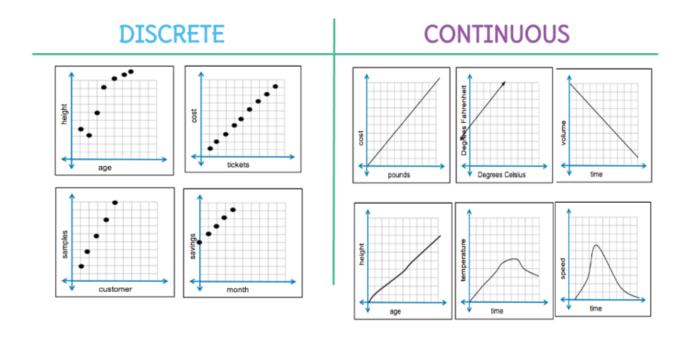
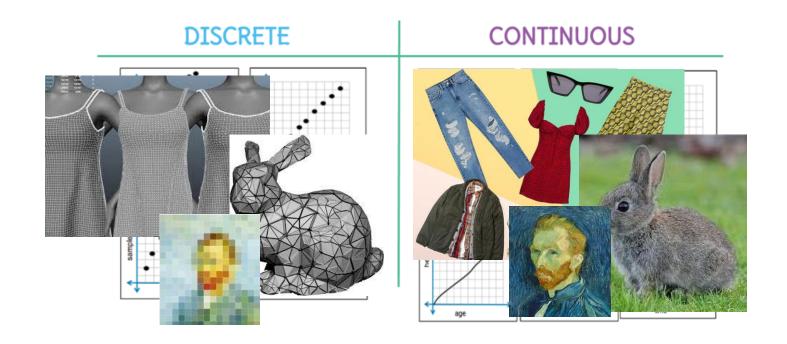
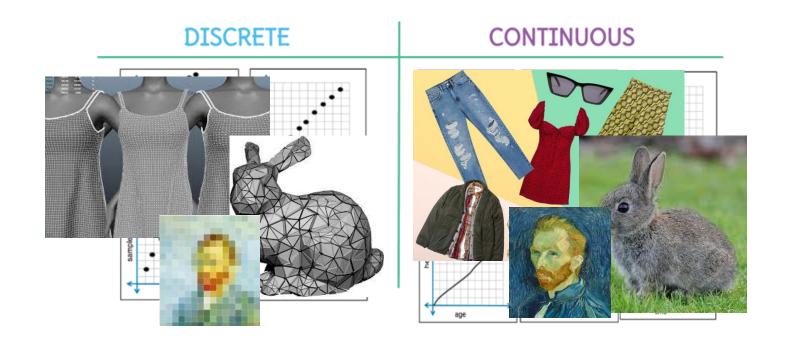


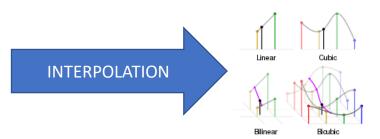
BEFORE THAT





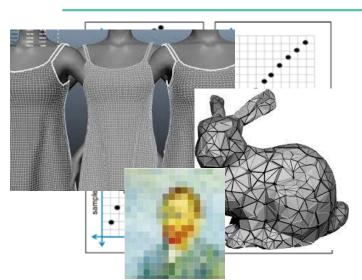


DISCRETIZATION

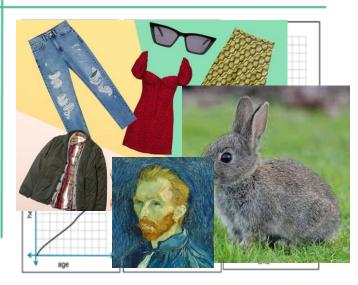


Differentiable : ∇f , Δf , $\frac{\partial u}{\partial x}$, ...





CONTINUOUS

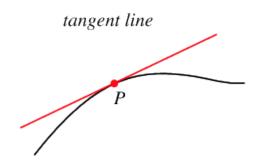


DISCRETIZATION

$$f(x, y, z, ...) = a single float$$

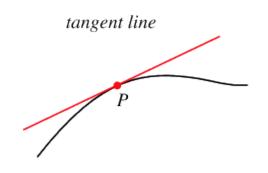
$$f(x, y, z, ...) = a single float$$

$$\frac{\partial f}{\partial x} = \text{How } f \text{ changes when } x \text{ changes a tiny bit}$$



$$f(x, y, z, ...) = a$$
 single float

$$\frac{\partial f}{\partial x}$$
 => How f changes when x changes a tiny bit



$$\nabla f = \left[\frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z}, \dots \right] \Rightarrow \text{How } f \text{ changes when } x, y, z, \dots \text{ change a tiny bit}$$

$$f(x, y, z, ...) = a single float$$



$$\nabla f = \left[\frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z}, \dots \right]$$

$$f\left(x + \frac{\partial f}{\partial x}, y + \frac{\partial f}{\partial y}, z + \frac{\partial f}{\partial z}, ...\right) =$$

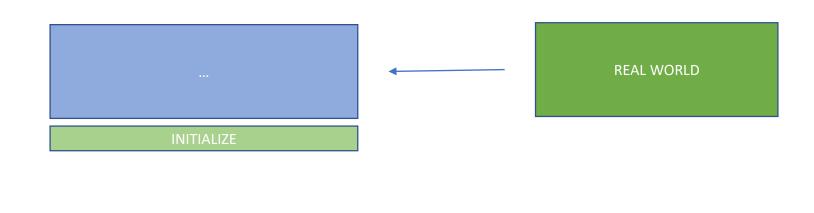
$$f(x, y, z, ...) = a single float$$

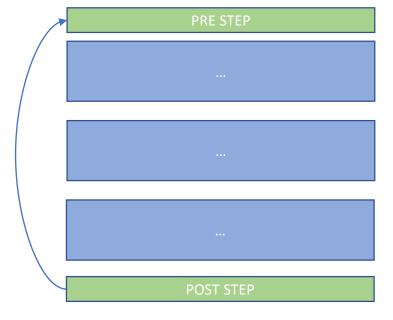
$$\nabla f = \left[\frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z}, \dots \right]$$

$$f\left(x - \frac{\partial f}{\partial x}, y - \frac{\partial f}{\partial y}, z - \frac{\partial f}{\partial z}, \dots\right) =$$

PHYSICS BASED ANIMATION







DISCRETIZATION REAL WORLD

INITIALIZE

PRE STEP

MEASURE DEFORMATION / CHANGE

PENALIZE

TIME INTEGRATION

POST STEP

DISCRETIZATION REAL WORLD

INITIALIZE

PRE STEP

MEASURE DEFORMATION / CHANGE

PENALIZE

TIME INTEGRATION

POST STEP

DISCRETIZATION



DISCRETE REPRESENTATION

LAGRANGIAN



Particle Fluid

Smoothed-particle hydrodynamics (SPH)

Spring Simulation

Position Based Dynamics /
Extended PBD





Tetrahedral Simulation
Tetrahedral FEM (Finite Element Method)

DISCRETE REPRESENTATION

LAGRANGIAN



Particle Fluid

Smoothed-particle hydrodynamics (SPH)

Spring Simulation
Position Based Dynamics /
Extended PBD





Tetrahedral Simulation
Tetrahedral FEM (Finite Element Method)

EULERIAN



Smoke Simulation

Voxel Based

DISCRETE REPRESENTATION

LAGRANGIAN



Particle Fluid

Smoothed-particle hydrodynamics (SPH)

Spring Simulation
Position Based Dynamics /
Extended PBD



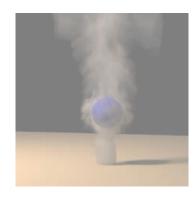


Tetrahedral Simulation
Tetrahedral FEM (Finite Element Method)



FLIP/PIC/APIC/POLYPIC/...

