

PRACTICAL CONSIDERATIONS IN EXPERIMENTAL  
COMPUTATIONAL SENSING

by

Phillip K. Poon



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As members of the Dissertation Committee, we certify that we have read the dissertation prepared by Phillip K. Poon titled Practical Considerations in Experimental Computational Sensing and recommend that it be accepted as fulfilling the dissertation requirement for the degree of Doctor of Philosophy.

Date: 9 December 2016

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Amit Ashok

Date: 9 December 2016

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Rongguang Liang

Date: 9 December 2016

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Michael E. Gehm

Final approval and acceptance of this dissertation is contingent upon the candidate's submission of the final copies of the dissertation to the Graduate College.

I hereby certify that I have read this dissertation prepared under my direction and recommend that it be accepted as fulfilling the dissertation requirement.

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Dissertation Director: Amit Ashok

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SIGNED: Phillip K. Poon

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## DEDICATION

For my wife. We moved from city to city. You stuck with me through the highs and lows. You cooked dinner for me when I came home from a long day. You did the chores so I could concentrate on research. You acted as both mother and father to our son while I wrote. You believed in me even when I did not. You sacrificed your dreams and goals so I could accomplish mine.

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## ABSTRACT

Implementing computational optical sensors often comes with various issues that many traditional sensors may not encounter.

## Chapter 1

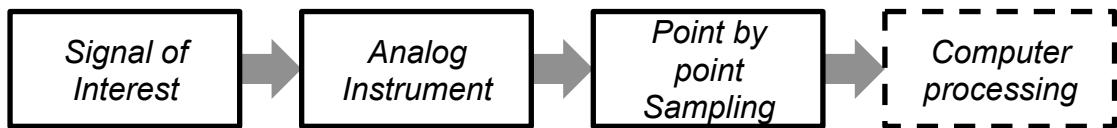
### Introduction

This chapter provides the motivation for the need to address the practical issues in experimental computational sensing. While computational sensing has the ability to ameliorate or eliminate trade-offs in many traditional isomorphic sensors, the sensor engineer is faced with a new set of challenges when designing a computational sensor. For example, while both computational and traditional isomorphic sensors often require calibration, a computational sensor can be more sensitive to calibration error due to the lack of redundancy in the measurement data. It is the author's hope that a full discussion on these various challenges will encourage more research on these issues.

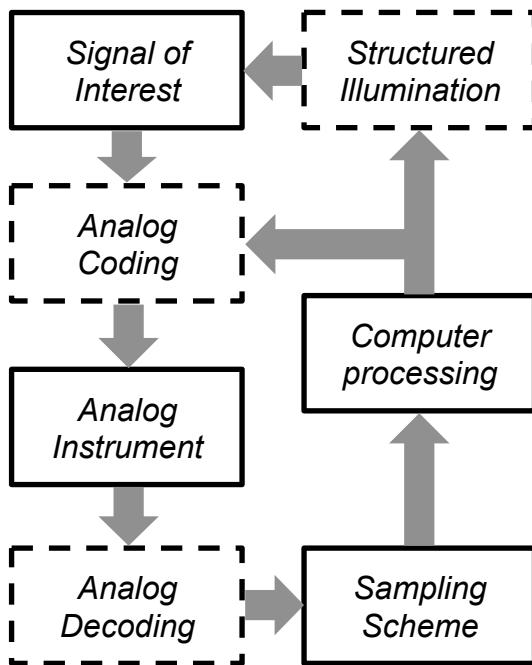
*Isomorphic sensing* is the concept that the measurement data of a sensor resembles the signal-of-interest [1]. For example, in a camera, the digital image looks like the object. In isomorphic sensing the analog hardware, analog-to-digital converter (ADC), and processing algorithms are separate components, see Figure 1.1.

*Computational sensing* is the concept that a joint design of the sensor, often through active *coding* (often called structured illumination) or passive *coding* of the analog signal, with inversion algorithms will outperform the isomorphic sensor, see Figure 1.2 [2]. An example of computational sensing is the Magnetic Resonance Imaging (MRI) technique, where the measurements are in Fourier space. While *isomorphic* sensors can provide flexible sensing in multiple applications, joint design of a *computational sensor* will lead to performance increases often in resource constrained scenarios. Throughout this chapter and the rest of this dissertation, I will provide many examples that highlight the differences between computational and isomorphic sensing.

Rather than a rigorous discussion, this chapter will discuss some of the major developments and concepts in the field of computational sensing on an intuitive level. This will familiarize the reader with important terminology and techniques common in the field of computational sensing. This chapter will also discuss some of the challenges I and many other experimentalists and engineers have faced when developing computational sensing prototypes. I will close this chapter with a brief



**Figure 1.1:** The signal-of-interest is incident upon the analog instrument. The analog instrument forms an isomorphism of the signal which is then periodically sampled point-by-point through an analog-to-digital converter (ADC) device. Once the signal is in digital form, post-processing algorithms are often used to perform various tasks such as noise reduction, detection, and classification. Notice that the analog instrument, sampling scheme, and processing are all separated.



**Figure 1.2:** In a computational sensor, coding, decoding, and structured illumination are used in addition to the analog instrument, the algorithms, and sampling scheme. The dashed boxes represent optional processes that may or may not be needed.

look ahead to the rest of the dissertation.

### 1.1 Isomorphic Sensing

In Greek, the word isomorphic loosely translates to “equal in form.” Traditional sensors perform isomorphic sensing. In the context of this dissertation, an isomorphic sensor is any sensor which attempts to produce measurement data that resembles the signal-of-interest. In this paradigm, the analog instrument, sampling scheme, and post-processing algorithms are separate components and processes.

I will discuss three important examples of isomorphic sensors: the pinhole camera, the photographic camera and the optical spectrometer<sup>1</sup>. These sensors have inspired many other optical and non-optical sensors throughout history, so it is natural to use them as examples for comparison when discussing computational sensing.

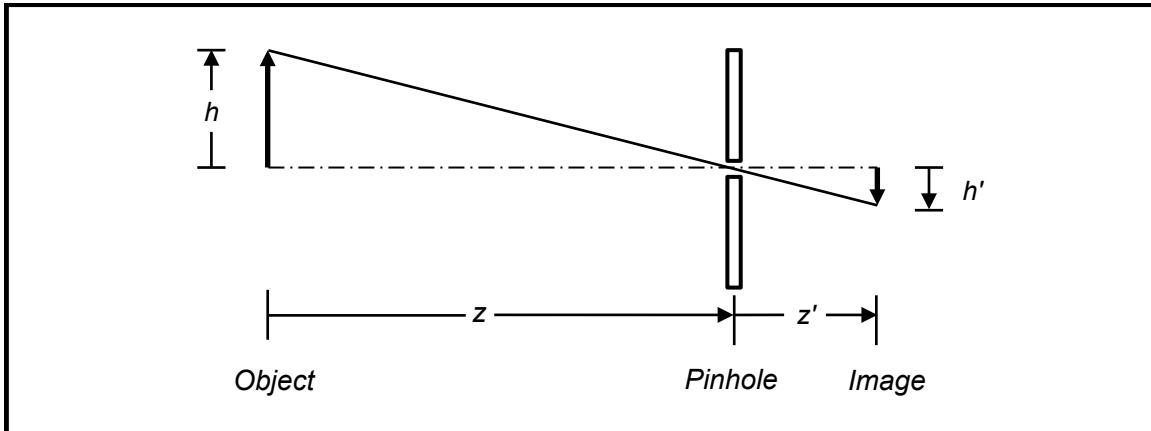
Before I continue, I want to define *measurement* because it can often be used in an informal manner. In this dissertation a measurement has a very specific meaning. A measurement is a process that converts a physical phenomena to a collection of data. The signal-of-interest is the physical phenomena that one is interested in quantifying. I will call the collection of data the measurement data. The word sensing has a less precise meaning and I will use it in an informal manner. Sensing is any act that uses techniques, instruments, or processes that produces measurement data.

In the photographic camera, the signal-of-interest is the intensity distribution of the object. The analog instrument consists of the lenses which are designed and fabricated to produce an image that looks like the object at the focal-plane array (FPA). The more the image resembles the object the better the optics. The FPA then samples the image and produces a digital representation of the intensity distribution of the object, the measurement data. If one is interested in performing a task such as detection or classification, the measurement data sent to a post processing algorithm to perform those tasks.

