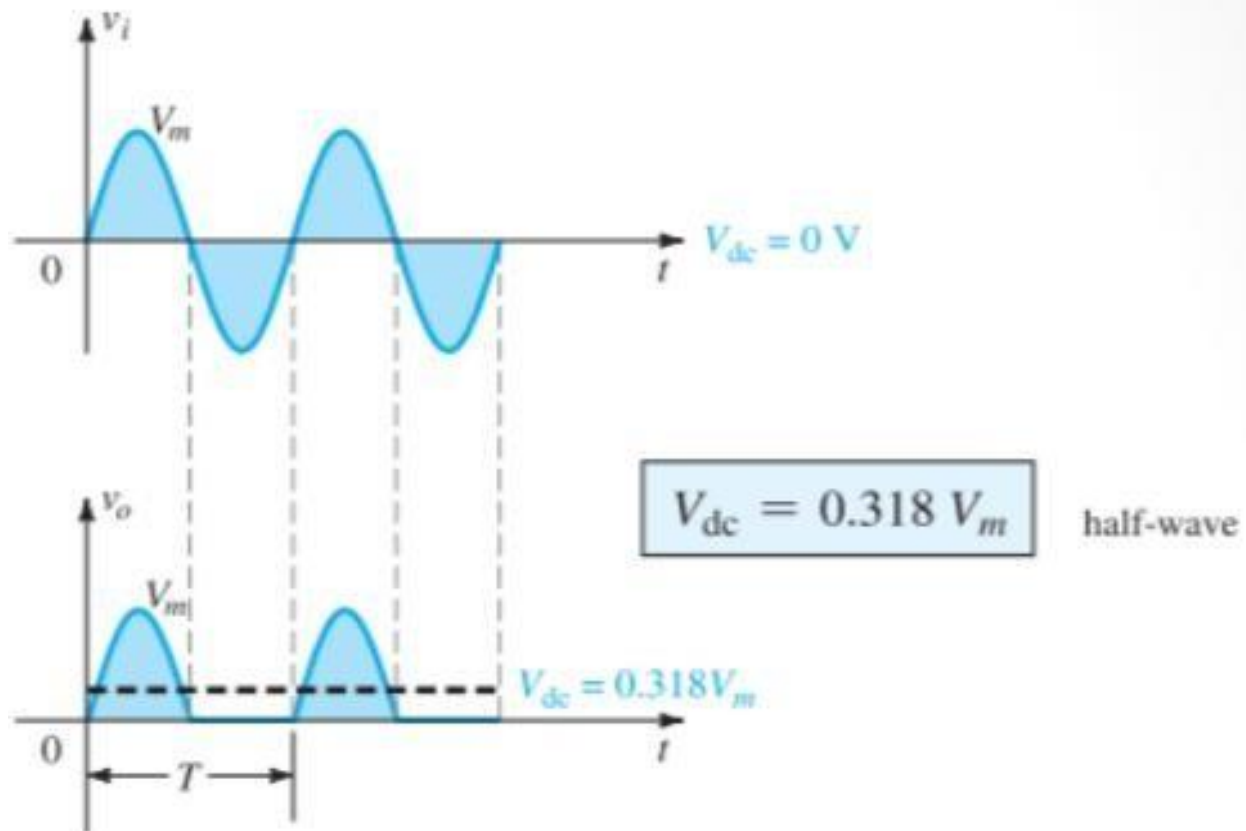
Conduction region ($0 \rightarrow T/2$).



Nonconduction region ($T/2 \rightarrow T$).

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Half Wave Rectifier contd.

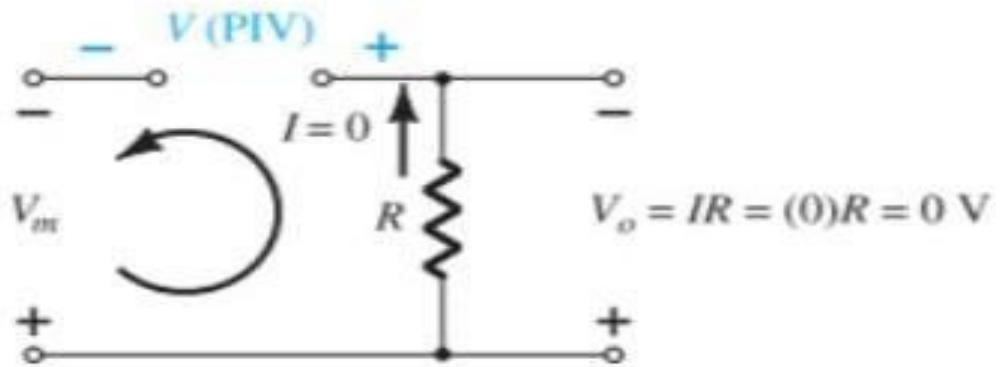


Half-wave rectified signal.

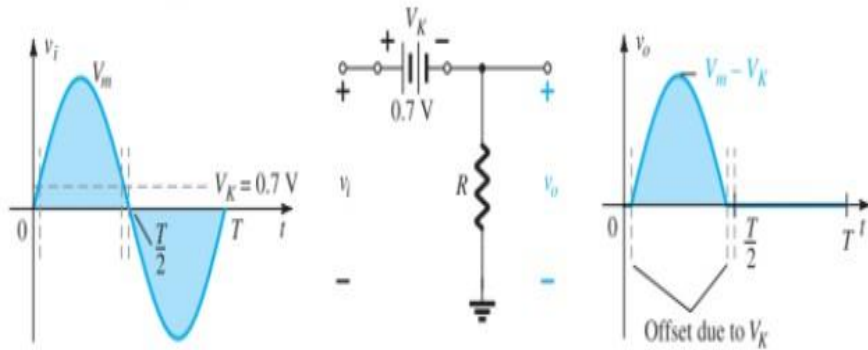
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Half Wave Rectifier contd.

PIV rating $\geq V_m$ half-wave rectifier



Effect of V_K on half-wave rectified signal.



Cross Over distortion

$$V_{dc} \cong 0.318(V_m - V_K)$$



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Unit 2 - Semiconductor Diode applications – Class 22 - Half wave rectifier – V_{dc} , I_{dc} , ripple factor & PIV

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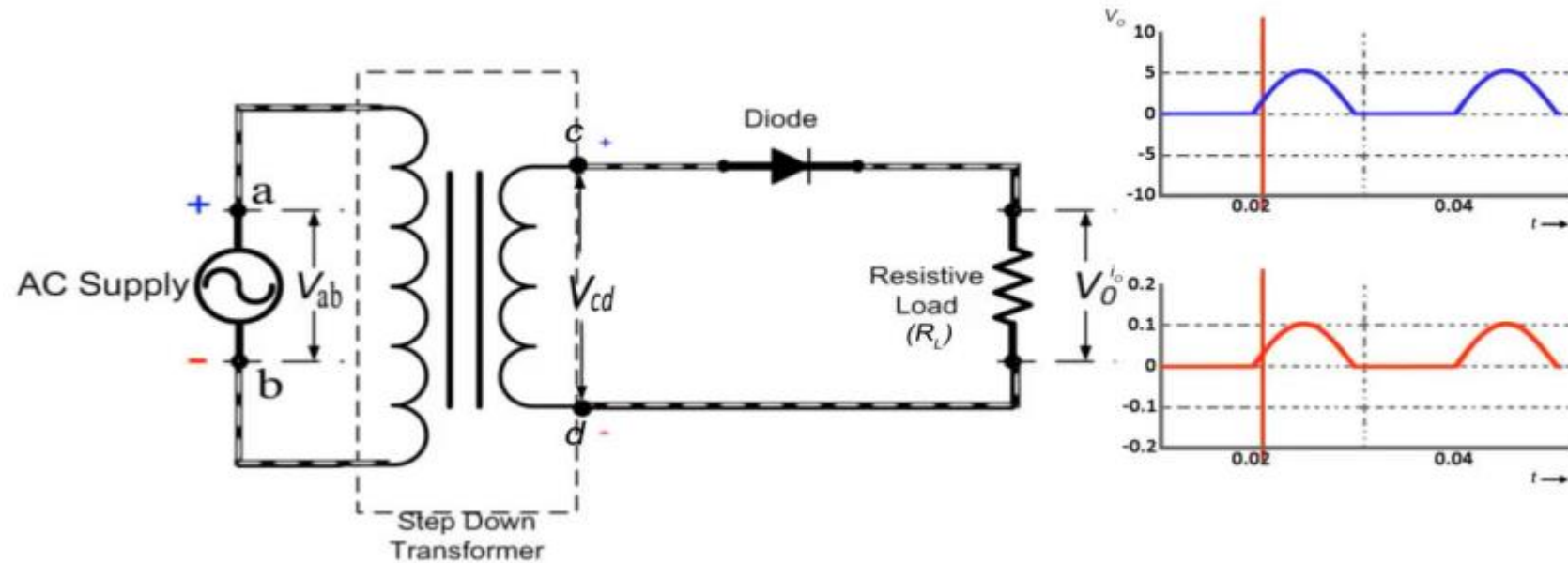
Unit 2 - Semiconductor Diode applications – Class 22 -
Half wave rectifier – V_{dc} , I_{dc} , ripple factor & PIV – text
book reference – section 2.6 – pages 76 to 78

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Unit 2 – Class 22 – HWR- V_{dc} , I_{dc} , ripple factor, PIV

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$$\text{Ripple Factor, } \gamma = \frac{\text{RMS value of AC component present in Rectifier Output}}{\text{Average Value of Rectifier Output}}$$

$$\gamma = \frac{I'_{rms}}{I_{dc}} = \frac{V'_{rms}}{V_{dc}}$$

where I'_{rms} and V'_{rms} are the rms value of alternating component of load current and voltage respectively.

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$$I'_{rms} = \sqrt{I_{rms}^2 - I_{dc}^2}$$

where I'_{rms} = rms value of AC Component

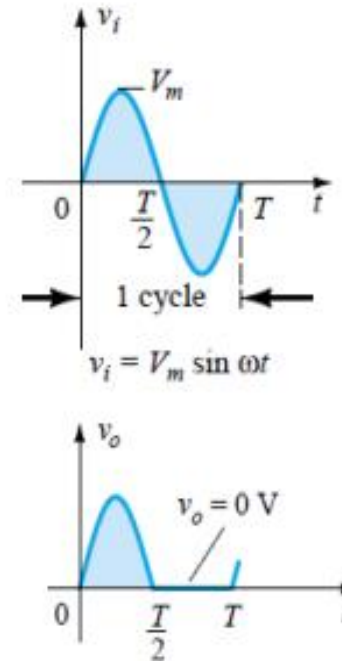
$$r = \frac{I'_{rms}}{I_{dc}} = \sqrt{\frac{(I_{rms}^2 - I_{dc}^2)}{I_{dc}^2}}$$

$$\boxed{r = 1.21} \quad \text{For HWR}$$

$$= \sqrt{\left(\frac{I_{rms}}{I_{dc}}\right)^2 - 1}$$

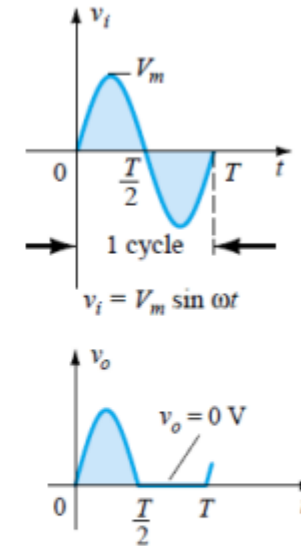
•T

$$\begin{aligned} V_{dc} &= \frac{1}{2\pi} \int_0^{2\pi} V_m \sin \omega t \, d\omega t \\ &= \frac{1}{2\pi} \int_0^{\pi} V_m \sin \omega t \, d\omega t \\ &= \frac{V_m}{2\pi} [-\cos \omega t]_0^{\pi} = \frac{V_m}{\pi} \end{aligned}$$



•T

$$\begin{aligned} V_{rms} &= \left[\frac{1}{2\pi} \int_0^{2\pi} (V_m \sin \omega t)^2 d\omega t \right]^{1/2} \\ &= \left[\frac{V_m^2}{2\pi} \int_0^{\pi} (\sin^2 \omega t) d\omega t \right]^{1/2} \\ &= \left[\frac{V_m^2}{2\pi} \int_0^{\pi} \left(\frac{1 - \cos 2\omega t}{2} \right) d\omega t \right]^{1/2} \\ V_{rms} &= \left[\frac{V_m^2}{2\pi} \left(\frac{\omega t}{2} - \frac{\sin 2\omega t}{2} \right)_0^{\pi} \right]^{1/2} = \frac{V_m}{2} \end{aligned}$$



•T

$$\begin{aligned} V_{ac} &= V - V_{dc} \\ V'_{rms} &= \left[\frac{1}{2\pi} \int_0^{2\pi} (V - V_{dc})^2 d\omega t \right]^{1/2} \\ &= \left[\frac{1}{2\pi} \int_0^{2\pi} (V^2 - 2V_{dc}V + V_{dc}^2) d\omega t \right]^{1/2} \\ &= [V_{rms}^2 - 2V_{dc}V + V_{dc}^2]^{1/2} \\ V'_{rms} &= [V_{rms}^2 - V_{dc}^2]^{1/2} \end{aligned}$$