EULERIAN



Smoke Simulation
Voxel Based



MPM
Material Point Method

DISCRETIZATION REAL WORLD

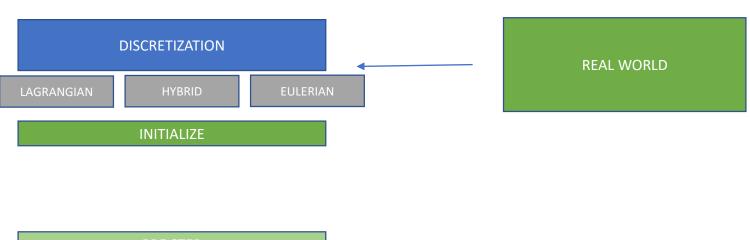
INITIALIZE

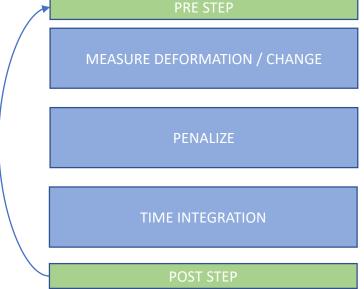
MEASURE DEFORMATION / CHANGE

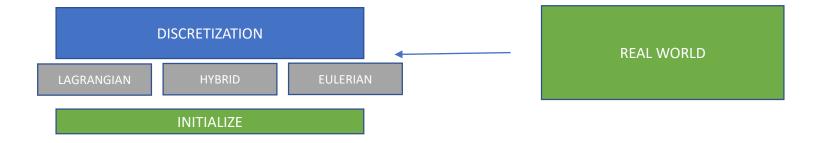
PENALIZE

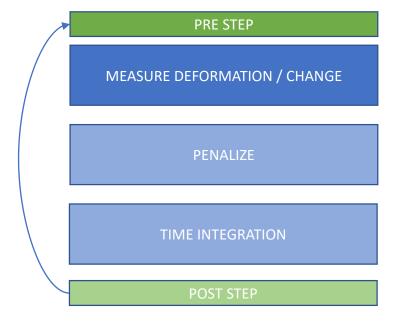
TIME INTEGRATION

POST STEP









DEFORMATION / CHANGE



DISCRETE MODEL

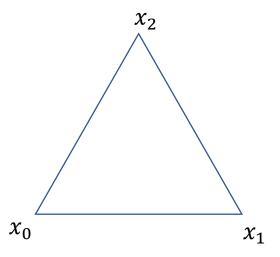
GEOMETRIC BASED

Distance

$$x_0$$
 x_1

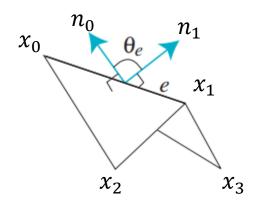
$$e = ||x_1 - x_0||$$

Area



$$A = \frac{\|(x_1 - x_0) \times (x_2 - x_0)\|}{2}$$

Dihedral Angle

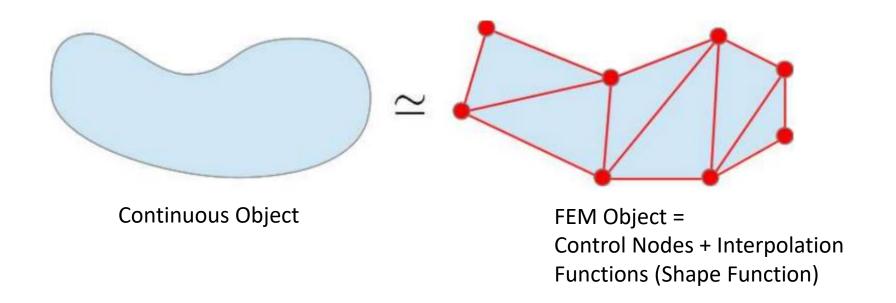


$$\theta = \arctan 2(|n_0 \times n_1|, n_0 \cdot n_1)$$

CONTINUOUS MODEL - FEM

CONTINUUM MECHANICS

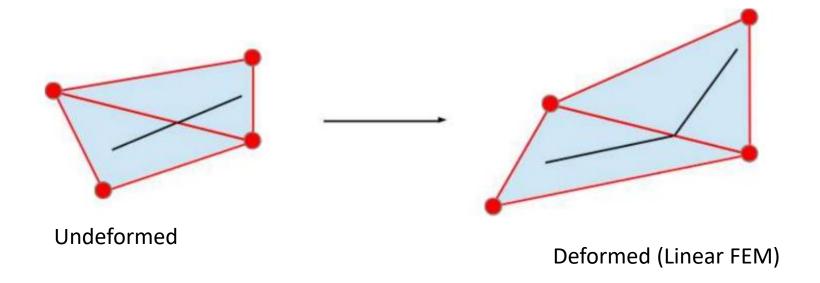
 GOAL: Use the object as a continuous medium to apply differential calculus and compute an elastic energy



CONTINUOUS MODEL - FEM

CONTINUUM MECHANICS

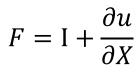
- Continuity of deformation depends on the Shape Function (Linear / Non-Linear)
- Build a continuous deformation field : u(x)



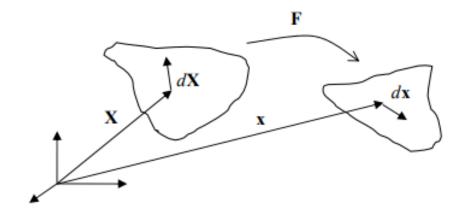
CONTINUUM MECHANICS - DEFORMATION GRADIENT

Deformation Gradient

$$F = \frac{\partial x_{i}}{\partial X_{j}} = \begin{vmatrix} \frac{\partial x}{\partial X} & \frac{\partial x}{\partial Y} \\ \frac{\partial y}{\partial X} & \frac{\partial y}{\partial Y} \end{vmatrix}$$



$$u = x - X$$



Rest

Deformed

CONTINUUM MECHANICS - DEFORMATION GRADIENT

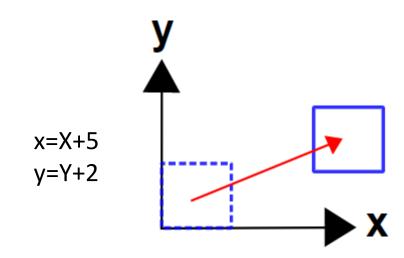
Deformation Gradient

$$F = \frac{\partial x_{i}}{\partial X_{j}} = \begin{vmatrix} \frac{\partial x}{\partial X} & \frac{\partial x}{\partial Y} \\ \frac{\partial y}{\partial X} & \frac{\partial y}{\partial Y} \end{vmatrix}$$

$$F = I + \frac{\partial u}{\partial X}$$

$$u = x - X$$

Rigid Displacement



$$F = I = \begin{vmatrix} 1 & 0 \\ 0 & 1 \end{vmatrix}$$

CONTINUUM MECHANICS - DEFORMATION GRADIENT

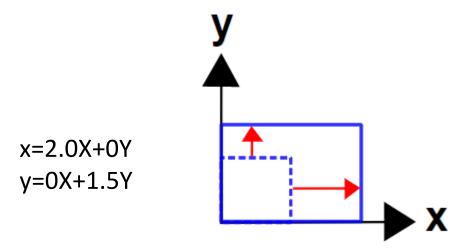
Deformation Gradient

$$F = \frac{\partial x_{i}}{\partial X_{j}} = \begin{vmatrix} \frac{\partial x}{\partial X} & \frac{\partial x}{\partial Y} \\ \frac{\partial y}{\partial X} & \frac{\partial y}{\partial Y} \end{vmatrix}$$

$$F = I + \frac{\partial u}{\partial X}$$

$$u = x - X$$

Stretching



$$F = \begin{vmatrix} 2.0 & 0 \\ 0 & 1.5 \end{vmatrix}$$

CONTINUUM MECHANICS – DEFORMATION GRADIENT

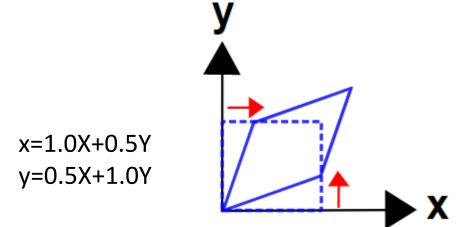
Deformation Gradient

$$F = \frac{\partial x_{i}}{\partial X_{j}} = \begin{vmatrix} \frac{\partial x}{\partial X} & \frac{\partial x}{\partial Y} \\ \frac{\partial y}{\partial X} & \frac{\partial y}{\partial Y} \end{vmatrix}$$

