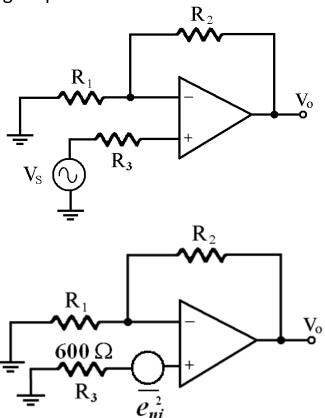
EE4341 TUTORIAL 4 SOLUTION

1a. (i) Non-inverting amplifier



 R_1 and R_2 are chosen such that $R_1/\!/R_2 = R_3$ for DC offset cancellation.

$$\overline{e_{ni}}^{2} = \overline{v_{n}}^{2} + \overline{i_{n}}^{2} \left(R_{3}^{2} + \left(R_{1} // R_{2}\right)^{2}\right) + 4kT \left(R_{3} + R_{1} // R_{2}\right)$$

$$= \overline{v_{n}}^{2} + \overline{i_{n}}^{2} \left(2R_{3}^{2}\right) + 8kTR_{3}$$

$$= 8 \times 10^{-16} + 9 \times 10^{-25} \left(2 \times 600^{2}\right) + 2 \times 1.656 \times 10^{-22} \times 600$$

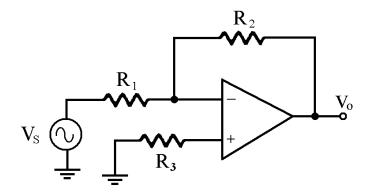
$$= 8 \times 10^{-16} + 6.48 \times 10^{-19} + 2 \times 10^{-17}$$

$$= 8.2 \times 10^{-16} \quad V^{2} / Hz$$

$$E_{ni} = \sqrt{\overline{e_{ni}}^{2}} \Delta f = \sqrt{8.2 \times 10^{-16} \times 20k} = 4.05 \text{ } \mu\text{V}$$

$$SNR(dB) = 20 \log \frac{V_{s}}{E_{ni}} = 20 \log \frac{5mV}{4.05 \mu V} = 61.8 \text{ } dB$$

1a. (ii) Inverting amplifier



The voltage gain for the noise voltage is non-inverting amplifier gain:

$$\therefore \overline{e_{no}}^{2} = \overline{e_{ni+}}^{2} \left(1 + \frac{R_{2}}{R_{1}}\right)^{2} = \overline{e_{ni+}}^{2} \left(\frac{R_{1} + R_{2}}{R_{1}}\right)^{2}$$

To reflect the noise at the inverting input:

$$\therefore \overline{e_{ni}}^{2} = \frac{\overline{e_{no}}^{2}}{(R_{2}/R_{1})^{2}} = \overline{e_{ni+}}^{2} \left(\frac{R_{1}+R_{2}}{R_{1}}\right)^{2} \left(\frac{R_{1}}{R_{2}}\right)^{2}$$

$$= \overline{e_{ni+}}^{2} \left(\frac{R_{1}+R_{2}}{R_{2}}\right)^{2} = \overline{e_{ni+}}^{2} \left(1+\frac{R_{1}}{R_{2}}\right)^{2}$$

$$E_{ni-} = \left(1+\frac{R_{1}}{R_{2}}\right) E_{ni+} = \left(1+\frac{1}{10}\right) \times 4.05 = 4.46 \mu V$$

$$SNR(dB) = 20 \log \frac{V_{s}}{E_{ni}} = 20 \log \frac{5mV}{4.46 \mu V} = 61 \text{ dB}$$

1b. (i) Non-inverting amplifier

$$\overline{e_{ni}}^{2} = \overline{v_{n}}^{2} + \overline{i_{n}}^{2} (2R_{3}^{2}) + 8kTR_{3}$$

$$= 16 \times 10^{-18} + 0 + 2 \times 1.656 \times 10^{-22} \times 600$$

$$= 3.6 \times 10^{-17} \quad V^{2} / Hz$$

$$E_{ni} = \sqrt{\overline{e_{ni}}^{2}} \Delta f = \sqrt{3.6 \times 10^{-17} \times 20k} = 0.85 \quad \mu V$$

