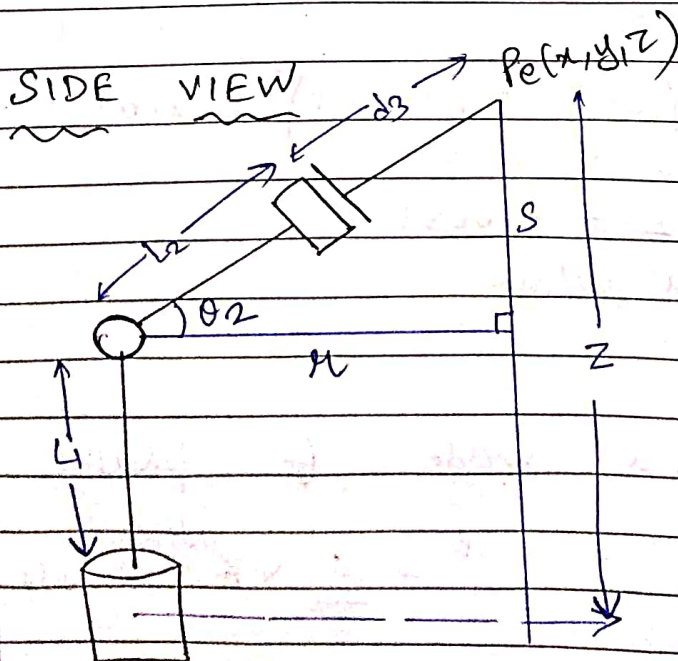
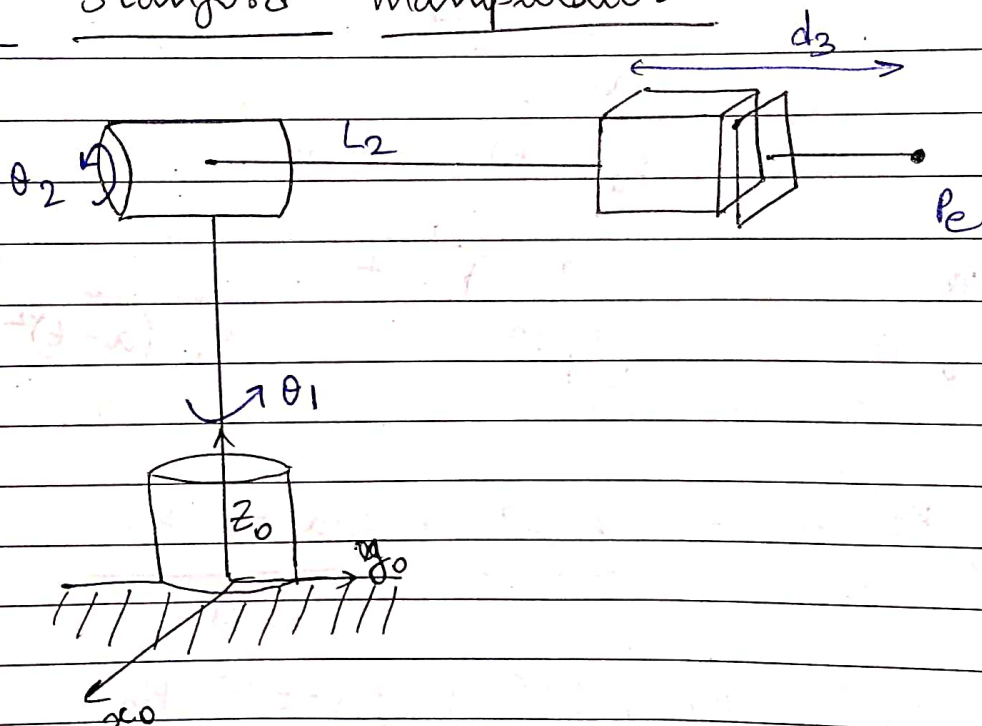
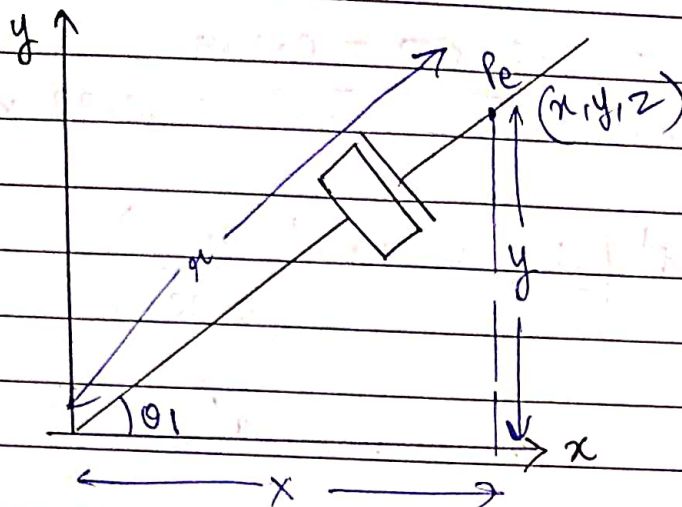