•T

$$V'_{rms} = [V_{rms}^2 - V_{dc}^2]^{1/2}$$

$$= \left[\left(\frac{V_m}{2} \right)^2 - \left(\frac{V_m}{\pi} \right)^2 \right]^{1/2} = 0.385V_m$$

$$\text{Ripple Factor } (Y_{HW}) = \frac{V'_{rms}}{V_{dc}} = \sqrt{\left(\frac{V_{rms}}{V_{dc}} \right)^2 - 1} = \sqrt{\left(\frac{V_m/2}{V_m/\pi} \right)^2 - 1} = 1.211$$



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Unit 2 - Semiconductor Diode applications – Class 23 & 24 - Full wave rectifier configuration & working ;Vdc, Idc, ripple factor,PIV & comparison

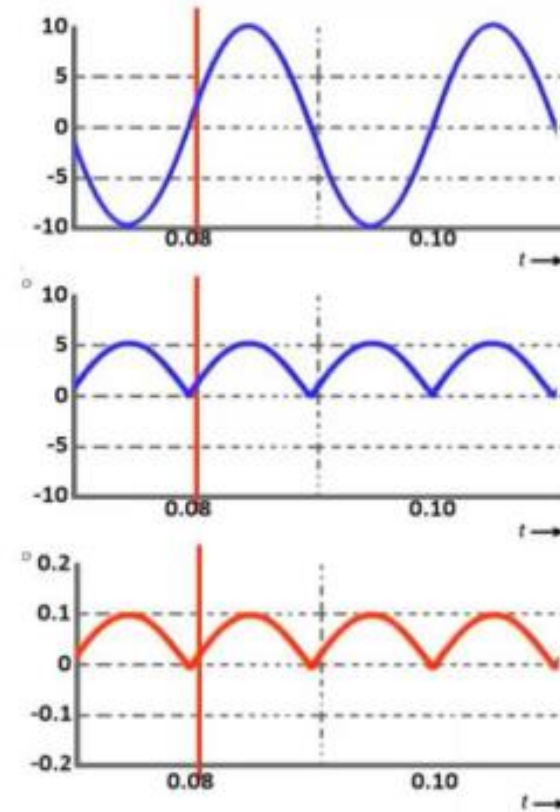
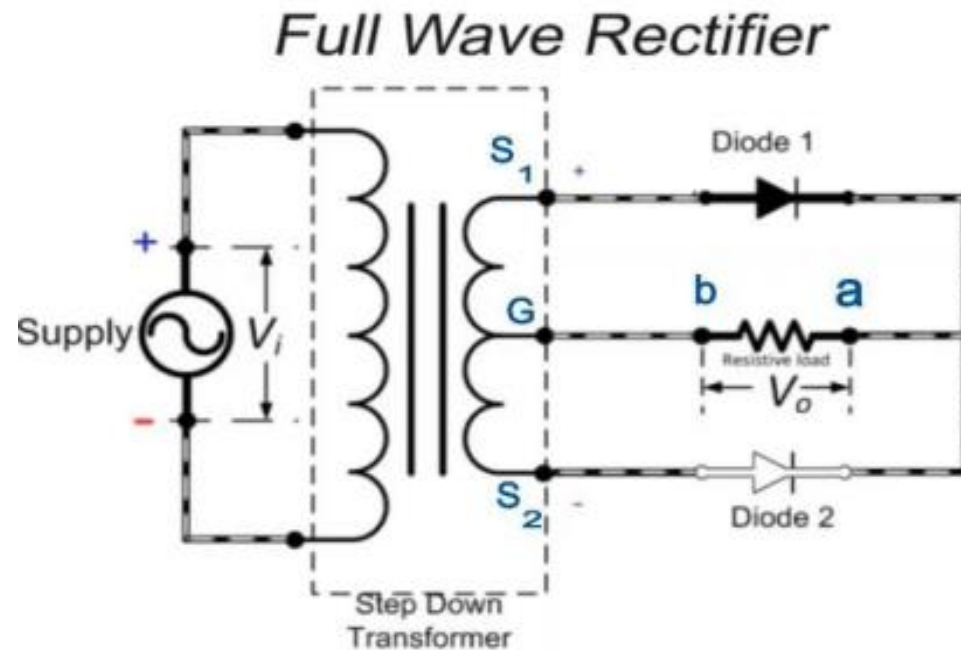
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Unit 2 - Semiconductor Diode applications – Class 23 & 24 - Text book reference – section 2.7 – pages 79 to 81

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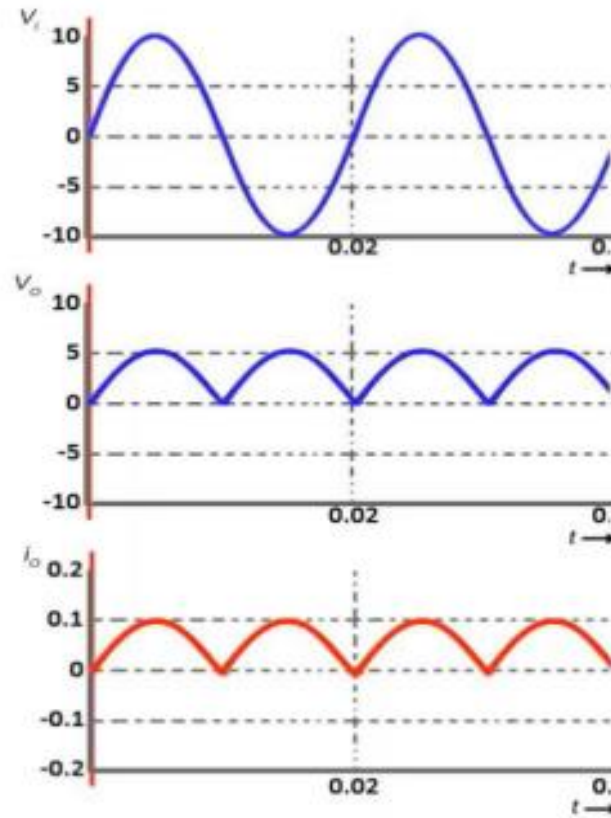
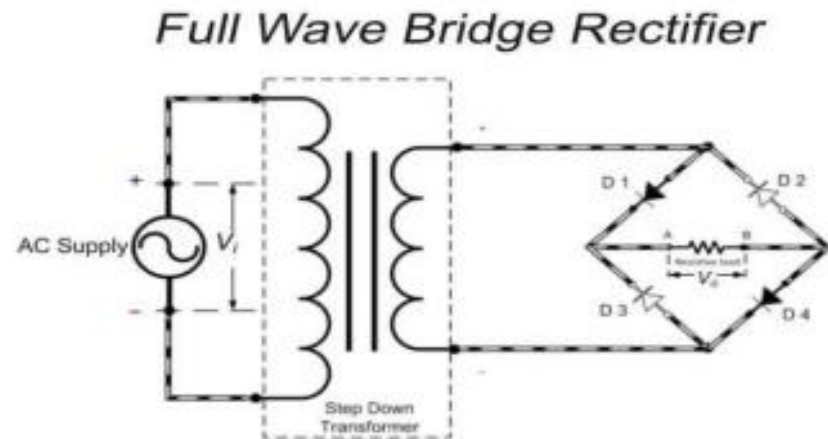
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ELECTRONIC PRINCIPLES AND DEVICES

Unit 2 – Class 23 & 24 – Full Wave Bridge Rectifier

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$$\text{Ripple Factor, } \gamma = \frac{\text{RMS value of AC component present in Rectifier Output}}{\text{Average Value of Rectifier Output}}$$

$$\gamma = \frac{I'_{\text{rms}}}{I_{\text{dc}}} = \frac{V'_{\text{rms}}}{V_{\text{dc}}}$$

where I'_{rms} and V'_{rms} are the rms value of alternating component of load current and voltage respectively.

•T

$$I'_{rms} = \sqrt{I_{rms}^2 - I_{dc}^2}$$

where I'_{rms} = rms value of AC Component

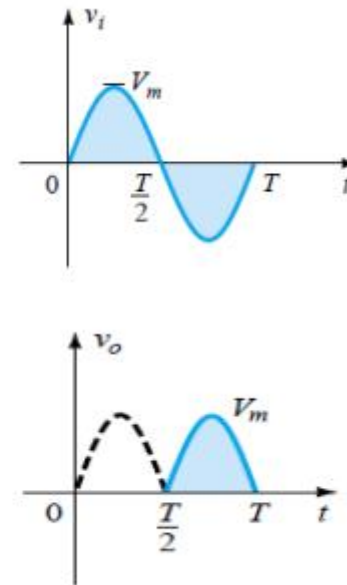
$$r = \frac{I'_{rms}}{I_{dc}} = \sqrt{\frac{(I_{rms}^2 - I_{dc}^2)}{I_{dc}^2}}$$

$$\boxed{r = 0.48} \text{ For FWR}$$

$$= \sqrt{\left(\frac{I_{rms}}{I_{dc}}\right)^2 - 1}$$

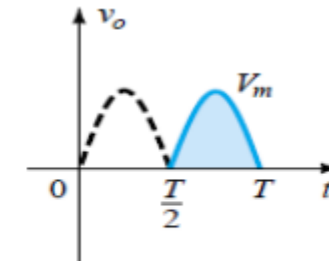
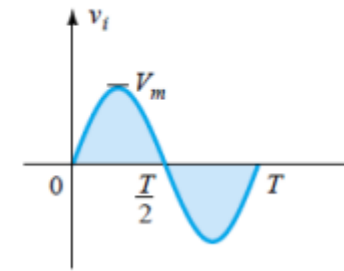
•T

$$\begin{aligned} V_{dc} &= \frac{1}{\pi} \int_0^{\pi} V_m \sin \omega t \, d\omega t \\ &= \frac{V_m}{\pi} [-\cos \omega t]_0^{\pi} \\ &= \frac{2V_m}{\pi} \end{aligned}$$



•T

$$\begin{aligned} V_{rms} &= \left[\frac{1}{\pi} \int_0^{\pi} (V_m \sin \omega t)^2 d\omega t \right]^{1/2} \\ &= \left[\frac{V_m^2}{\pi} \int_0^{\pi} \left(\frac{1 - \cos 2\omega t}{2} \right) d\omega t \right]^{1/2} \\ &= \left[\frac{V_m^2}{2\pi} \int_0^{\pi} (1 - \cos 2\omega t) d\omega t \right]^{1/2} \\ &= \left[\frac{V_m^2}{2\pi} \left(\omega t_0^{\pi} - \frac{\sin 2\omega t^{\pi}}{2} \right) \right]^{1/2} = \left[\frac{V_m^2}{2\pi} (\pi - 0) \right]^{1/2} = \frac{V_m}{\sqrt{2}} \end{aligned}$$



•T

$$\begin{aligned} V_{ac} &= V - V_{dc} \\ V'_{rms} &= \left[\frac{1}{2\pi} \int_0^{2\pi} (V - V_{dc})^2 d\omega t \right]^{1/2} \\ &= \left[\frac{1}{2\pi} \int_0^{2\pi} (V^2 - 2V_{dc}V + V_{dc}^2) d\omega t \right]^{1/2} \\ &= [V_{rms}^2 - 2V_{dc}V + V_{dc}^2]^{1/2} \\ V'_{rms} &= [V_{rms}^2 - V_{dc}^2]^{1/2} \end{aligned}$$

•T

$$\begin{aligned} V'_{rms} &= [V_{rms}^2 - V_{dc}^2]^{1/2} \\ &= \left[\left(\frac{V_m}{\sqrt{2}} \right)^2 - \left(\frac{2V_m}{\pi} \right)^2 \right]^{1/2} = 0.308V_m \end{aligned}$$

$$\begin{aligned} \text{Ripple Factor } (Y_{HW}) &= \frac{V'_{rms}}{V_{dc}} = \sqrt{\left(\frac{V_{rms}}{V_{dc}} \right)^2 - 1} = \sqrt{\left(\frac{V_m/\sqrt{2}}{2V_m/\pi} \right)^2 - 1} \\ &= 0.48 \end{aligned}$$

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Unit 2 – Class 23 & 24 – Comparison

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Measure	HWR Ideal	HWR Practical	CT-Ideal	CT-Practical	Bridge- Ideal	Bridge-Practical
I_{dc}	$\frac{I_m}{\pi}$	$\frac{I_m}{\pi}$	$\frac{2I_m}{\pi}$	$\frac{2I_m}{\pi}$	$\frac{2I_m}{\pi}$	$\frac{2I_m}{\pi}$
V_{dc}	$\frac{V_m}{\pi}$	$\frac{V_m - V_k}{\pi}$	$\frac{2V_m}{\pi}$	$\frac{2(V_m - V_k)}{\pi}$	$\frac{2V_m}{\pi}$	$\frac{2(V_m - 2V_k)}{\pi}$
I_{rms}	$\frac{I_m}{2}$	$\frac{I_m}{2}$	$\frac{I_m}{\sqrt{2}}$	$\frac{I_m}{\sqrt{2}}$	$\frac{I_m}{\sqrt{2}}$	$\frac{I_m}{\sqrt{2}}$
V_{rms}	$\frac{V_m}{2}$	$\frac{V_m - V_k}{2}$	$\frac{V_m}{\sqrt{2}}$	$\frac{V_m - V_k}{\sqrt{2}}$	$\frac{V_m}{\sqrt{2}}$	$\frac{V_m - 2V_k}{\sqrt{2}}$
PIV	V_m	V_m	$2V_m$	$2V_m - V_k$	V_m	$V_m - V_k$

•T

Sl No.	Parameter	HWR	FWR
1	V'_{rms}	$0.385V_m$	$0.305V_m$
2	Efficiency	40.6%	81.2%
3	Ripple factor	1.21	0.48