$$F = I + \frac{\partial u}{\partial X}$$

$$u = x - X$$

Shear



$$F = \begin{vmatrix} 1.0 & 0.5 \\ 0.5 & 1.0 \end{vmatrix}$$

CONTINUUM MECHANICS – DEFORMATION GRADIENT

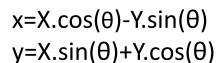
Deformation Gradient

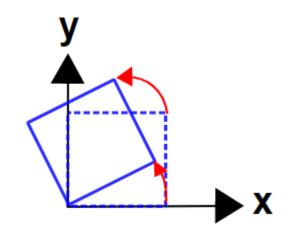
$$F = \frac{\partial x_{i}}{\partial X_{j}} = \begin{vmatrix} \frac{\partial x}{\partial X} & \frac{\partial x}{\partial Y} \\ \frac{\partial y}{\partial X} & \frac{\partial y}{\partial Y} \end{vmatrix}$$

$$F = I + \frac{\partial u}{\partial X}$$

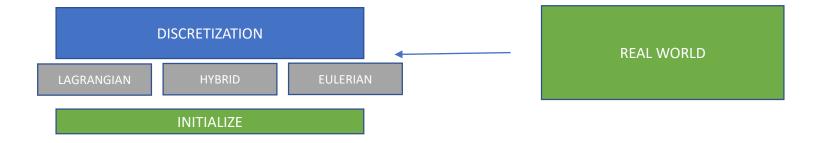
$$u = x - X$$

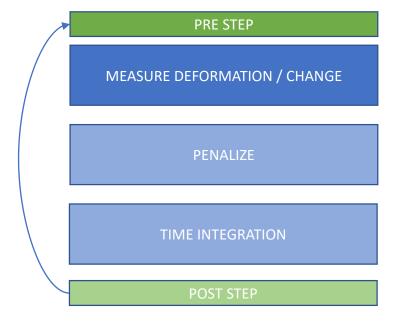
Rigid Rotation

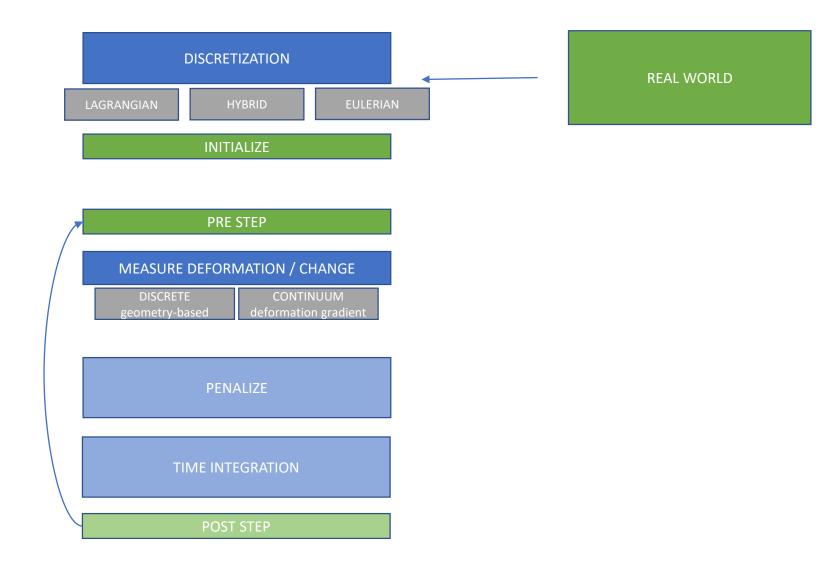


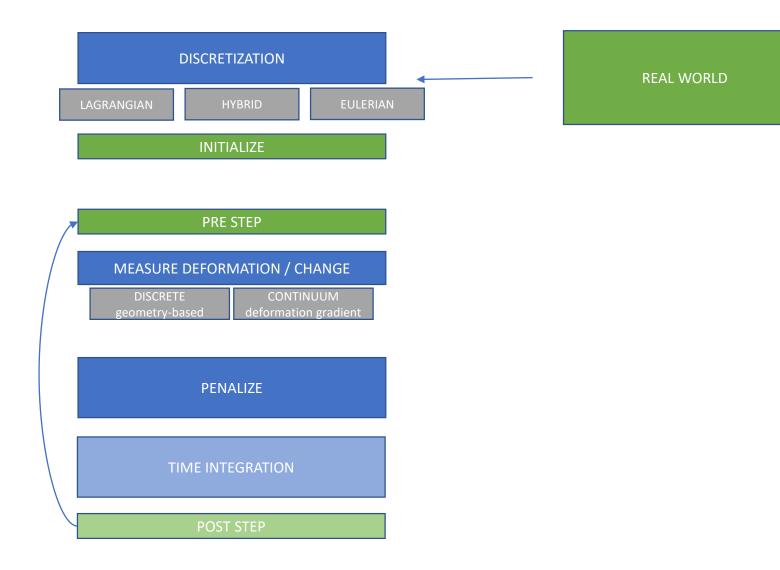


$$F = \begin{vmatrix} \cos(\theta) & -\sin(\theta) \\ \sin(\theta) & \cos(\theta) \end{vmatrix}$$









PENALIZE



PENALIZE

- FORCE BASED
- VELOCITY BASED (IMPULSE)
- POSITION BASED

PENALIZE

- FORCE BASED
- VELOCITY BASED (IMPULSE)
- POSITION BASED

ENERGY FROM DISCRETE MODEL

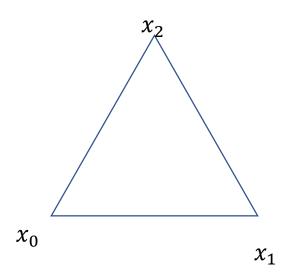
GEOMETRIC DEFORMATION

• Geometric Deformation => Energy (positive scalar function)

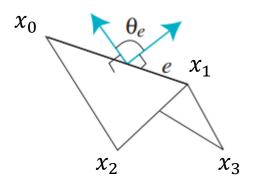
Distance Constraint

 x_0 x_1

Area Constraint



Bending Constraint



ENERGY FROM DISCRETE MODEL

GEOMETRIC DEFORMATION

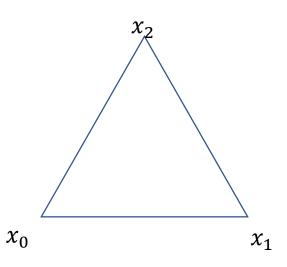
• Geometric Deformation => Energy (positive scalar function)

Distance Constraint



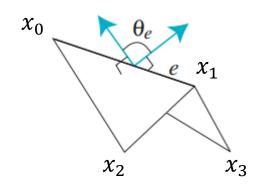
 $C(x0, x1) = (1 - ||e||/||\bar{e}||)^2 ||\bar{e}||$

Area Constraint



 $C(x0, x1, x2) = (1 - ||A||/||\bar{A}||)^2 ||\bar{A}||$

Bending Constraint



 $C(x0, x1, x2, x3) = (\theta_e - \bar{\theta}_e)^2 ||\bar{e}||/\bar{h}_e$

ENERGY FROM DISCRETE MODEL

GEOMETRIC DEFORMATION

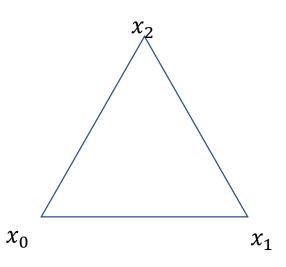
Geometric Deformation => Energy (positive scalar function)

Distance Constraint

 x_0 x_1

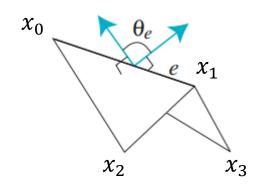
 $C(x0, x1) = (1 - ||e||/||\bar{e}||)^2 ||\bar{e}||$

