

# **Chapter 4**

## **State-space Solutions**



## Existence and Uniqueness of Solution

Consider linear time-varying state equation

$$\dot{x} = A(t)x + B(t)u, \quad x(t_0) = x_0, \quad t \in [t_0, t_a] \quad (1)$$

- If all elements of  $A(t)$  and  $B(t)$  and the input  $u(t)$  are real and continuous on  $[t_0, t_a]$ , then solution of state equation (1) exists and is unique. These conditions can be satisfied by many physical systems.
- The above conditions can be relaxed to:

$$(a) \quad \int_{t_0}^{t_a} |a_{ij}(t)| dt < \infty, \quad i, j = 1, 2, \dots, n;$$

$$(b) \quad \int_{t_0}^{t_a} [b_{ij}(t)]^2 dt < \infty, \quad i, j = 1, 2, \dots, n, \quad j = 1, 2, \dots, p;$$

$$(c) \quad \int_{t_0}^{t_a} [u_j(t)]^2 dt < \infty, \quad j = 1, 2, \dots, p$$

- For LTI systems, (a) and (b) are automatically satisfied, so condition (c) suffices to guarantee the existence and uniqueness of solution.



## Solution of State Equation:

- LTI system:

$$\dot{\mathbf{x}}(t) = A\mathbf{x}(t) + B\mathbf{u}(t), \quad \mathbf{x}(t_0) = x_0 \quad (2)$$

$$\mathbf{y}(t) = C\mathbf{x}(t) + D\mathbf{u}(t) \quad (3)$$

- Premultiplying  $e^{-At}$  on both sides of (2),

$$e^{-At}\dot{\mathbf{x}}(t) - e^{-At}A\mathbf{x}(t) = e^{-At}B\mathbf{u}(t)$$

Applying the fact that  $Ae^{At} = e^{At}A$ ,

$$\frac{d}{dt}(e^{-At}\mathbf{x}(t)) = e^{-At}B\mathbf{u}(t)$$

- Integrating from  $t_0$  to  $t$  yields

$$e^{-At}\mathbf{x}(t) - e^{-At_0}\mathbf{x}(t_0) = \int_{t_0}^t e^{-A\tau}B\mathbf{u}(\tau)d\tau$$

or yet

$$\mathbf{x}(t) = e^{A(t-t_0)}\mathbf{x}(t_0) + \int_{t_0}^t e^{A(t-\tau)}Bu(\tau)d\tau \quad (4)$$



Observe from (4) that the state response is the sum of the zero input response and zero state response (superposition). The output is then

$$\mathbf{y}(t) = C e^{A(t-t_0)} \mathbf{x}(t_0) + C \int_{t_0}^t e^{A(t-\tau)} B u(\tau) d\tau + D \mathbf{u}(t) \quad (5)$$

- The key is to compute the state transition matrix  $e^{At}$ .

$$e^{At} = I + tA + \frac{t^2}{2!}A^2 + \dots$$

- Method 1: Apply the method of Chapter 3: (1) Compute the eigenvalues of  $A$ ; (2) Find  $h(\lambda)$  of degree  $n - 1$  such that  $h(\lambda_i) = e^{\lambda_i t}$  (or  $h^{(i)}(\lambda_i) = (e^{\lambda t})^{(i)}|_{\lambda=\lambda_i}$ ) where  $\lambda_i$ ,  $i = 1, 2, \dots, n$  are the eigenvalues of  $A$ ; and (3)  $e^{At} = h(A)$ .
- Method 2: Use diagonal or Jordan form: (1) Compute  $T$  such that  $A = T \hat{A} T^{-1}$ , where  $\hat{A}$  is a Jordan form; (2)  $e^{At} = T e^{\hat{A}t} T^{-1}$ . Note that  $e^{\hat{A}t}$  is computed in Chapter 3.
- Method 3: Use Laplace inverse transform:

$$e^{At} = \mathcal{L}^{-1}(sI - A)^{-1}$$



**Example 4.1** Consider the state equation with  $t_0 = 0$ :

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & -1 \\ 1 & -2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$

Since

$$(sI - A)^{-1} = \begin{bmatrix} s & 1 \\ -1 & s+2 \end{bmatrix}^{-1} = \begin{bmatrix} (s+2)/(s+1)^2 & -1/(s+1)^2 \\ 1/(s+1)^2 & s/(s+1)^2 \end{bmatrix}$$

$$e^{At} = \mathcal{L}^{-1}(sI - A)^{-1} = \begin{bmatrix} (1+t)e^{-t} & -te^{-t} \\ te^{-t} & (1-t)e^{-t} \end{bmatrix}$$

Hence,

$$\mathbf{x}(t) = \begin{bmatrix} (1+t)e^{-t} & -te^{-t} \\ te^{-t} & (1-t)e^{-t} \end{bmatrix} \mathbf{x}(0) + \begin{bmatrix} -\int_0^t (t-\tau)e^{-(t-\tau)}u(\tau)d\tau \\ \int_0^t [1-(t-\tau)]e^{-(t-\tau)}u(\tau)d\tau \end{bmatrix}$$



