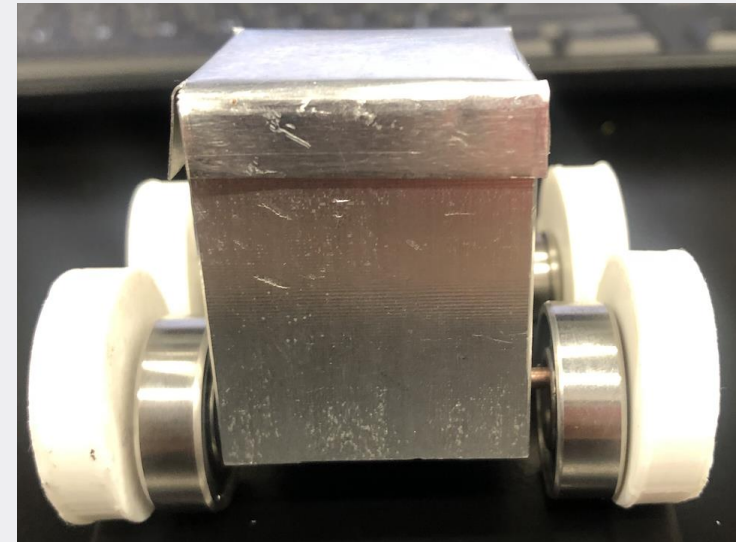
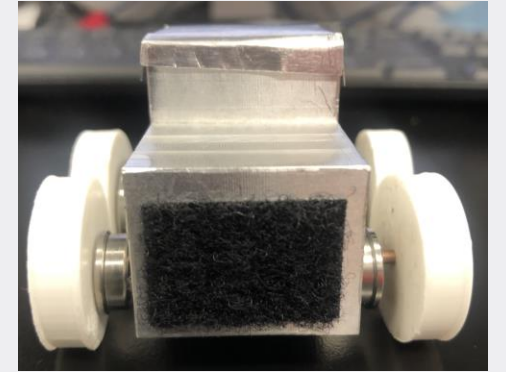
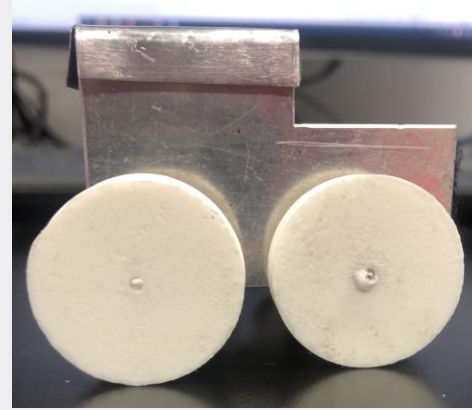


