

ME639-ITR

8-1

SolutionGiven ^{end} points

A (0.4, 0.06, 0.1)

B (0.4, 0.01, 0.1)

APPLYING POLYNOMIAL TRAJECTORY METHOD

$$e(t) = b_0 + b_1 t + b_2 t^2 + b_3 t^3 + b_4 t^4 + b_5 t^5$$

↪ end
effector
position

Given boundary conditions

at $t = t_0$

$$e(t) = e_0$$

velocity $\leftarrow v(t) = v_0$

acceleration $\leftarrow a(t) = a_0$

& at $t = t_1$

$$e(t) = e_1$$

$$v(t) = v_1$$

$$a(t) = a_1$$

So, at $t = t_0$, $e_0 = (0.4, 0.06, 0.1)$, $v_0 = 0$, $a_0 = 0$
 and at $t = t_1$, $e_1 = (0.4, 0.01, 0.1)$, $v_1 = 0$, $a_1 = 0$

also $t_0 = 0$

$$\Rightarrow e_0 = b_0 = [0.4, 0.06, 0.1]$$

$$v_0 = b_1 = 0$$

$$a_0 = 2b_2 = 0$$

let $t_f = 1 \text{ sec}$ \Rightarrow end effector reaches point B in 1 sec

$$e_1 = b_0 + b_3 + b_4 + b_5 = [0.4, 0.01, 0.1]$$

$$v_1 = 3b_3 + 4b_4 + 5b_5 = 0$$

$$a_1 = 6b_3 + 12b_4 + 20b_5 = 0$$

Solving the equations we get

$$b_0 = [0.4 \quad 0.06 \quad 0.1]$$

$$b_1 = 0$$

$$b_2 = 0$$

$$b_3 = [0 \quad -0.5 \quad 0]$$

$$b_4 = [0 \quad 0.75 \quad 0]$$

$$b_5 = [0 \quad -0.3 \quad 0]$$

Q-3

Solⁿ

For a SCARA manipulator.

$m_1, m_2, m_3 \rightarrow$ mass of links

Equation of torques.

$l_1, l_2, l_3 \rightarrow$ length of links

$$\rightarrow d_{11} \ddot{q}_1 + d_{12} \ddot{q}_2 - m_2 l_1 l_2 \sin q_2 \dot{q}_1 \dot{q}_2 - 2m_3 l_1 l_2 \sin q_2 \dot{q}_1 \dot{q}_2$$

$$- \dot{q}_2^2 (m_2 l_1 l_2 + 2m_3 l_1 l_2) \sin q_2 = \tau_1$$

$$\rightarrow d_{21} \ddot{q}_1 + d_{22} \ddot{q}_2 + d_{23} \ddot{q}_3 + \frac{1}{2} \dot{q}_1^2 (m_2 l_1 l_2 + 2m_3 l_1 l_2) \sin q_2 = \tau_2$$

$$\rightarrow d_{32} \ddot{q}_2 + d_{33} \ddot{q}_3 + 1 = \tau_3$$

where $d_{11}, d_{12}, d_{22}, d_{32}$ are effective moment of Inertia about respective axis.