ME 639

ASSIGNMENT-4(1) RRP Stanford manipulator

TOP VIEW



For Inverse Kinematics (referring Section 4.3.2 of textbook)

From Side view

$$\theta_2 = \tan^{-1} \left(\frac{S}{r} \right)$$

$$S = Z - L_1$$

$$r^2 = x^2 + y^2$$

Also for d3 $(L_2 + d_3)^2 = S^2 + r^2$

$$\Rightarrow L_2 + d_3 = \sqrt{S^2 + r^2}$$

$$\Rightarrow d_3 = \sqrt{S^2 + r^2} - L_2$$

Given i end effector position (P_e)

$$P_e = x, y, z, L_1, L_2$$

let $x = 0.20 \text{ m}$

$y = 0.25 \text{ m}$

$z = 0.30 \text{ m}$

$L_1 = 0.20 \text{ m}$

$L_2 = 0.20 \text{ m}$

From top view

$$\theta_1 = \tan^{-1} \left(\frac{y}{x} \right)$$

Substituting the values of x, y, z, L_1, L_2

$$S = z - L_1 = 0.3 - 0.2 = 0.1 \text{ m}$$

$$r = \sqrt{x^2 + y^2} = \sqrt{0.2^2 + 0.25^2} = 0.32 \text{ m}$$

$$\theta_2 = \tan^{-1} \left(\frac{S}{r} \right) = \tan^{-1} \left(\frac{0.1}{0.32} \right)$$