Petros Sklavounos  
KangHyuk (Chris) Lee

# DAP: Catapult Car

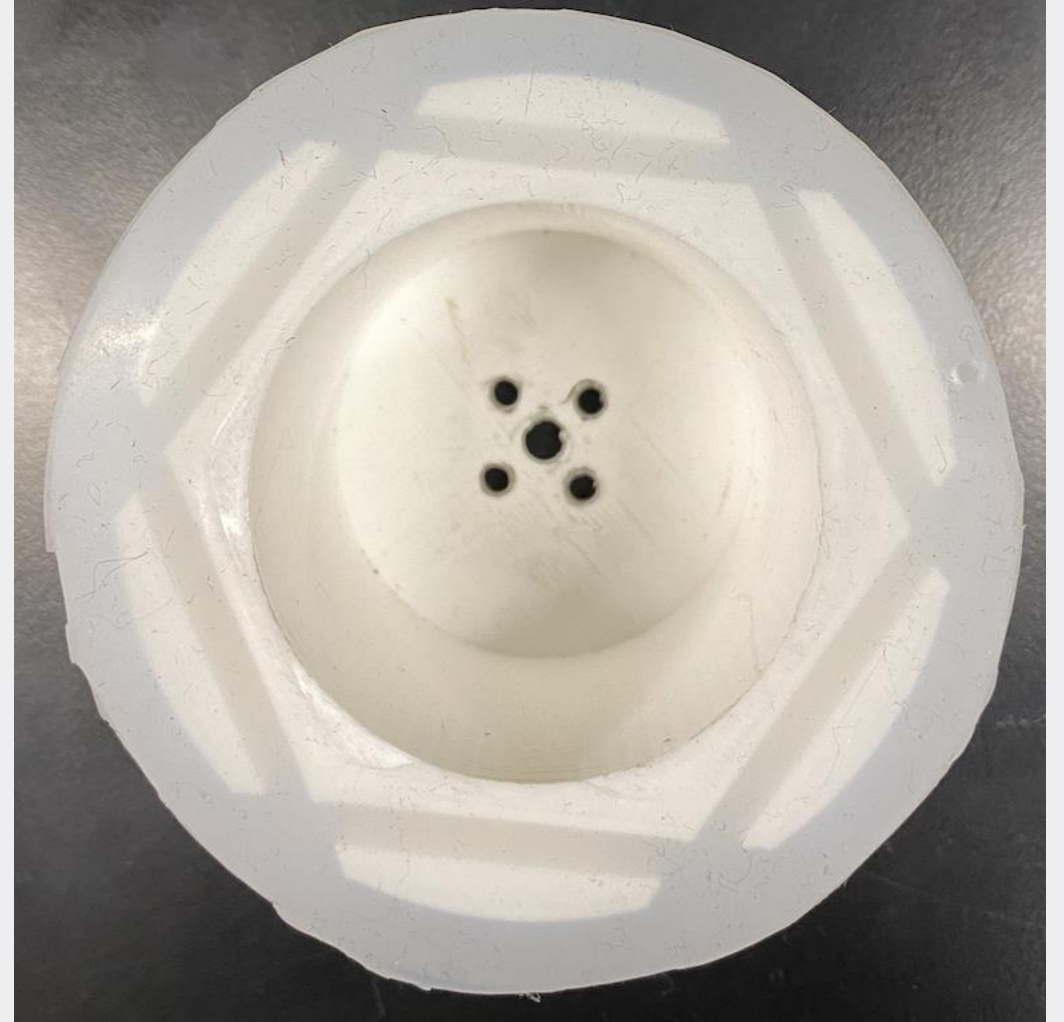
# Design

- Low build and wide axle for stability
- Bearings for weight and increased stability
- Compact mass for "point-mass" effect
- Press-fitted wheels for directional stability and build quality



# Construction

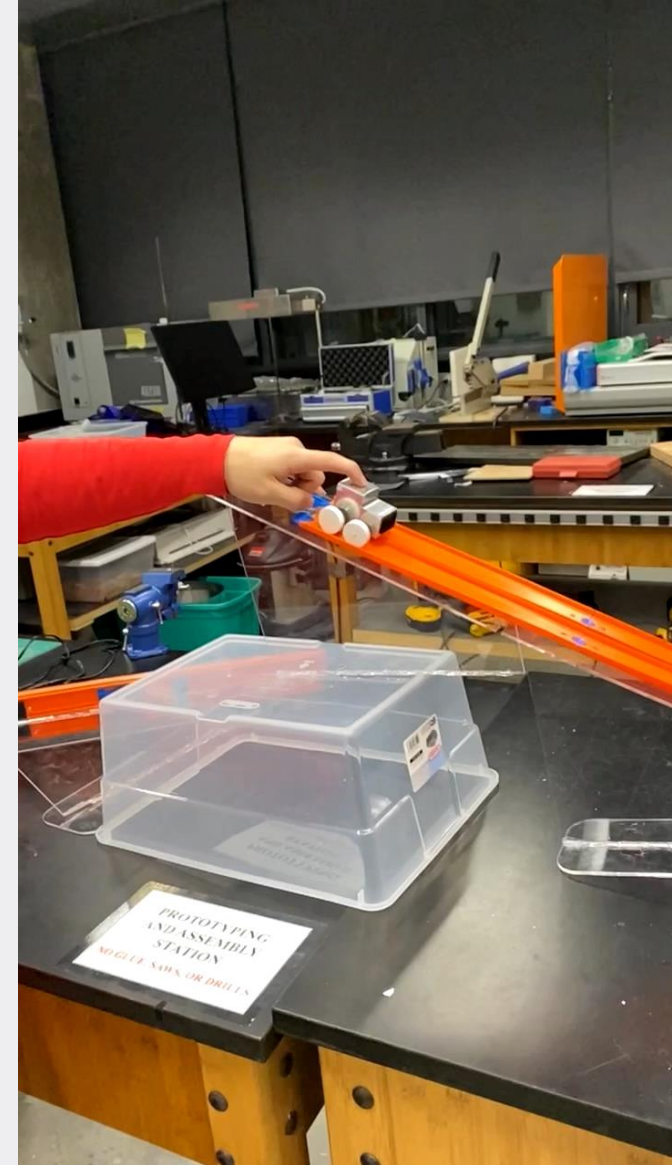
1. Aluminum block machined with Sinisa
2. Axle design review with Brian
3. Wheel design consultation with Jeanette
4. Re-evaluation and testing