There are two major sub-systems in the photographic camera which determine how well it performs: the optics and the FPA. Ideally, the optics (the analog instrument in this case) will produce a point-spread function (PSF) which is at the physical limit set by diffraction given the aperture size. For example, in a task such

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<sup>1</sup>I will call the optical spectrometer just a spectrometer from now on, even though there are many instruments called spectrometers that are concerned with optical spectra

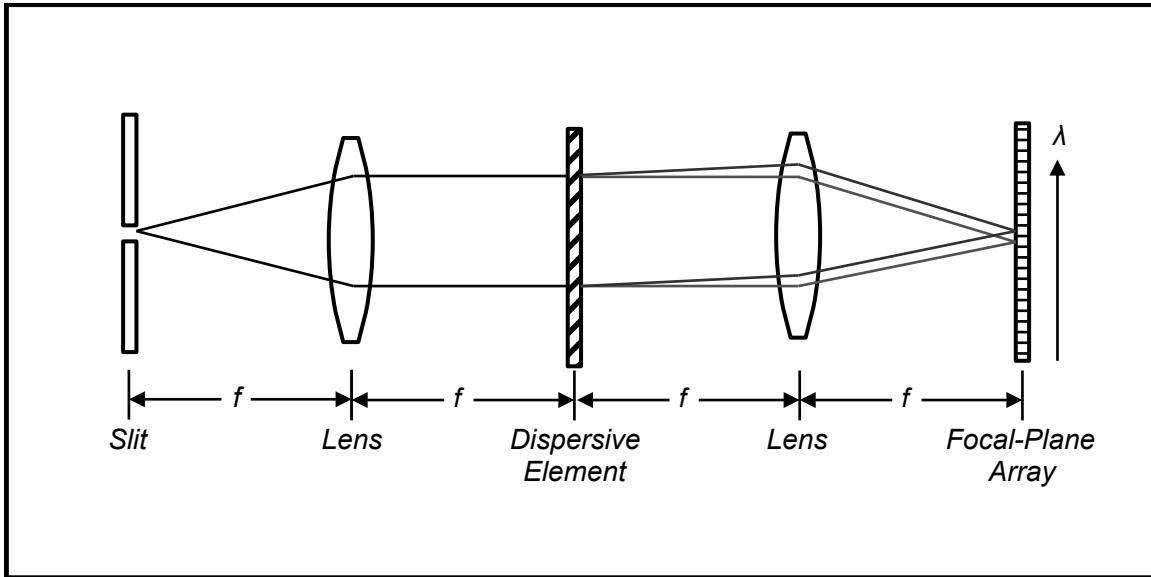


**Figure 1.3:** A pinhole camera is a simple imaging system that forms an image without a lens or mirror. This is due to the ray nature of light. A small hole will only admit a small amount of rays from an object point that is radiating light. Each point on a object emits light at different angles, and the image formed is a superposition of different rays. The smaller the hole, the less blurry the image. However, small holes also limit the amount of light

as the detection of a star from several neighboring stars in the night sky, if the PSF is much larger than the center to center separation of the two stars in the optical image, it will be difficult to detect. Even if the PSF is small enough, the FPA must sample at a fine enough pixel-to-pixel spacing, called the *pixel pitch*, to accurately reproduce the intensity variations at the scale which is pertinent to the task. Intuitively, this makes sense because if the stars are imaged onto a single pixel, then one cannot ever hope to be able to accurately detect the star without some other prior or side information.

The pinhole camera consists of a small hole and a box which prevents any light except from the pinhole from entering, see Figure 1.3. The pinhole camera is useful for imaging in parts of the electromagnetic spectrum and particles for which there is no direct analog to the refractive lens or reflective mirror. Like the photographic camera, the smaller the PSF diameter, the better the spatial resolution. Unfortunately, in the traditional pinhole camera, the only way to reduce the PSF diameter is by decreasing the diameter of the pinhole which reduces the amount of light.

In the spectrometer, the signal of interest is the spectrum of the object. The optics are designed to take the incoming light and separate various wavelength components, see Figure 1.4. The part of the spectrometer which is used to physically isolate the wavelengths is called a *monochromator*. The monochromator contains a prism or diffraction grating which creates a wavelength dependent angular separation. The result is a spectral intensity as a function of position at the FPA. The FPA



**Figure 1.4:** An isomorphic slit spectrometer with a 4F configuration. The slit limits the lateral extent of the object (or intermediate image). The light from the slit is collimated and separated into different angles based on the wavelength. A second lens then images wavelength shifted copies of the slit on the image plane where the detector is. As the slit size decreases, less light is allowed, but one gains spectral resolution by rejected light from neighboring locations on the object.

and post-processing algorithms are used in the same manner as the photographic camera, which is to sample the spatially varying intensity (which is now encoding spectral information) creating a digital version of it and to perform various tasks on the measurement data. For now, I will concentrate on the slit spectrometer, which measures the spectrum at a single spatial location on the object.

In the spectrometer, one of the important performance metrics is *spectral resolution*, which I denote  $\delta_\lambda$ . The spectral resolution is the smallest difference in wavelength the instrument can discern. Large spectral resolutions can degrade the spectrometers ability to discern important parts of the spectrum. Similarly with the camera, the FPA must have a pixel pitch which is small enough to correctly sample the variations in the spectrum.

The point-by-point nature of isomorphic sensing is both a strength and a source of weakness. The strength comes from the straightforward and intuitive architecture of the isomorphic sensor. Each subsystem: the optics, the focal-plane array (FPA), and the post-processing can be designed and constructed separately as long as they meet their individual specifications. As long as the signal-to-noise ratio (SNR) is sufficient and the sampling rate is high enough, one is guaranteed to recover the signal.

One of the weaknesses of the isomorphic approach is the ability to measure low SNR signals. Because the signal-of-interest is sampled in a completely parallel fashion at each exposure, each pixel contributes a certain amount of noise. If the noise dominates, the measurement fidelity decreases forcing the operator to increase the exposure time. For weak signals, the exposure time can become prohibitive and for temporally dynamic signals this leads to a loss of resolution. Indeed, one of the major engineering trade-offs faced by traditional spectrometer designers is that when one attempts to increase the light collection (increased slit-width) the spectral resolution  $\delta_\lambda$  degrades. Similarly, in the pinhole camera, there is a throughput versus spatial resolution trade-off, increasing the size of the pinhole degrades the PSF.

It would be easy to assume that recent progress in machine learning and statistical signal processing combined with the dramatic increase in computing power that one could simply post-process poor measurements and obtain useful data. However, this is not possible due to the an important theorem in information theory called the *data processing inequality* [3]. The information content of a signal cannot be increased through post-processing.

Another weakness of isomorphic sensing is that the separation of the analog instrument, the sampling scheme, and the data processing algorithms lead to increased size, weight and power-cost (SWAP-C). As I mentioned in the photographic camera, the optics must be designed to produce a small PSF. For demanding applications, the optical design and fabrication can be the most expensive component of the sensor. While the price of FPAs sensitive to the visible wavelength region have fallen, FPAs sensitive to certain parts of the electromagnetic spectrum can be quite expensive or non-existent [4, 5].

In many cases, the signal is redundant and high resolution sampling becomes a waste of resources, such as data storage and communications bandwidth. A good example is in photography where often the post-processing takes the digital image and applies a compression algorithm which looks for patterns in the signal and reduces the file size, discarding much of the sample data [6].

The isomorphic sensor approach has served humanity well, however with all the weakness that I have discussed, there is a need for sensors which can operate in low-SNR conditions, with fewer measurement time, fewer measurements, or at lower SWAP-C while still producing useful information relevant to the sensor task. I will now begin to discuss some of major techniques in computational sensing that can be used to address some or all of the issues that I just stated.

## 1.2 Development of Multiplexing in Sensing

*Multiplexing* in sensing is the idea that each measurement sample is a physical combination of various parts of the analog signal-of-interest. Multiplexing is a powerful tool that can be exploited by the sensor designer to eliminate or relax SNR related trade-offs.

A simple example which illustrates the usefulness of multiplex sensing is weighing objects. In this example, one needs to weigh 100 sheets of paper. Assume that the measurement error of the scale is insignificant. Isomorphic sensing means one would need to measure each sheet of paper individually, requiring 100 measurements.

If the measurement error of the scale is on the order of the weight of a single sheet, measuring each sheet individually produces a large measurement error. In order to reduce the error to an acceptable SNR one needs to make several measurements per sheet.

However, one can measure all 100 sheets at the same time. Since the weight of all 100 sheets is much larger than the measurement error of the scale, one can dramatically increase the precision of the measurement. If each sheet is the same weight, then the measurement process is finished.

The weighing problem is analogous to the spectroscopy example. As discussed earlier in section 1.1, there is trade-off between light collection and spectral resolution. Increasing the slit-width to increase the amount of light has the effect of degrading the spectral resolution  $\delta_\lambda$ . Around the late 1940's and early 1950's, several important papers and inventions demonstrated the effectiveness of multiplexing in spectroscopy. At the time the FPA was non-existent, so in the slit spectrometer shown in Figure 1.4, where the FPA is pictured, there was actually another slit. To record the intensity at each spectral channel, either the dispersive element or the exit slit had to be mechanically translated, making the measurements even slower by a factor of  $N_\lambda$ , the number of spectral channels of interest.

Golay was the first to propose multiplexing the slit spectrometer by creating a pattern of binary (1's and 0's) entrance and exit slits [7]. In the Golay multi-slit spectrometer, the patterns of entrance and exit slits are matched based on mathematically useful properties. Intuitively, the ability to use multiple entrance and exit slits increases the optical throughput of the spectrometer. In communications theory, the process of structuring the data from the source to the receiver is referred to as coding. Similarly, in computational sensing, the transmission of information

between an object signal-of-interest and the sensor is considered a coding problem [1]. In the multi-slit spectrometer, the entrance slits act to code the spectrum while the exit slits decode the coded spectrum. Golay's idea dramatically increased the optical throughput without degrading the spectral resolution.

Another example that is pertinent to this dissertation is coded aperture imaging. Coded aperture imaging can be thought of as the multiplexed version of a pinhole camera. As mentioned earlier in section 1.1, there is a trade-off between the throughput and spatial resolution. However in many fields, such as high-energy particle imaging, refractive lenses and reflective mirrors are non-existent or underdeveloped. By using multiple pinholes the throughput is increased without sacrificing spatial resolution. However, the pattern of the pinholes (which is the code) must be carefully designed in order for the reconstruction to be feasible. Fenimore, Canon, and Gottesman were among the first to create an elegant solution to coded aperture design called uniformly redundant arrays [8, 9]. The uniformly redundant array increases throughput without significantly degrading the spatial resolution.

In summary, multiplexing has the ability to eliminate classic trade-offs in isomorphic sensors: signal strength or resolution. Modern researchers are still actively developing novel ways to implement multiplexing to increase resolution and sensitivity in the spatial domain [10, 11], spectral domain [12, 13], and temporal domain [14, 15]. However, multiplexing is not without its own set of challenges. As I mentioned, the coding must often be designed to obtain feasible signal reconstruction. I now discuss inverse problems in computational sensing.