$$\theta_2 = 0.3029^{\text{R}}$$

$$\theta_2 = 17.35^{\circ}$$

for

$$\theta_1 = \tan^{-1} \left(\frac{y}{x} \right)$$

$$\theta_1 = \tan^{-1} \left(\frac{0.25}{0.20} \right)$$

$$\theta_1 = 0.896^{\text{R}}$$

$$\theta_1 = 51.34^{\circ}$$

$$d_3 = \sqrt{S^2 + r^2} - L_2$$

$$= \sqrt{0.32^2 + 0.1^2} - 0.2$$

$$= 0.335 - 0.2$$

$$= 0.135 \text{ m}$$

$$d_3 = 0.135 \text{ m}$$

Forward Kinematics

$$\text{let } \theta_1 = 51.34^\circ$$

$$L_1 = 0.2 \text{ m}$$

$$\theta_2 = 17.35^\circ$$

$$L_2 = 0.2 \text{ m}$$

$$d_3 = 0.135 \text{ m}$$

$$\text{Now, } \cos \theta_2 = \frac{x}{L_2 + d_3}$$

$$\Rightarrow (\cos 17.35^\circ) \times (0.2 + 0.135) = x$$

$$\Rightarrow \boxed{x = 0.32 \text{ m}}$$

$$\text{Now } \cos \theta_1 = \frac{x}{r}$$

$$\Rightarrow x = r \cos \theta_1 = 0.32 \cos 51.34^\circ$$

$$\boxed{x \approx 0.2 \text{ m}}$$

$$\sin \theta_1 = \frac{y}{r}$$

$$\Rightarrow y = r \sin \theta_1 = 0.32 \sin 51.34^\circ$$

$$\boxed{y \approx 0.25 \text{ m}}$$

$$z = s + L_1$$

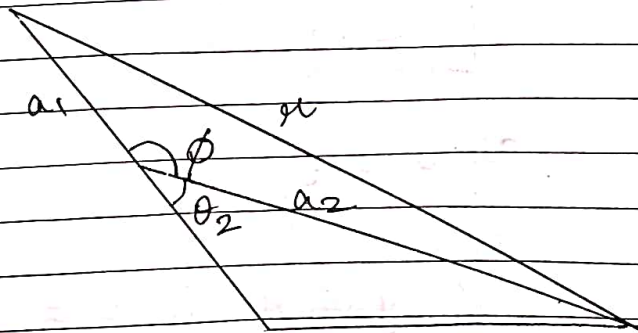
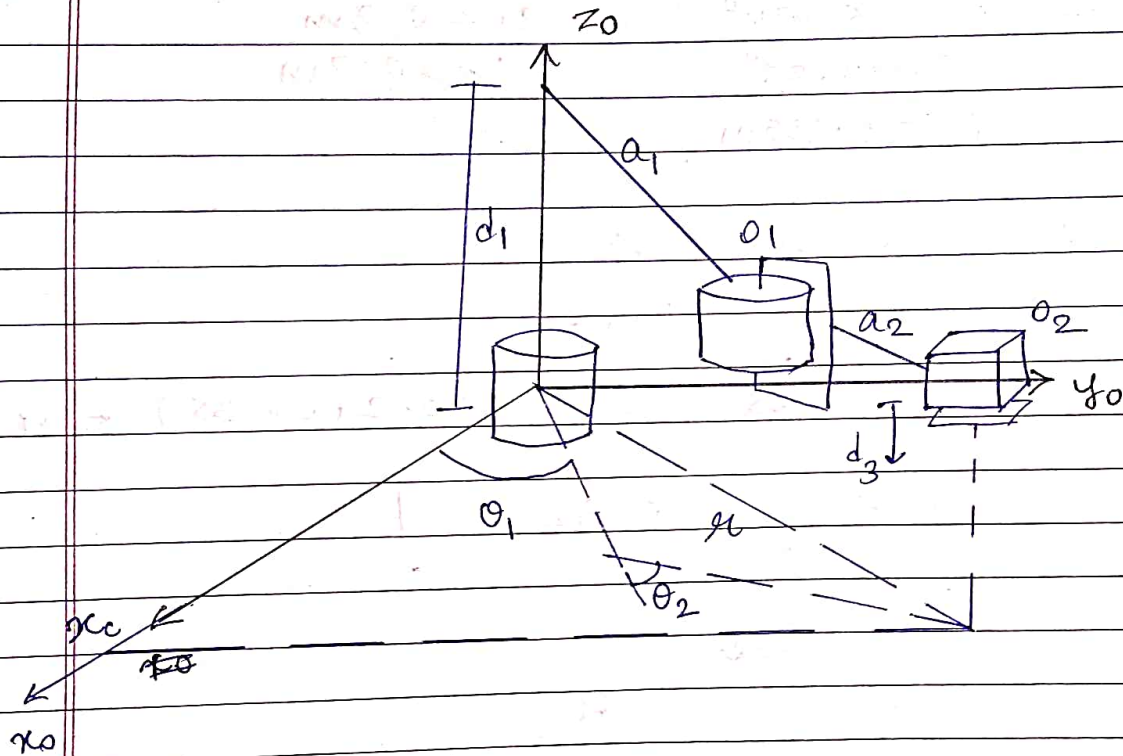
$$z = \cancel{r} (L_2 + d_3) \sin \theta_2 + L_1$$

$$z = (0.2 + 0.135) \sin 17.35 + 0.2$$

$$\boxed{z \approx 0.30 \text{ m}}$$

(2)

RRP SCARA MANIPULATOR



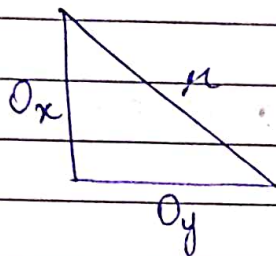
$$\phi + \theta_2 = 180^\circ$$

$$r^2 = a_1^2 + a_2^2 - 2a_1a_2 \cos \phi$$

$$\cos \phi = \frac{a_1^2 + a_2^2 - r^2}{2a_1a_2}$$

$$\therefore \cos(180^\circ - \theta_2) = -\cos \theta_2 = \cos \phi$$

$$\Rightarrow \cos \theta_2 = - \left(\frac{a_1^2 + a_2^2 - r^2}{2a_1 a_2} \right) \quad \text{--- (1)}$$