**Example 4.2** Consider the LTI system

$$\dot{x} = \begin{bmatrix} 2 & -1 & -1 \\ 0 & -1 & 0 \\ 0 & 2 & 1 \end{bmatrix} x + \begin{bmatrix} 7 \\ 2 \\ 3 \end{bmatrix} u$$

To find  $e^{At}$ , we first calculate the eigenvalues of  $A$ :

$$|\lambda I - A| = (\lambda - 2)(\lambda + 1)(\lambda - 1) = 0$$

Thus,

$$\lambda_1 = 2, \lambda_2 = 1, \lambda_3 = -1$$

Since the eigenvalues are distinct, there are three independent eigenvectors. We now find their corresponding eigenvectors by solving:

$$\begin{bmatrix} 2 & -1 & -1 \\ 0 & -1 & 0 \\ 0 & 2 & 1 \end{bmatrix} \begin{bmatrix} v_{i1} \\ v_{i2} \\ v_{i3} \end{bmatrix} = \lambda_i \begin{bmatrix} v_{i1} \\ v_{i2} \\ v_{i3} \end{bmatrix}$$

We have

$$v_1 = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}, v_2 = \begin{bmatrix} 1 \\ 0 \\ 1 \end{bmatrix}, v_3 = \begin{bmatrix} 0 \\ 1 \\ -1 \end{bmatrix}$$



Note that  $A = T\Sigma T^{-1}$ , where  $T = [v_1 \ v_2 \ v_3]$ , i.e.

$$T = \begin{bmatrix} 1 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 1 & -1 \end{bmatrix}, \quad T^{-1} = \begin{bmatrix} 1 & -1 & -1 \\ 0 & 1 & 1 \\ 0 & 1 & 0 \end{bmatrix}$$

and

$$\Sigma = \text{diag}\{2, 1, -1\}$$

Thus,

$$\begin{aligned} e^{At} &= Te^{\Sigma t}T^{-1} = \begin{bmatrix} 1 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 1 & -1 \end{bmatrix} \begin{bmatrix} e^{2t} & 0 & 0 \\ 0 & e^t & 0 \\ 0 & 0 & e^{-t} \end{bmatrix} \begin{bmatrix} 1 & -1 & -1 \\ 0 & 1 & 1 \\ 0 & 1 & 0 \end{bmatrix} \\ &= \begin{bmatrix} e^{2t} & -e^{2t} + e^t & -e^{2t} + e^t \\ 0 & e^{-t} & 0 \\ 0 & e^t - e^{-t} & e^t \end{bmatrix} \end{aligned}$$



The above showed the case where  $A$  is diagonalizable. In general, for a given matrix  $A$ , you may only be able to transform it to the Jordan form. For example, if there exists a similarity transformation matrix  $T$  such that  $T^{-1}AT = J$ , where

$$J = \begin{bmatrix} \lambda_1 & 1 & 0 & 0 & 0 \\ 0 & \lambda_1 & 1 & 0 & 0 \\ 0 & 0 & \lambda_1 & 0 & 0 \\ 0 & 0 & 0 & \lambda_1 & 0 \\ 0 & 0 & 0 & 0 & \lambda_2 \end{bmatrix}$$

Then,

$$e^{At} = Te^{Jt}T^{-1} = T \begin{bmatrix} e^{\lambda_1 t} & te^{\lambda_1 t} & \frac{1}{2!}t^2e^{\lambda_1 t} & 0 & 0 \\ 0 & e^{\lambda_1 t} & te^{\lambda_1 t} & 0 & 0 \\ 0 & 0 & e^{\lambda_1 t} & 0 & 0 \\ 0 & 0 & 0 & e^{\lambda_1 t} & 0 \\ 0 & 0 & 0 & 0 & e^{\lambda_2 t} \end{bmatrix} T^{-1}$$



Let us have a more detailed look at the 3rd order case. For general  $3 \times 3$  with  $\det(\lambda I - A) = (\lambda - \lambda_0)^3$ , i.e.  $\lambda_1 = \lambda_2 = \lambda_3 = \lambda_0$ , we want to find  $T$  so that  $T^{-1}AT = J$  or  $A = TJT^{-1}$ , where  $J$  has the following 3 canonical forms:

$$\begin{aligned} &1) \begin{bmatrix} \lambda_0 & 0 & 0 \\ 0 & \lambda_0 & 0 \\ 0 & 0 & \lambda_0 \end{bmatrix}, \quad 2) \begin{bmatrix} \lambda_0 & 1 & 0 \\ 0 & \lambda_0 & 1 \\ 0 & 0 & \lambda_0 \end{bmatrix} \\ &3) \begin{bmatrix} \lambda_0 & 1 & 0 \\ 0 & \lambda_0 & 0 \\ 0 & 0 & \lambda_0 \end{bmatrix} \quad \text{or} \quad \begin{bmatrix} \lambda_0 & 0 & 0 \\ 0 & \lambda_0 & 1 \\ 0 & 0 & \lambda_0 \end{bmatrix} \end{aligned}$$

The first canonical form happens

- when  $A$  has three linearly independent eigenvectors, i.e.  $(\lambda_0 I - A)v = 0$  yields  $v_1, v_2, v_3$  that spans  $\mathcal{R}^3$ .
- mathematically, when  $nullity(\lambda_0 I - A) = 3$ , namely,

$$rank(\lambda_0 I - A) = 3 - nullity(\lambda_0 I - A) = 0$$

- So, if  $rank(\lambda_0 I - A) = 0$ , we know there are 3 independent eigenvectors to diagonalize  $A$ .