Area Constraint

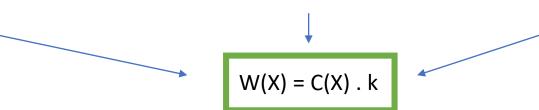


 $C(x0, x1, x2) = (1 - ||A||/||\bar{A}||)^2 ||\bar{A}||$

Bending Constraint



 $C(x0, x1, x2, x3) = (\theta_e - \bar{\theta}_e)^2 ||\bar{e}||/\bar{h}_e$



CONTINUUM MECHANICS - DEFORMATION TO ENERGY



$$F = I + \frac{\partial u}{\partial X}$$

CONTINUUM MECHANICS – DEFORMATION TO ENERGY

Deformation Gradient

Strain

Constitutive Model

Energy

$$F = I + \frac{\partial u}{\partial X}$$

Linear Cauchy

$$E = \frac{1}{2}(F^T + F) - I$$

Non-linear Green

$$E = \frac{1}{2}(F^T F - I)$$

CONTINUUM MECHANICS – DEFORMATION TO ENERGY



 $F = I + \frac{\partial u}{\partial X}$

Strain

Linear Cauchy

$$E = \frac{1}{2}(F^T + F) - I$$

Non-linear Green

$$E = \frac{1}{2}(F^T F - I)$$

Constitutive Model

- Saint-Venant Kirchhoff
- Corotated Linear Elasticity
- Neo-Hookean
- ..

User Parameters $\lambda = \frac{vY}{(1+v)(1-2v)}$ $\mu = \frac{Y}{2(1+v)}$

Energy

CONTINUUM MECHANICS – DEFORMATION TO ENERGY



 $F = I + \frac{\partial u}{\partial X}$

Strain

Linear Cauchy

$$E = \frac{1}{2}(F^T + F) - I$$

Non-linear Green

$$E = \frac{1}{2}(F^T F - I)$$

Constitutive Model Strain Energy Density Function (ψ)

- Saint-Venant Kirchhoff
- Corotated Linear Elasticity
- Neo-Hookean

$$\Psi(\mathbf{F}) = \mu \mathbf{E} : \mathbf{E} + \frac{\lambda}{2} tr^2(\mathbf{E})$$

User Parameters Poisson ratio (v) Young's modulus (Y)

$$\lambda = \frac{vY}{(1+v)(1-2v)}$$

$$\mu = \frac{Y}{2(1+v)}$$

Lamé constants (μ, λ)

Energy

CONTINUUM MECHANICS – DEFORMATION TO ENERGY



• Linear Cau

Constitutive Model Strain Energy Density Function (ψ)

Energy



Linear Cauchy

Strain

$$E = \frac{1}{2}(F^T + F) - I$$

Non-linear Green

$$E = \frac{1}{2}(F^T F - I)$$

- Corotated Linear Elasticity
- Neo-Hookean
- ...

$$\Psi(\mathbf{F}) = \mu \|\mathbf{S} - \mathbf{I}\|_F^2 + (\lambda/2) \operatorname{tr}^2(\mathbf{S} - \mathbf{I})$$

$$\mathbf{F} = \mathbf{RS}$$

User Parameters

Poisson ratio (v)

Young's modulus (Y)

Lamé constants (μ , λ)

$$\lambda = \frac{vY}{(1+v)(1-2v)}$$

$$\mu = \frac{Y}{2(1+v)}$$

CONTINUUM MECHANICS – DEFORMATION TO ENERGY



$F = I + \frac{\partial u}{\partial X}$

Strain

Linear Cauchy

$$E = \frac{1}{2}(F^T + F) - I$$

Non-linear Green

$$E = \frac{1}{2}(F^T F - I)$$

Constitutive Model Strain Energy Density Function (ψ)

Energy

- Saint-Venant Kirchhoff
- Corotated Linear Elasticity
- Neo-Hookean
- ...

$$\Psi(I_1, I_3) = \frac{\mu}{2} (I_1 - \log(I_3) - 3) + \frac{\lambda}{8} \log^2(I_3)$$

$$I_1 = \operatorname{tr}(\mathbf{F}^T \mathbf{F})$$

$$I_3 = \det(\mathbf{F}^T \mathbf{F})$$

Lamé constants (μ, λ)

User Parameters

Poisson ratio (v)

Young's modulus (Y)

$$\lambda = \frac{vY}{(1+v)(1-2v)}$$

$$\mu = \frac{Y}{2(1+v)}$$

CONTINUUM MECHANICS – DEFORMATION TO ENERGY



 $F = I + \frac{\partial u}{\partial X}$

Strain

Linear Cauchy

$$E = \frac{1}{2}(F^T + F) - I$$

Non-linear Green

$$E = \frac{1}{2}(F^T F - I)$$

Constitutive Model Strain Energy Density Function (ψ)

scale by volume

- Saint-Venant Kirchhoff
- Corotated Linear Elasticity
- Neo-Hookean
- ..

Energy

W(X)

Lamé constants (μ, λ)

User Parameters

Poisson ratio (v)

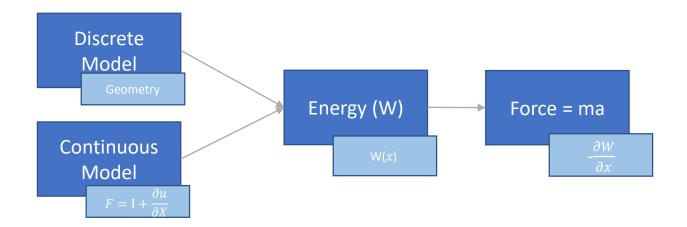
Young's modulus (Y)

$$\lambda = \frac{vY}{(1+v)(1-2v)}$$

$$\mu = \frac{Y}{2(1+v)}$$

DEFINITIONS

• A force is the negative of the derivate(slope) of the potential energy

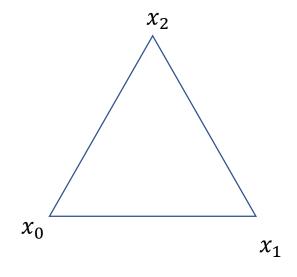


ILLUSTRATIONS

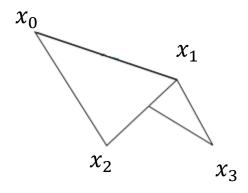
Distance Constraint To Forces

$$f0 = \frac{\partial W}{\partial x_0} \qquad \qquad f1 = \frac{\partial W}{\partial x_1}$$

Area Constraint to Forces



Bending Constraint to Forces



$$f0 + f1 = (0,0)$$

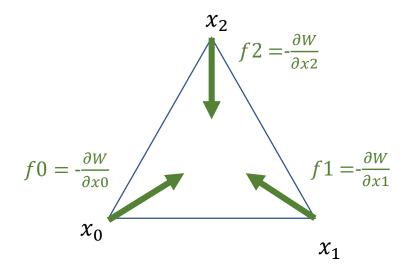
ILLUSTRATIONS

Distance Constraint
To Forces

$$f0 = -\frac{\partial W}{\partial x_0} \qquad \qquad x_1$$

$$f1 = -\frac{\partial W}{\partial x_1}$$

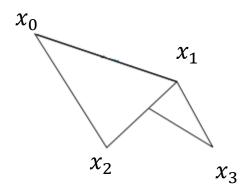
Area Constraint to Forces



$$f0 + f1 = (0,0)$$

$$f0 + f1 + f2 = (0,0)$$

Bending Constraint to Forces

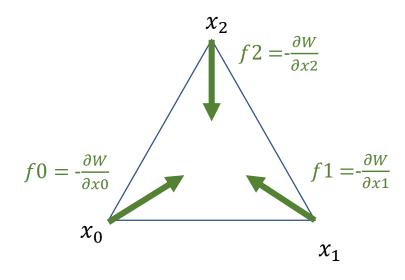


ILLUSTRATIONS

Distance Constraint To Forces

$$f0 = \frac{\partial W}{\partial x_0} \qquad \qquad f1 = \frac{\partial W}{\partial x_1}$$