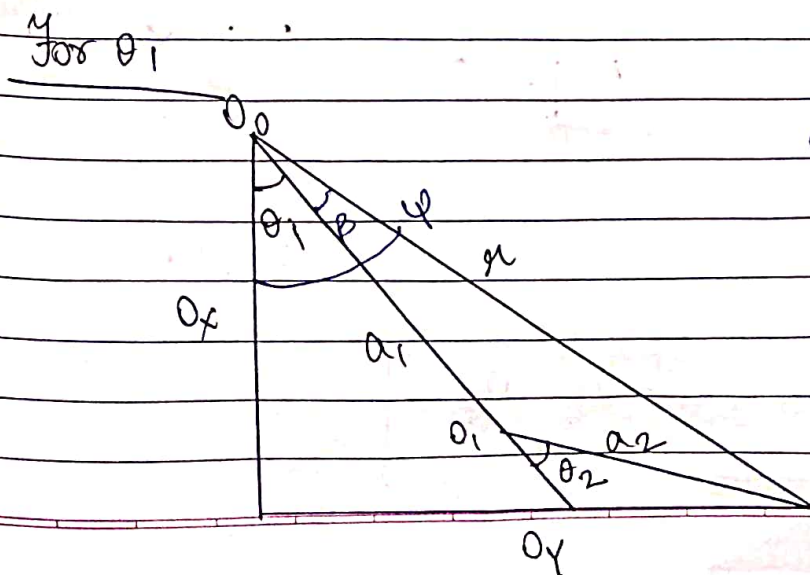


$$r^2 = O_x^2 + O_y^2$$

From eqⁿ (1)

$$\tan \theta_2 = \frac{\sin \theta_2}{\cos \theta_2} = \sqrt{\frac{1}{\cos^2 \theta_2} - 1}$$

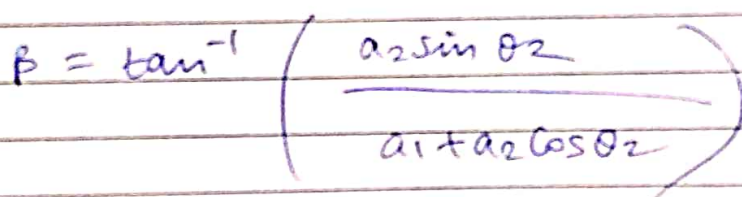
$$\theta_2 = \tan^{-1} \left(\sqrt{\frac{1}{\cos^2 \theta_2} - 1} \right)$$



$$\theta_1 + \beta = \psi$$

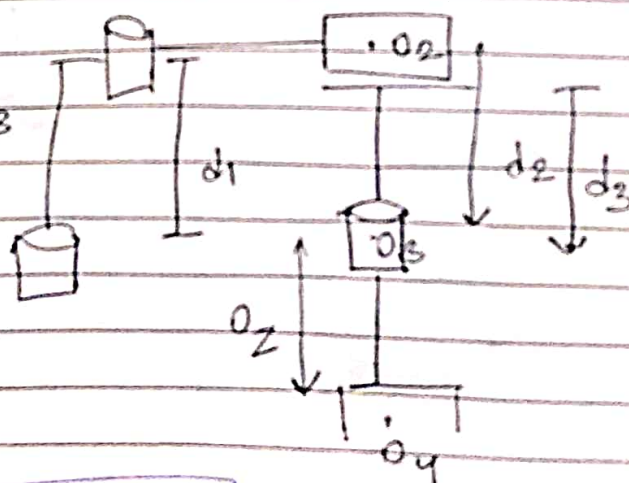
$$\theta_1 = \psi - \beta$$

$$\psi = \tan^{-1} \left(\frac{O_y}{O_x} \right)$$



$$\Rightarrow \theta_1 = \psi - \beta$$

$$\theta_1 = \tan^{-1} \left(\frac{O_y}{O_x} \right) = \tan^{-1} \left(\frac{a_2 \sin \theta_2}{a_1 + a_2 \cos \theta_2} \right)$$