For the case 2),  $J = \begin{bmatrix} \lambda_0 & 1 & 0 \\ 0 & \lambda_0 & 1 \\ 0 & 0 & \lambda_0 \end{bmatrix}$ .

- this happens when  $(\lambda_0 I - A)v$  yields only one linearly independent solution, i.e.  $nullity(\lambda_0 I - A) = 1$  and  $rank(\lambda_0 I - A) = 3 - 1 = 2$
- 

$$A[v_1 \ v_2 \ v_3] = [v_1 \ v_2 \ v_3] \begin{bmatrix} \lambda_0 & 1 & 0 \\ 0 & \lambda_0 & 1 \\ 0 & 0 & \lambda_0 \end{bmatrix}$$

$$\implies [\lambda_0 v_1, v_1 + \lambda_0 v_2, v_2 + \lambda_0 v_3] = [Av_1, Av_2, Av_3]$$

That is,

$$(A - \lambda_0 I)v_1 = 0$$

$$(A - \lambda_0 I)v_2 = v_1, \text{ (find the generalized eigenvector } v_2)$$

$$(A - \lambda_0 I)v_3 = v_2, \text{ (find the generalized eigenvector } v_3)$$



For Case 3),  $J = \begin{bmatrix} \lambda_0 & 1 & 0 \\ 0 & \lambda_0 & 0 \\ 0 & 0 & \lambda_0 \end{bmatrix}$  or  $J = \begin{bmatrix} \lambda_0 & 0 & 0 \\ 0 & \lambda_0 & 1 \\ 0 & 0 & \lambda_0 \end{bmatrix}$

- this happens when  $(\lambda_0 I - A)v = 0$  yields two linearly independent eigenvectors, i.e.  $nullity(\lambda_0 I - A) = 2$  and  $rank(\lambda_0 I - A) = 3 - 2 = 1$
- 

$$A[v_1 \ v_2 \ v_3] = [v_1 \ v_2 \ v_3] \begin{bmatrix} \lambda_0 & 1 & 0 \\ 0 & \lambda_0 & 0 \\ 0 & 0 & \lambda_0 \end{bmatrix}$$

$$\implies [\lambda_0 v_1, v_1 + \lambda_0 v_2, \lambda_0 v_3] = [Av_1, Av_2, Av_3]$$

That is,

$$\begin{aligned} (A - \lambda_0 I)v_1 &= 0 \\ (A - \lambda_0 I)v_2 &= v_1, \quad (\text{find the generalized eigenvector } v_2) \\ (A - \lambda_0 I)v_3 &= 0 \end{aligned}$$

So,  $v_1$  and  $v_3$  are directly computed eigenvectors while  $v_2$  is the generalized eigenvector.



### Example 4.3

$$A = \begin{bmatrix} -1 & 1 \\ -1 & 1 \end{bmatrix}, \det(\lambda I - A) = \lambda^2 \implies \lambda_1 = \lambda_2 = 0$$

- *Two repeated eigenvalues with  $\text{rank}(0 \times I - A) = 1$ . Hence, there is only one independent eigenvector:*

$$(A - 0 \times I)v_1 = 0 \implies v_1 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

- *Generalized eigenvector:  $(A - 0 \times I)v_2 = v_1 \implies v_2 = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$*

- $T = [v_1 \ v_2] = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix}, T^{-1} = \begin{bmatrix} 1 & 0 \\ -1 & 1 \end{bmatrix}.$

$$A = T J T^{-1} = T \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} T^{-1},$$

$$e^{At} = T e^{Jt} T^{-1} = T \begin{bmatrix} e^{0t} & t e^{0t} \\ 0 & e^{0t} \end{bmatrix} T^{-1} = \begin{bmatrix} 1-t & t \\ -t & 1+t \end{bmatrix}$$



## Modal form

- Suppose  $A$  has complex eigenvalues. Since  $A$  has only real coefficients, complex eigenvalues must be in the form complex conjugate.
- For example,  $A$  has two real and two complex eigenvalues, then,

$$J = T^{-1}AT = \begin{bmatrix} \lambda_1 & 0 & 0 & 0 \\ 0 & \lambda_2 & 0 & 0 \\ 0 & 0 & \alpha + \beta & 0 \\ 0 & 0 & 0 & \alpha - j\beta \end{bmatrix}$$

which is not useful in practice.