Area Constraint to Forces



$$f0 + f1 = (0,0)$$

$$f0 + f1 + f2 = (0,0)$$

Bending Constraint to Forces

$$f0 = \frac{\partial W}{\partial x_0}$$

$$x_0$$

$$f1 = \frac{\partial W}{\partial x_1}$$

$$x_1$$

$$f3 = \frac{\partial W}{\partial x_3}$$

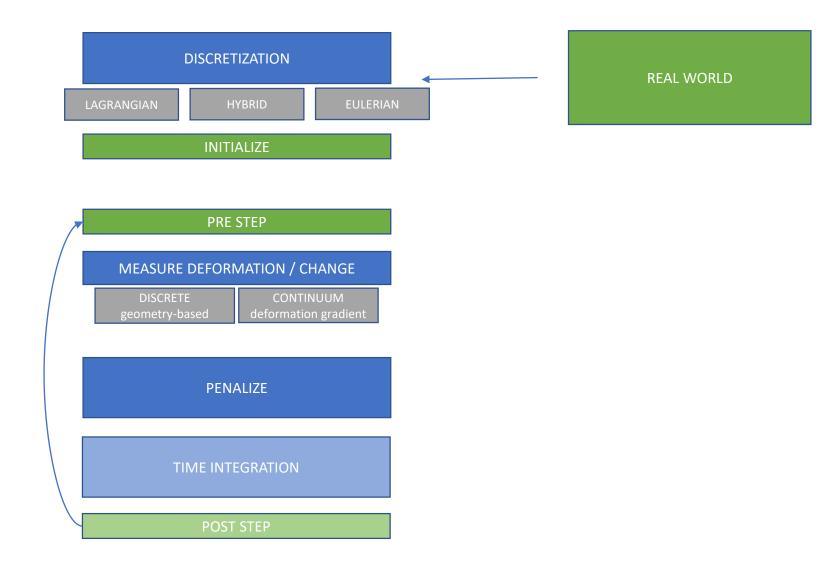
$$f2 = \frac{\partial W}{\partial x_2}$$

$$x_2$$

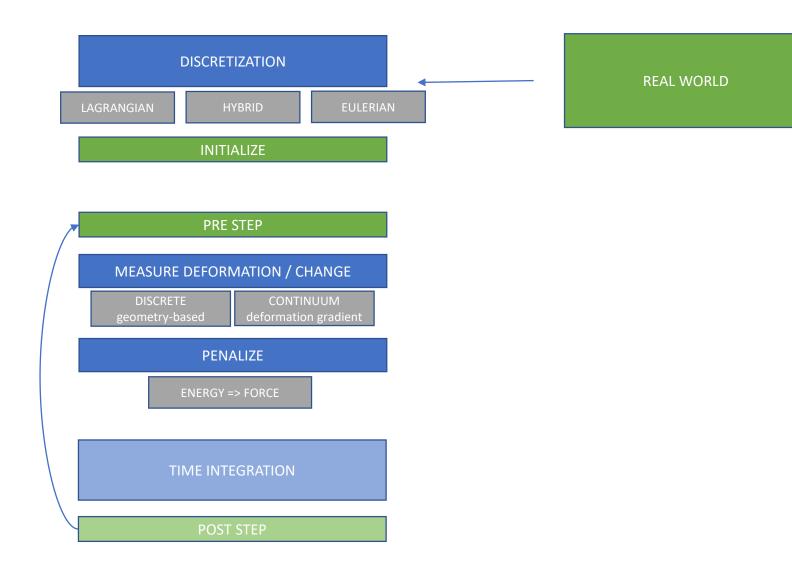
$$x_3$$

$$f0 + f1 + f2 + f3 = (0,0,0)$$

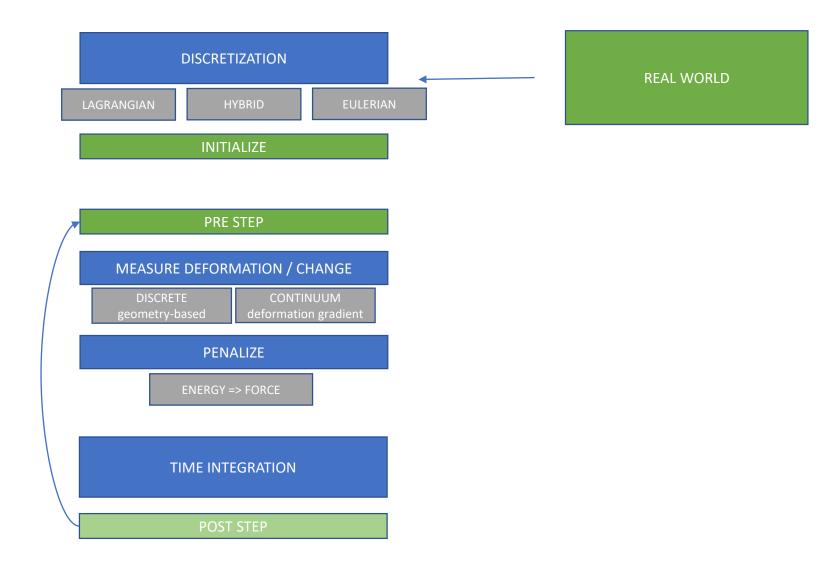
WHAT DO SOLVERS DO



WHAT DO SOLVERS DO

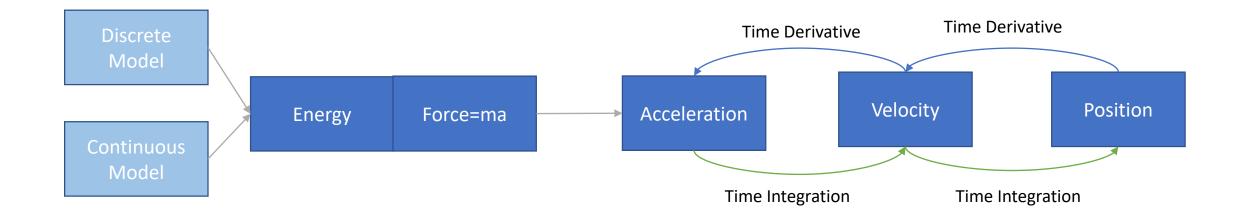


WHAT DO SOLVERS DO



TIME INTEGRATION

PARTICLE STATE



TIME INTEGRATION

EXPLICIT INTEGRATOR

- Forward Euler (Explicit Euler)
- Runge Kutta (RK2, RK4, RK...)
- Mid point

- Easy to implement
- Conditionally stable

- Backward Euler (Implicit Euler)
- Higher order methods

- Difficult to implement
- Unconditionally stable

TIME INTEGRATION

h : timestep (float)

m: mass (float)

v : current velocity(vector2)

p : current position(vector2)

f(): force function (vector2)

TIME INTEGRATION

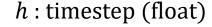


$$next_v = v + h \frac{f(p)}{m}$$
$$next_p = p + hv$$

```
h: timestep (float)m: mass (float)v: current velocity(vector2)p: current position(vector2)
```

f(): force function (vector2)

TIME INTEGRATION



m: mass (float)

v : current velocity(vector2)

p : current position(vector2)

f() : force function (vector 2)

EXPLICIT INTEGRATOR

$$next_v = v + h \frac{f(p)}{m}$$
$$next_p = p + hv$$

$$next_v = v + h \frac{f(next_p)}{m}$$

$$next_p = p + h next_v$$

TIME INTEGRATION



h : timestep (float)

m: mass (float)

v : current velocity(vector2)

p : current position(vector2)

f(): force function (vector2)

EXPLICIT INTEGRATOR

- Single line
- Conditionally stable

- Solve sparse system
- Unconditionally stable

$$\mathbf{next}_{-}\mathbf{v} = \mathbf{v} + h \frac{f(p)}{m}$$

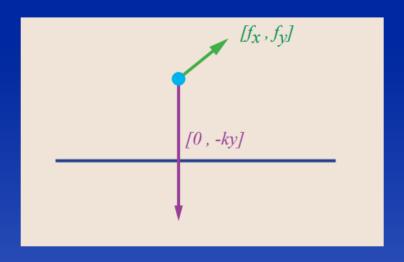
$$next_p = p + hv$$

$$next_v = v + h \frac{f(next_p)}{m}$$

$$next_p = p + h next_v$$

Example: particle-on-line

- A particle *P* in the plane.
- Interactive "dragging" force $[f_x, f_y]$.
- A penalty force [0,-ky] tries to keep P on the x-axis.