### 1.3 Forward Models and Inverse Problems

In the computational sensing community, a model that explains the mapping of the signal-of-interest to the measurement data is called the *forward model*. The problem of taking the observed data and calculating a reconstruction of the signal-of-interest or task-specific parameters is called the *inverse problem*.

As you can imagine, solving inverse problems of isomorphic measurements, when one is concerned with reconstruction of the signal-of-interest, tend to be straightforward. In the weighing problem, the measurement is also the reconstruction. In the slit spectrometer, where the forward model can be simply the continuous to discrete mapping of the spectrum. The spectrum is the interpolated measurement.

Of course, one can begin to add levels of complexity to the forward model to

account for various physical aspects of the sensor, such as the fact the FPA cannot measure certain wavelength regions or the noise in our measurements. But again, assuming proper sampling and enough SNR, the reconstruction of the isomorphic signal is the measurement. This simplicity is one reason why isomorphic sensing still dominates at the consumer level despite all of the drawbacks I discussed earlier in section 1.1.

However, the multiplexing of signal information forces one to develop computational steps to solving the inverse problem. In the multiplexed weighing problem, a significant complication occurs when each sheet of paper has a different weight. Now solving the inverse problem is not as straightforward. In algebra, given only 1 equation and 100 unknowns, the problem is underdetermined. Similarly given a 1 measurement of all 100 sheets is also an underdetermined problem. What one can do is try measuring different combinations of the 100 sheets, each new combination provides a new equation to work with reducing the error. Naively, one might assume that randomly choosing 100 unique combinations and solve 100 equations using algebra. This works fine when there is no measurement error. However, in the presence of noise, in many applications including the weighing problem, random combinations are not the best way to conduct the coding. They are sub-optimal in terms of reconstruction error. This lead many to begin working on optimal coding strategies of signals for sensing and is major topic in this dissertation.

In summary, the forward model of a sensor is essentially accounting for the physics which govern the measurement. While the solving the inverse problem is a mathematical problem which attempts to either reconstruct the object or to calculate task-specific data from the measurement data. Unfortunately, not all multiplexing forward models codes have mathematically elegant inversion steps. Often the physics of the situation force non-isomorphic measurements which require a computational step to solve the inverse problem.

#### 1.4 Indirect Imaging

While Golay, Fennimore, and others were leveraging multiplexing to eliminate trade-offs in traditional sensors, an entirely disparate group of researchers were working on imaging techniques for which there was no isomorphic analog. In these cases the physics of the sensing modality prevents a point-by-point sampling of the signal-of-interest. Indirect imaging refers to sensing schemes which include X-

ray Computed Tomography (CT), Single-Photon Emission Computed Tomography (SPECT), Positron Emission Tomography (PET), MRI and certain forms of sonic and radio wave imaging. All require a data-processing or reconstruction step to solve an inverse problem [16].

Perhaps one of the most successful early examples of indirect imaging which led to the rise of inverse problems in sensing is the development of radar. While early radar was concerned with the detection and distance of an object, development of imaging radar began after World War II. Imaging radar and specifically Synthetic Aperture Radar (SAR) can use time delay information combined with the Doppler effect and interference of coherent radio waves to create high resolution images of terrain and buildings.

In medicine, a common imaging modality is X-Ray CT. In X-Ray CT, computational inversion is required to reconstruct a 2 or 3-dimensional function from 1 or 2-dimensional measurement data. The forward model can be simple: In a collimated beam architecture with a 1-dimensional detector array, each sample from each pixel on the array is proportional to the total number of x-ray photons that have not been absorbed by the object [17]. The inversion relies on computing the inverse Radon transform [18].

Indirect imaging is a subfield of computational sensing. Due to the medical and military applications of these computational sensors, there has been an intense push to reduce measurement time and improve task-specific and reconstruction results. Many of the techniques from other subfields of computational sensing have been brought to bear for indirect imaging [19, 20].

I have discussed the development of multiplex sensing and indirect imaging and how the ideas from both subfields are analogous in terms of producing a non-isomorphic measurement. However a major step in practical implementation of computational sensing is being able to obtain the measurements in a quick, reliable and efficient manner. Computational sensing as a field would not exist without the most important invention in optics and photonics of the 20th century, the digital image sensor<sup>2</sup>.

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<sup>2</sup> staring array, staring-plane array, focal-plane array (FPA), focal-plane, and image sensor are all synonymous

## 1.5 The Digital Imaging Revolution

The invention of the Charge-Coupled Device (CCD) FPA by Boyle and Smith in 1969 was a major breakthrough for entire fields and industries who depended on the reliable sampling, storage and transmission of optical signals [21]. The CCD is the first integrated circuit device that could reliably convert an optical image to a digital signal. Until then one either had to use film or bulky tubes that required an electron beam to be scanned across an image scene, such as the Image orthicon [22].

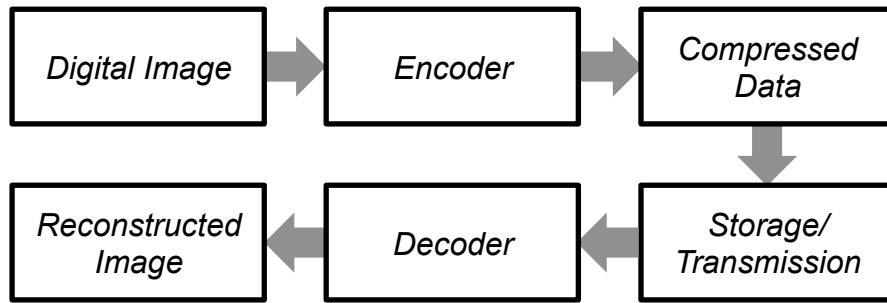
The invention of the digital camera by Sasson followed shortly after [23]. Several years later the first digital spectrometer was invented. In the digital spectrometer the exit slit of the monochromator was replaced by the CCD, which allowed for instant and simultaneous measurement of the entire spectrum in a compact architecture [24].

The development of the Complementary Metal–Oxide–Semiconductor (CMOS) FPA was also important. While in scientific settings, it could not rival the quality of the CCD, its cheaper cost brought digital imaging to the consumer level. Other technology like the digital computer and computer networking also provided major contributions to the democratization of imaging and optical sensing. While scientific grade optical instrumentation was and is still expensive, the researcher could at least capture, process, and share measurement data with significantly less effort. Without it, the field of computational sensing would not exist.

Algorithms for efficient and reliable storage and transmission of digital images became more important. Over time the pixel count continued to increase and the sheer volume of digital image and video data being generated and transmitted over networks began to outpace improvements in storage and transmission capacity. While many engineers developed new technology to combat the hardware limitations of storage and transmission. This also led to a renewed effort by researchers to develop more efficient image and video compression algorithms [25, 26].

Compression techniques all follow the same basic process, see Figure 1.5. Once the CCD samples the optical signal and produces the measurement data, the encoder uses the compression algorithm to look for redundancies in the data and produce a compact representation of the signal-of-interest. The compressed data can then either be stored or transmitted or both. The decoder solves the inverse problem of reconstructing the image.

In the next section I will discuss how many of the techniques and algorithms used



**Figure 1.5:** A general flowchart for image and data compression techniques. The digital image is analyzed by the encoder and compressed into a compressed form where it can be efficiently stored or transmitted. The decoder takes the compressed image and converts it back into an image that resembles the original digital image.

in computational sensing are inspired by the techniques used by the image processing and digital communications community. This is because one of the major efforts of computational sensing is to make resource efficient measurements to reduce the total amount of measurements, whereas in image processing and communications, measurement data is often corrupted, missing, or too large for efficient storage and transmission.

## 1.6 Compressive Sensing

Traditionally, in order to increase the resolution of a sensor, one had to increase the number of measurements. This means that the SWAP-C must also increase. A camera with just a few megapixels FPA costs less than one with hundreds of megapixels. The cost of designing the optics will also need to scale to provide enough optical resolution. In a perfect world, one could capture all the information one needs from just a few measurements.

With a discrete signal one needs at least as many measurements as there are signal elements to solve the inverse problem. If the number of measurements is fewer, then the inverse problem is underdetermined. Conventional signal processing dictates that accurate reconstruction of the signal-of-interest is highly improbable. Fortunately, a signal acquisition technique called *compressive sensing* allows one to design sensors that solve these types of highly underdetermined inverse problems.

As discussed earlier, much of the data being generated by sensors are redundant. Images, spectra, video, and audio data of real-world signals tend to exhibit patterns or redundancies that can be exploited. This allows a compression algorithm to significantly reduce the amount of data needed to represent the signal.

