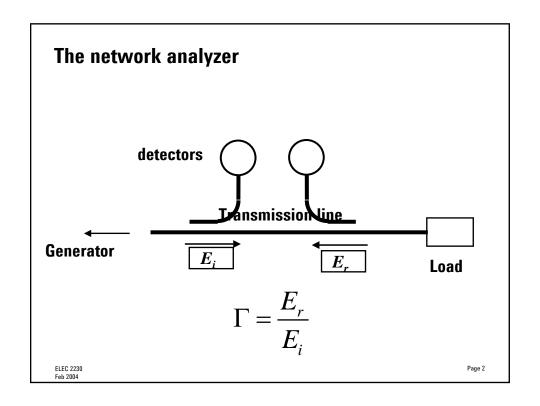
RF and Microwave Transmission Lines

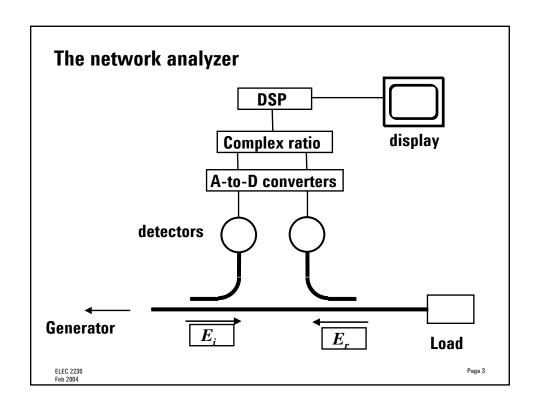
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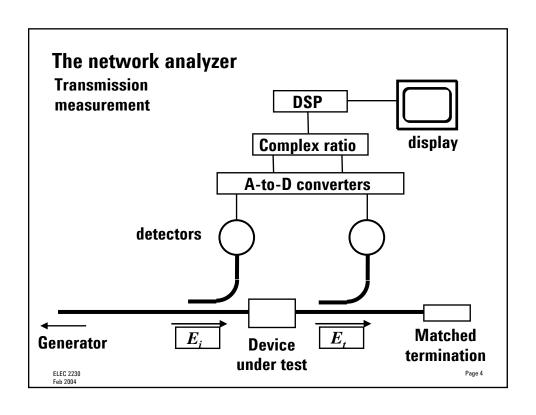
Section 5

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February 2004

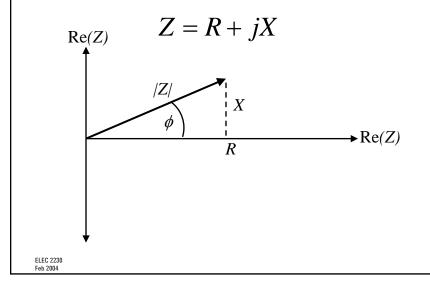


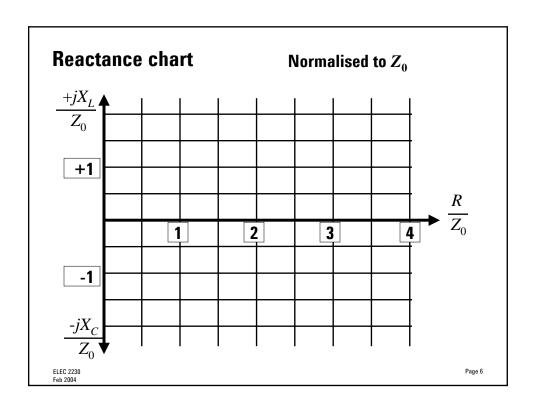


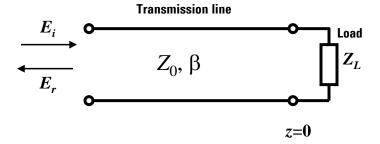


Impedance and Admittance relationships

Termination impedance is, in general, complex







ELEC 2230 Feb 2004 Page 7

Terminated lossless transmission line

Incident wave

$$E_i = V^+ e^{-j\beta z}$$

Reflected wave

$$E_r = V^- e^{+j\beta z}$$

Ratio of voltage to current for travelling wave on the transmission line must be \boldsymbol{Z}_0

But since the termination $Z_L \neq Z_0$ the ratio of voltage to current at the load must be Z_L and a reflected wave must be excited to satisfy that condition.