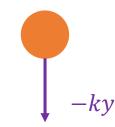


- Suppose you want P to stay within a miniscule ε of the x-axis when you try to pull it off with a huge force f_{max} .
- How big does k have to be? How small must h be?

Baraff, David, and Andrew Witkin. "Implicit Methods: how to not blowup." ACM Transactions on Graphics (SIGGRAPH 1997) (1997).

TIME INTEGRATION

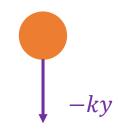




• A spring force -ky tries to keep the particle on the blue line

TIME INTEGRATION

у



• A spring force -ky tries to keep the particle on the blue line

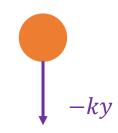
EXPLICIT INTEGRATOR

$$next_y = y + h \frac{-ky}{m}$$

$$next_y = y + h \frac{-k \cdot next_y}{m}$$

TIME INTEGRATION

у



• A spring force -ky tries to keep the particle on the blue line

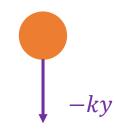
EXPLICIT INTEGRATOR

$$next_y = y + h \frac{-ky}{m}$$

$$next_y = y + h \frac{-k. next_y}{m}$$

TIME INTEGRATION

У



• A spring force -ky tries to keep the particle on the blue line

EXPLICIT INTEGRATOR

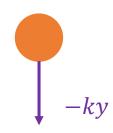
$$next_y = y + h \frac{-ky}{m}$$

$$next_y = y + h \frac{-k \cdot next_y}{m}$$

$$next_y + h \frac{k \cdot next_y}{m} = y$$

TIME INTEGRATION

У



• A spring force -ky tries to keep the particle on the blue line

EXPLICIT INTEGRATOR

$$next_y = y + h \frac{-ky}{m}$$

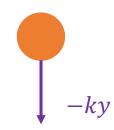
$$next_y = y + h \frac{-k \cdot next_y}{m}$$

$$next_y + h \frac{k \cdot next_y}{m} = y$$

$$next_y(1 + \frac{hk}{m}) = y$$

TIME INTEGRATION

У



• A spring force -ky tries to keep the particle on the blue line

EXPLICIT INTEGRATOR

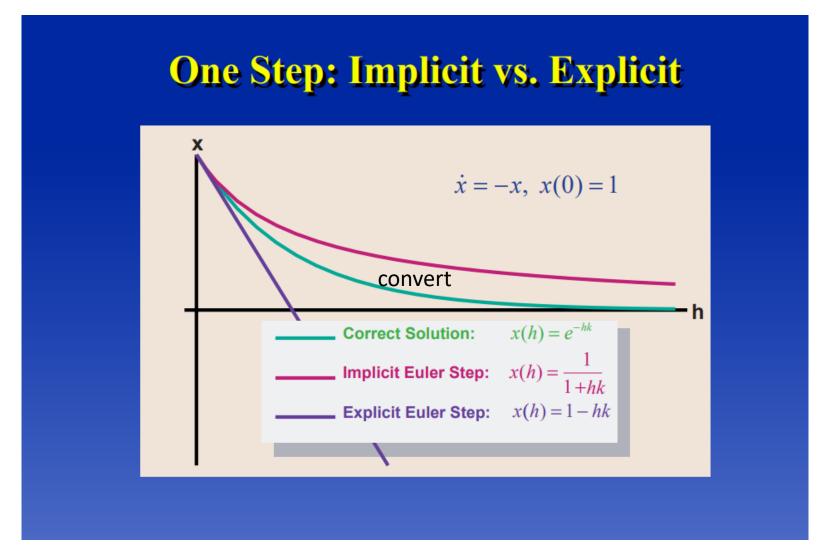
$$next_y = y + h \frac{-ky}{m}$$

$$next_y = y + h \frac{-k \cdot next_y}{m}$$

$$next_y + h \frac{k \cdot next_y}{m} = y$$

$$next_y(1 + \frac{hk}{m}) = y$$

$$next_y = \frac{y}{1 + \frac{hk}{m}}$$



Baraff, David, and Andrew Witkin. "Implicit Methods: how to not blowup." ACM Transactions on Graphics (SIGGRAPH 1997) (1997).

VARIATIONAL IMPLICIT EULER

$$next_v = v + h \frac{f(next_p)}{m}$$

$$next_p = p + h next_v$$

VARIATIONAL IMPLICIT EULER

$$next_v = v + h \frac{f(next_p)}{m}$$

$$next_p = p + h next_v$$



$$v_{n+1} = v_n + hM^{-1}f(x_{n+1})$$

$$x_{n+1} = x_n + hv_{n+1}$$

VARIATIONAL IMPLICIT EULER

$$v_{n+1} = v_n + hM^{-1}f(x_{n+1})$$
$$x_{n+1} = x_n + hv_{n+1}$$

$$x_{n+1} = x_n + h(v_n + hM^{-1}f(x_{n+1}))$$

$$x_{n+1} = x_n + hv_n + h^2M^{-1}f(x_{n+1}))$$

$$x_{n+1} - x_n - hv_n = h^2M^{-1}f(x_{n+1}))$$

$$M(x_{n+1} - x_n - hv_n) = h^2f(x_{n+1})$$

VARIATIONAL IMPLICIT EULER

$$M(x_{n+1} - x_n - hv_n) = h^2 f(x_{n+1})$$

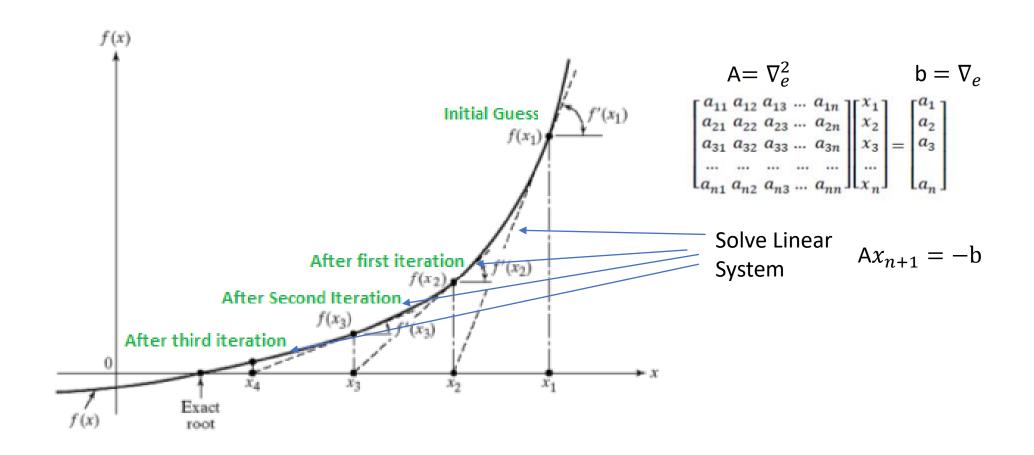


$$e(x_{n+1}) = \frac{1}{2h^2} (x_{n+1} - x_n - hv_n)^T M(x_{n+1} - x_n - hv_n) + W(x_{n+1})$$

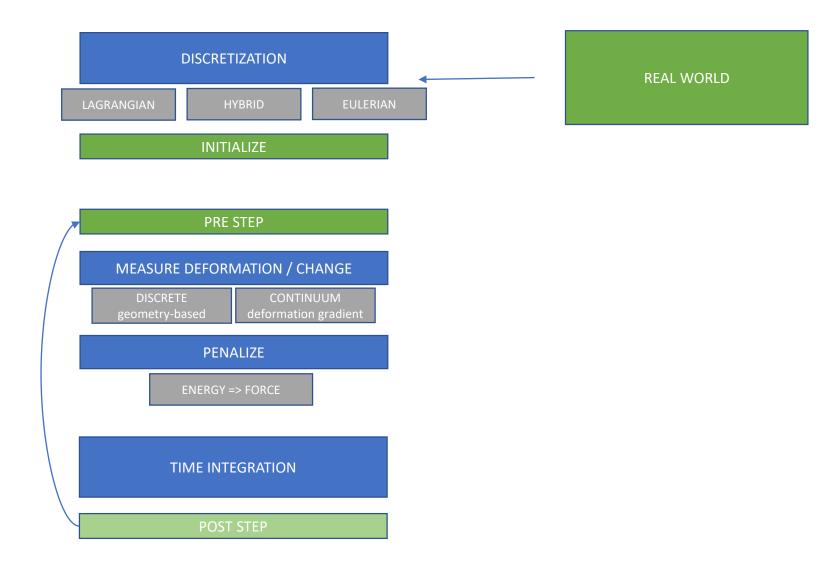
Minimize the scalar function e(...) with argument x_{n+1}