$$O_2 = d_1 - d_2 - d_3$$


$$d_3 = d_1 - d_2 - 0_3$$

Finding θ_4

$$T_0^4 = \begin{bmatrix} c_{12}c_4 + s_{12}s_4 & s_{12}c_4 - c_{12}s_4 & 0 & a_1c_1 + a_2c_2 \\ s_{12}c_4 - c_{12}s_4 & -c_{12}c_4 - s_{12}s_4 & 0 & a_1s_1 + a_2s_2 \\ 0 & 0 & -1 & -d_3 - d_4 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\theta_4 = \theta_1 + \theta_2 - \alpha \quad \text{where} \quad \alpha = \tan^{-1} \left(\frac{x_{12}}{x_{11}} \right)$$

$$\text{of } R = \begin{bmatrix} c_\alpha + s_\alpha & 0 \\ s_\alpha - c_\alpha & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

Final equations are

$$\theta_2 = \tan^{-1} \left(\frac{\sqrt{1-B^2}}{B} \right) \quad \text{where} \quad B = \frac{x^2 + y^2 - a_1^2 - a_2^2}{2a_1a_2}$$

$$\theta_1 = \tan^{-1} \left(\frac{y}{x} \right) - \tan^{-1} \left(\frac{a_2 \sin \theta_2}{a_1 + a_2 \cos \theta_2} \right)$$

$$d_3 = d_1 - d_2 - d_4$$

$$\theta_4 = \theta_1 + \theta_2 - \alpha \quad \text{where} \quad \alpha = \tan^{-1} \left(\frac{x_{12}}{x_{11}} \right) \quad \text{of}$$

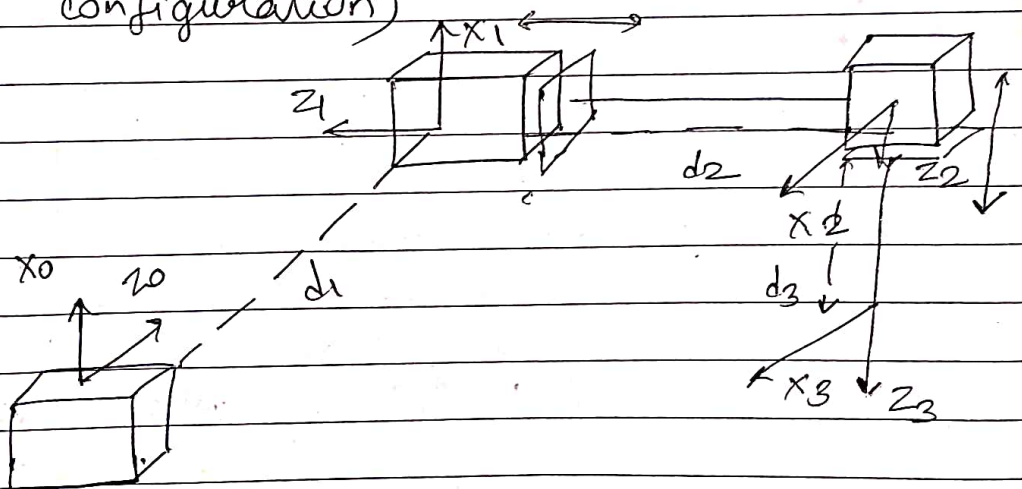
$$R = \begin{bmatrix} c_\alpha & s_\alpha & 0 \\ s_\alpha & -c_\alpha & 0 \\ 0 & 0 & -1 \end{bmatrix}$$

(3) joint velocity using end effector cartesian velocities.

$$\dot{x} = J(q) \dot{q}$$

$$\dot{q} = (J^{-1}) \cdot (\dot{x})$$

(7) DH parameter for a 3D printer (PPP configuration)



DH parameters

	a_i	α_i	d_i	θ_i
0-1	0	90	d_1	0
1-2	0	90	$-d_2$	-90
2-3	0	0	d_3	0

$$T_0^3 = T_0^1 T_1^2 T_2^3$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & -1 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 1 & 0 & -d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_0^3 = \begin{bmatrix} 0 & 0 & -1 & -d_3 \\ 0 & -1 & 0 & d_2 \\ -1 & 0 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