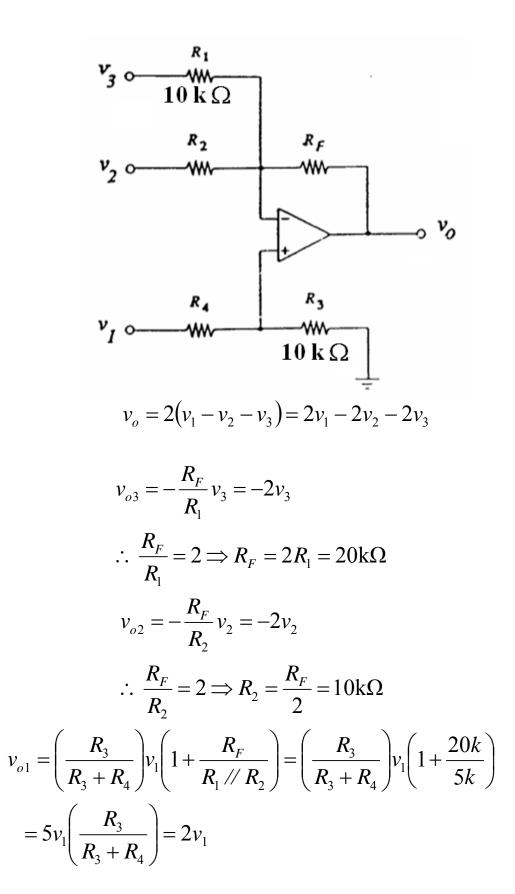
$$SNR(dB) = 20 \log \frac{V_{s}}{E_{ni}} = 20 \log \frac{5mV}{0.85 \mu V} = 75.4 \text{ dB}$$

(ii) Inverting amplifier:

$$E_{ni-} = \left(1 + \frac{R_1}{R_2}\right) E_{ni+} = \left(1 + \frac{1}{10}\right) \times 0.85 = 0.94 \mu V$$

$$SNR(dB) = 20 \log \frac{V_s}{E_{ni}} = 20 \log \frac{5mV}{0.94 \mu V} = 74.5 \text{ dB}$$

2.



$$\therefore \frac{5R_3}{R_3 + R_4} = 2 \Rightarrow R_4 = \frac{3R_3}{2} = 15k\Omega$$

$$R_n = R_1 // R_2 // R_F = 10k // 10k // 20k = 4k\Omega$$

 $R_p = R_4 // R_3 = 15k // 10k = 6k\Omega$

The non-inverting amplifier gain for the noise:

$$A_{v} = 1 + \frac{R_{F}}{R_{1} / / R_{2}} = 1 + \frac{20k}{5k} = 5$$

The -3dB bandwidth of the non-inverting amplifier:

$$f_A = \frac{GBW}{A} = \frac{10^6}{5} = 200kHz$$

$$\begin{split} E_{no} &= A_{\nu} \overline{\left[e_{n\nu}^{2}\right]} \left(f_{ce} \ln \frac{1.57 f_{A}}{f_{L}} + 1.57 f_{A} - f_{L} \right) + \\ &\left(R_{p}^{2} + R_{n}^{2} \right) \overline{\left[e_{n\nu}^{2}\right]} \left(f_{ci} \ln \frac{1.57 f_{A}}{f_{L}} + 1.57 f_{A} - f_{L} \right) + 4kT \left(R_{p} + R_{n} \right) \left(1.57 f_{A} - f_{L} \right) \right]^{\frac{1}{2}} \\ &= 5 \left[\left(20 \times 10^{-9} \right)^{2} \left(200 \ln \frac{314k}{1} + 314k - 1 \right) + \\ &\left(\left(6k \right)^{2} + \left(4k \right)^{2} \right) \left(0.5 \times 10^{-12} \right)^{2} \left(2000 \ln \frac{314k}{1} + 314k - 1 \right) + \\ &1.656 \times 10^{-20} \left(6k + 4k \right) \left(314k - 1 \right) \right]^{\frac{1}{2}} \\ &E_{no} = 5 \left[1.27 \times 10^{-10} + 4.41 \times 10^{-12} + 5.20 \times 10^{-11} \right]^{\frac{1}{2}} = 67.64 \mu V \\ &E_{no,p-p} = 6.6 E_{no,ems} = 6.6 \times 67.64 \mu V = 0.45 m V \end{split}$$