



Engineering Notes

ENGINEERING NOTES are short manuscripts describing new developments or important results of a preliminary nature. These Notes should not exceed 2500 words (where a figure or table counts as 200 words). Following informal review by the Editors, they may be published within a few months of the date of receipt. Style requirements are the same as for regular contributions (see inside back cover).

Unit Quaternion from Rotation Matrix

F. Landis Markley*
NASA Goddard Space Flight Center,
Greenbelt, Maryland 20771

DOI: 10.2514/1.31730

Introduction

It is well known that a 3×3 proper orthogonal rotation matrix, or attitude matrix, can be expressed in terms of a quaternion

$$\mathbf{q} = [q_1 \quad q_2 \quad q_3 \quad q_4]^T \quad (1)$$

as [1,2]

A

$$= \begin{bmatrix} q_1^2 - q_2^2 - q_3^2 + q_4^2 & 2(q_1q_2 + q_3q_4) & 2(q_1q_3 - q_2q_4) \\ 2(q_1q_2 - q_3q_4) & -q_1^2 + q_2^2 - q_3^2 + q_4^2 & 2(q_2q_3 + q_1q_4) \\ 2(q_1q_3 + q_2q_4) & 2(q_2q_3 - q_1q_4) & -q_1^2 - q_2^2 + q_3^2 + q_4^2 \end{bmatrix} \quad (2)$$

where the quaternion is assumed to have unit norm

$$\|\mathbf{q}\|^2 \triangleq \mathbf{q}^T \mathbf{q} = q_1^2 + q_2^2 + q_3^2 + q_4^2 = 1 \quad (3)$$

Often one must find the quaternion corresponding to a given rotation matrix. Of the many methods that have been proposed for performing this computation [3–9], Shepperd's algorithm [5], which is singularity free and requires only one square root, has been the most widely applied. In this Note, we review Shepperd's algorithm and present a variant that always produces a normalized quaternion even if numerical errors cause the matrix A to be only approximately orthogonal. This modification of Shepperd's algorithm also provides a very efficient method for computing an exactly orthogonal matrix that is close to an approximately orthogonal matrix.

Shepperd's Algorithm

The following relations for all the products of two quaternion components are easily derived from Eqs. (2) and (3):

$$4q_i^2 = 1 + A_{ii} - A_{jj} - A_{kk} = 1 - \text{tr}A + 2A_{ii} \quad (4a)$$

$$4q_4^2 = 1 + A_{11} + A_{22} + A_{33} = 1 - \text{tr}A + 2 \text{tr}A \quad (4b)$$

$$4q_iq_j = A_{ij} + A_{ji} \quad (4c)$$

$$4q_iq_k = A_{jk} - A_{kj} \quad (4d)$$

where $\{i, j, k\}$ is a cyclic permutation of $\{1, 2, 3\}$, and $\text{tr}A$ denotes the trace of A . Shepperd's algorithm first compares the right sides of Eqs. (4a) and (4b) to see which of the quantities q_i^2 for $i = 1, 2, 3, 4$ is largest. The unusual form of expressing the rightmost member of Eq. (4b) shows that this is equivalent to finding the largest of $\text{tr}A$ and A_{ii} , saving some computation. Note that all the quantities $4q_i^2$ are positive, and that Eq. (3) or Eqs. (4a) and (4b) show that they sum to 4. Thus, at least one of the right-hand sides of Eqs. (4a) and (4b) must be greater than or equal to unity.

In the case that q_4^2 is larger than any of the other q_i^2 , Shepperd's algorithm computes q_4 from Eq. (4b) and the other components from Eq. (4d), giving

$$q_4 = \pm \frac{1}{2}(1 + A_{11} + A_{22} + A_{33})^{1/2} \quad (5a)$$

$$q_i = (A_{jk} - A_{kj})/4q_4 \quad \text{for } i = 1, 2, 3 \quad (5b)$$

We observe the well-known twofold sign ambiguity in the quaternion. If q_i for $i \neq 4$ is the largest quaternion component in magnitude, it is computed from Eq. (4a) and the other quaternion components are computed from Eqs. (4c) and (4d), giving