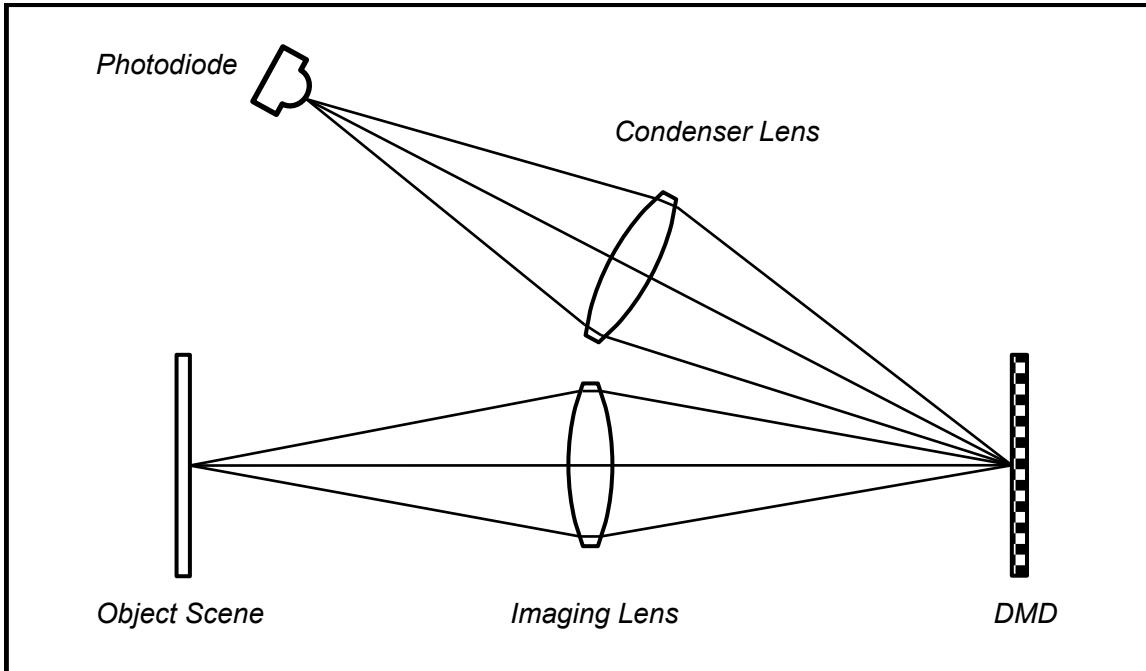
There is a class of compression algorithms called lossy [27]. In lossy compression, not only are redundancies exploited but data that is deemed insignificant to the signal quality is discarded. Only the most important part of the signal is kept as part of the compressed representation of the original signal. When the signal is uncompressed, the amount of data is less than the original measured data. The difference in quality is often unnoticeable to a human observer. In both lossless and lossy compression, the goal is to obtain a *sparse* representation of the signal. A sparse representation means that the signal can be well approximated with only a few non-zero elements in a representation basis. A representation basis is a basis in which the signal-of-interest is sparse. For example, most natural images are sparse in the Fourier basis. The representation basis is typically not the native basis of the signal-of-interest, i.e. pixel number or spectral channel.

Researchers pointed out that traditional sensors tend to produce vast amounts of measurement data, but often the majority of data is redundant and discarded in the compression step [28, 29, 30]. This led to the idea that sensors can be designed to directly measure the most relavent data in a signal, suggesting a measurement scheme that can measure a compressed form of the signal. This is the idea behind compressive sensing sometimes known as *compressive sampling*. If the measurements are compressive then it should be possible to significantly reduce the number of measurements to accurately reconstruct the signal.

Note that there is a distinction between compressive sensing and the traditional approach of sensing and then compressing. In the traditional approach, compression algorithms operate as a post-processing step. Therefore, a traditional compression algorithm will have access to the entire signal to look for redundancies and convert it into a sparse representation. In compressive sensing, one attempts the compression directly and therefore do not have access to the entire uncompressed signal. The algorithms must assume that the signal has a sparse representation.

The question of how to actually measure or code the analog signal to directly obtain compressed data is also important. Fortunately, random coding tends to work well in many instances when the signal has a sparse representation. However in many cases, designed codes can significantly outperform random coding. I will discuss other types of coding schemes that can be used to outperform random codes.

The idea of compressive sensing seems to be similar to the concept of multiplex sensing. However, there is an important distinction to be made. In compressive sensing, the aim is to obtain the relavent information in as few measurements as



**Figure 1.6:** A single pixel camera architecture. The object scene (or intermediate image) is imaged onto a DMD. Each micro-mirror of DMD reflects light towards the photodiode or to another direction. This acts as a point-by-point multiplication of the discrete image with the DMD pattern. The condenser lens sums any light reflected by the DMD and focuses it onto the photodiode. This can be described mathematically as a vector multiplication of the image with the DMD pattern.

possible. In multiplexing, the goal is to overcome limitations mainly due to lack of SNR. Many compressive sensing schemes also employ multiplexing.

One useful example of compressive sensing versus traditional sensing is the single pixel camera [10]. The single pixel camera is a multiplexing camera architecture that uses time sequential random measurements and recovers the image in significantly fewer measurements (equal to number of exposures  $\times$  pixels) than the conventional camera, see Figure 1.6. Another example is the Coded Aperture Snapshot Spectral Imaging (CASSI) architecture [31], which can reconstruct a spectral data cube in significantly fewer FPA exposures than a traditional spectral imaging architecture.

Another important distinction is between reconstruction and task-specific sensing. Task-specific sensing tends to refer to measurement techniques that attempt to directly perform tasks such as detection, classification, and estimation without the intermediate step of reconstructing the high-dimensional signal. Compressive sensing is useful not just of overcoming resolution limitations in reconstruction but for task-specific sensing. For example, in facial recognition the goal is detection of an individual person. Reconstruction of the face image is simply an intermediate step, therefore, one can develop a compressive sensing scheme that is optimal for

direct facial detection, skipping the step of image reconstruction [32].

Computational sensors can overcome classic engineering trade-offs in sensor design. However, there is a unique set of challenges related to computational sensing.

### 1.7 Practical Considerations in Computational Sensing

So far I have discussed the development of computational sensing techniques and how they are used to ameliorate trade-offs in traditional sensor design. Computational sensing as a field is continuing to grow at a rapid pace. The number of journal publications related to computational sensing has steadily increased every year since 2008 [33]. There is now a major Optical Society of America (OSA) meeting dedicated to computational sensing [34] and textbooks dedicated to its study and development [1, 35]. While it is a powerful approach to radically new sensor architectures, textbooks and papers tend to focus on architecture concepts and positive results. Little attention is given towards the practical issues one faces when implementing computational sensors. For example, calibration is a major topic in this dissertation. In many talks and papers on computational sensing, calibration is barely mentioned or relegated to a minor paragraph.

Calibration is the process of quantifying the response of a sensor in order to produce an accurate forward model. While many traditional sensors also require calibration, computational sensors tend to be more sensitive to calibration error.

There are two main reasons for this. The first reason is simply due to the fact that non-isomorphic measurements require a computational step to solve an inverse problem. The algorithms rely on accurate knowledge of the forward model to separate measurement data due to the instrument and data due to the signal-of-interest.

The second reason is due to the lack of redundancy of measurement data in compressive sensing. The redundancies that are typically deemed wasteful in traditional sensing, can also be used by post-processing algorithms to solve the inverse problem in a robust fashion to correct for missing or corrupted data [36]. In compressive sensing, only a few numbers are used to represent many. If the few numbers are misinterpreted due to poor calibration, it can have a drastic impact on the performance of the estimation algorithm. I will illustrate in this dissertation the calibration challenges in several computational sensors.

Calibration has become a major drawback in compressive sensing. A consumer

cannot be expected to spend time calibrating every time the instrument is physically bumped, the air temperature or pressure changes. In high dimensional compressive sensors like hyperspectral imagers, the calibration time can last hours.

Another issue facing sensors that rely on multiplexing is lack of dynamic range. In the context of optics, if more photons are being combined onto a single detector pixel, there is a higher chance of saturating the detector or operating in a non-linear regime. This is one of the potential issues faced by single-pixel compressive sensing architectures. The SCOUT architecture attempts to alleviate this by “spreading” the photons onto more pixels for a compressive measurement.

Another hurdle in the implementation of practical computational sensing is the need for prior knowledge. For example, in *compressive imaging* one must assume the signal is sparse in some basis. Fortunately most realistic objects can be treated as such with many commonly known bases, such as a wavelet basis. However, sometimes one needs to image something that is difficult to represent in any known basis. One needs to resort to generating training data. Training requires one to generate many different examples of the signal. This becomes time and computationally expensive. Another example for the need of prior knowledge is the AFSSI-C, a computational spectral classifier which requires knowledge of the standard deviation of the probability density function of the noise to perform spectral classification in the least number of measurements as possible.

Reducing the number of detector elements is often the goal in computational sensing. A notable example is the single pixel camera is an architecture. However, the single pixel camera requires several time sequential measurements. Each measurement displays a different DMD pattern to create a randomly encoded measurements [10]. The drawback to this architecture is that one must point the camera at the object scene until enough measurements have been collected for proper reconstruction. A complication arises when this architecture is used to image temporally varying object scenes. One must display the DMD patterns even faster and reduce the exposure time to keep up. As a result the SNR may begin to degrade.

A possible way to mitigate this issue is to do all the encoding in parallel. However, a completely parallel approach would require a lens, a DMD (or coded aperture), and a detector pixel for each measurement. Since each lens uses a different entrance pupil, this means that each detector pixel will have a different view of the object scene. This drastically scales the complexity of the architecture and algorithms. In this dissertation, I will discuss a compromise to parallel coding, in two different

computational sensors, by using a common entrance pupil and a CCD.

Much of the optimal measurement codes are simultaneously positive and negative measurement weights. In reality, with incoherent light one is unable to make negative measurements. One is often forced into situations where one must record two sets of measurements and subtract one set of measurements from the positive set of measurements. This means an additional noise term is added to each effective measurement.

Algorithms engineered to solve the inverse problems often do not account for the non-negativity of many physical situations. For example, in spectral unmixing where the problem is to solve for the concentration of each material given a mixed spectrum. A non-negative fractional abundance that sums to one is a physical requirement. However, there is a lack of sparsity promoting algorithms that are able to enforce both the non-negativity and the sum to one constraint.

A major issue in both the theoretical and experimental compressive sensing community is a lack of code design schemes. For the most part random measurements techniques are dominant because they obey well known theoretical results which guarantee reconstruction with high probability [30, 37, 38]. However, designed codes have been shown to outperform random codes in various applications. Intuitively, designed codes which can take into account prior knowledge of the physical limitations of the sensing task and additional statistical assumptions of the signal-of-interest should be able to outperform random measurements. For example, I will show in the AFSSI-C, I will demonstrate that adaptively designed Principal Component Analysis (PCA) codes dramatically outperform random codes in low SNR environments.