# Performance and Test Results

- Outperformed expectations
- Able to stay on track without silicone on wheels
- Stable, fast, and attaches well with contact board

Sneak preview



# Calculations

## STATES

- 1) CAR'S FINAL SPEED @ CATAPULT
- 2) CATAPULT ARM'S FINAL ANGULAR SPEED
- 3) DISTANCE TRAVELLED BY CATAPULTED MR SJ

## DRAWING OF ENTIRE SYSTEM



## STATE 1: CONSERVATION OF ENERGY

$M = M_c + m_w + m_{\text{frame}}$   
 $Mgh = KE_{\text{linear}} + KE_{\text{rotational}} + W_f$   
 $Mgh = \frac{Mv_f^2}{2} + \frac{NI\omega^2}{2} + W_f$

*Annotations:*  
 -  $M = M_c + m_w + m_{\text{frame}}$ :  $M_c$  is car,  $m_w$  is wheels,  $m_{\text{frame}}$  is frame.  
 -  $W_f$ : frictional work, set to zero due to size and number of wheels.  
 -  $\omega$ : angular velocity.

Assumption that axles will allow 2 pairs of wheels to move

$\hookrightarrow Mgh = \frac{Mv_f^2}{2} + I\omega^2 \quad (1)$

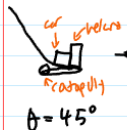
$\omega = \frac{v_f}{r} \quad (2)$

$(2) \text{ in } (1): Mgh = \frac{Mv_f^2}{2} + I\frac{v_f^2}{r^2}$

Finally  $v_f: Mgh = v_f^2 \left( \frac{M}{2} + \frac{I}{r^2} \right)$

$v_f^2 = \frac{Mgh}{\left( \frac{M}{2} + \frac{I}{r^2} \right)}, v_f = \left( \frac{Mgh}{\left( \frac{M}{2} + \frac{I}{r^2} \right)} \right)^{\frac{1}{2}}$

## STATE 2: CONSERVATION OF ANGULAR MOMENTUM



$L_i = L_f$  Inelastic collision due to velcro

$\vec{L} = m\vec{r} \times \vec{v}$

$|\vec{L}| = m|\vec{r}||\vec{v}|$  scalar components

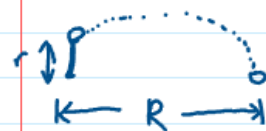
$\hookrightarrow Mrv_i = (M+m_{\text{catapult}})rv_f$

$\hookrightarrow v_f = \frac{Mrv_i}{(M+m_{\text{cat}})r}$

substituting state 1  $v_f$  into state 2  $v_i$

$\frac{M(Mgh)^{\frac{1}{2}}}{\left( \frac{M}{2} + \frac{I}{r^2} \right)^{\frac{1}{2}} (M+m_{\text{cat}})}$

## STATE 3: PROJECTILE RANGE



Range equation:  $R = \frac{v_i^2 \sin(2\theta)}{g}$   
*Annotation:*  $v_i$  is  $v_f$  of STATE 2

$\therefore R = \frac{\left[ \frac{M(Mgh)^{\frac{1}{2}}}{\left( \frac{M}{2} + \frac{I}{r^2} \right)^{\frac{1}{2}} (M+m_{\text{cat}})} \right]^2 \sin(2\theta)}{g}$