$$q_i = \pm \frac{1}{2}(1 + A_{ii} - A_{jj} - A_{kk})^{1/2} \quad (6a)$$

$$q_j = (A_{ij} + A_{ji})/4q_i \quad (6b)$$

$$q_k = (A_{ik} + A_{ki})/4q_i \quad (6c)$$

$$q_4 = (A_{jk} - A_{kj})/4q_i \quad (6d)$$

where $\{i, j, k\}$ is a cyclic permutation of $\{1, 2, 3\}$ as before. Shuster and Natanson have commented on the relation between the four possible branches in Shepperd's algorithm and the method of sequential rotations [10]. Shepperd's algorithm is guaranteed to produce a precisely normalized quaternion only if A is precisely orthogonal.

Modification of Shepperd's Algorithm

For the modification of Shepperd's algorithm, we consider the four 4-component vectors

$$\mathbf{x}^{(i)} \triangleq 4q_i\mathbf{q} \quad \text{for } i = 1, 2, 3, 4 \quad (7)$$

Each of the four components of each $\mathbf{x}^{(i)}$ is given by the right side of one of the equations of Eqs. (4), so these vectors are easily computable from the components of the rotation matrix. Explicitly,

Received 20 April 2007; revision received 4 September 2007; accepted for publication 20 September 2007. This material is declared a work of the U.S. Government and is not subject to copyright protection in the United States. Copies of this paper may be made for personal or internal use, on condition that the copier pay the \$10.00 per-copy fee to the Copyright Clearance Center, Inc., 222 Rosewood Drive, Danvers, MA 01923; include the code 0731-5090/08 \$10.00 in correspondence with the CCC.

*Aerospace Engineer, Guidance, Navigation, and Control Systems Engineering Branch, Code 591.

$$\mathbf{x}^{(1)} = \begin{bmatrix} 1 + A_{11} - A_{22} - A_{33} \\ A_{12} + A_{21} \\ A_{13} + A_{31} \\ A_{23} - A_{32} \end{bmatrix} \quad (8a)$$

$$\mathbf{x}^{(2)} = \begin{bmatrix} A_{21} + A_{12} \\ 1 + A_{22} - A_{33} - A_{11} \\ A_{23} + A_{32} \\ A_{31} - A_{13} \end{bmatrix} \quad (8b)$$

$$\mathbf{x}^{(3)} = \begin{bmatrix} A_{31} + A_{13} \\ A_{32} + A_{23} \\ 1 + A_{33} - A_{11} - A_{22} \\ A_{12} - A_{21} \end{bmatrix} \quad (8c)$$

$$\mathbf{x}^{(4)} = \begin{bmatrix} A_{23} - A_{32} \\ A_{31} - A_{13} \\ A_{12} - A_{21} \\ 1 + A_{11} + A_{22} + A_{33} \end{bmatrix} \quad (8d)$$

Equation (7) shows that each of the $\mathbf{x}^{(i)}$ is a scalar multiple of \mathbf{q} , so we can obtain the unit quaternion by computing and normalizing any one of the $\mathbf{x}^{(i)}$

$$\mathbf{q} = \pm \mathbf{x}^{(i)} / \|\mathbf{x}^{(i)}\| \quad (9)$$

As in Shepperd's method, choosing the $\mathbf{x}^{(i)}$ corresponding to the maximum value of q_i^2 minimizes numerical errors. This selection is made by Shepperd's procedure of finding the largest of $\text{tr}A$ and A_{ii} .

This method of extracting a quaternion from a rotation matrix requires the same number of square roots as Shepperd's method, namely one, but one more division and a few more additions and multiplications. A slightly modified form of this method was previously used to extract a quaternion from a scalar multiple of the attitude matrix [11].