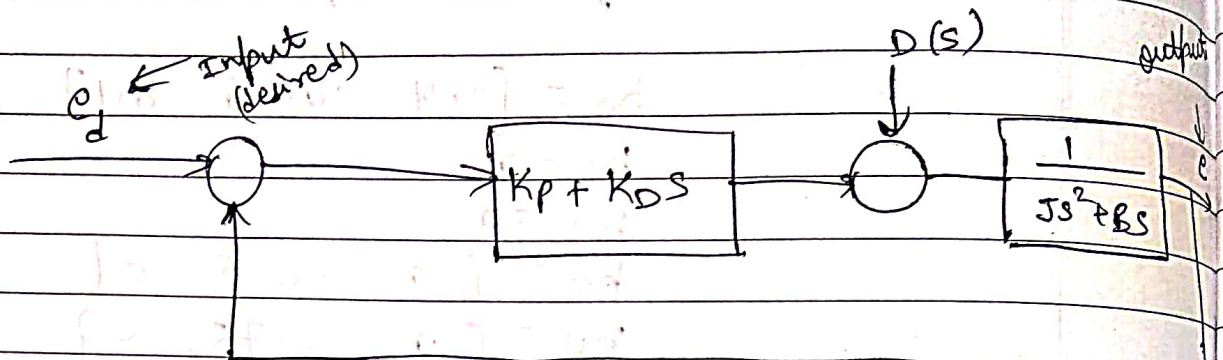
BLOCK DIAGRAMS

GoodLuck

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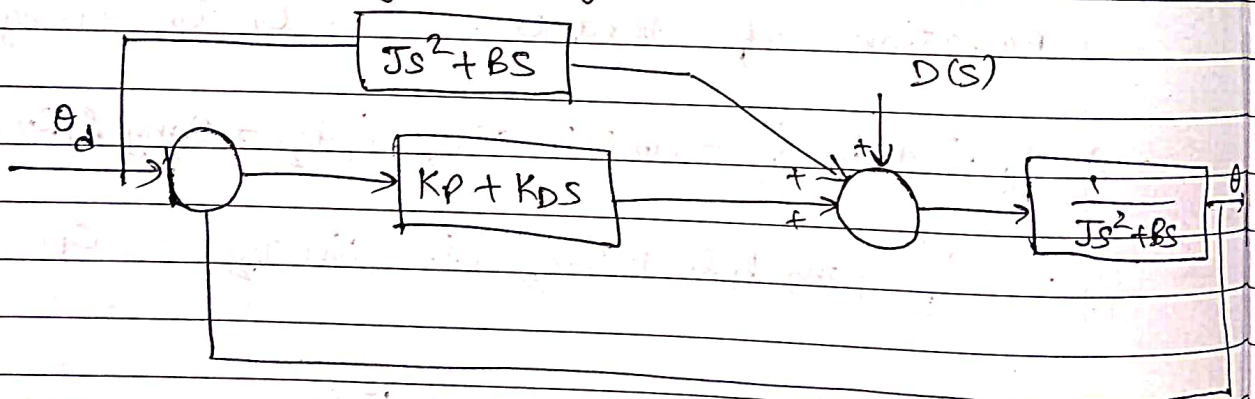
(a) PD Controller



Control equations

$$J_{eff} \ddot{e} + (B_{eff} + K_D) \dot{e} - K_P (e_d - e_s) = -K_D \dot{e}_d = -d(t)$$