•T

SI No.	Bridge-FWR	CT- FWR
1	Lesser PIV	Comparatively higher PIV
2	Centre tap transformer not required	Centre tap transformer required
3	Uniform input for both half cycles	Difficult to balance both the half cycles due to CT
4	No isolation between Input and output	Isolation due to CT-Transformer
5	4 diodes are required	2 diodes are required
6	More voltage drop due to two diodes in the path	Comparatively less voltage drop due to only one diode in the path
7	Lesser rectification efficiency	Comparatively better



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Unit 2 - Semiconductor Diode applications – Class 26 – Problems on Half Wave Rectifier

Ms. Ashwini

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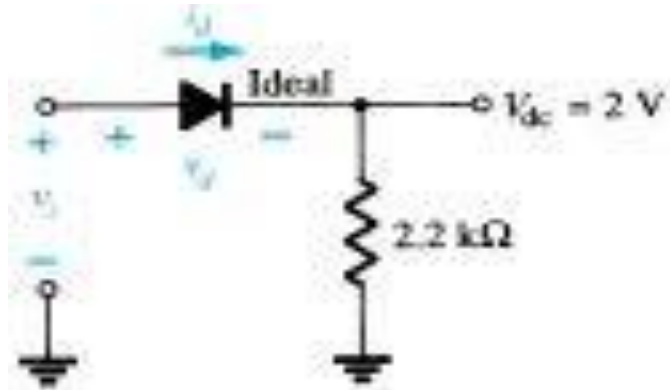
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Unit 2 - Semiconductor Diode applications – Class 26 – Text book reference – Section 2.6 – Pages 77 to 80

Ms. Ashwini

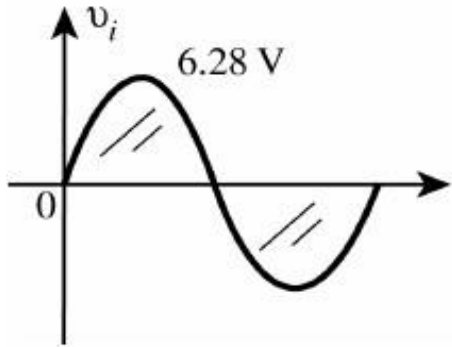
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Assuming an ideal diode, sketch v_i , v_d , and i_d for the half-wave rectifier. The input is a sinusoidal waveform with a frequency of 60Hz

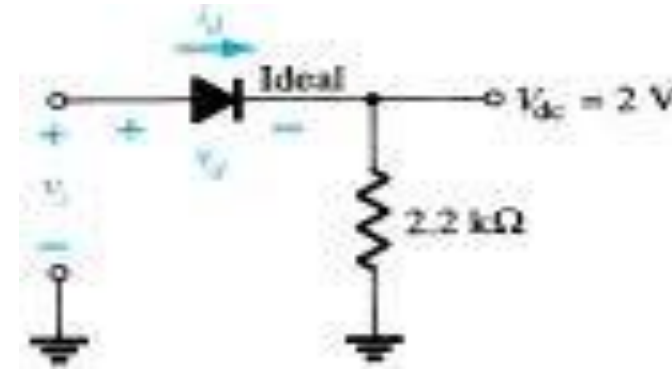
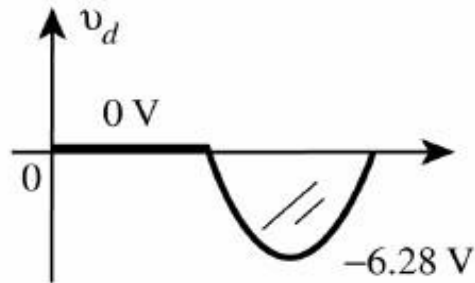
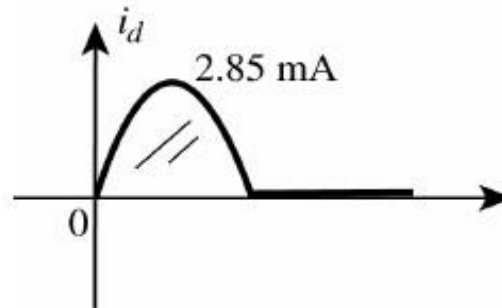


Solution:

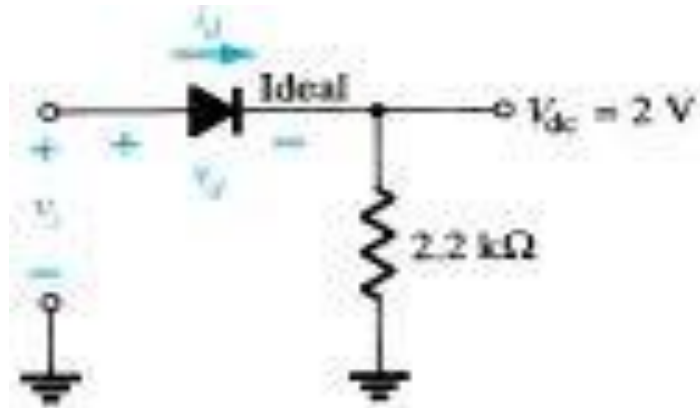
$$V_{dc} = 0.318 V_m \Rightarrow V_m = \frac{V_{dc}}{0.318} = \frac{2 \text{ V}}{0.318} = 6.28 \text{ V}$$



$$I_m = \frac{V_m}{R} = \frac{6.28 \text{ V}}{2.2 \text{ k}\Omega} = 2.85 \text{ mA}$$



Assuming a silicon diode ($V_T 0.7\text{ V}$), sketch v_i , v_d , and i_d for the half-wave rectifier. The input is a sinusoidal waveform with a frequency of 60 Hz

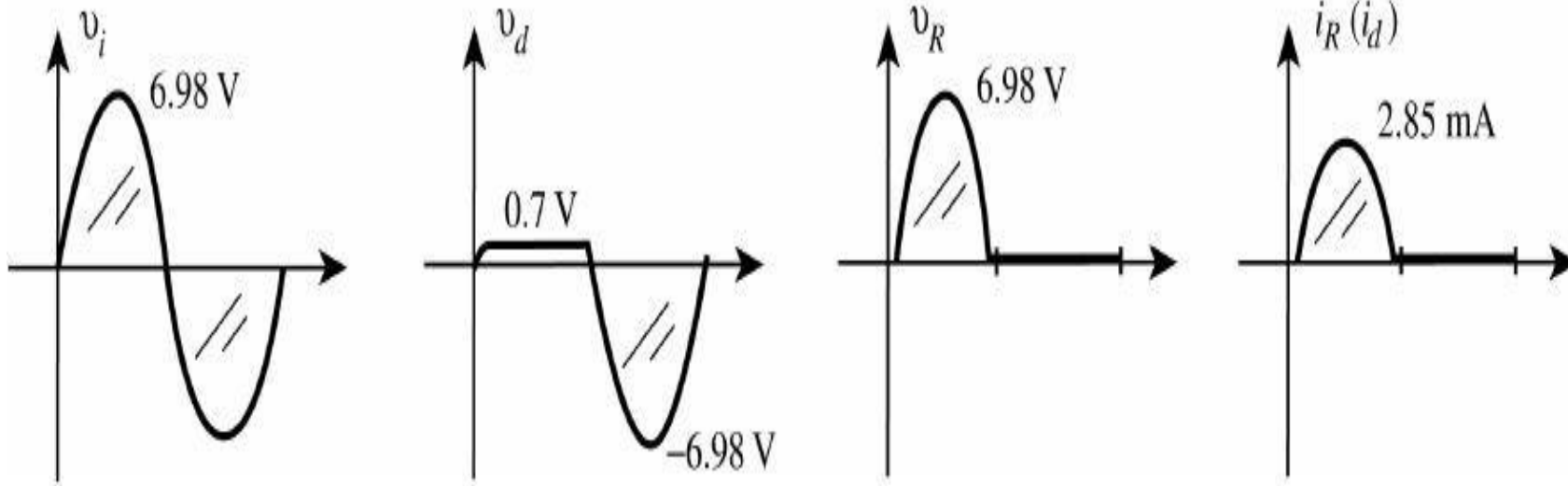


Solution:

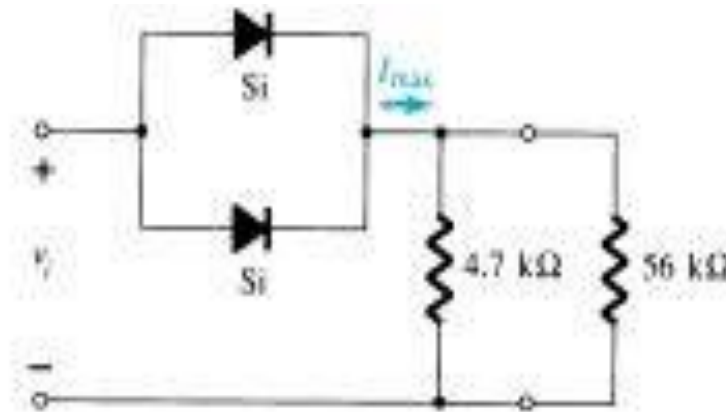
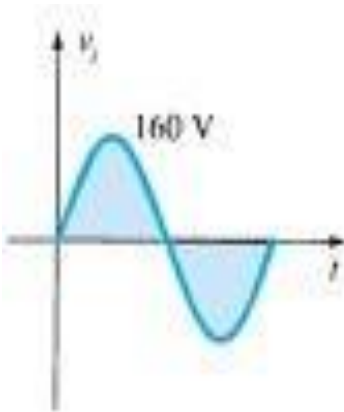
Using $V_{dc} \cong 0.318(V_m - V_T)$

$$2 \text{ V} = 0.318(V_m - 0.7 \text{ V})$$

Solving: $V_m = 6.98 \text{ V} \cong 10:1$ for $V_m:V_T$



- (a) Given $P_{\max} = 14 \text{ mW}$ for each diode shown, determine the maximum current rating of each diode (using the approximate equivalent model).
- (b) Determine I_{\max} for $V_{\max} 160 \text{ V}$.
- (c) Determine the current through each diode at V_{\max} using the results of part (b).
- (d) If both the diodes are present, compare I_{diode} with the maximum current rating of the diode?
- (e) If only one diode is present, compare I_{diode} with the maximum current rating of the diode?



Solution:

$$(a) \quad P_{\max} = 14 \text{ mW} = (0.7 \text{ V})I_D$$
$$I_D = \frac{14 \text{ mW}}{0.7 \text{ V}} = \mathbf{20 \text{ mA}}$$

$$(b) \quad 4.7 \text{ k}\Omega \parallel 56 \text{ k}\Omega = 4.34 \text{ k}\Omega$$
$$V_R = 160 \text{ V} - 0.7 \text{ V} = 159.3 \text{ V}$$
$$I_{\max} = \frac{159.3 \text{ V}}{4.34 \text{ k}\Omega} = \mathbf{36.71 \text{ mA}}$$

$$(c) \quad I_{\text{diode}} = \frac{I_{\max}}{2} = \frac{36.71 \text{ mA}}{2} = \mathbf{18.36 \text{ mA}}$$

d) $I_{\text{diode}} = 18.36 \text{ mA}$; maximum rating = 20 mA . Diode is safe

e) $I_{\text{diode}} = 36.71 \text{ mA}$; maximum rating = 20 mA ; Diode gets damaged

Numerical - A diode whose internal resistance is $20\ \Omega$ is to supply power to a $1\text{K}\Omega$ load from a 110 V source of supply. Calculate (i) the peak load current
(ii) r.m.s load current
(iii) peak inverse voltage
(iv) output DC voltage.
Draw the circuit diagram with all the component values.