- It can be further transformed to the modal form:

$$\begin{aligned} T_1^{-1}JT_1 &= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & j & -j \end{bmatrix} \begin{bmatrix} \lambda_1 & 0 & 0 & 0 \\ 0 & \lambda_2 & 0 & 0 \\ 0 & 0 & \alpha + j\beta & 0 \\ 0 & 0 & 0 & \alpha - j\beta \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0.5 & -0.5j \\ 0 & 0 & 0.5 & 0.5j \end{bmatrix} \\ &= \begin{bmatrix} \lambda_1 & 0 & 0 & 0 \\ 0 & \lambda_2 & 0 & 0 \\ 0 & 0 & \alpha & \beta \\ 0 & 0 & -\beta & \alpha \end{bmatrix} = \bar{A} \end{aligned}$$

- Matlab: `[am,bm,cm,dm,T]=canon(a,b,c,d,'modal')`



Let us consider the zero-input response  $e^{At}\mathbf{x}(0)$ . Consider an example of Jordan block, we have

$$e^{At} = T \begin{bmatrix} e^{\lambda_1 t} & te^{\lambda_1 t} & t^2 e^{\lambda_1 t}/2 & 0 & 0 \\ 0 & e^{\lambda_1 t} & te^{\lambda_1 t} & 0 & 0 \\ 0 & 0 & e^{\lambda_1 t} & 0 & 0 \\ 0 & 0 & 0 & e^{\lambda_1 t} & 0 \\ 0 & 0 & 0 & 0 & e^{\lambda_2 t} \end{bmatrix} T^{-1}$$

It is clear that every entry of  $e^{At}$  is a linear combination of  $\{e^{\lambda_1 t}, te^{\lambda_1 t}, t^2 e^{\lambda_1 t}, e^{\lambda_2 t}\}$ .

- If every eigenvalue has negative real part, then any zero-input response will approach 0 as  $t \rightarrow \infty$ .
- If  $A$  has an eigenvalue with a positive real part, then most zero input responses will go unbounded as  $t \rightarrow \infty$ .
- If  $A$  has some eigenvalues with zero real part and all with index 1 and the remaining eigenvalues all have negative real parts, then zero-input response will not go unbounded. However, if the index is 2 or higher, some zero-input responses may go unbounded, for example, if  $A$  has eigenvalue 0 with index 2,  $e^{At}$  will contain  $\{1, t\}$  and hence some zero-input responses may go unbounded.



## State Transition Matrix of LTI system $\dot{x} = Ax + Bu$

**Definition 4.1** *The state transition matrix is defined as the  $n \times n$  matrix solution  $\Phi(t - t_0)$  of the equation*

$$\dot{\Phi}(t - t_0) = A\Phi(t - t_0), \quad \Phi(0) = I, \quad t \geq t_0 \quad (6)$$

**Definition 4.2** *A fundamental matrix of the LTI system is the solution to the matrix equation*

$$\dot{\Psi}(t) = A\Psi(t), \quad \Psi(t_0) = H, \quad t \geq t_0, \quad (7)$$

where  $H$  is any nonsingular matrix.

Clearly, fundamental matrix is not unique (different  $H$  results in different solution).

**Lemma 4.1** *One fundamental matrix can be derived by  $n$  linearly independent solutions of the state equation*

$$\dot{x}(t) = Ax(t), \quad x(t_0) = x_0$$



*Proof* Let the  $n$  linearly independent solutions of the state equation be given by  $x_i(t)$ ,  $i = 1, 2, \dots, n$  and  $\mathbf{X}(t) = [x_1(t) \ x_2(t) \ \cdots \ x_n(t)]$ . Then,  $\dot{x}_i(t) = Ax_i(t)$  and

$$\begin{aligned}\dot{\mathbf{X}}(t) &= [\dot{x}_1(t) \ \dot{x}_2(t) \ \cdots \ \dot{x}_n(t)] \\ &= [Ax_1(t) \ Ax_2(t) \ \cdots \ Ax_n(t)] = A\mathbf{X}(t)\end{aligned}$$

$\mathbf{X}(t_0) = [x_1(t_0) \ x_2(t_0) \ \cdots \ x_n(t_0)] = H$  is nonsingular. Hence,  $\mathbf{x}(t)$  is a fundamental matrix.

**Lemma 4.2** *A fundamental matrix of the LTI system can be given by*

$$\Psi(t) = e^{At}, \quad t \geq t_0 \quad (8)$$

*Proof* Note that  $\dot{\Psi}(t) = \frac{de^{At}}{dt} = Ae^{At} = A\Psi(t)$ ,  $t \geq t_0$ . Also, since  $e^{At_0}$  is nonsingular for any  $t_0$ , set  $H = e^{At_0}$ . The result follows from Definition 4.2.

**Lemma 4.3** *Given a fundamental matrix of the LTI system, the state transition matrix  $\Phi(t - t_0)$  can be given by*

$$\Phi(t - t_0) = \Psi(t)\Psi^{-1}(t_0), \quad t \geq t_0 \quad (9)$$



*Proof* It follows from (9) that

$$\dot{\Phi}(t - t_0) = \dot{\Psi}(t)\Psi^{-1}(t_0) = A\Psi(t)\Psi^{-1}(t_0) = A\Phi(t - t_0)$$

Also, when  $t = t_0$ ,

$$\Phi(0) = \Phi(t_0 - t_0) = \Psi(t_0)\Psi^{-1}(t_0) = I$$

**Lemma 4.4** *The state transition matrix is unique and independent of  $\Psi(t)$ .*

*Proof* By the ODE theory, given the initial condition, the solution of (6) is unique. Further, if  $\Psi_1(t)$  and  $\Psi_2(t)$  are two fundamental matrices, then there exists a nonsingular matrix  $P$  such as  $\Psi_2(t) = \Psi_1(t)P$ . Hence,

$$\Phi(t - t_0) = \Psi_2(t)\Psi_2^{-1}(t_0) = \Psi_1(t)PP^{-1}\Psi_1^{-1}(t_0) = \Psi_1(t)\Psi_1^{-1}(t_0)$$

That is,  $\Phi(t - t_0)$  is independent of the choice  $\Psi(t)$ .