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Total voltage

$$V(z) = E_i + E_r = V^+ e^{-j\beta z} + V^- e^{+j\beta z}$$

Total current

$$I(z) = \frac{V^{+}}{Z_{0}} e^{-j\beta z} - \frac{V^{-}}{Z_{0}} e^{+j\beta z}$$

So, at the load, where z = 0

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Page 9

Terminated lossless transmission line

So, at the load, where z = 0

$$Z_L = \frac{V(0)}{I(0)} = \frac{V^+ + V^-}{V^+ - V^-} Z_0$$

Now, solve for

$$V^{-} = \frac{Z_L - Z_0}{Z_L + Z_0} V^{+}$$

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Recall that the reflection coefficient is

$$\Gamma = \frac{V^{-}}{V^{+}} = \frac{Z_L - Z_0}{Z_L + Z_0}$$

And can write the total voltage and current as

$$V(z) = V^{+} \left[e^{-j\beta z} + \Gamma e^{+j\beta z} \right]$$

$$I(z) = \frac{V^{+}}{Z_{0}} \left[e^{-j\beta z} - \Gamma e^{+j\beta z} \right]$$

ELEC 2230 Feb 2004

Page 11

Terminated lossless transmission line

At any point on the line, (z = -l)

$$\Gamma(l) = \frac{V^- e^{-j\beta l}}{V^+ e^{+j\beta l}} = \Gamma(0)e^{-2j\beta l}$$

So note that, as you move along the line, the magnitude of the reflection coefficient is unchanged. The phase of the reflection coefficient increases by $2\beta l$ - the electrical length.

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Or the impedance seen looking in to the line looking towards the load is

$$Z_{in} = \frac{V(-l)}{I(-l)} = \frac{V^{+} \left[e^{+j\beta l} + \Gamma e^{-j\beta l} \right]}{V^{+} \left[e^{+j\beta l} - \Gamma e^{-j\beta l} \right]} Z_{0}$$
$$= \frac{\left[1 + \Gamma e^{-2j\beta l} \right]}{\left[1 - \Gamma e^{-2j\beta l} \right]} Z_{0}$$

ELEC 2230 Feb 2004 Page 13

Transmission line impedance equation

Can re-arrange as

$$Z_{in} = Z_{0} \frac{(Z_{L} + Z_{0})e^{+j\beta l} + (Z_{L} - Z_{0})e^{-j\beta l}}{(Z_{L} + Z_{0})e^{+j\beta l} - (Z_{L} - Z_{0})e^{-j\beta l}}$$

$$Z_{0} \frac{Z_{L}\cos\beta l + jZ_{0}\sin\beta l}{Z_{0}\cos\beta l + jZ_{L}\sin\beta l}$$

$$= Z_{0} \frac{Z_{L} + jZ_{0}\tan\beta l}{Z_{0} + jZ_{L}\tan\beta l}$$

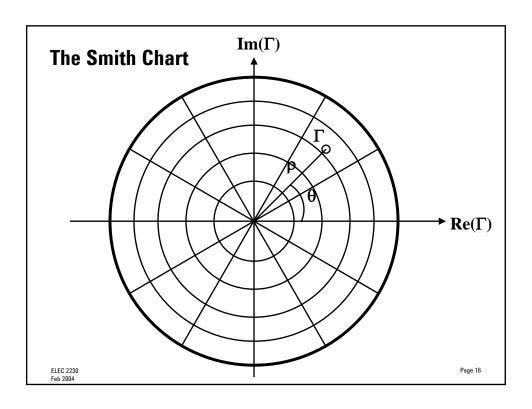
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Tool to help understand and solve transmission line problems

It is a polar polar plot of reflection coefficient G overlaid with contours of constant resistance and reactance

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{\frac{Z_L}{Z_0} - 1}{\frac{Z_L}{Z_0} + 1} = \frac{z - 1}{z + 1}$$

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Now consider some specific values of \boldsymbol{Z}_{L}

(a) Short circuit: $Z_L = 0$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{0 - Z_0}{0 + Z_0} = -1$$

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Page 17

The Smith Chart

Now consider some specific values of \boldsymbol{Z}_{L}

(b) Open circuit: $Z_L = \infty$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{1 - \frac{Z_0}{Z_L}}{1 + \frac{Z_0}{Z_L}} = \frac{1 - \frac{Z_0}{\infty}}{1 + \frac{Z_0}{\infty}} = +1$$

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Now consider some specific values of \boldsymbol{Z}_L

(c) Match: $Z_L = Z_0$ (z = 1)

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{z - 1}{z + 1} = 0$$

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Page 19

The Smith Chart

Now consider some specific values of ${oldsymbol{Z}}_L$

(d) Inductor: z = 0 + j1

$$\Gamma = \frac{z-1}{z+1} = \frac{j-1}{j+1} = \frac{(j-1)(-j+1)}{(j+1)(-j+1)} = j$$

(e) Capacitor: z = 0 - j1

$$\Gamma = \frac{z-1}{z+1} = \frac{-j-1}{-j+1} = \frac{(-j-1)(j+1)}{(-j+1)(j+1)} = -j$$

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Now consider some specific values of $\boldsymbol{Z}_{\!L}$

(d) Inductive impedance: z = 1 + j1

$$\Gamma = \frac{z-1}{z+1} = \frac{1+j-1}{1+j+1} = \frac{j}{2+j} = \frac{1+2j}{5}$$

(e) Capacitive impedance: z = 1 - jI

$$\Gamma = \frac{z-1}{z+1} = \frac{1-j-1}{1-j+1} = \frac{-j}{2-j} = \frac{1-2j}{5}$$

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