Solution – Refer Class Notes



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Unit 2 – Semiconductor Diode applications – Class 27 & 28 – Problems on CT Full Wave Rectifier & Bridge Rectifier

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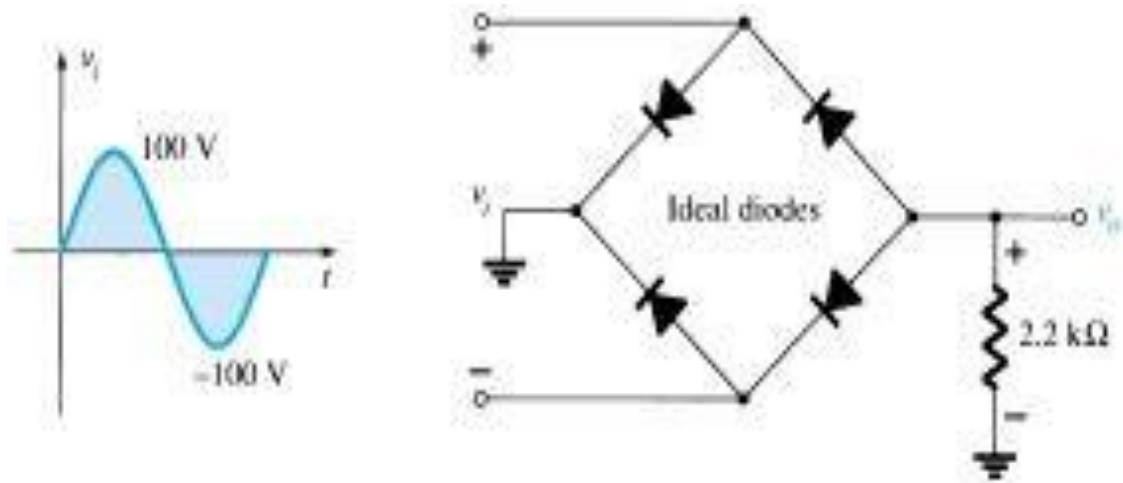
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**Unit 2 – Class 27 & 28 – Problems on CT Full Wave
Rectifier & Bridge Rectifier – Text book reference – 81
to 84 & 776 to 778**

ELECTRONIC PRINCIPLES AND DEVICES

Unit 2 – Class 27 & 28 - Solved example

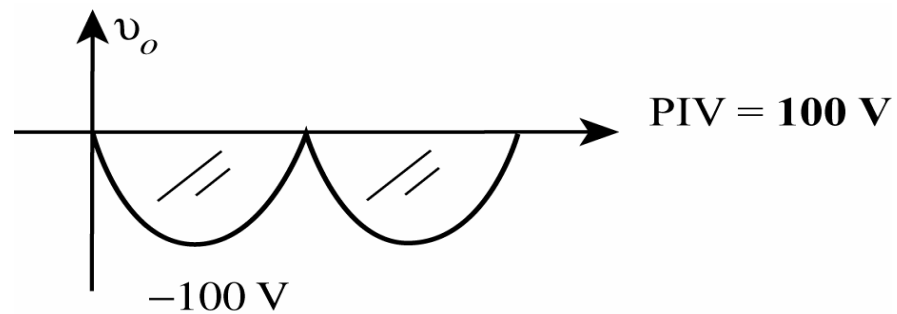
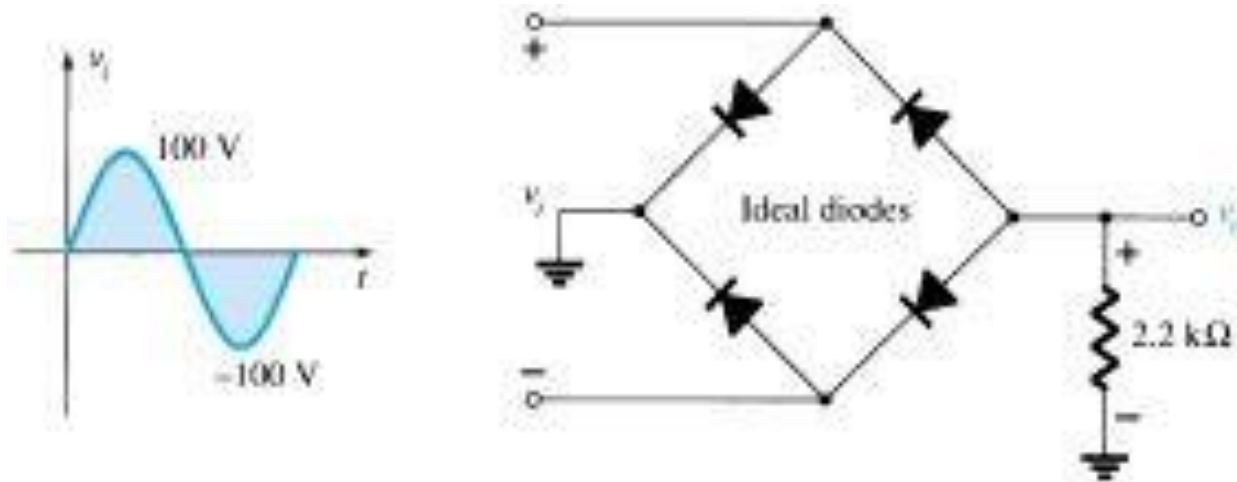
Determine V_o and the required PIV rating of each diode for the configuration



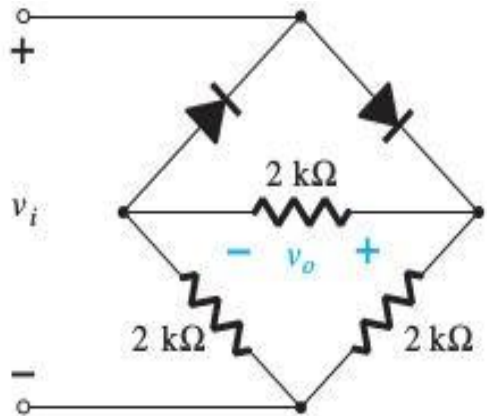
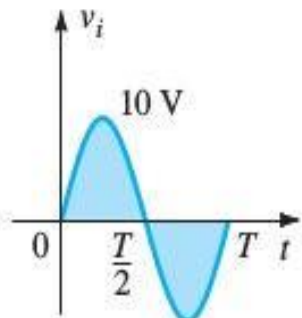
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Unit 2 – Class 27 & 28 - Solved example

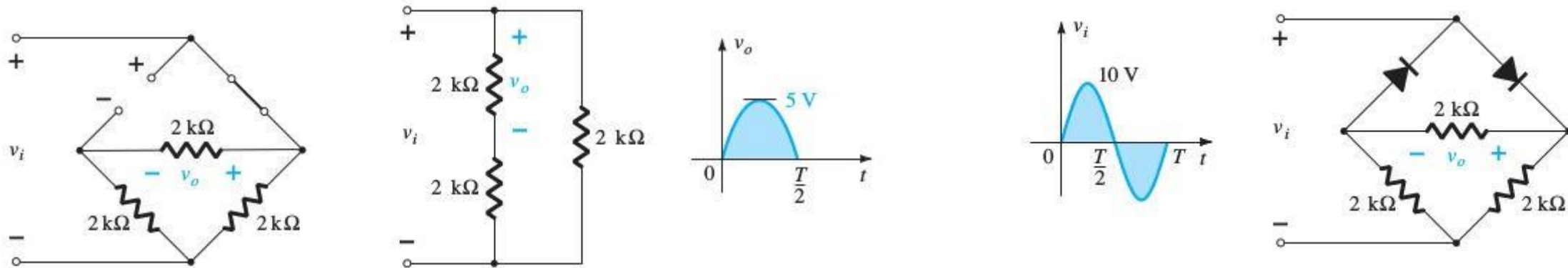
Solution:



Determine the output waveform for the network and calculate the output dc level and the required PIV of each diode.

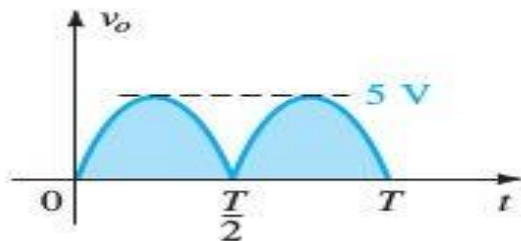


Solution:



$$V_{o\max} = (2/4) V_{i\max} = (2/4) (10\text{ V}) = 5\text{ V}$$

$$V_{\text{dc}} = 0.636(5\text{ V}) = 3.18\text{ V}$$



A full-wave bridge rectifier with a 120-V rms sinusoidal input has a load resistor of 1 k.

- (a) If silicon diodes are employed, what is the dc voltage available at the load?
- (b) Determine the required PIV rating of each diode.
- (c) Find the maximum current through each diode during conduction.
- (d) What is the required power rating of each diode?

Solution:

$$\begin{aligned}\text{(a)} \quad V_m &= \sqrt{2} (120 \text{ V}) = 169.7 \text{ V} \\ V_{L_m} &= V_{i_m} - 2V_D \\ &= 169.7 \text{ V} - 2(0.7 \text{ V}) = 169.7 \text{ V} - 1.4 \text{ V} \\ &= 168.3 \text{ V} \\ V_{dc} &= 0.636(168.3 \text{ V}) = \mathbf{107.04 \text{ V}}\end{aligned}$$

$$\text{(b)} \quad \text{PIV} = V_m(\text{load}) + V_D = 168.3 \text{ V} + 0.7 \text{ V} = \mathbf{169 \text{ V}}$$

$$\text{(c)} \quad I_D(\text{max}) = \frac{V_{L_m}}{R_L} = \frac{168.3 \text{ V}}{1 \text{ k}\Omega} = \mathbf{168.3 \text{ mA}}$$

$$\begin{aligned}\text{(d)} \quad P_{\max} &= V_D I_D = (0.7 \text{ V}) I_{\max} \\ &= (0.7 \text{ V})(168.3 \text{ mA}) \\ &= \mathbf{117.81 \text{ mW}}\end{aligned}$$

In a centre- tap FWR $R_L = 1\text{K}\Omega$, Each diode has forward bias dynamic resistance $r_d = 10\Omega$ Voltage across half secondary winding is $220\sin 314t$.

Find I_{dc} , I_m , I_{rms} , r , η (Efficiency).

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Unit 2 – Class 27 & 28 - Solved example

Solution:

Given, $V_m = 220\text{V}$

$$I_m = (V_m - V_k) / (R_d + R_l)$$

$$I_{dc} = 2I_m / \pi = 138.173\text{mA} \quad \text{and} \quad I_{rms} = I_m / \sqrt{2} = 153.53\text{mA}$$

$$R_F = \frac{[I_{rms}^2 - I_{dc}^2]^{1/2}}{I_{dc}} = 0.484$$

$$P_{dc} = I_{dc}^2 R_l = 19.09\text{W} \quad \text{and} \quad P_{ac} = I_{rms}^2 (R_l + R_d) = 23.8\text{W}$$

$$\eta = P_{dc} / P_{ac} = 80.21\%$$

1. In a two diode FWR using Si diodes, the RMS voltage across each half of the transformer secondary is 100V. The load resistance is $975\ \Omega$ and each diode has a forward resistance of $25\ \Omega$. Find (i) Average current (ii) Average output voltage (iii) PIV of diode.

Ans: $V_{dc} = 87.39V$, $I_{dc} = 0.089A$ and $PIV = 282V$.

2. A Bridge rectifier with ideal diodes has an ac source of RMS value 220 V, 50Hz connected to the primary of transformer. If the load resistance is $200\ \Omega$ and turns ratio of transformer is 4:1, find the dc output voltage, dc output current and output frequency.

Ans: $V_{dc} = 49.5V$, $I_{dc} = 0.247A$ and $f_o = 100Hz$.



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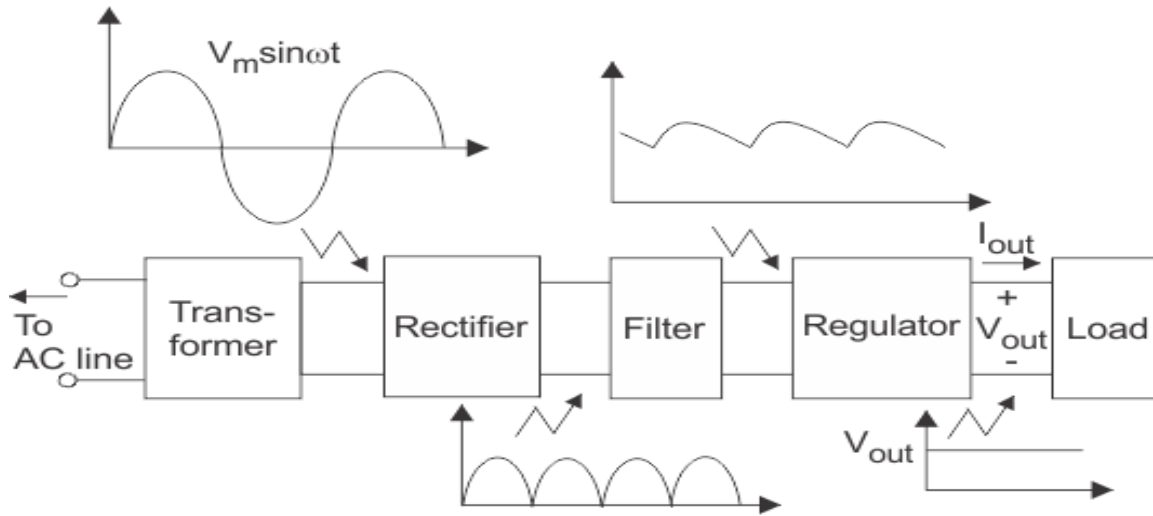
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Unit 2 – Class 29 – Shunt Capacitor Working

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Components of typical linear power supply

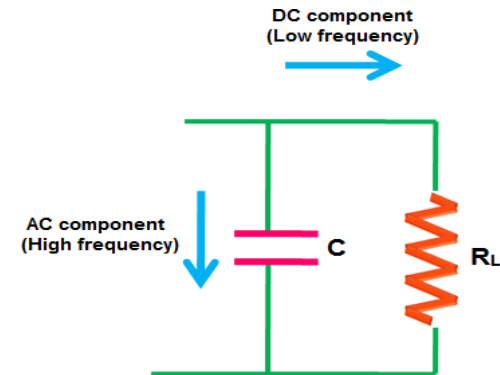
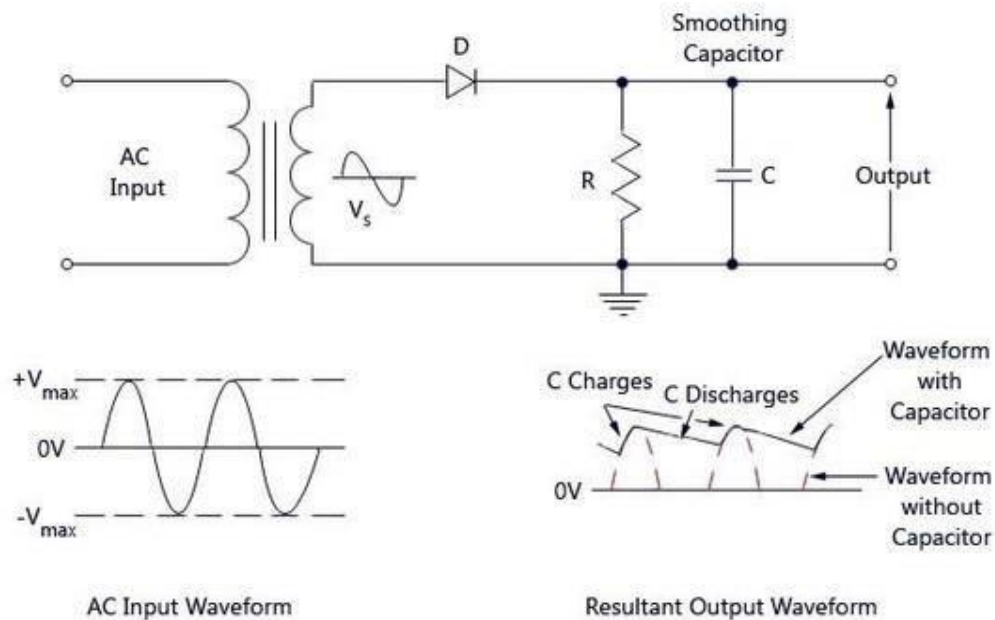
An electronic circuit which passes desired electrical component & blocks/reduces unwanted is called as filter