These issues and others will be discussed in a case study manner throughout this dissertation. I will now discuss the organization of this dissertation and the three separate computational sensors I have built and how I have tried to mitigate and resolve some of the practical issues associated with computational sensing.

## 1.8 Dissertation Overview

I used this chapter to cover the major concepts of computational sensing. More importantly, I provided the major topic of discussion for this dissertation, the challenges that remain towards developing practical computational sensors. I will use the next chapter as an opportunity to provide a more detailed and mathematically

rigorous look at the various coding schemes that are popular in computational sensing, as well as the ones I have used. This includes a discussion of the mathematical methods that I and my collaborators developed and deployed in the AFSSI-C: Bayes rule, Log-Likelihood Ratios, and the Maximum a Posteriori decision technique. A more rigorous treatment of compressive sensing will also be provided which includes several important results from the compressive sensing community. I will also discuss several estimation and task-specific sensing algorithms that I used during the development of the three computational sensors in my work.

Chapter 3 will introduce a new system architecture for compressive target tracking—the Static Computational Optical Undersampled Tracker (SCOUT). This system is designed to overcome a variety of challenges that typically arise in traditional optical sensing approaches. It provides several advantages over the single-pixel camera architecture, notably it can capture many simultaneous encodings of the field-of-view with a single camera exposure. I will present experimental results that validate the performance of the proposed architecture.

Chapter 4 will discuss an important experimental prototype which demonstrates adaptive spectral image classification. The system is a major experimental advancement compared to current computational spectral imaging architectures which focus on reconstruction. Furthermore, the ability to perform adaptive measurements, where each code is designed based on the history of prior measurement data allows this instrument to outperform traditional spectral imaging architectures by a factor of 100 in low SNR scenarios.

Chapter 5 will discuss current efforts to experimentally demonstrate compressive spectral unmixing. Often in spectral imaging, the spectra present in the field-of-view of each pixel is actually a mixture of several spectra, a mixed spectrum. Spectral unmixing is the task of inferring the fraction of each constituent spectrum in the mixed spectrum. I employ a unique architecture for computational spectral sensing which uses no diffraction gratings or refracting prisms but relies on the wavelength dependent nature of the birefringence in an Liquid Crystal on Silicon (LCOS). I will demonstrate the effectiveness of various compressive sensing measurement schemes to outperform a traditional sensor in significantly fewer measurements.

Chapter 6 will summarize the dissertation and provide my perspective on how the field should approach the issues in practical computational optical sensing.

## Chapter 2

### Formalism

I will use this chapter to cover several important mathematical concepts which are required for the reader to understand the advantages and disadvantages of computational sensing. I will first discuss the advantages that Hadamard and S-Matrix multiplexing provide compared to the isomorphic sensor to create a context for the discussion of the Fellgett advantage. Then I will discuss Principal Component Analysis (PCA), a technique for finding useful discriminating features from seemingly complicated data. I will also cover the fundamentals of Bayesian statistics and how it can be used to update one's belief in a hypothesis given new data. Then I will cover important topics in compressive sensing: sparsity, incoherence, and the restricted isometry property (RIP) and discuss an optimization problem that allows one to reconstruct sparse signals from compressively sampled data.

To simplify the math and notation, I shall try to work with discrete representations of signals when possible. Any discrete linear process can be written as a matrix multiplication

$$\mathbf{g} = \mathbf{H}\mathbf{f} + \mathbf{e} \quad (2.1)$$

where  $\mathbf{g}$  is a vector of measurement data and  $\mathbf{f}$  is a discrete representation of the object signal-of-interest and  $\mathbf{H}$  is the matrix which describes the measurement process and  $\mathbf{e}$  is additive noise. For brevity I will refer to  $\mathbf{f}$  as the object and  $\mathbf{H}$  as either the sensing matrix or the measurement matrix. Equation (2.1) represents the forward model in a wide variety of computational sensors. The object  $\mathbf{f}$  is a vector in  $N$  dimensional vector space and the measurement  $\mathbf{g}$  is a vector in  $N_m$  dimensional vector space. In general  $N_m \neq N$ .

Equation (2.1) is an extremely useful way to represent optical phenomena, since it allows one to take advantage of many attractive numerical techniques which are dedicated to linear systems. For the most part, classical optics—the ray and wave nature of light—can be approximated as linear. The solutions to the paraxial wave equation are linear in free space and in most glasses. Similarly, paraxial optics can be modeled using a sequence of matrix multiplications. While just an approximation, tracing the paraxial Chief and Marginal ray is enough to calculate the third-order

Seidel aberrations.

## 2.1 Isomorphic Sensing

In an isomorphic measurement, where the goal is a one-to-one mapping of object points to measurement points, the measurement matrix is represented with the identity matrix

$$\mathbf{H} = \mathbf{I} \quad (2.2)$$

One can get an idea of how much error exists in an isomorphic measurement by invoking the weighing example [39]. Say there are 4 objects with true unknown weights  $f_1, f_2, f_3, f_4$ . The measured weights are  $g_1, g_2, g_3, g_4$  with additive noise  $e_1, e_2, e_3, e_4$ .

$$\begin{bmatrix} g_1 \\ g_2 \\ g_3 \\ g_4 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} f_1 \\ f_2 \\ f_3 \\ f_4 \end{bmatrix} + \begin{bmatrix} e_1 \\ e_2 \\ e_3 \\ e_4 \end{bmatrix} \quad (2.3)$$

Since this is isomorphic sensing, the estimated weights  $\hat{\mathbf{f}}$  are the measurements  $\mathbf{g}$

$$\hat{\mathbf{f}} = \mathbf{g}. \quad (2.4)$$

Where the error between the estimated weights and the actual weights is  $\epsilon = \hat{\mathbf{f}} - \mathbf{f}$ . For simplicity, I assume a zero mean distribution for the noise. Therefore, the isomorphic measurements are unbiased.<sup>1</sup> For an unbiased estimator, the Mean Squared Error (MSE) of the estimated weights is the variance

$$E[\epsilon^2] = E[(\hat{\mathbf{f}} - \mathbf{f})^2] = \sigma^2. \quad (2.5)$$

This puts a lower bound on the MSE for an isomorphic measurement.

## 2.2 Multiplexing

As I discussed in Chapter 1, multiplexing is a technique for overcoming SNR related trade-offs in isomorphic sensing. In a multiplexed measurement, each element in the measurement vector  $\mathbf{g}$  is a weighted linear combination of the elements in the object vector. Therefore the measurement matrix  $\mathbf{H}$  is no longer an identity matrix.

---

<sup>1</sup>Unbiased means that on average the estimator will produce the ground truth

### 2.2.1 Coding Schemes

A Hadamard matrix of order  $N$  is defined as a matrix  $\mathbf{H}_N$  as the  $N \times N$  matrix whose elements consist of +1's and -1's and satisfies the following property:

$$\mathbf{H}_N^T \mathbf{H}_N = \mathbf{H}_N \mathbf{H}_N^T = N \mathbf{I}_N \quad (2.6)$$

where  $\mathbf{I}_N$  is an  $N \times N$  identity matrix.

In computational spectroscopy and imaging, Hadamard codes are extremely popular. Hadamard codes are provably optimal in the case where one is allowed to take a full set of measurements, meaning that  $\mathbf{f}$  and  $\mathbf{g}$  from Equation (2.1) are both vectors in  $N$  dimensional space [39].

A Hadamard multiplexed measurement is written as

$$\begin{bmatrix} g_1 \\ g_2 \\ g_3 \\ g_4 \end{bmatrix} = \begin{bmatrix} +1 + 1 + 1 + 1 \\ +1 - 1 + 1 + 1 \\ +1 - 1 - 1 + 1 \\ +1 - 1 - 1 + 1 \end{bmatrix} \begin{bmatrix} f_1 \\ f_2 \\ f_3 \\ f_4 \end{bmatrix} \quad (2.7)$$

In the weighing example, negative measurements are realized by using a balancing scale instead of a spring scale. This means that in the first measurement all 4 items are placed in the same pan. In the second measurement items 1 and 3 are in the same pan while items 2 and 4 are in the opposite pan, and so on [39]. With four equations and four unknowns, one can solve for the estimates using basic algebra.

The MSE of the  $m^{th}$  measurement

$$E[(\hat{f}_m - f_m)^2] = \frac{1}{4}\sigma^2. \quad (2.8)$$

which is 4 times lower than using an isomorphic measurement scheme. In general, the MSE of a Hadamard measurement is

$$\text{MSE} = \frac{\sigma^2}{N} \quad (2.9)$$

where  $N$  is the dimension of the object vector  $\mathbf{f}$ , which is equal to the number of measurements  $N_m$ . Hotelling proved in 1944 that for a measurement matrix with elements  $h_{mn} \in \{-1, +1\}$ , the lowest possible MSE for the case of a full set of measurements with a linear unbiased estimator is  $\text{MSE} = \frac{\sigma^2}{N}$  [1]. Therefore, one cannot possibly do better than Hadamard coding in this case.

In many practical cases in computational sensing, making a code with simultaneous positive and negative modulation of the signal is not possible. While this

may be possible using incoherent light where a phase delay maybe used to produce a negative electric field. For incoherent light, the system response is linear in intensity [40].