From (8) and (9), the state transition matrix is given by  $\Phi(t - t_0) = e^{A(t-t_0)}$ . Thus, the solution of the state equation can be expressed as

$$x(t) = \Phi(t - t_0)x(t_0) + \int_{t_0}^t \Phi(t - \tau)Bu(\tau)d\tau, \quad t \geq t_0 \quad (10)$$



## Properties of State Transition Matrix

- $\Phi(0) = I$ .
- $\Phi^{-1}(t - t_0) = [\Psi(t)\Psi^{-1}(t_0)]^{-1} = \Psi(t_0)\Psi^{-1}(t) = \Phi(t_0 - t)$ .
- $\Phi(t_2 - t_1)\Phi(t_1 - t_0) = \Psi(t_2)\Psi^{-1}(t_1)\Psi(t_1)\Psi^{-1}(t_0) = \Psi(t_2)\Psi^{-1}(t_0) = \Phi(t_2 - t_0)$ .
- $\dot{\Phi}(t - t_0) = A\Phi(t - t_0) = \Phi(t - t_0)A$ .
- $\frac{d}{dt}\Phi^{-1}(t - t_0) = \frac{d}{dt}\Phi(t_0 - t) = -A\Phi(t_0 - t) = -\Phi(t_0 - t)A$ .



## Discretization

- Consider the continuous-time system:

$$\dot{\mathbf{x}}(t) = A\mathbf{x}(t) + B\mathbf{u}(t) \quad (11)$$

$$\mathbf{y}(t) = C\mathbf{x}(t) + D\mathbf{u}(t) \quad (12)$$

- For computation or controller design, the system is to be discretized.
- Assuming sampling period of  $T$  and considering zero order hold for control input, i.e.  $u(t) = u(kT) := u(k)$ ,  $kT \leq t \leq (k+1)T$  for  $k = 0, 1, 2, \dots$ . Then,

$$\begin{aligned} \mathbf{x}(k+1) &= e^{AT}\mathbf{x}(k) + \int_{kT}^{(k+1)T} e^{A[(k+1)T-\tau]} B\mathbf{u}(\tau) d\tau \\ &= e^{AT}\mathbf{x}(k) + \int_0^T e^{\alpha A} d\alpha B\mathbf{u}(k) \end{aligned} \quad (13)$$

Hence, if we compute only the response at  $t = kT$ , (11)-(12) becomes

$$\mathbf{x}(k+1) = A_d\mathbf{x}(k) + B_d\mathbf{u}(k) \quad (14)$$

$$\mathbf{y}(k) = C_d\mathbf{x}(k) + D_d\mathbf{u}(k) \quad (15)$$



- where

$$A_d = e^{AT}, \quad B_d = \int_0^T e^{A\tau} d\tau B, \quad C_d = C, \quad D_d = D$$

- Note that if  $A$  is non-singular,

$$\begin{aligned} \int_0^T e^{A\tau} d\tau &= \int_0^T \left( I + A\tau + A^2 \frac{\tau^2}{2!} + \dots \right) d\tau \\ &= TI + \frac{T^2}{2!} A + \frac{T^3}{3!} A^2 + \dots \\ &= A^{-1} \left( TA + \frac{T^2}{2!} A^2 + \frac{T^3}{3!} A^3 + \dots + I - I \right) \\ &= A^{-1}(e^{AT} - I) = A^{-1}(A_d - I) \end{aligned}$$

- Thus,

$$B_d = A^{-1}(A_d - I)B$$

- Matlab: `[Ad,Bd]=c2d(A,B,T)`

Conversion from continuous-time state equation to discrete-time one under sampling period  $T$



**Example 4.4** Consider LTI system

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ 0 & -2 \end{bmatrix} x + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u, \quad t \geq 0$$

Given sampling period  $T = 0.1s$ , find the discretized state-space model.