Types of Filters:

- ❖ AC Filter
- ❖ DC Filter

- The filter is an electronic device that allows dc components and blocks the ac components of the rectifier output is said to be DC filter
- Filter is made up of a combination of components such as capacitors, resistors, and inductors
- A capacitor allows the ac component and blocks the dc component. The inductor allows the dc component and blocks the ac component
- A capacitor is connected in parallel to rectifier to form Shunt Capacitor Filter

Capacitor C is connected in shunt/parallel with load resistor (R_L)



The capacitor provides high resistive path to dc components (low-frequency signal) and low resistive path to ac components (high-frequency signal)

Unit 2 – Class 29 - Shunt Capacitor Filter for Half – Wave Rectifier

- The main duty of the capacitor filter is to short the ripples to the ground and blocks the pure DC (DC components), so that it flows through the alternate path and reaches output load resistor R_L
- The flow of AC components through the capacitor is nothing but the charging of a capacitor

Ripple Factor for Capacitor Filter of a Half Wave Rectifier is given by

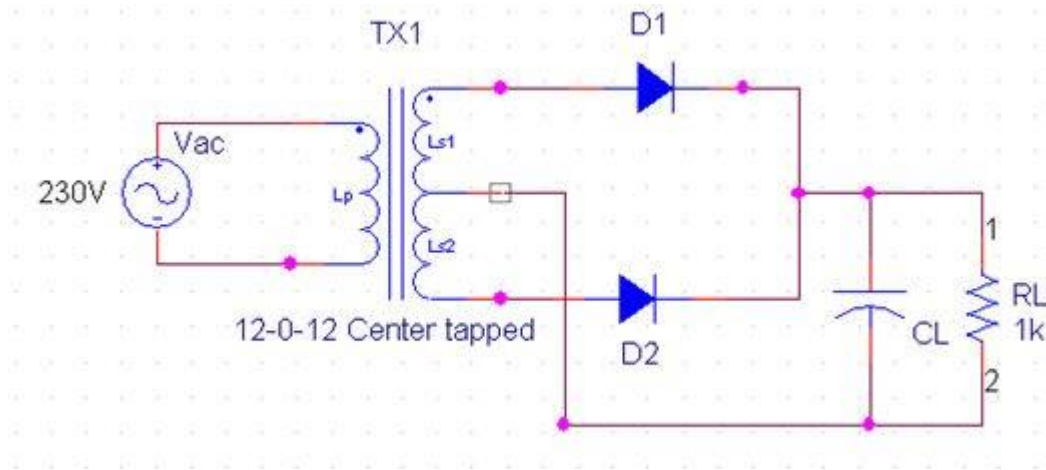
$$\text{Ripple Factor for a capacitor filter (HWR)} = 1 / (2\sqrt{3} f C R_L)$$

f – Frequency of Rectified Signal

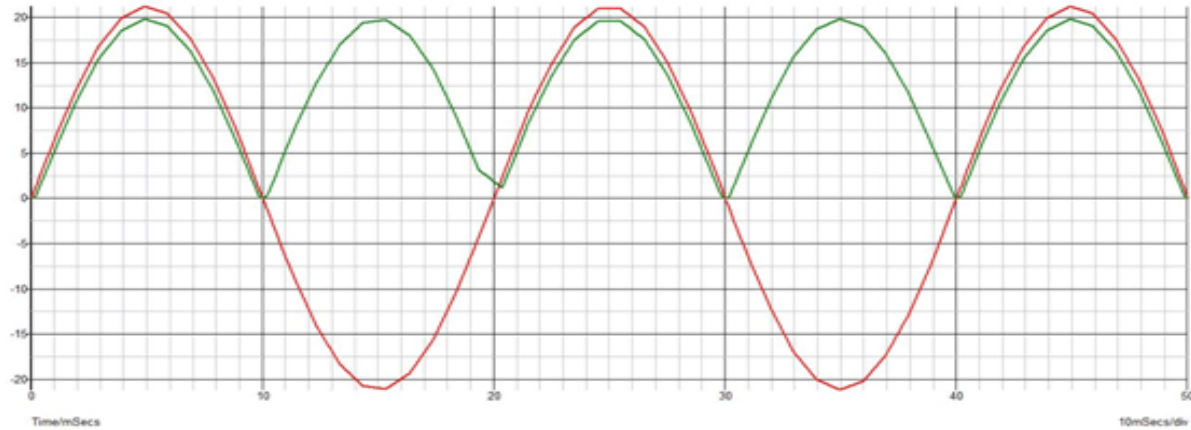
R_L – Value of Load resistor

C – Capacitance of the Shunt Capacitor

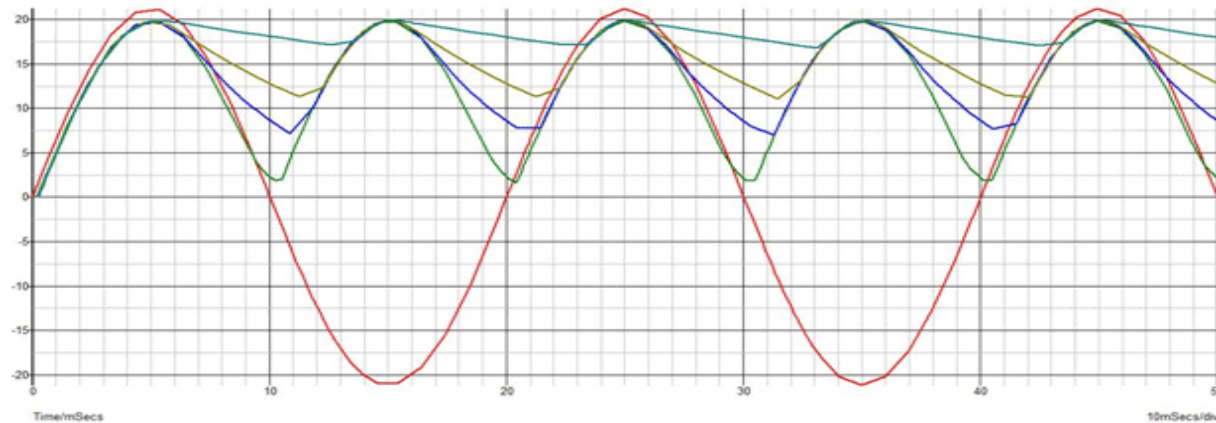
Unit 2 – Class 29 - Shunt Capacitor Filter for Centre-Tapped Full Wave Rectifier

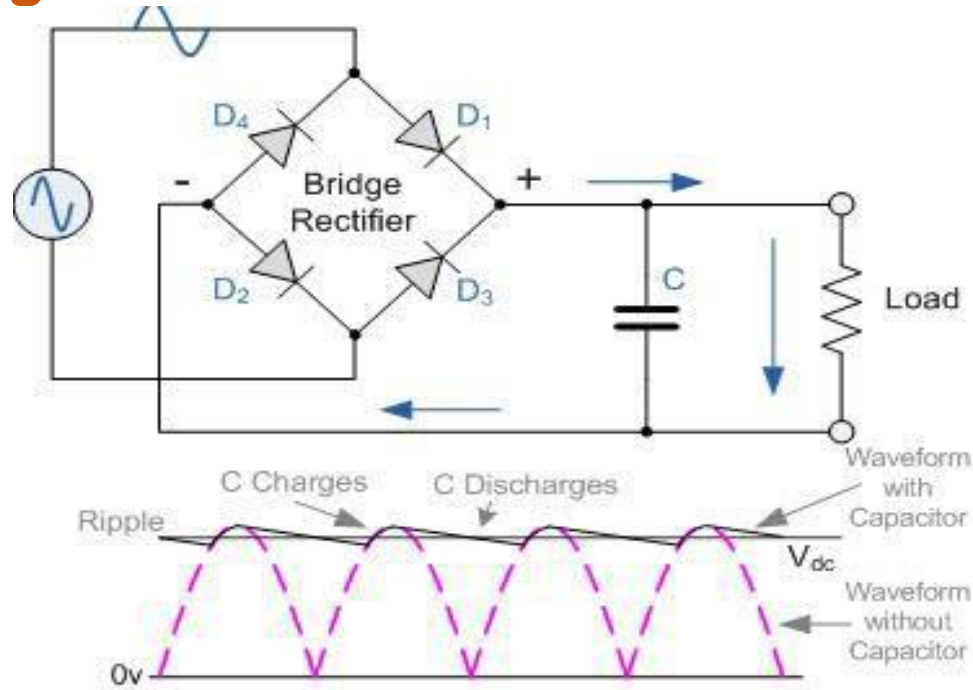


- The pulsating Direct Current (DC) produced by the full wave rectifier contains both AC and DC components
- DC current that contains both DC components and AC components reaches the filter, the DC components experience a high resistance from the capacitor whereas the AC components experience a low resistance from the capacitor



Filter output for different values of shunt capacitor





- AC components fluctuate with respect to time while the DC components remain constant with respect to time
- So the AC components present in the pulsating DC is an unwanted signal

Unit 2 – Class 29 - Shunt Capacitor Filter for Bridge Rectifier

The capacitor filter present at the output removes the unwanted AC components. Thus, a pure DC is obtained at the load resistor R_L

Ripple Factor for a capacitor filter (FWR) = $1 / (4\sqrt{3} f C R_L)$

f – Frequency of Rectified Signal

R_L – Value of Load resistor

C – Capacitance of the Shunt Capacitor

Above Expression Holds the same meaning for both the Full Wave Rectifier Circuits



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UNIT-2: Semiconductor Diode and Applications – Class 30 – Problems on Shunt Capacitor filter

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UNIT-2: – Class 30 – Text book reference – Section 15.3 – Page 777

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Question No. 1: A half wave rectifier, operated from a 50Hz supply uses a $1000\mu\text{F}$ capacitance connected in parallel to the load of rectifier. What will be the minimum value of load resistance that can be connected across the capacitor if the ripple% not exceeds 5?

Solution: For a half wave filter,

$$\text{Ripple Factor} = \frac{1}{2\sqrt{3} f C R_L}$$

$$= \frac{1}{\{2\sqrt{3} * 50 * 10^{-3} * R_L\}}$$

$$R_L = \frac{10^3}{5\sqrt{3}}$$

$$R_L = 115.47\Omega$$

Question No. 2: A $100\mu\text{F}$ capacitor when used as a filter has 15V ac across it with a load resistor of $2.5\text{K}\Omega$. If the filter is the full wave and supply frequency is 50Hz , what is the percentage of ripple frequency in the output?

Solution:

For a full wave rectifier,

Ripple factor, $\gamma = \frac{1}{4\sqrt{3} f C R_L}$

$$= \frac{1}{4\sqrt{3}} * 50 * 10^{-3} * 2.5$$

$$= 0.01154.$$

So, ripple factor is 1.154%

Question No. 3: A full wave rectifier uses a capacitor filter with $500\mu\text{F}$ capacitor and provides a load current of 200mA at 8% ripple. Calculate the dc voltage.

Solution:

The ripple factor for Full Wave Rectifier

$$\gamma = \frac{I_L}{4\sqrt{3} f C V_{DC}}$$

$$V_{DC} = \frac{200 \times 10^{-3}}{4\sqrt{3} \times 50 \times 500 \times 8}$$

$$V_{DC} = 14.43\text{V}$$

Question No. 4: A shunt capacitor of value $500\mu\text{F}$ fed rectifier circuit. The dc voltage is 14.43V . The dc current flowing is 200mA . It is operating at a frequency of 50Hz . What will be the value of peak rectified voltage?

Solution:

We know, $V_m = V_{dc} + I_{dc}/4fC$

$$= 14.43 + \{200 / (200 \times 500)\} 10^3$$

$$= 14.43 + 2 = 16.43\text{V}$$

$$V_m = 16.43\text{V}$$

Q. No. 1 Calculate the ripple factor of a capacitor filter connected to a full wave rectifier, $C=50\mu F$ if the peak rectified output voltage is 30V and a load current is 50mA

Solution:

$$\gamma = \frac{V_{r(rms)}}{V_{dc}}, V_{r(rms)} = \frac{I_{DC}}{4\sqrt{3}fc},$$

$$V_{dc} = V_m - \frac{I_{DC}}{4fc}$$

$$\text{given } V_{dc} = 30V, I_{DC} = 50mA,$$

$$f = 50Hz, C = 50\mu F,$$

$$\text{sustituting the values, } \gamma = 0.043$$

Question: 64) Draw the circuit diagram of a centre tapped FWR with capacitor filter. If the filter capacitor is 120 micro F and load current of 80mA calculate the %ripple of the output. The FWR is operating from 50Hz supply and develops a peak rectified voltage of 25V.