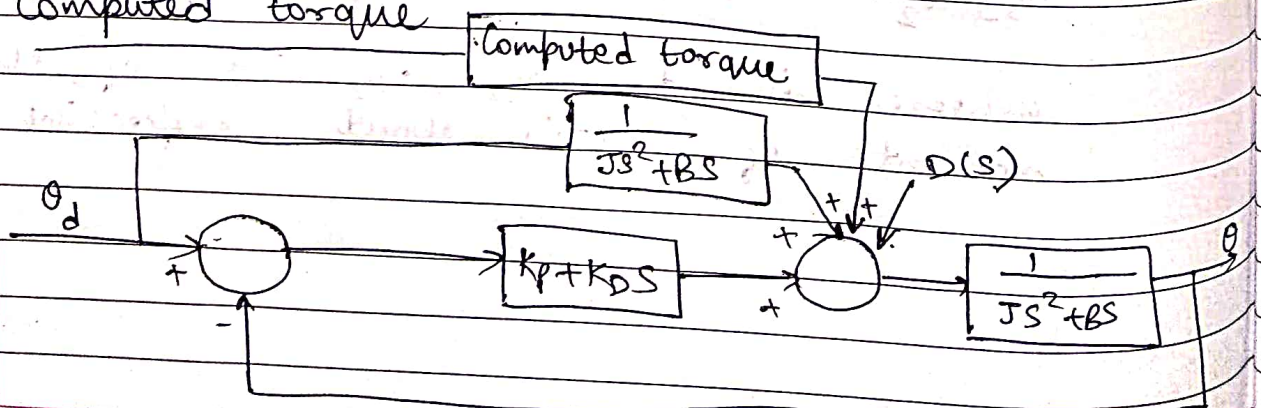
(b) PD with feed forward



Control equation

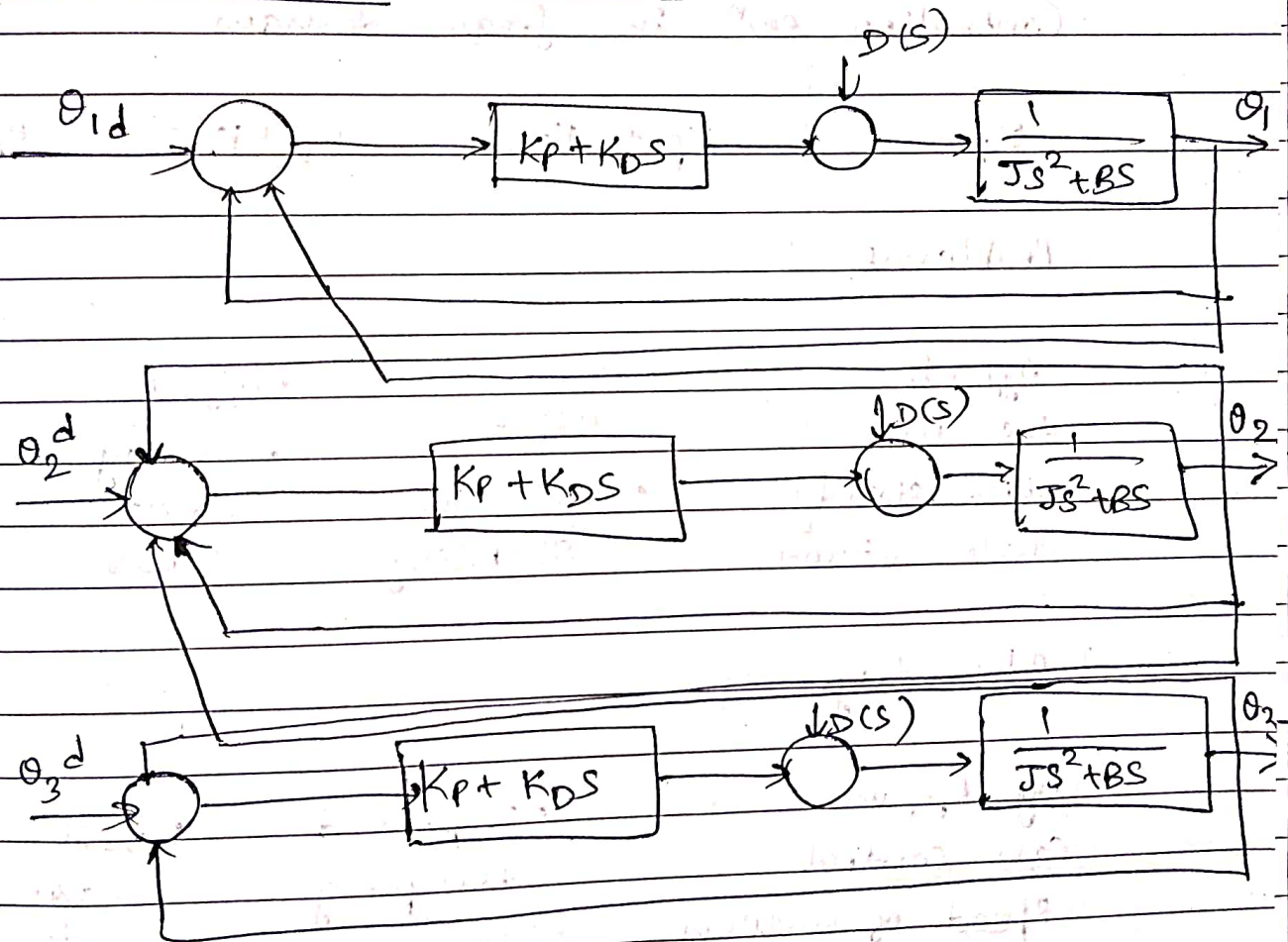
$$(\theta_d - \theta) (K_P + K_D S) + \theta_d (J S^2 + B S) - D(S) = \theta (J S^2 + B S)$$

(c) PD with Computed torque



$$J(\ddot{\theta}_d - \ddot{\theta}) + (B + K_D)(\dot{\theta}_d - \dot{\theta}) + K_P(\theta_d - \theta) + \tau_{\text{compe Computed}} = d(t)$$

(D) Multivariable Control



Control eqns

(7)	P (P.I.)	P.I.	P.D.	P.I.D.
Controller eq ⁿ in time domain	K_p	$K_p + K_I \int dt$	$K_p + K_D \frac{d}{dt}$	$K_p + K_I \int dt + K_D \frac{d}{dt}$

Controller eqⁿ in freq. domain

K_p	$K_p + \frac{K_I}{s}$	$K_p + K_D s$	$K_p + \frac{K_I}{s} + K_D s$
Problems			

Offset due to which steady state error	<ul style="list-style-type: none"> • Slow response • Issue in stability 	<ul style="list-style-type: none"> • offset • steady state error 	<ul style="list-style-type: none"> K_p - decreases rise time
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Advantage

By K_p , we can control speed of system	<ul style="list-style-type: none"> • Improved damping • Zero offset • No steady state error 	<ul style="list-style-type: none"> • Less max. peak overshoot • reduce rise time, settling time • ↑ rise Bandwidth 	<ul style="list-style-type: none"> K_I - eliminates steady state error K_D - decreases max. peak overshoot & settling time
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