- Find  $e^{At}$ :

$$(sI - A)^{-1} = \begin{bmatrix} s & -1 \\ 0 & s + 2 \end{bmatrix}^{-1} = \begin{bmatrix} \frac{1}{s} & \frac{1}{s(s+2)} \\ 0 & \frac{1}{s+2} \end{bmatrix}$$

By taking inverse Laplace transform,

$$e^{At} = \begin{bmatrix} 1 & 0.5(1 - e^{-2t}) \\ 0 & e^{-2t} \end{bmatrix}$$

- Compute:

$$A_d = e^{AT} = \begin{bmatrix} 1 & 0.5(1 - e^{-2T}) \\ 0 & e^{-2T} \end{bmatrix} = \begin{bmatrix} 1 & 0.091 \\ 0 & 0.819 \end{bmatrix}$$

$$B_d = \left( \int_0^T e^{At} dt \right) B = \int_0^T \begin{bmatrix} 1 & 0.5(1 - e^{-2t}) \\ 0 & e^{-2t} \end{bmatrix} dt \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0.005 \\ 0.091 \end{bmatrix}$$



## Solution of Discrete-time State Equation

- From the state equation

$$\mathbf{x}(k+1) = A\mathbf{x}(k) + B\mathbf{u}(k)$$

by recursion, we have

$$\mathbf{x}(k) = A^k \mathbf{x}(0) + \sum_{m=0}^{k-1} A^{k-1-m} B \mathbf{u}(m) \quad (16)$$

and the output is

$$\mathbf{y}(k) = C A^k \mathbf{x}(0) + \sum_{m=0}^{k-1} C A^{k-1-m} B \mathbf{u}(m) + D \mathbf{u}(k)$$

- $A^k$  is called *transition matrix* like  $e^{At}$  in continuous-time case.
- For Jordan block

$$\hat{A} = \begin{bmatrix} \lambda_1 & 1 & 0 & 0 & 0 \\ 0 & \lambda_1 & 1 & 0 & 0 \\ 0 & 0 & \lambda_1 & 0 & 0 \\ 0 & 0 & 0 & \lambda_1 & 0 \\ 0 & 0 & 0 & 0 & \lambda_2 \end{bmatrix} \implies A^k = T \begin{bmatrix} \lambda_1^k & k\lambda_1^{k-1} & k(k-1)\lambda_1^{k-2}/2 & 0 & 0 \\ 0 & \lambda_1^k & k\lambda_1^{k-1} & 0 & 0 \\ 0 & 0 & \lambda_1^k & 0 & 0 \\ 0 & 0 & 0 & \lambda_1^k & 0 \\ 0 & 0 & 0 & 0 & \lambda_2^k \end{bmatrix} T^{-1}$$



Let us consider the zero-input response  $A^k \mathbf{x}(0)$ . Consider an example of Jordan block, we have

$$A^k = T \begin{bmatrix} \lambda_1^k & k\lambda_1^{k-1} & k(k-1)\lambda_1^{k-2}/2 & 0 & 0 \\ 0 & \lambda_1^k & k\lambda_1^{k-1} & 0 & 0 \\ 0 & 0 & \lambda_1^k & 0 & 0 \\ 0 & 0 & 0 & \lambda_1^k & 0 \\ 0 & 0 & 0 & 0 & \lambda_2^k \end{bmatrix} T^{-1}$$

It is clear that every entry of  $A^k$  is a linear combination of  $\{\lambda_1^k, k\lambda_1^{k-1}, k^2\lambda_1^{k-2}, \lambda_2^k\}$ .

- If every eigenvalue has its magnitude less than 1, then any zero-input response will approach 0 as  $k \rightarrow \infty$ .
- If  $A$  has an eigenvalue with magnitude greater than 1, then most zero input responses will go unbounded as  $k \rightarrow \infty$ .
- If  $A$  has some eigenvalues with magnitude 1 and all with index 1 and the remaining eigenvalues all have magnitudes less than 1, then zero-input response will not go unbounded. However, if the index is 2 or higher, some zero-input responses may go unbounded, for example, if  $A$  has eigenvalue 1 with index 2,  $A^k$  contains  $\{1, k\}$  and hence some zero-input responses may go unbounded.



**Equivalent State Equations:** Consider the n-dimensional state equation:

$$\dot{\mathbf{x}}(t) = A\mathbf{x}(t) + B\mathbf{u}(t) \quad (17)$$

$$\mathbf{y}(t) = C\mathbf{x}(t) + D\mathbf{u}(t) \quad (18)$$

Suppose we now introduce a state transformation  $\bar{\mathbf{x}} = P\mathbf{x}$ , where  $P$  is non-singular. Then, from (17)-(18) we have

$$\dot{\bar{\mathbf{x}}}(t) = \bar{A}\bar{\mathbf{x}}(t) + \bar{B}\mathbf{u}(t) \quad (19)$$

$$\mathbf{y}(t) = \bar{C}\bar{\mathbf{x}}(t) + \bar{D}\mathbf{u}(t) \quad (20)$$

where

$$\bar{A} = PAP^{-1}, \quad \bar{B} = PB, \quad \bar{C} = CP^{-1}, \quad \bar{D} = D.$$

- (19)-(20) is said to be (algebraically) equivalent to (17)-(18).
- The matrix  $D$ , called direct transmission part between input and output, is independent of the state transformation.
- It can be easily shown that

$$\bar{\Delta}(\lambda) = \det(\lambda I - \bar{A}) = \det(\lambda I - A) = \Delta(\lambda)$$

$$\hat{G}(s) = \bar{C}(sI - \bar{A})^{-1}\bar{B} + \bar{D} = C(sI - A)^{-1}B + D = G(s)$$



Two state equations are said to be *zero state equivalent* if they have the same transfer matrix,

$$C(sI - A)^{-1}B + D = \bar{C}(sI - \bar{A})^{-1}\bar{B} + \bar{D}$$

i.e.