In the case where one has the ability to make a full set of measurements but is limited to elements of +1's and 0's, an S-Matrix code minimizes the MSE [39]. In the weighing example, a spring balance rather than a two pan scale analogous to this situation.

$$\begin{bmatrix} g_1 \\ g_2 \\ g_3 \\ g_4 \end{bmatrix} = \begin{bmatrix} 0 & +1 & +1 & +1 \\ +1 & +1 & 0 & 0 \\ +1 & 0 & +1 & 0 \\ +1 & 0 & 0 & +1 \end{bmatrix} \begin{bmatrix} f_1 \\ f_2 \\ f_3 \\ f_4 \end{bmatrix} \quad (2.10)$$

So items 2, 3, and 4 are weighed together, then 1 and 2, and so on. Solving the system of equations in a silimar fashion as before in the Hadamard weighing example we find that the mean square error for the  $m^{th}$  measurement when weighing 4 items is

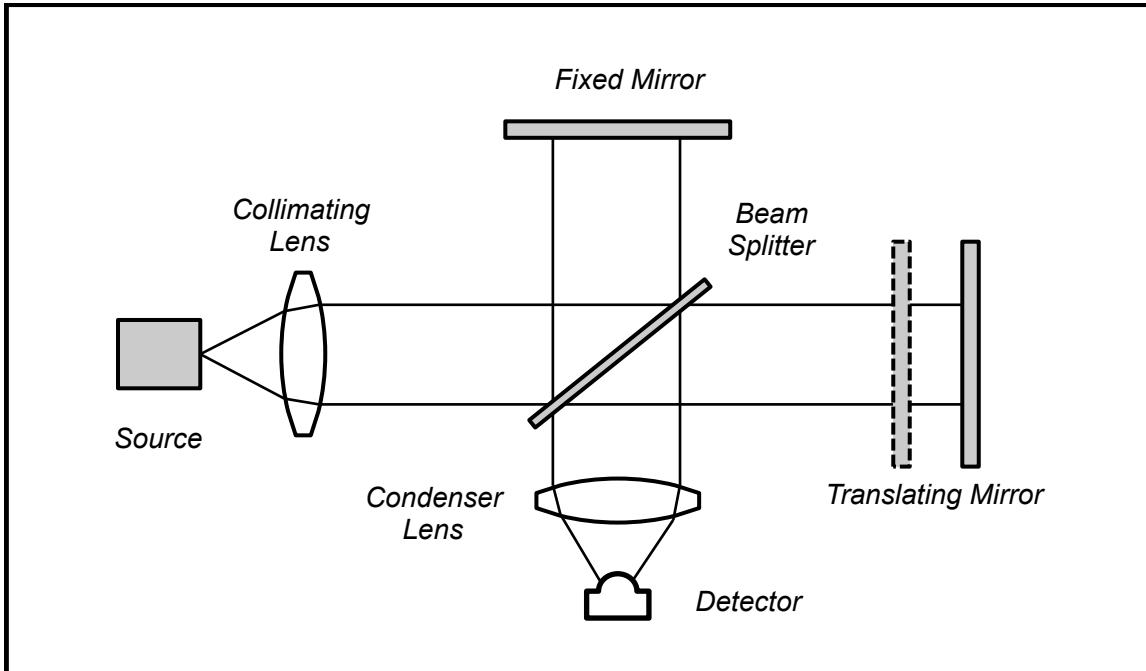
$$\text{MSE} = E[(\hat{f}_m - f_m)^2] = \frac{7}{9}\sigma^2. \quad (2.11)$$

Which reduced the MSE compared to the isomorphic measurement scheme but has higher MSE compared to the Hadamard measurement scheme. The MSE of the S-Matrix is approximately a factor of 4 increase compared to the Hadamard matrix coding scheme.

In the case when the full set of measurements are available ( $N_m = N$ ), I have just shown that Hadamard codes are optimal. It would seem as if random coding would have no use if one is able to utilize Hadamard codes. However, they should not be ignored because in compressive sensing, certain theoretical guarantees exist for random coding that do not exist for Hadamard and S-Matrix codes. Sometimes, the physics of the situation forces a random coding scheme.

### 2.2.2 The Fellgett Advantage

The *Fellgett advantage* is the improvement in SNR that occurs when an instrument takes multiplexed measurements compared to isomorphic measurements [41, 42]. Physically the Fellgett advantage occurs because a single detector element produces a noise contribution whether it is sampling a single part of the signal or multiple parts of the signal. Maximizing the signal-to-noise ratio (SNR) of the estimated object signal-of-interest for a given system throughput and detector noise is major design consideration in computational optical sensing particularly in the area



**Figure 2.1:** The architecture of the Fourier Transform Spectrometer resembles the Michelson interferometer. One of the mirrors is translated back and forth. The interferogram is the detected intensity versus mirror delay which is related to the autocorrelation of signal. The Fourier transform of the autocorrelation provides the spectrum.

of spectroscopy. There are two notable ways to accomplish multiplexing in spectroscopy: Hadamard multiplexing in dispersive spectrometers and interferometric based multiplexing such as the Fourier Transform Spectrometer (FTS).

The FTS architecture is similar to the Michelson interferometer, see Figure 2.1. The FTS operates by taking the autocorrelation of the complex electric field as a function of time delay by moving one of the mirrors in the interferometer [42]. The Wiener-Khinchin theorem says that for a wide-sense stationary random process, the Fourier transform of the autocorrelation is the power spectral density [43]. Thus a computational post-processing step is required to reconstruct the spectrum from the measured autocorrelation data. Since the FTS measures combinations of multiple wavelengths at each detector readout, it also exhibits the Fellgett advantage. It turns out that in a FTS the MSE obtained is a factor of two greater than the Hadamard multiplexing spectrometer [44].

$$\text{MSE} = 2 \frac{\sigma^2}{N_\lambda} \quad (2.12)$$

where  $N_\lambda$  is the number of spectral channels.

### 2.3 Principal Component Analysis

Principal component analysis (PCA) is a technique that attempts to recast a dataset in manner that finds correlations in data that may not be evident in their native basis and creates a set of basis vectors in which the data has a low dimensional points al representation. PCA works by producing a set of vectors that point along the direction of maximum variance while being simultaneously orthogonal to each other. These are called the *principal components*. The first principal component vector is parallel to the direction of maximum variance. The second principal component points in the direction that also maximizes variance but is orthogonal to the first principal component. The third principal component is orthogonal to the first and second principal components and points in the direction that maximizes the variance given those constraints. And so on.

Imagine one has a dataset  $\mathbf{S}$  which consists of  $N$  spectra with  $N_\lambda$  spectral channels. Instead of looking at the data as just intensity versus spectral channel, PCA attempts to construct a set of new vectors (also called features) that show as much variation in the spectra as possible. In other words, first direction (principal component) is used to recast the data to look as different (uncorrelated) as possible. This allows us to discriminate the data, as best we can with just one direction. The second principal component is the direction that provides the second most ability to discriminate the data, and so on.

Now I will discuss some of the math behind PCA. The covariance matrix is defined as

$$\mathbf{C}_\mathbf{S} = \frac{1}{N} \mathbf{S} \mathbf{S}^T. \quad (2.13)$$

Each element in the covariance matrix  $C_{smn}$  is the covariance of the  $m^{th}$  spectrum  $\mathbf{s}_m$  and the  $n^{th}$  spectrum  $\mathbf{s}_n$ .

$$C_{smn} = \frac{1}{N} \mathbf{s}_m \mathbf{s}_n^T. \quad (2.14)$$

A large covariance means they look alike and therefore are difficult to disambiguate. Geometrically, it means that  $\mathbf{s}_m$  and  $\mathbf{s}_n$  tend to point in the same direction (assuming their length is approximately the same). If the entire collection of spectra  $\mathbf{S}$  were mutually orthogonal, being able to tell one spectrum apart from another would be easy. You would just have a collection of spikes at different spectral channels. The covariance matrix in this case would be a diagonal matrix. Therefore, it is desirable to have covariance matrices that are diagonal matrices since they indicate low correlation between the datasets and improves one's ability to distinguish between the

data.

Since there is typically some redundancy between spectra, the off-diagonal elements of the covariance matrix will be non-zero. PCA allows one to recast the data to make it as uncorrelated as possible in a new basis.

$$\mathbf{Y} = \mathbf{PS} \quad (2.15)$$

where  $\mathbf{Y}$  is the data projected onto the principal component basis  $\mathbf{P}$ . The *rows* of matrix  $\mathbf{P}$  are the principal components. The covariance of the projected data

$$\mathbf{C}_\mathbf{Y} = \frac{1}{N} \mathbf{Y} \mathbf{Y}^T \quad (2.16)$$

is a now diagonal matrix. Indeed, the principal components are the optimal way to discriminate the spectra in the dataset [45]. It turns out the principal components are the *eigenvectors of the covariance matrix  $\mathbf{C}_S$  are the principal components* [46].