Orthogonalization

Strapdown inertial systems often employ the numerical integration of a rotation matrix that can lose orthogonality due to accumulation of roundoff error. Various methods have been proposed to restore orthogonality, some approximate or iterative and often requiring matrix inversion [12–14]. Equations (8) and (9) provide an exact (within machine precision) noniterative method for restoring orthogonality by simply substituting the result of Eq. (9) into Eq. (2) to produce a new matrix A_{orth} . The normalization condition of Eq. (3) guarantees that A_{orth} is orthogonal. Because Eq. (2) is a homogeneous quadratic function of \mathbf{q} , the square root in Eq. (9) can be avoided if we only need to compute A_{orth} and not \mathbf{q} ; the matrix elements of A_{orth} are rational functions of the matrix elements of A . This computation is much less expensive than any previously proposed for orthogonalization.

Conclusions

It is interesting to see how well this procedure recovers an orthogonal matrix from a rotation matrix corrupted by computational errors. The computational errors are modeled as independent random numbers uniformly distributed in $[\varepsilon, -\varepsilon]$ added to each component of the true rotation matrix. The measure of performance is the rotation angle vector $\boldsymbol{\theta}$ representing the rotation from A_{orth} to the true rotation matrix. Numerical simulation or analysis to lowest nonzero order in ε shows that $\boldsymbol{\theta}$ has zero mean and that the expectation of $|\boldsymbol{\theta}|^2$ is $(7q_i^{-2} - 1)\varepsilon^2/12 \text{ rad}^2$, where q_i is the quaternion component on the right side of Eq. (7) corresponding to the particular instance of Eqs. (8a–8d) used to compute the quaternion. This is the component having the largest magnitude, and the quaternion normalization

condition of Eq. (3) ensures that $1 \leq q_i^{-2} \leq 4$. This shows the importance of choosing the $\mathbf{x}^{(i)}$ corresponding to the maximum value of q_i^2 ; otherwise the errors could be unbounded. With the optimal choice, the standard deviation of the attitude error, the square root of the expectation of $|\boldsymbol{\theta}|^2$, will be between $\varepsilon/\sqrt{2}$ and $3\varepsilon/2 \text{ rad}$. Averaging the expectation of $|\boldsymbol{\theta}|^2$ over uniformly distributed random rotation matrices (i.e., for quaternions uniformly distributed on the unit sphere S^3 in four-dimensional space) gives an overall attitude error standard deviation of $0.964\varepsilon \text{ rad}$.

This method does not solve the orthogonal Procrustes problem, which finds the orthogonal matrix closest to A in the Frobenius norm, that is, the orthogonal matrix A_{orth} minimizing $\|A_{\text{orth}} - A\|_F^2$, or equivalently the quaternion minimizing $\|A(q) - A\|_F^2$, where the Frobenius norm of an $N \times N$ real matrix is defined as

$$\|M\|_F^2 = \sum_{i,j=1}^N M_{ij}^2$$

The solution to the Procrustes problem can be found by a modification of Shuster's quaternion estimator (QUEST) [15] or of Davenport's q method [9,16]. The latter finds the quaternion representation of the closest orthogonal matrix as the eigenvector with the largest eigenvalue of the symmetric 4×4 matrix

$$K \equiv \begin{bmatrix} A + A^T - I_{3 \times 3} \text{tr}A & \mathbf{z} \\ \mathbf{z}^T & \text{tr}A \end{bmatrix} \quad (10)$$

where $I_{3 \times 3}$ is the 3×3 identity matrix and

$$\mathbf{z} \equiv \begin{bmatrix} A_{23} - A_{32} \\ A_{31} - A_{13} \\ A_{12} - A_{21} \end{bmatrix} \quad (11)$$

Under the same assumptions on the errors in A , the standard deviation of the angular errors resulting from the Procrustes method is $\varepsilon/\sqrt{2} \text{ rad}$ independent of the true rotation matrix. We see that the Procrustes method produces a result that is somewhat closer to the truth in these random error tests, but with significantly greater computational burden. The difference between the two methods is negligible for the level of numerical errors expected in computing the attitude matrix, however. It should also be emphasized that the Procrustes method is not optimal unless the errors in A are isotropic [17].

Acknowledgment

I would like to thank Malcolm Shuster for many fruitful discussions. I would also like to thank an anonymous reviewer for a valuable observation that motivated the entire Conclusions section.