VARIATIONAL IMPLICIT EULER

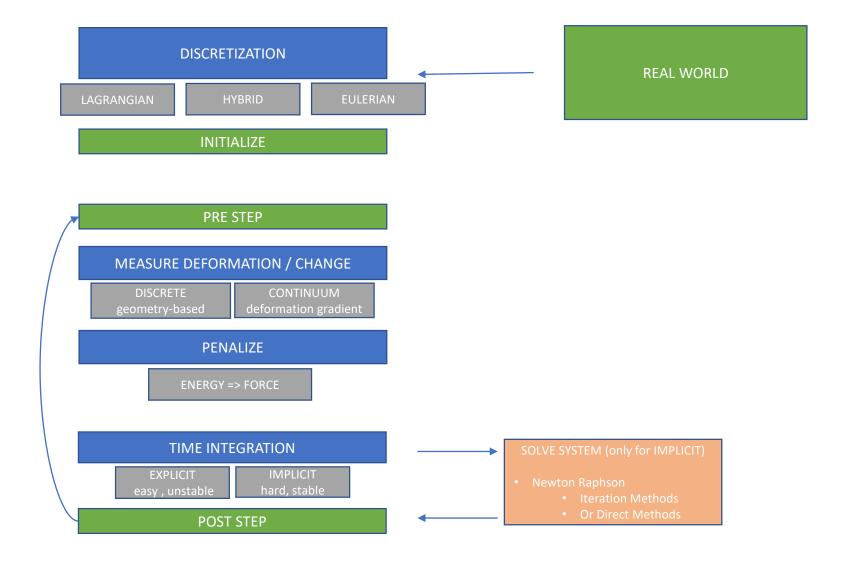
Minimize this scalar function with Newton Iterations