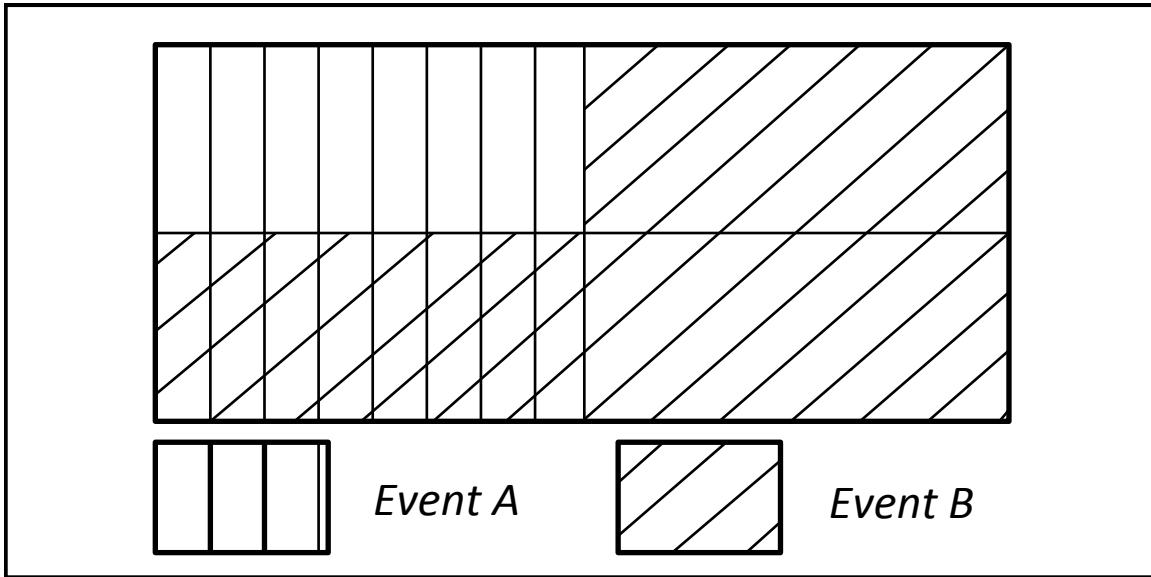
Since the full set of principal components forms a basis, each spectra  $\mathbf{s}$  in  $\mathbf{S}$  can be written as a superposition of principal components without any error

$$\mathbf{s} = \sum_{n=1}^{N_\lambda} \gamma_n \mathbf{p}_\lambda \quad (2.17)$$

Where  $\gamma_n$  is the  $n^{th}$  eigenvalue associated with eigenvector  $\mathbf{p}_n$ . In many cases, only a few of the first principal components are needed in the summation to approximate the original data well,  $M \ll N_\lambda$ . Note that each eigenvector has an associated eigenvalue. The eigenvalues are also informative because the relative magnitude of the eigenvalue can tell us how many principal components are really needed to discriminate all of the spectra [47]. The magnitude of the eigenvalue  $\gamma_n$  tells us how well useful the associated eigenvector is at discriminating the data.

This is another reason why PCA is so useful. It can be used as a way to perform dimensionality reduction. In other words, seemingly complicated data can be summarized by only for few principal components by exploiting the correlations between the data. This concept is analogous to lossy compression in signal processing. Simply project the data onto the first several principal components associated with the largest  $M$  eigenvalues. The data now has an approximately sparse representation.

In will show in Chapter 4, that the AFSSI-C relies on a variation of Principal Component Analysis (PCA) for discriminating between spectra. In addition to PCA, the AFSSI-C uses a Bayesian technique to create adaptive codes. I will now discuss some of fundamentals of Bayesian statistics.



**Figure 2.2:** Graphical demonstration of joint probability. The probability of event  $A$  is  $P(A) = 3/4$ . The probability of event  $B$  is  $P(B) = 3/4$ . The joint probability of events  $A$  and  $B$  is  $P(A \cap B) = 1/4$ . The probability of event  $A$  occurring given that event  $B$  has occurred is  $P(A|B) = 1/3$ . This is consistent with the equation  $P(A \cap B) = P(A|B)P(B)$

## 2.4 Bayesian Statistics

A hypothesis is nothing more than a claim or premise that one is interested in verifying. In imaging and spectroscopy, one example is that at a certain location in the field of view, the hypothesis is that a spectrum is present. Another hypothesis is that the mean value of the signal is some value. Often times one is interested in estimating parameters of stochastic processes, which we denote  $\theta$ .

Bayesian statistics allows one to treat the hypothesis or parameters as random variables rather than deterministic constants. At the heart of Bayesian approaches is Bayes' theorem, which is a way of computing probabilities of a hypothesis given some evidence which are related to the hypothesis. For example, Bayes' theorem can be used to decide which of two bags of candy has been opened or if a spectrum is present. The idea is that one can make a more informed calculation of probability if one is able to update the probability given some new piece of evidence that one may have not had at the beginning.

The derivation of Bayes' theorem follows from the definition of conditional probability. The conditional probability of event  $A$  occurring given that  $B$  occurred is:

$$P(A|B) = \frac{P(A \cap B)}{P(B)} \quad (2.18)$$

this can be seen graphically in Figure 2.2. Solving for the joint probability  $P(A \cap B)$  gives

$$P(A \cap B) = P(A | B) P(B) \quad (2.19)$$

since the joint probability commutes  $P(A \cap B) = P(B \cap A)$ , we can also write

$$P(A \cap B) = P(B | A) P(A) \quad (2.20)$$

equating the right hand sides of Equation 2.19 and Equation 2.20 gives use Bayes' theorem (also called Bayes' rule)

$$P(A | B) = \frac{P(A) P(B | A)}{P(B)} \quad (2.21)$$

One interpretation of Bayes' theorem is called the Diachronic interpretation, which says that conditional probability of the hypothesis or parameter given knowledge of some evidence or measurement data is given by

$$P(\theta | g) = \frac{P(\theta) P(g | \theta)}{P(g)} \quad (2.22)$$

The term  $P(\theta | g)$  is called the *posterior*. It represents the belief in the hypothesis given the data. The term  $P(\theta)$  is called the *prior*.  $P(g | \theta)$  is called the *likelihood*.  $P(\theta)$  is called the normalizing constant, which computed to ensure that the posterior probabilities sum to 1. The normalizing constant can be written as

$$P(\theta) = \sum_i P(\theta_i) P(g_i | \theta_i) \quad (2.23)$$

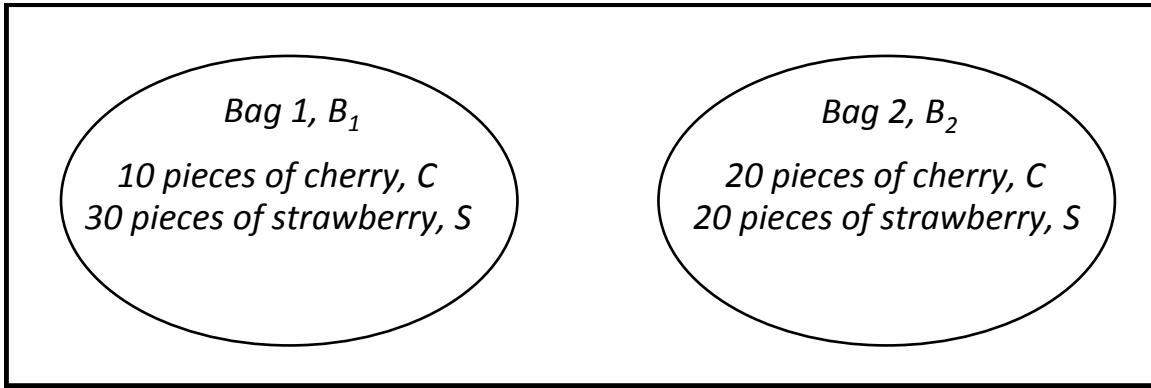
One can repeatedly apply Bayes' theorem given new measurement data.

#### 2.4.1 Example: Updating Probabilities with Bayes' Theorem

I will use a simple example to illustrate how to update probabilities using Bayes' theorem, see Figure 2.3. Imagine I have two bags of candy, Bag 1, which I denote  $B_1$ , and Bag 2, which I denote  $B_2$ . Bag 1 has 10 pieces of cherry flavored candy, denoted as  $C$ , and has 30 pieces of strawberry flavored candy, denoted as  $S$ . Bag 2,  $B_2$ , has 20 pieces of cherry candy and 20 pieces of strawberry candy. At the beginning, the prior probability of selecting bag 1 or bag 2 is both equal

$$P(B_1) = P(B_2) = \frac{1}{2} \quad (2.24)$$

Someone then picks a bag at random and takes out a piece of candy that turns out to be strawberry flavor. They do not state which bag was selected, only that the



**Figure 2.3:** Two bags are present:  $B_1$  and  $B_2$ . The probability of choosing either bag is  $P(B_1) = P(B_2) = 1/2$ . Bag 1 has 40 pieces of candy: 10 pieces of cherry candy so  $P(C|B_1) = 1/4$  and 30 pieces of strawberry so  $P(S|B_1) = 3/4$ . Bag 2 has 40 pieces of candy: 20 pieces of cherry candy so  $P(C|B_2) = 2/4$  and 20 pieces of strawberry so  $P(S|B_2) = 2/4$ . If someone selects one of the bags at random then selects a piece of candy from that bag. If the candy is identified but the bag is not, then one can use Bayes' theorem to update the probability of either bag being selected.

candy they randomly selected from the bag was strawberry. What is the probability that bag 1 was the one selected given that I know the candy is strawberry? I can use Bayes' theorem to compute this

$$P(B_1 | S) = \frac{P(B_1) P(S | B_1)}{P(S)} \quad (2.25)$$

$P(S | B_1)$  is the probability of selecting strawberry given that they pick bag 1, which is  $3/4$ .  $P(S)$  is the probability of selecting a strawberry candy from either bag 1 or bag 2, which  $5/8$ . Thus

$$P(B_1 | S) = \frac{\left(\frac{1}{2}\right) \left(\frac{3}{4}\right)}{\left(\frac{5}{8}\right)} = \frac{3}{5} \quad (2.26)$$

Similarly, the probability that the person chose bag 2 is  $P(B_2 | S) = 2/5$ . Qualitatively, this makes sense, since bag 1 contained more strawberry flavored candy, the probability that bag 1 was chosen should increase since it has more strawberry candy and the probability that bag 2 was chosen should decrease.