References

- [1] Markley, F. L., "Parameterization of the Attitude," *Spacecraft Attitude Determination and Control*, edited by J. R. Wertz, and D. Reidel, Dordrecht, The Netherlands, 1978, pp. 414–416.
- [2] Shuster, M. D., "A Survey of Attitude Representations," *Journal of the Astronautical Sciences*, Vol. 41, No. 4, Oct.–Dec. 1993, pp. 439–517.
- [3] Grubin, C., "Derivation of the Quaternion Scheme via the Euler Axis and Angle," *Journal of Spacecraft and Rockets*, Vol. 7, No. 10, Oct. 1970, pp. 1261–1263.
- [4] Klumpp, A. R., "Singularity-Free Extraction of a Quaternion from a Direction-Cosine Matrix," *Journal of Spacecraft and Rockets*, Vol. 13, No. 12, Dec. 1976, pp. 754–755.
- [5] Shepperd, S. W., "Quaternion from Rotation Matrix," *Journal of Guidance and Control*, Vol. 1, No. 3, May–June 1978, pp. 223–224.
- [6] Spurrier, R. A., "Comment on Singularity-Free Extraction of a Quaternion from a Direction-Cosine Matrix," *Journal of Spacecraft and Rockets*, Vol. 15, No. 4, July–Aug. 1978, p. 255.
- [7] Klumpp, A. R., "Reply by Author to R. A. Spurrier," *Journal of Spacecraft and Rockets*, Vol. 15, No. 4, July–Aug. 1978, p. 256.
- [8] Grubin, C., "Quaternion Singularity Revisited," *Journal of Guidance and Control*, Vol. 2, No. 3, May–June 1979, pp. 255–256.
- [9] Bar-Itzhack, I. Y., "New Method for Extracting the Quaternion from a

- Rotation Matrix,” *Journal of Guidance, Control, and Dynamics*, Vol. 23, No. 6, Nov.–Dec. 2000, pp. 1085–1087.
- [10] Shuster, M. D., and Natanson, G. A., “Quaternion Computation from a Geometric Point of View,” *Journal of the Astronautical Sciences*, Vol. 41, No. 4, Oct.–Dec. 1993, pp. 545–556.
- [11] Markley, F. L., “New Quaternion Attitude Estimation Method,” *Journal of Guidance, Control, and Dynamics*, Vol. 17, No. 2, March–April 1994, pp. 407–409.
- [12] Bar-Itzhack, I. Y., and Fegley, K. A., “Orthogonalization Techniques of a Direction Cosine Matrix,” *IEEE Transactions on Aerospace and Electronic Systems*, Vol. 5, No. 5, Sept. 1969, pp. 798–804. doi:10.1109/TAES.1969.309878
- [13] Carta, D. G., and Lackowski, D. H., “Estimation of Orthogonal Transformations in Strapdown Inertial Systems,” *IEEE Transactions on Automatic Control*, Vol. 17, No. 1, Feb. 1972, pp. 97–100. doi:10.1109/TAC.1972.1099871
- [14] Bar-Itzhack, I. Y., and Meyer, J., “On the Convergence of Iterative Orthogonalization Processes,” *IEEE Transactions on Aerospace and Electronic Systems*, Vol. 12, No. 2, March 1976, pp. 146–151. doi:10.1109/TAES.1976.308289
- [15] Shuster, M. D., and Oh, S. D., “Three-Axis Attitude Determination from Vector Observations,” *Journal of Guidance and Control*, Vol. 4, No. 1, Jan.–Feb. 1981, pp. 70–77.
- [16] Markley, F. L., and Mortari, M., “Quaternion Attitude Estimation Using Vector Measurements,” *Journal of the Astronautical Sciences*, Vol. 48, Nos. 2–3, April–Sept. 2000, pp. 359–380.
- [17] Shuster, M. D., “The Generalized Wahba Problem,” *Journal of the Astronautical Sciences*, Vol. 54, No. 2, April–June 2006, pp. 245–259.