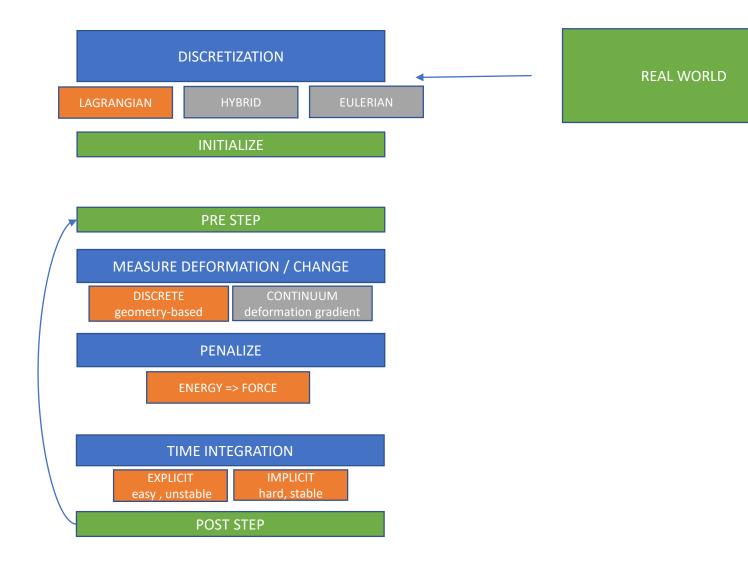
WHAT DO SOLVERS DO



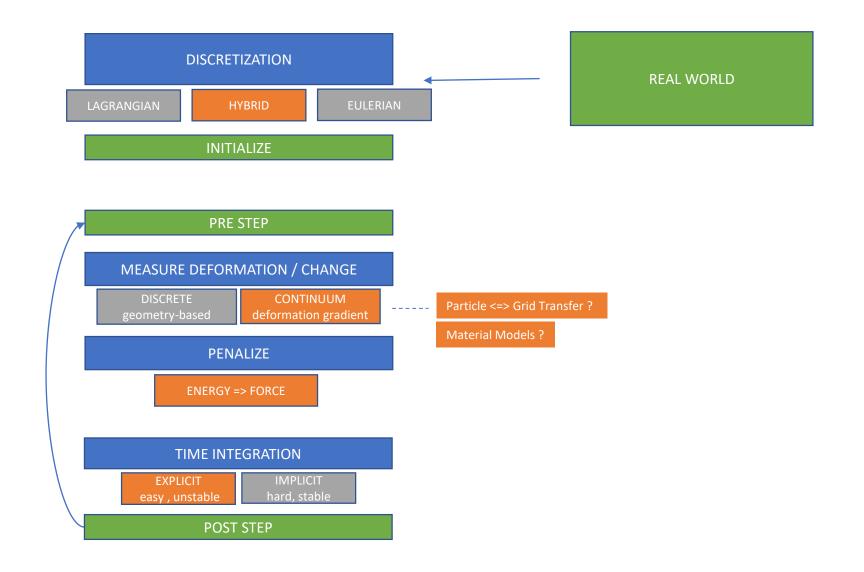
WHAT DO SOLVERS DO



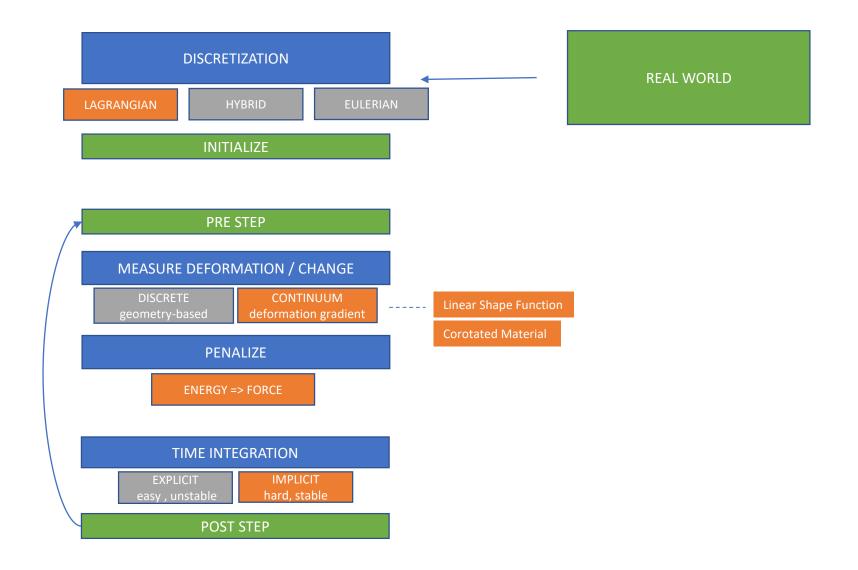
DISCRETE SHELLS



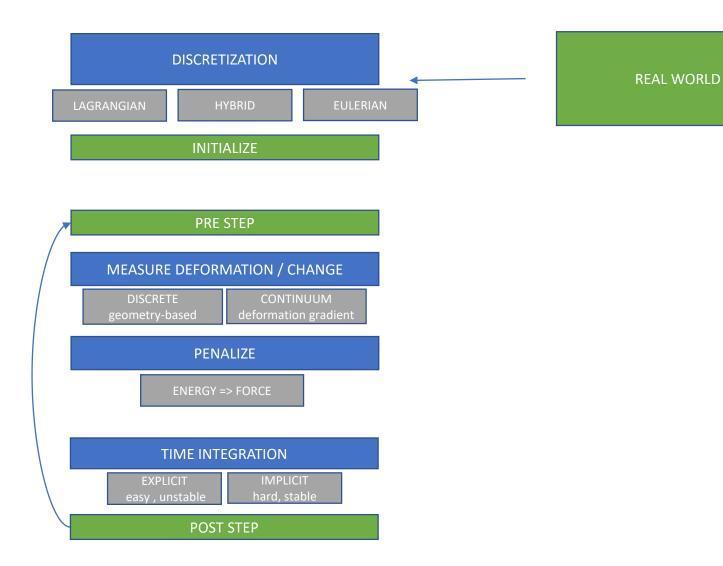
EXPLICIT MPM

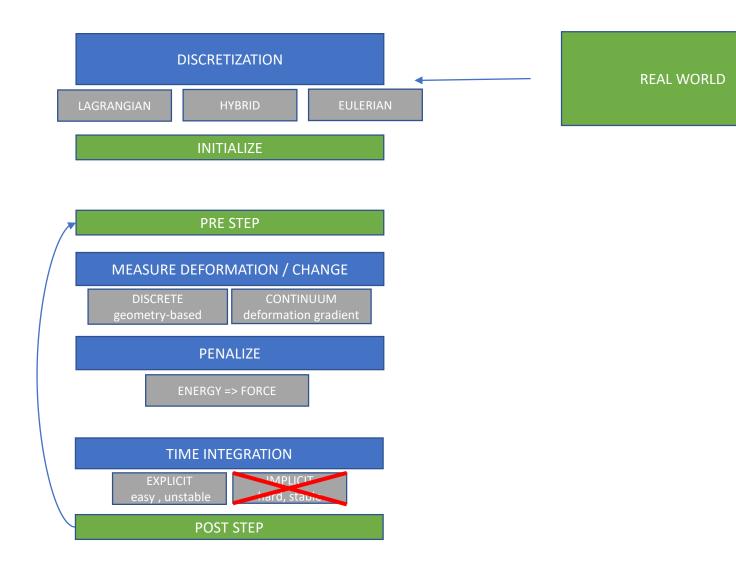


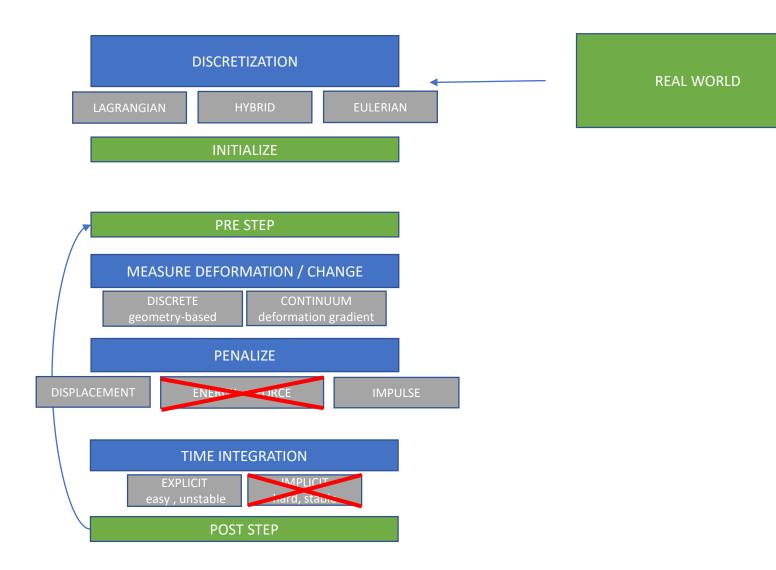
IMPLICIT COROTATED LINEAR FEM

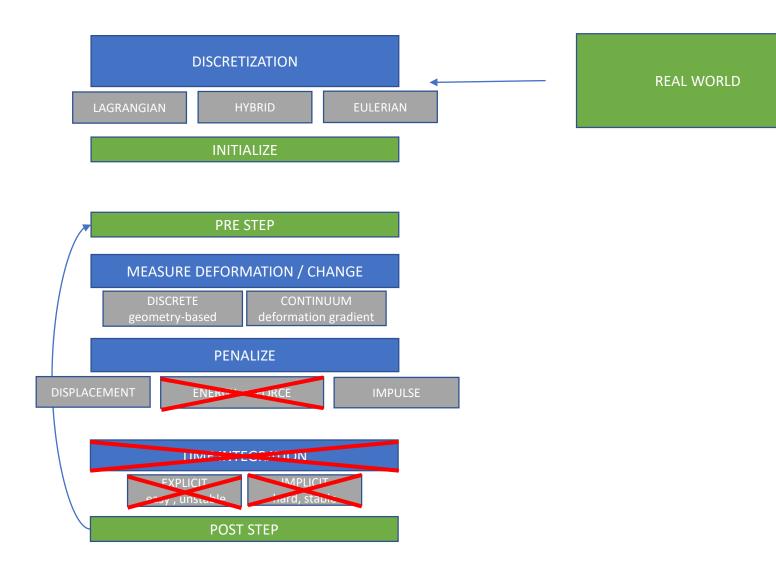


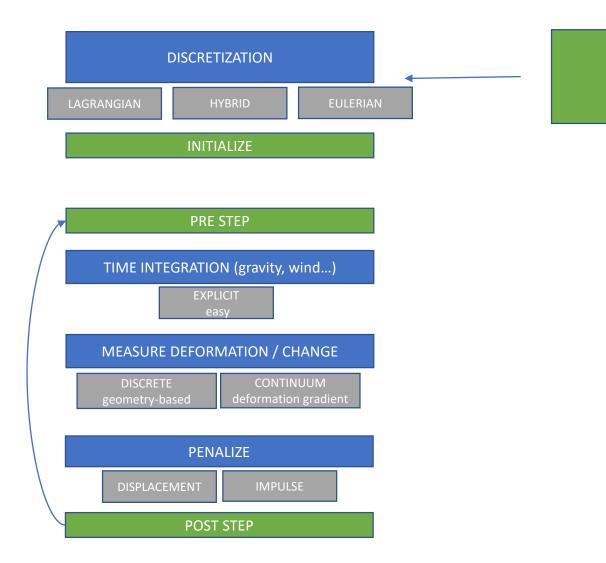
(X)PBD, nCloth, Bullet ...



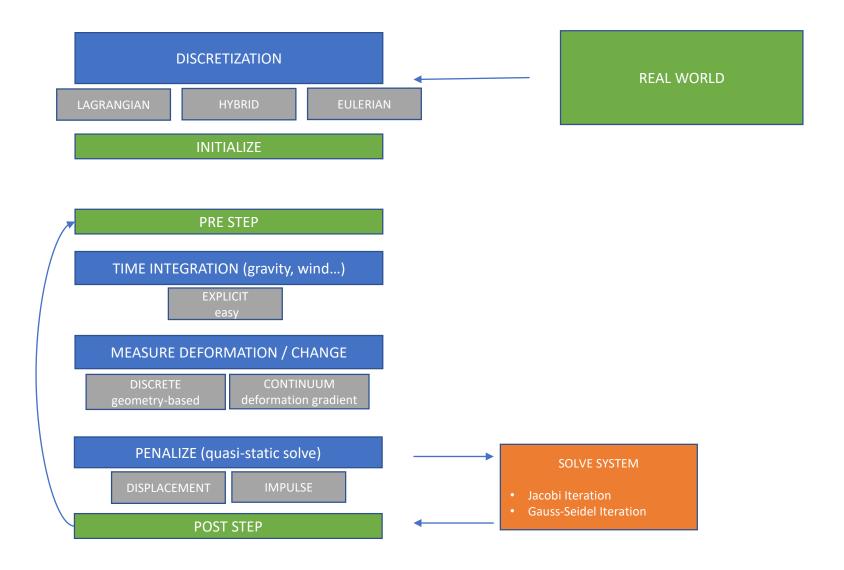








REAL WORLD



WHAT DID WE LEARN!

- Three discretizations
- Discrete vs Continuous
- Time Integrators (Explicit vs Implicit)
- FEM is not about tetrahedron but continuity
- Implicit integration is hard => Workaround (PBD ...)



BEYOND THIS PRESENTATION

- Penalty Method vs Lagrange Multiplier
- Direct vs Iterative Linear Solver
- Collision Detection (Discrete vs Continuous)
- Quasi-Static vs Dynamic
- Linear System Assembly
- Other Techniques (SPH / FDM)