$V_{rms} = 1.92$, $V_{dc} = 21.66$, $R = 8.8\%$ - For Solution Refer Class Notes

Question: 65) A 500 micro F capacitor filter provides a load current of 200mA at 8% ripple to a FWR . Calculate the peak value of the rectified voltage obtained from a 50Hz supply and the DC voltage across the filter capacitor. Draw the circuit diagram. FWR – For Solution Refer Class Notes

$V_{dc} = 14.4$, $V_m = 16.4$

Question : 68) Calculate the size of capacitor filter needed to obtain a filtered Dc voltage of 24V having 5% ripple at a load of 150mA from a full wave rectifier operating with a supply of 60HZ – For Solution – Refer Class Notes

$V_{rms}=12V, c=300\text{micro}$

Question:66) Calculate the size of capacitor filter needed to obtain a filtered DC voltage of 24V having 15% ripple at a load of 150mA from a half wave rectifier operating with a supply of 60Hz. – For Solution Refer Class Notes

$R_L=160, C=200\text{micro}$

Question:43) A Bridge rectifier with ideal diode has a ac source of RMS value 220V 50Hz connected to the primary of transformer. If the load resistance is 200 ohm and the turn ratio of transformer 4:1 find the DC voltage , dc output current and output frequency

$V_{dc}=49.51$,,, $i_{dc}=0.247$,,, $f_o=100$

Question :44) In a two diode FWR using Si diodes, the RMS voltage across each half of the transformer secondary is 100V. The load resistance is 975 ohm and each diode has a forward resistance of 25 ohm find Average current , Average output voltage and PIV

$V_{dc}=89.52$,,, $i_{dc}=89.58\text{mA}$,,, $piv=282.14$

Question : 45) A full wave bridge rectifier is constructed with si diode and source of $V_{rms} = 120V$ has a load resistance of $1K$. Determine DC voltage across R_L , PIV rating of each diode, find the Max current through each diode during conduction, what is the required power rating of each diode

$V_{dc} = 107.14V$, $piv = 169V$, $i_m = 168.3mA$, $P = 117.81mW$

Question : 46) A center tapped full wave rectifier constructed with si diode has a secondary coil voltage of $V_{rms} 20V$ with the load resistance of $1.5K$ Determine I_m , I_{dc} and V_{rms} across R_L

$I_m = 18.38mA$, $i_{dc} = 11.7mA$, $v_{rms} = 19.5V$

Question :) 2 diode FWR with secondary winding voltage 100V , load resistance 1K. Find all the parameter

$$V_m=141.42,,i_m=14.72,,i_{dc}=89.6\text{mA},,p_{iv}=281.44$$

Question :47) A full wave bridge rectifier constructed with si diode has a secondary coil voltage of V_{rms} 20V with the load resistance of 1.5K Determine I_m , I_{dc} and V_{rms} across RL

$$V_m=28.28,,,,i_m=18.38\text{mA},,i_{dc}=11.7\text{mA},,V_{rms}=19.5$$

Question : Centre tap FWR with load resistance 1K and dynamic resistance of diode 10 ohm with secondary winding voltage $200\sin(314t)$. Find all the parameter

$I_m=197.32$,,, $i_{dc}=125.617$,,, $v_{dc}=126.87$,,, $i_{rms}=139.526$,,, $E=80.25$,,, $R=0.48$

Question : Center Tapped FWR with ideal diode with V_{rms} 200V and load resistance 2K, Find all the parameter

**$V_m=282.8$,,, $i_m=141.4mA$,,, $i_{dc}=90.03mA$,,, $v_{dc}=180.06$... $i_{rms}=0.099$
 $Piv=565.6$,,, $r=0.483$**

Question : A diode with internal resistance 20 ohm is to supply power to a 1K load from 110V source of supply ,find all parameter (HWR)

$$V_m=110, i_m=107.16\text{mA}, i_{rms}=53.58\text{mA}, p_{iv}=110, v_{dc}=34.8$$

Question : A semi conductor diode having internal resistance 20 ohm is used HWR if applied voltage is $50\sin\omega t$ and R_L 800 ohm . Find all the parameter.

$$I_m=0.06, i_{dc}=19\text{mA}, i_{rms}=30\text{mA}, v_{dc}=15.69, E=40.11$$



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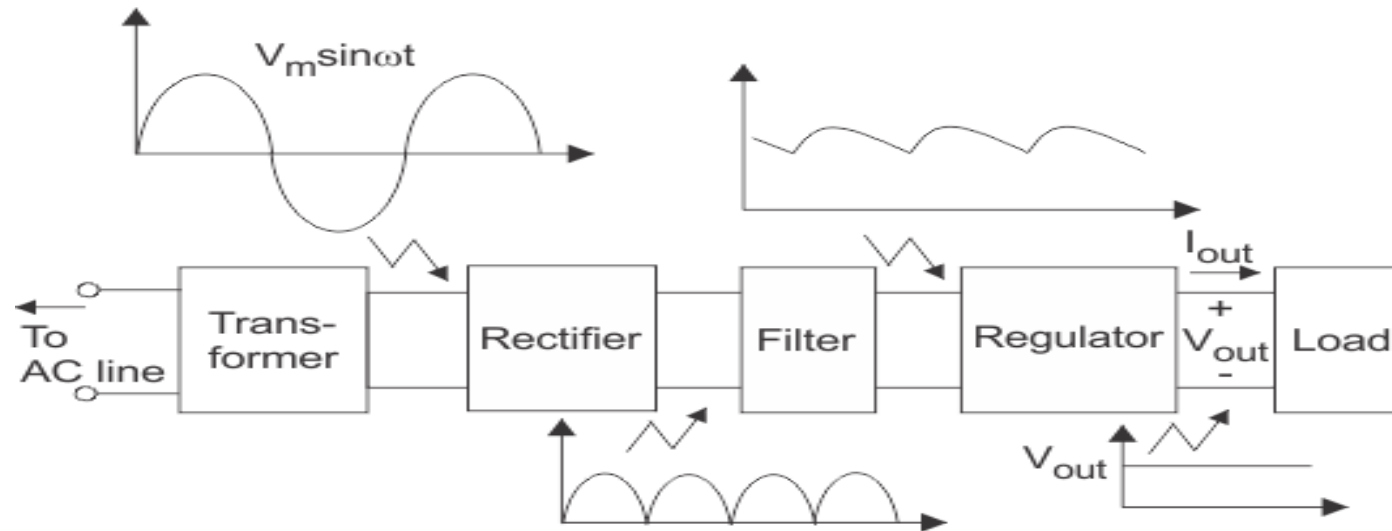
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UNIT-2: Class 32 to 34 –Zener diode Voltage Regulator – 3 cases

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Components of typical linear power supply

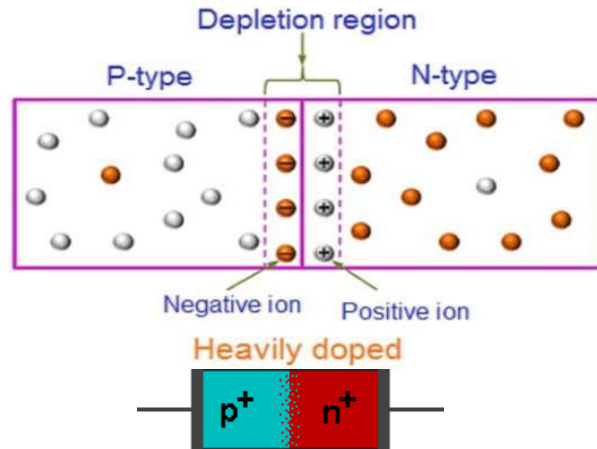
Filtered-Fluctuating signal to smooth constant DC signal is the output of Regulator Circuit

Voltage Regulating Device:

❖ Zener Diode

- Heavily Doped PN-Junction Device Specially Designed to operate under breakdown region
- Zener Diode under Forward Bias & Reverse Bias, its functioning is controlled by the current
- Zener Diode under forward Bias condition works like a normal semiconductor diode
- Zener Diode under reverse bias condition acts like Voltage regulator

Structure of Zener Diode



Symbol of Zener Diode

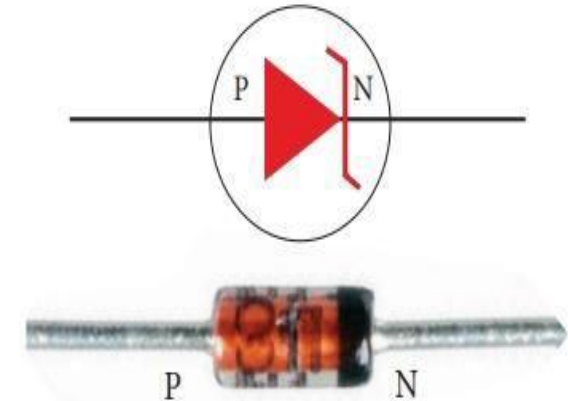


Figure (a) Zener diode and its symbol
(The black colour ring denotes the negative terminal of the Zener diode)

V-I Characteristics of Zener Diode

V-I Characteristics of
Zener Diode in Forward
Bias Condition

V-I Characteristics of
Zener Diode in Reverse
Bias Condition

Forward Bias & Reverse Bias

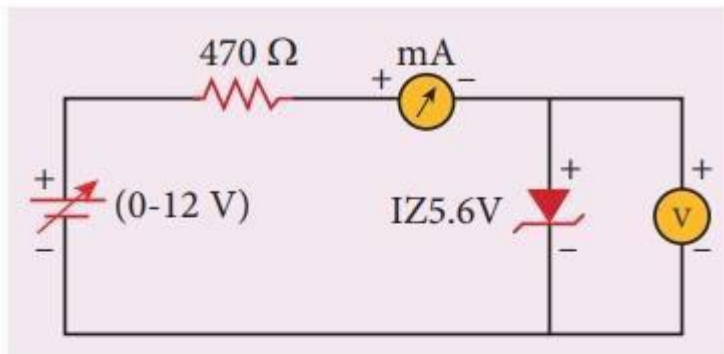


Figure (b) Zener diode in forward bias

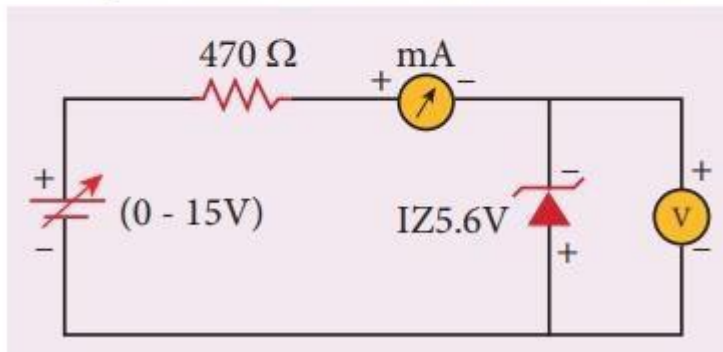
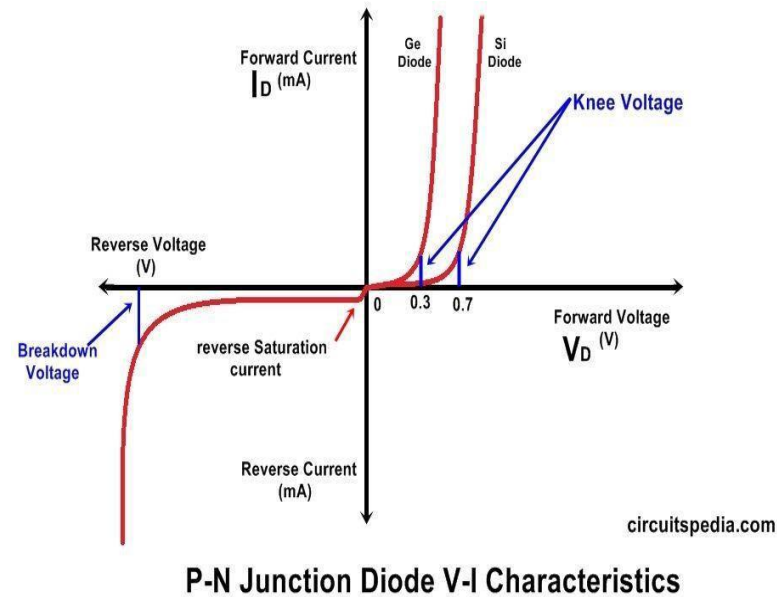
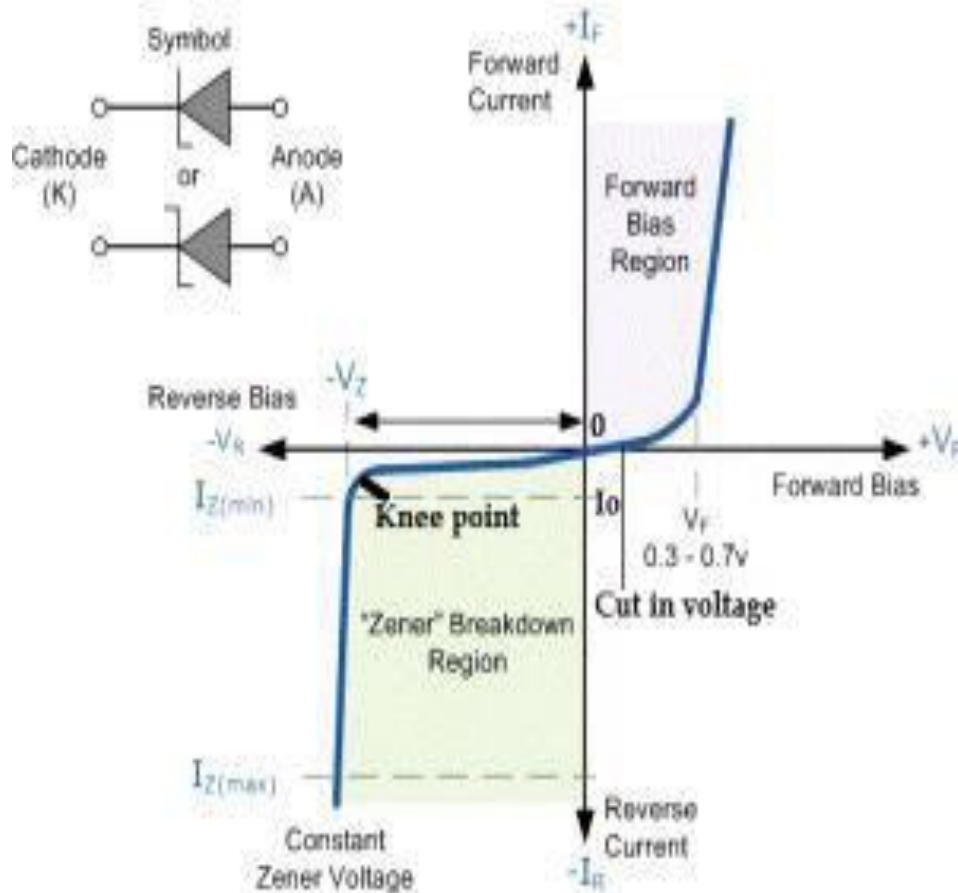