End effector position

$$x = -d_3$$

$$y = d_2$$

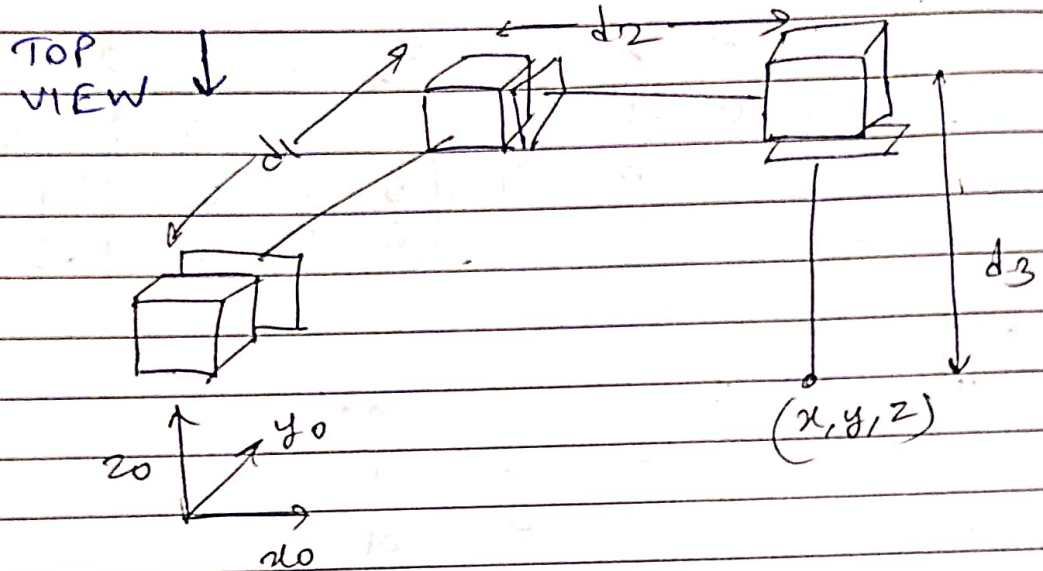
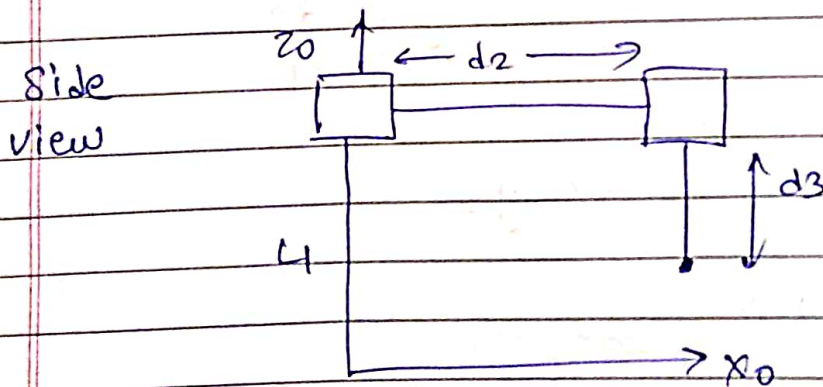
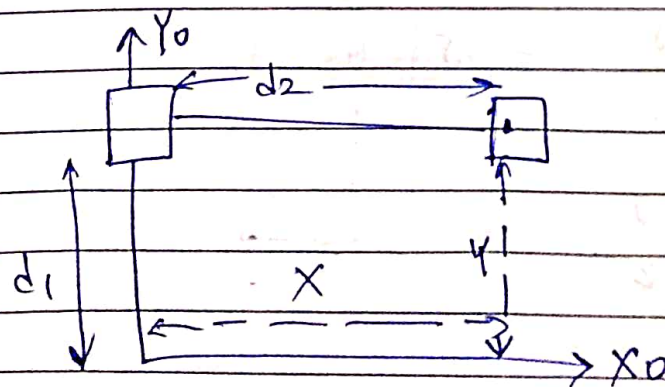
$$z = d_1$$

end effector velocity

$$V = J \dot{x}$$

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} = J \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \vdots \\ \dot{\theta}_n \end{bmatrix}$$

(8)

INVERSE KINEMATICS FOR
3D PRINTER (PPP)SIDE
VIEWTop
view

Ans

$$d_1 = Y$$

$$d_2 = X$$

$$d_3 = L - Z$$