$$D + CBs^{-1} + CABs^{-2} + CA^2Bs^{-3} + \dots = \bar{D} + \bar{C}\bar{B}s^{-1} + \bar{C}\bar{A}\bar{B}s^{-2} + \bar{C}\bar{A}^2\bar{B}s^{-3} -$$

**Theorem 4.1** *Two linear time-invariant state equations  $\{A, B, C, D\}$  and  $\{\bar{A}, \bar{B}, \bar{C}, \bar{D}\}$  are zero-state equivalent or have the same transfer matrix if and only if  $D = \bar{D}$  and*

$$CA^mB = \bar{C}\bar{A}^m\bar{B}, \quad m = 0, 1, 2, \dots$$

Clearly, algebraic equivalence implies zero-state equivalence but the converse is generally not true.

See Example 4.4 of page 96 (C.T. Chen) where the state equations for system 1:

$$\dot{x} = 0x + 0u, \quad y = 0.5u$$

and for system 2:  $\dot{x} = x, \quad y = 0.5x + 0.5u$ . The zero-state responses of the above systems are the same but they are not algebraically equivalent.



## Linear Time-Varying Systems

- State equations:

$$\dot{\mathbf{x}}(t) = A(t)\mathbf{x}(t) + B(t)\mathbf{u}(t) \quad (21)$$

$$\mathbf{y}(t) = C(t)\mathbf{x}(t) + D(t)\mathbf{u}(t) \quad (22)$$

where  $\mathbf{x} \in \mathcal{R}^n$  is the state,  $\mathbf{u} \in \mathcal{R}^m$  is the input and  $\mathbf{y} \in \mathcal{R}^p$  is the output.

- $A(t)$ ,  $B(t)$ ,  $C(t)$ ,  $D(t)$  are continuous, real-valued functions on  $[t_0, \infty)$ .
- Input  $\mathbf{u}(t)$  is piecewise continuous.



- Scalar ODE:  $\dot{x} = ax \implies x(t) = e^{at}x(0)$ .
- Matrix case:  $\dot{\mathbf{x}}(t) = A\mathbf{x} \implies \mathbf{x}(t) = e^{At}\mathbf{x}(0)$ .
- Time-varying scalar ODE:  $\dot{x} = a(t)x \implies x(t) = e^{\int_0^t a(\tau)d\tau}x(0)$  since

$$\frac{d}{dt}e^{\int_0^t a(\tau)d\tau} = a(t)e^{\int_0^t a(\tau)d\tau} = e^{\int_0^t a(\tau)d\tau}a(t)$$

- For time-varying matrix case:  $\dot{\mathbf{x}}(t) = A(t)\mathbf{x}(t)$ , is

$$\mathbf{x}(t) = e^{\int_0^t A(\tau)d\tau}\mathbf{x}(0)$$

a solution?

- Answer is no in general. Since

$$e^{\int_0^t A(\tau)d\tau} = I + \int_0^t A(\tau)d\tau + \frac{1}{2} \left( \int_0^t A(\tau)d\tau \right) \left( \int_0^t A(s)ds \right) + \dots$$

but

$$\begin{aligned} \frac{d}{dt} \left( e^{\int_0^t A(\tau)d\tau} \right) &= A(t) + \frac{1}{2}A(t) \left( \int_0^t A(s)ds \right) + \frac{1}{2} \left( \int_0^t A(\tau)d\tau \right) A(t) + \dots \\ &\neq A(t)e^{\int_0^t A(\tau)d\tau} \end{aligned}$$



## Fundamental matrix:

- Consider  $\dot{\mathbf{x}} = A(t)\mathbf{x}$ .
- Suppose for every initial state  $\mathbf{x}_i(t_0)$ ,  $i = 1, 2, \dots, n$ , the solution is  $\mathbf{x}_i(t)$ .
- Let  $\mathbf{X} = [\mathbf{x}_1 \ \mathbf{x}_2 \ \dots \ \mathbf{x}_n]$ . If  $\mathbf{X}(t_0)$  is non-singular,  $\mathbf{X}(t)$  is called *fundamental matrix* which is non-singular.
- Fundamental matrix is not unique.

**Example 4.5** Consider

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 0 \\ t & 0 \end{bmatrix} \mathbf{x}(t)$$

*i.e.*

$$\dot{x}_1(t) = 0, \quad \dot{x}_2(t) = tx_1(t)$$

*Then,*

$$x_1(t) = x_1(0), \quad x_2(t) = \int_0^t \tau x_1(0) d\tau + x_2(0) = 0.5t^2 x_1(0) + x_2(0)$$



Hence,

$$\begin{aligned}\mathbf{x}(0) &= \begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \implies \mathbf{x}(t) = \begin{bmatrix} 1 \\ 0.5t^2 \end{bmatrix} \\ \mathbf{x}(0) &= \begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix} = \begin{bmatrix} 1 \\ 2 \end{bmatrix} \implies \mathbf{x}(t) = \begin{bmatrix} 1 \\ 0.5t^2 + 2 \end{bmatrix}\end{aligned}$$

Since the two initial states are independent,

$$\mathbf{X}(t) = \begin{bmatrix} 1 & 1 \\ 0.5t^2 & 0.5t^2 + 2 \end{bmatrix}$$

is a fundamental matrix.