Figure (c) Zener diode in reverse bias

V-I Characteristics of Semiconductor Diode



Forward Bias & Reverse Bias Curves Zener Diode Parameters



- Knee Voltage
- Forward Current Rating
- Forward Resistance
- I_{Zmin}
- I_{Zmax}
- Zener Breakdown Voltage (V_Z)
- Maximum Power Rating
i.e $P_{Zmax} = (V_Z) \cdot (I_{Zmax})$

- It is normally used as voltage reference
- Zener diodes are used in voltage stabilizers or shunt regulators
- Zener diodes are used in switching operations
- Zener diodes are used in clipping and clamping circuits
- Zener diodes are used in various protection circuits

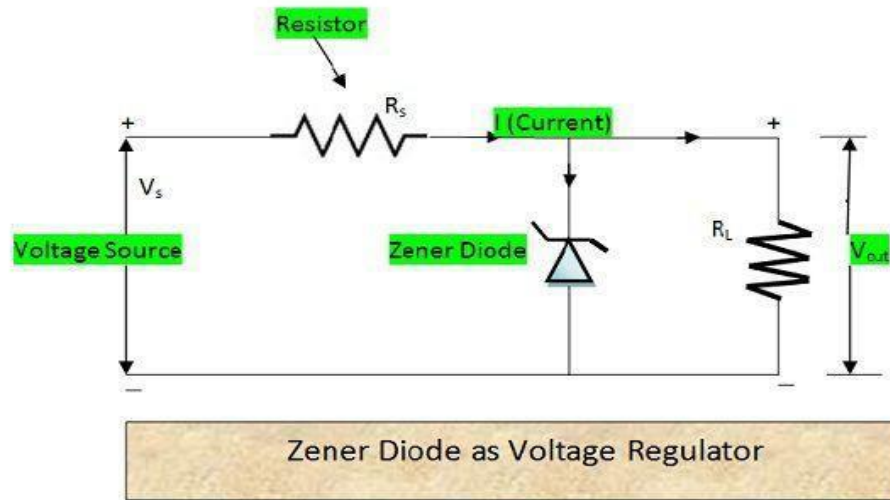
Regulator is an electronic circuit maintains one of the output electrical parameter to be constant

Current Regulator: Output Current to be constant even though input current or output voltage is changing

Voltage Regulator: Output Voltage to be constant even though input voltage or output current is changing

Zener Diode Exhibit the Property of Voltage regulator

Zener Diode as Voltage regulator, it operates as Line Regulator & Load Regulator



Line Regulator: V_{in} is Varying But I_{out} is constant; circuit should maintain V_{out} to be Constant

Load Regulator: I_{out} is Varying But V_{in} is constant; circuit should maintain V_{out} to be Constant



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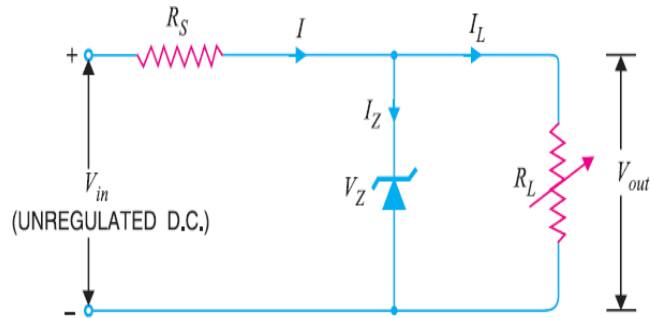
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UNIT-2: Class 32 to 34 – Zener diode voltage regulator

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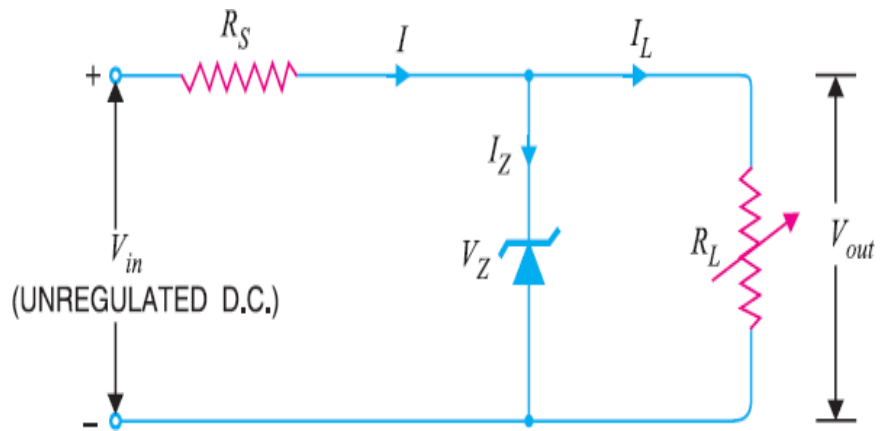
Conditions required to operate Zener Diode as Voltage Regulator



- Zener Diode should be in Reverse Biased Condition
- V_{in} should be Greater than V_Z
- I_Z should be greater than I_{Zmin}
- I_Z should be less than or equal to I_{Zmax}
- R_L should be Greater than R_{Lmin}

The Property of Voltage regulator to maintain output voltage to be constant even though there is variation in input voltage but output/load current is constant

i.e. V_{in} is varying but I_L or I_{out} is constant



From KVL we have,

$$V_{in} = I.R_S + V_Z \text{----- 1}$$

Where $V_Z = V_{out}$ (zener diode & R_L are in parallel combination)

From KCL we have,

$$I = I_Z + I_L \text{----- 2}$$

Part -1: V_{in} is Increasing; I_{out}/I_L is Constant;

From Equation- 1 We have, $V_{in} \uparrow = I.R_s \uparrow + V_z$

From Equation – 2 We have, $I \uparrow = I_z \uparrow + I_L \uparrow$
Constant

Therefore V_{out} is constant

Part -2: V_{in} is Decreasing; I_{out}/I_L is Constant;

From Equation- 1 We have, $V_{in} \downarrow = I.R_s \downarrow + V_z$

From Equation – 2 We have, $I \downarrow = I_z \downarrow + I_L \uparrow$
Constant

Therefore V_{out} is constant

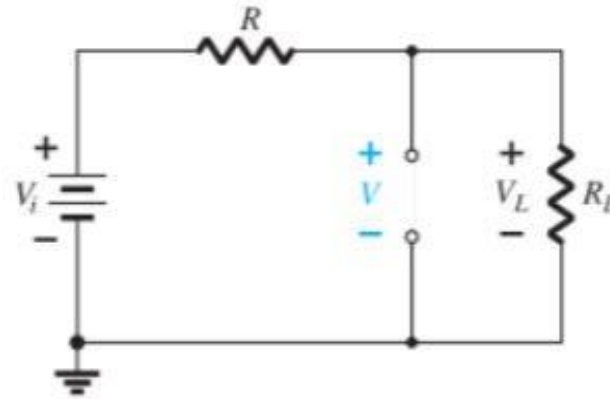
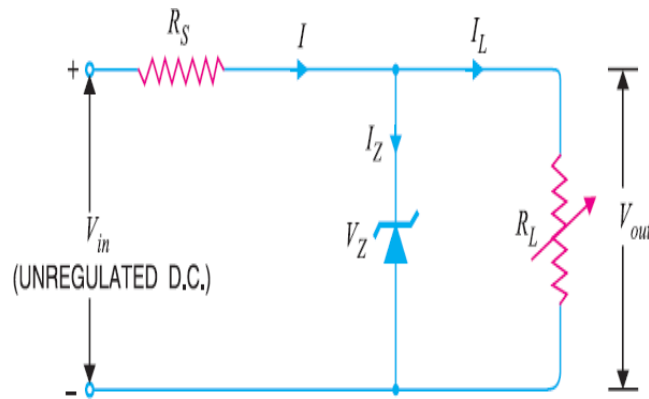
It can be operated as Voltage Regulator by Keeping V_{in} & I_{out} both to be constant i.e. Fixed V_i and fixed R_L

It can be operated as Voltage Regulator by Keeping V_{in} variable & I_{out} to be constant i.e. Changing V_i and fixed R_L

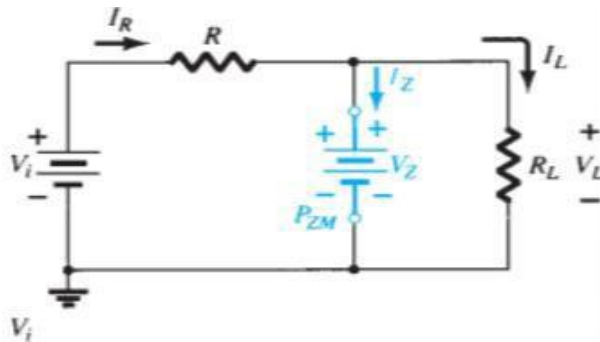
It can be operated as Voltage Regulator by Keeping V_{in} constant & I_{out} to be variable i.e. Fixed V_i and Changing R_L

It can be operated as Voltage Regulator by Keeping V_{in} variable & I_{out} both to be constant i.e. Changing V_i and Changing R_L

CASE-1: Fixed V_i and fixed R Voltage Regulator



Determining the state of the Zener diode.



Substituting the Zener equivalent for the "on" situation.

CASE-1: Fixed V_i and fixed R Voltage Regulator

1. Determine the state of the Zener diode by removing it from the network and calculating the voltage across the resulting open circuit.

$$V = V_L = \frac{R_L V_i}{R + R_L}$$

2. Substitute the appropriate equivalent circuit and solve for the desired unknowns.

$$V_L = V_Z$$

$$I_R = I_Z + I_L$$

$$I_Z = I_R - I_L$$

$$I_L = \frac{V_L}{R_L}$$

$$I_R = \frac{V_R}{R} = \frac{V_i - V_L}{R}$$

$$P_Z = V_Z I_Z$$

CASE-2: Fixed V_{in} and Variable R_L Voltage Regulator

$$V_L = V_Z = \frac{R_L V_i}{R_L + R}$$

$$R_{L_{min}} = \frac{R V_Z}{V_i - V_Z}$$

$$I_{L_{max}} = \frac{V_L}{R_L} = \frac{V_Z}{R_{L_{min}}}$$

$$V_R = V_i - V_Z$$

$$I_R = \frac{V_R}{R}$$

$$I_Z = I_R - I_L$$

$$I_{L_{min}} = I_R - I_{ZM}$$

$$R_{L_{max}} = \frac{V_Z}{I_{L_{min}}}$$

CASE-3: Variable V_{in} and Fixed R_L Voltage Regulator

$$V_L = V_Z = \frac{R_L V_i}{R_L + R}$$

$$V_{i_{\min}} = \frac{(R_L + R)V_Z}{R_L}$$

$$I_{R_{\max}} = I_{ZM} + I_L$$

$$V_{i_{\max}} = V_{R_{\max}} + V_Z$$

$$V_{i_{\max}} = I_{R_{\max}} R + V_Z$$

CASE-4: Variable V_{in} and Variable R_L Voltage Regulator

$$R_{smin} = \frac{V_{imax} - V_z}{I_{zmax} - I_{Lmin}} \quad R_{smax} = \frac{V_{imin} - V_z}{I_{zmin} - I_{Lmax}}$$



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UNIT-2: Semiconductor Diode and Applications

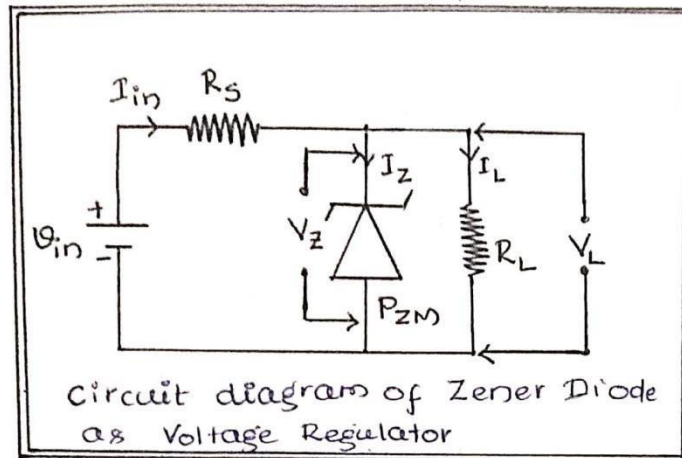
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List of Formulae for CASE-1: V_{in} & R_s are fixed

①

#1 ZENER DIODE AS VOLTAGE REGULATOR



CASE 1: V_{in} & R_s are fixed

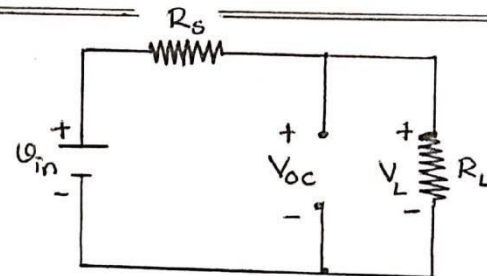
✓ Step 1: Determine the state of Zener diode [ON/OFF] by removing it from the circuit & calculating the voltage across the resulting open circuit.

i.e



∴ Voltage drop across open circuit is nothing but voltage drop across " R_L ".

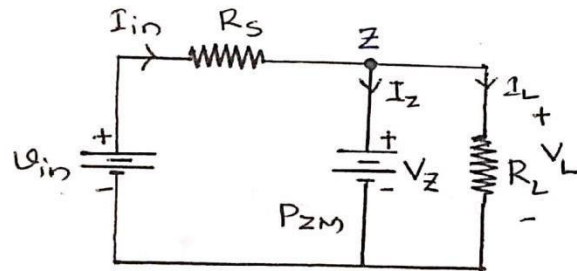
Hence - $V_{oc} = V_L = \frac{V_{in} R_L}{R_s + R_L} \rightarrow (1)$



If $V_{oc} = V_L > V_Z$ then Zener diode is in 'ON' state; $V_{oc} < V_Z$ then Zener-off

List of Formulae for CASE-1: V_{in} & R_s are fixed; Continues...

✓ step 2: If Zener diode is I_{in} ON state [Confirmed from eq (1)]
then equate V_L to V_Z or $V_L = V_Z$



Replacing ON state Zener diode by equivalent battery ' V_Z '

Apply KCL at node 'Z'

we get $I_{in} = I_Z + I_L$

where $I_L = \frac{V_L}{R_L}$

∴ from circuit we get

$$V_{in} = I_{in} R_s + V_Z$$

$$I_{in} R_s = V_{in} - V_Z \quad \therefore \quad I_{in} = \frac{V_{in} - V_Z}{R_s}$$

Power dissipated in Zener diode is $P_Z = V_Z I_Z$

List of Formulae for CASE-2: V_{in} fixed & R_L Variable

CASE ii: V_{in} is fixed but R_L is variable: ②

↳ Too small value of R_L will result in a voltage V_L across the load resistor less than V_Z and the Zener diode will be in OFF state. [Minimum Load Resistor should be used]

$$\text{W.K.T } V_L = V_Z = \frac{R_L V_{in}}{R_S + R_L} \Rightarrow V_Z [R_S + R_L] = R_L V_{in}$$

$$\text{or } V_Z R_S + V_Z R_L = R_L V_{in}$$

$$R_L V_{in} - V_Z R_L = V_Z R_S \quad \therefore \boxed{R_{Lmin} = \frac{V_Z R_S}{V_{in} - V_Z}}$$

✓ When $R_L = R_{Lmin}$ then $I_L \rightarrow I_{Lmax}$ & it is given by $\boxed{I_{Lmax} = \frac{V_Z}{R_{Lmin}}}$

✓ Determine I_{in} i.e. $\boxed{I_{in} = \frac{V_{in} - V_Z}{R_S}}$

✓ If I_{ZM} is mentioned as part of data then

$$\boxed{I_{Lmin} = I_{in} - I_{ZM}}$$

where $I_{ZM} \rightarrow$ Zener Maximum Current

Then $\boxed{R_{Lmax} = \frac{V_Z}{I_{Lmin}}}$

List of Formulae for CASE-3: V_{in} Variable & R_L fixed

CASE iii: V_{in} is variable but R_L is fixed:

↳ V_{in} should be sufficiently large to turn ON the Zener diode

∴ The minimum turn-ON voltage required is

$$V_{in[min]} = \frac{[R_L + R_S] V_Z}{R_L} \quad \left[\because V_Z = V_L = \frac{V_{in} R_L}{R_S + R_L} \right]$$

↳ The Maximum value of V_{in} is limited by Zener maximum current i.e. I_{Zmax} or I_{ZM}

$$\therefore I_{in[max]} = I_{Zmax} + I_L \quad \left[\text{where } I_L \text{ is fixed because } R_L \text{ is constant} \right]$$

Hence

$$V_{in[max]} = I_{in[max]} R_S + V_Z$$

List of Formulae for CASE-4: V_{in} & R_L both are Variable

③

CASE IV: BOTH V_{in} & R_L Varying:

Let V_{in} varies between $V_{in(min)}$ to $V_{in(max)}$ & R_L between R_{Lmin} to R_{Lmax} ; the one need to design the zener diode as voltage regulator with the constant output voltage by choosing the appropriate value of R_S & also maintaining the I_Z range within I_{Zmin} to I_{Zmax} .

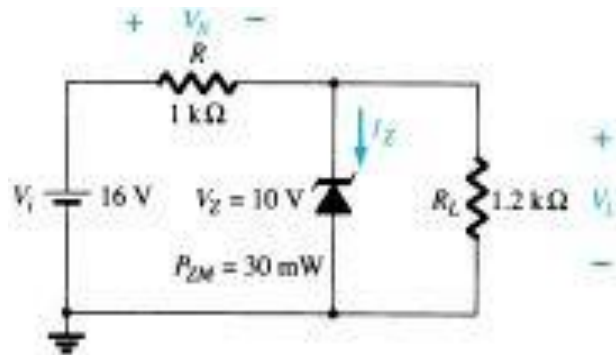
✓ Condition for R_{Smin} is

$$R_{Smin} = \frac{V_{in(max)} - V_Z}{I_{Zmax} + I_{Lmin}}$$

✓ Condition for R_{Smax} is

$$R_{Smax} = \frac{V_{in(min)} - V_Z}{I_{Zmin} + I_{Lmax}}$$

Question No. 1: For the following Zener diode network, determine V_L , V_R , I_Z , and P_Z .



Solution:

$$V = \frac{R_L V_i}{R + R_L} = \frac{1.2 \text{ k}\Omega (16 \text{ V})}{1 \text{ k}\Omega + 1.2 \text{ k}\Omega} = 8.73 \text{ V}$$

Since V_L is less than V_Z , the diode is in the “off” state.
Substituting the open-circuit equivalent will result in;

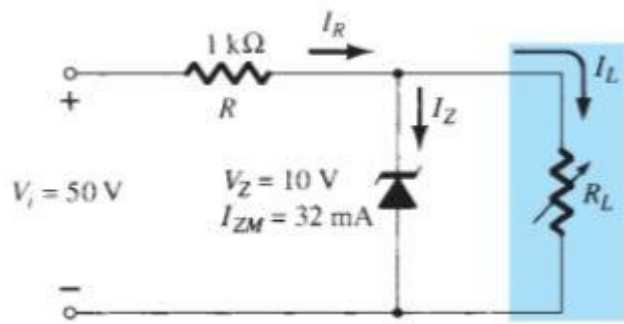
$$V_L = V = 8.73 \text{ V}$$

$$V_R = V_i - V_L = 16 \text{ V} - 8.73 \text{ V} = 7.27 \text{ V}$$

$$I_Z = 0 \text{ A}$$

$$P_Z = V_Z I_Z = V_Z (0 \text{ A}) = 0 \text{ W}$$

Question No. 2: Find the range of load resistance and the maximum power rating for the circuit?



Solution:

a) To determine the value of R_L that will turn the Zener diode on

$$R_{L_{\min}} = \frac{RV_Z}{V_i - V_Z} = \frac{(1 \text{ k}\Omega)(10 \text{ V})}{50 \text{ V} - 10 \text{ V}} = \frac{10 \text{ k}\Omega}{40} = 250 \text{ }\Omega$$

The voltage across the resistor R

$$V_R = V_i - V_Z = 50 \text{ V} - 10 \text{ V} = 40 \text{ V}$$

$$I_R = \frac{V_R}{R} = \frac{40 \text{ V}}{1 \text{ k}\Omega} = 40 \text{ mA}$$

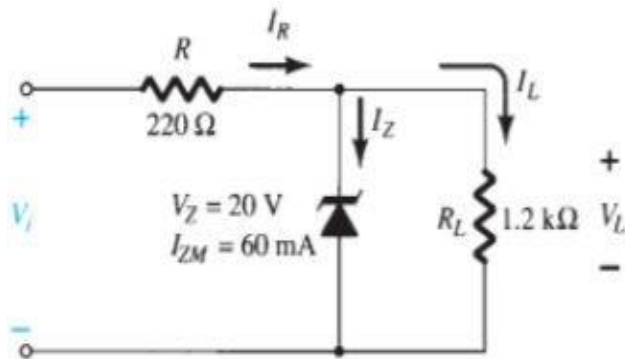
Solution: Continues

$$I_{L_{\min}} = I_R - I_{ZM} = 40 \text{ mA} - 32 \text{ mA} = 8 \text{ mA}$$

$$R_{L_{\max}} = \frac{V_Z}{I_{L_{\min}}} = \frac{10 \text{ V}}{8 \text{ mA}} = 1.25 \text{ k}\Omega$$

$$\begin{aligned} \text{(b) } P_{\max} &= V_Z I_{ZM} \\ &= (10 \text{ V})(32 \text{ mA}) = 320 \text{ mW} \end{aligned}$$

Question No. 3: Determine the range of values of V_i that will maintain Zener diode in the “on” state?



Solution: from problem statement,
 $R=220\Omega$, $R_L=1.2k\Omega$, $V_Z=20V$,
 $I_{ZM}=60mA$

$$I_{R_{max}} = I_{ZM} + I_L$$

$$V_{i_{max}} = V_{R_{max}} + V_Z$$

$$V_{i_{max}} = I_{R_{max}} R + V_Z$$

$$V_L = V_Z = \frac{R_L V_i}{R_L + R}$$

$$V_{i_{min}} = \frac{(R_L + R) V_Z}{R_L}$$

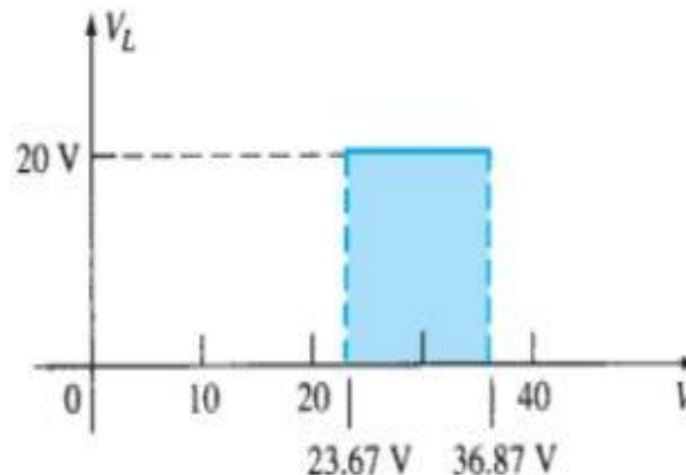
Solution: Continues

$$V_{i_{\min}} = \frac{(R_L + R)V_Z}{R_L} = \frac{(1200 \Omega + 220 \Omega)(20 \text{ V})}{1200 \Omega} = 23.67 \text{ V}$$

$$I_L = \frac{V_L}{R_L} = \frac{V_Z}{R_L} = \frac{20 \text{ V}}{1.2 \text{ k}\Omega} = 16.67 \text{ mA}$$

$$I_{R_{\max}} = I_{ZM} + I_L = 60 \text{ mA} + 16.67 \text{ mA} \\ = 76.67 \text{ mA}$$

$$V_{i_{\max}} = I_{R_{\max}} R + V_Z \\ = (76.67 \text{ mA})(0.22 \text{ k}\Omega) + 20 \text{ V} \\ = 16.87 \text{ V} + 20 \text{ V} \\ = 36.87 \text{ V}$$



Question No. 4: Design a Zener diode regulator that maintains output voltage at 10V for an input voltage variation $20V \pm 10\%$ and a load current variation of $30mA \pm 20\%$. Given $I_{zmin} = 2mA$ and $P_{zmax} = 0.5W$

Solution: It is a case of both input voltage and output current varying Voltage regulator

$$R_{smin} = \frac{V_{imax} - V_z}{I_{zmax} - I_{Lmin}} \quad R_{smax} = \frac{V_{imin} - V_z}{I_{zmin} - I_{Lmax}}$$

Solution: Continues

$$V_i = 20 \pm 2, V_{i\min} = 18V, V_{i\max} = 22V$$

$$I_L = 30 \pm 6, I_{L\min} = 24mA, I_{L\max} = 36mA, V_z = 10V$$

$$I_{z\min} = 2mA, I_{z\max} = \frac{P_{Z\max}}{V_z} = 50mA, \text{ substituting the values}$$

$$R_{s\min} = 162\Omega, R_{s\max} = 210\Omega$$

NOTE: In every design problem circuit should be drawn



THANKYOU

Department of Electronics and Communication