## State Transition Matrix:

- $\Phi(t, t_0) := \mathbf{X}(t)\mathbf{X}^{-1}(t_0)$  is called *the state transition matrix*.
- The state transition matrix is the unique solution of

$$\frac{\partial}{\partial t}\Phi(t, t_0) = A(t)\Phi(t, t_0) \quad (23)$$

with initial condition  $\Phi(t_0, t_0) = I$ .

- Properties:

$$\begin{aligned}\Phi(t, t) &= I \\ \Phi^{-1}(t, t_0) &= [\mathbf{X}(t)\mathbf{X}^{-1}(t_0)]^{-1} = \mathbf{X}(t_0)\mathbf{X}^{-1}(t) = \Phi(t_0, t) \\ \Phi(t, t_0) &= \Phi(t, t_1)\Phi(t_1, t_0)\end{aligned}$$

for every  $t$ ,  $t_0$  and  $t_1$ .



## Solution of State-space Equation of LTV system

$$\mathbf{x}(t) = \Phi(t, t_0)\mathbf{x}_0 + \int_{t_0}^t \Phi(t, \tau)B(\tau)\mathbf{u}(\tau)d\tau, \quad t \geq t_0 \quad (24)$$

Hence, the output is

$$\begin{aligned} \mathbf{y}(t) &= C(t)\mathbf{x}(t) + D(t)\mathbf{u}(t) \\ &= C(t)\Phi(t, t_0)\mathbf{x}_0 + \int_{t_0}^t C(t)\Phi(t, \tau)B(\tau)\mathbf{u}(\tau)d\tau + D(t)\mathbf{u}(t) \end{aligned} \quad (25)$$



**Example 4.6** Consider

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ -g + v_e u_0 / (m_0 + u_0 t) \end{bmatrix}, \quad \mathbf{x}(0) = 0$$

where  $x_1(t)$  and  $x_2(t)$  are respectively the altitude and velocity of an ascending rocket. Assuming that the mass supply is exhausted at time  $t_e > 0$ . Calculate the state trajectory on  $[0, t_e]$ .

It is easy to obtain

$$\Phi(t, \tau) = \begin{bmatrix} 1 & t - \tau \\ 0 & 1 \end{bmatrix}$$

With  $\mathbf{x}(0) = 0$ , the zero-state response is

$$\begin{aligned} \mathbf{x}(t) &= \int_0^t \begin{bmatrix} 1 & t - \sigma \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ -g + v_e u_0 / (m_0 + u_0 \sigma) \end{bmatrix} d\sigma \\ &= \begin{bmatrix} -gt^2/2 - (v_e m_0 / u_0)(1 + u_0 t / m_0) \ln(1 + u_0 t / m_0) \\ -gt + v_e \ln(1 + u_0 t / m_0) \end{bmatrix}, \quad t \in [0, t_e] \end{aligned}$$



At  $t_e$ , the thrust becomes zero but the rocket will not stop. For  $t > t_e$ ,

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ -g \end{bmatrix}$$

and the state trajectory needs to be calculated.

Denote the remaining mass of the rocket by

$$m_e = m_0 + u_0 t_e$$

Then,

$$\mathbf{x}(t_e) = \begin{bmatrix} -gt_e^2/2 - v_e t_e + (v_e m_e / u_0) \ln(m_e / m_0) \\ -gt_e + v_e \ln(m_e / m_0) \end{bmatrix}$$

Hence, the state response is

$$\begin{aligned} \mathbf{x}(t) &= \Phi(t, t_e) \mathbf{x}(t_e) + \int_{t_e}^t \Phi(t, \sigma) \begin{bmatrix} 0 \\ -g \end{bmatrix} d\sigma \\ &= \begin{bmatrix} -v_e t_e + v_e (t + m_0 / u_0) \ln(m_e / m_0) - gt^2/2 \\ v_e \ln(m_e / m_0) - gt \end{bmatrix}, \quad t \geq t_e \end{aligned}$$

The above is valid until the altitude reaches zero again.



## Exercise:

1. An oscillation can be generated by

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \mathbf{x}$$

Show that its solution is

$$\mathbf{x}(t) = \begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix} \mathbf{x}(0)$$

2. Use two different methods to find the unit-step response of

$$\begin{aligned} \dot{x} &= \begin{bmatrix} 0 & 1 \\ -2 & -2 \end{bmatrix} x + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u \\ y &= [2 \quad 3]x \end{aligned}$$

3. Given

$$A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -6 & -11 & -6 \end{bmatrix}, \quad A = \begin{bmatrix} 2 & 0 & 1 \\ 0 & 2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

find  $e^{At}$ .



### 3. Discretize the system

$$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} 0 & 1 \\ -2 & -2 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} \\ y &= [2 \ 3] \mathbf{x}\end{aligned}$$

with  $T = 1$  and  $T = \pi$ .

### 4. Find a fundamental matrix and the state transition matrix of

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 \\ 0 & t \end{bmatrix} \mathbf{x}$$