Now to continue the example. Imagine the first piece of candy is put back into the bag from where it came from. Then another piece of candy is drawn from the same bag, which turns out to be cherry flavor. Now one must update the probabilities with this new piece of information. One can keep using Bayes' theorem. The posteriors from the last draw  $m - 1$  are now used as the priors for the current update.

$$P(B_1 | C)_m = \frac{P(C | B_1) P(B_1 | S)_{m-1}}{P(C)} \quad (2.27)$$

$$P(B_2 | C)_m = \frac{P(C | B_2) P(B_2 | S)_{m-1}}{P(C)} \quad (2.28)$$

The probability of drawing a cherry flavored candy assuming bag 1 was chosen remains constant since the ratio of cherry to strawberry did not change for either bag, so  $P(C | B_1) = 1/4$  and the probability of drawing a cherry flavored candy assuming bag 2 was chosen is  $1/2$ . We now must use Equation 2.23 to compute the normalizing constant, otherwise the posterior probabilities will not sum to 1. In this case  $P(C) = 7/20$ . Plugging these numbers into Equations 2.27 and 2.28 gives the updated posterior probabilities

$$P(B_1 | C)_m = \frac{3}{7} \approx 0.43 \quad (2.29)$$

$$P(B_2 | C)_m = \frac{4}{7} \approx 0.57 \quad (2.30)$$

Intuitively, drawing a cherry flavored candy has reduced our belief that bag 1 was chosen since bag 1 consist of only  $1/4$  cherry flavor candy while bag 2 consisted of  $1/2$  cherry candy. This sequence can be continued, until a threshold has been reached for one of the posterior probabilities.

#### 2.4.2 Maximum A Posteriori

Imagine a situation similar to the candy example, where given a set of hypotheses,  $\{\mathbf{h}_1, \mathbf{h}_2, \dots, \mathbf{h}_{N_c}\}$ , one is interested in finding which hypothesis is the most likely, after new measurement  $g_m$  is made. The method of Maximum A Posteriori (MAP) says the hypothesis  $\mathbf{h}_k$  which maximizes the posterior probability is the most likely one.

$$\hat{\mathbf{h}}_{map} = \arg \min_k p(\mathbf{h}_k | g) \quad (2.31)$$

Using Bayes' theorem I can rewrite Equation 2.31 as

$$\hat{\mathbf{h}}_{map} = \arg \min_k \frac{p(g | \mathbf{h}_k) p(\mathbf{h}_k)}{p(g)} \quad (2.32)$$

Maximizing the posterior is now equal to maximizing the likelihood and prior. In certain cases, one needs to decide between two sets of parameters or hypotheses. One can do an analogous technique of comparing the posteriors by using a ratio

$$\frac{p(\mathbf{h}_i|g)}{p(\mathbf{h}_j|g)} = \frac{p(g|\mathbf{h}_i)}{p(g|\mathbf{h}_j)} \frac{p(\mathbf{h}_i)}{p(\mathbf{h}_j)} \quad (2.33)$$

If the ratio is larger than some threshold value then one chooses parameter  $h_i$  and if the ratio is less than the threshold then one chooses  $h_j$ . Similar to the earlier example of updating the posterior based on new data, one can update the Maximum A Posteriori (MAP) decision based on new data. Define the likelihood ratio of the  $m^{th}$  measurement as

$$\Lambda_m = \frac{p(g_m|\mathbf{h}_i)}{p(g_m|\mathbf{h}_j)} \quad (2.34)$$

After each new set of measurement data  $g_m$  is collected, one can update the posterior ratios by multiplying the likelihood ratio from the old set of data with the likelihood ratio of the new set of data. The ratio which includes all the updates from measurement  $m = 1$  to measurement  $m = N_m$  is written as

$$\frac{p(\mathbf{h}_i|\{g\}_{N_m})}{p(\mathbf{h}_j|\{g\}_{N_m})} = \prod_{m=1}^{N_m} \Lambda_m \frac{p(\mathbf{h}_i)}{p(\mathbf{h}_j)} \quad (2.35)$$

where the notation  $\{g\}_{N_m}$  represents the set of all data from measurement  $m$  to  $N_m$ .

In summary, Bayesian statistics is a useful way to update one's belief in a hypothesis or estimate a set of parameters. Bayes' theorem can be used to merge new measurement data and the probability of a hypothesis before the data was known. This is very similar the approach taken by the Adaptive Feature Specific Spectrometer (AFSS) and the AFSSI-C [48, 49].

## 2.5 Compressive Sensing

The fundamental approach of compressive sensing is that rather than sampling at a high rate and then compressing the sampled data, one can dramatically reduce the number of samples if each sample is in a compressed form. In Chapter 1, I gave some intuitive understanding of how compressive sensing works, but there are certain mathematical concepts that the reader should understand in order to have a full appreciation of the practical challenges in computational sensing. So, I will now discuss some of the formalism of compressive sensing and some techniques to compressively sampling signals. In order to understand why compressive sensing is so powerful I will first discuss the conventional sampling strategy.

### 2.5.1 The Nyquist-Shannon Sampling Theorem

One of the most important results concerning the *sampling* of continuous signals is the Nyquist-Shannon sampling theorem (often referred to as the *sampling theorem* for short). The sampling theorem says that exact reconstruction of a continuous *bandlimited signal*  $f(x)$  is possible if the sampling frequency  $f_s$  is atleast twice the maximum frequency  $B$  of the signal [50]. Assuming that a bandlimited signal  $f(x)$  has been sampled according to the sampling theorem, then exact recovery from the discrete samples  $f_n$  is guaranteed.

However, if the sampling frequency is less than twice the maximum bandwidth  $f_s < 2B$ , then aliasing may occur in the reconstruction. Aliasing is the effect that high frequencies in the original signal will be represented as lower frequencies after reconstruction and information contained in the high frequencies will be potentially lost [51].

Given a spatial length  $l$ , the number of measurement samples is

$$N_m = f_s l \quad (2.36)$$

Since  $f_s$  must be at least twice the maximum frequency of the signal there is a lower bound on the number of samples needed to recover the signal with no loss of information

$$N_m \geq 2l \cdot \max |F\{f(x)\}| \quad (2.37)$$

where  $F\{f(x)\}$  is the Fourier Transform of the signal  $f(x)$ .

It is important to clarify a small but important distinction between the meaning of sampling and the meaning of a measurement. A measurement is any process that maps physical phenomena which contains a signal-of-interest into measurement data. The measurement data may or may not be discrete. Sampling has a more precise mathematical definition. It is the process of mapping a continuous signal into a sequence of discrete numbers which are called the samples.

### 2.5.2 Sparsity, Incoherence, and the Restricted Isometry Property

There are two definitions of compressive sensing: The definition based on sparsity, incoherence, and the restricted isometry property (RIP) and the practical definition.

The sparsity-incoherence definition asserts that true compressive sensing is when the number of measurements  $N_m \ll N$  and certain properties called sparsity, incoherence, and RIP are satisfied. Under this definition, in the absence of noise, several

theorems guarantee high probability of exact reconstruction given a specific type of optimization algorithm. Under this framework, random measurement codes tend to have theoretically attractive properties that make them ideal for compressive sensing [52, 28, 35, 37]. The practical definition asserts that compressive sensing occurs anytime the number of elements in the measurement is much less than the dimensionality of the original signal and the signal is reconstructed with a small amount of error.

At first glance, compressive sensing seems to go against the Nyquist-Shannon sampling theorem, however the sampling theorem's guarantee of exact reconstruction of a continuous signal relies on the assumption of a bandlimited signal and uniform periodic sampling.

Most continuous signals  $f(x)$  can be written as a discrete summation of orthonormal basis functions

$$f(x) = \sum_{n=1}^N x_n \Psi_n(x), \quad (2.38)$$

where  $x_n$  are the coefficients. I will call the vector  $\mathbf{x} = [x_1 \ x_2 \ \dots \ x_N]^T$  the representation vector of the signal and  $\Psi$  the representation basis. This allows us to rewrite the signal as a matrix multiplication

$$\mathbf{f} = \Psi \mathbf{x}. \quad (2.39)$$

As I discussed in Chapter 1, any vector  $\mathbf{x}$  is sparse when all but a few of its entries are zero. A vector is called  $K$ -sparse when it has at most  $K$  non-zero entries.

$$\mathbf{x} : \|\mathbf{x}\|_0 \leq K \quad (2.40)$$

In real situations, signals with strictly sparse representation vectors are unlikely. Fortunately, it is possible to have approximately sparse representation vectors, which are called *compressible*. In other words, the sorted magnitudes of the coefficients  $|x_n|$  quickly decay. When a signal has an expansion in terms of a compressible representation vector, we can intuitively understand Equation (2.38). Discarding smaller coefficients will not significantly degrade the information in the signal [37].<sup>2</sup>

The concept of *sparsity* is important in compressive sensing. Sparsity determines how efficiently one can acquire the signals. All things being equal, if  $K$  decreases,

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<sup>2</sup>From now on, I will use the words sparse and compressible interchangeably. But it is important to realize there is a difference.

then the probability of achieving exact recovery increases. Sparse representations of the signal are not the only important prerequisite for high probability reconstruction.

In practice, the signal is sampled in a different basis than the representation basis. For example, while many natural signals have a sparse or compressible representation in various wavelet bases or Fourier bases, sampling using the representation basis is not practical in many cases. Often a sensing basis  $\mathbf{H}$  is used to perform the sampling. In traditional Nyquist-Shannon sampling, the sensing basis is a collection of delta functions. In compressive imaging experiments, the sensing basis is the binary random coded aperture mask [10]. In an LCOS based compressive sensing spectrometer, the sensing basis is a finite set of spectral filters [53, 54]. In short, the representation basis allows a signal to be represented as a sparse vector, while the sensing basis is composed of the functionals that one samples with. The equation which combines these concepts to model a compressive measurement is

$$\mathbf{g} = \mathbf{H}\Psi\mathbf{x} = \mathbf{H}\mathbf{f} \quad (2.41)$$

where  $\mathbf{g}$  is a  $N_m \times 1$  measurement vector,  $\mathbf{H}$  is a  $N_m \times N$  measurement vector,  $\Psi$  is a  $N \times N$  matrix and  $\mathbf{x}$  is an  $N \times 1$  vector.

One important concept in compressive sensing is coherence. The coherence between the sensing basis  $\mathbf{H}$  and the representation basis  $\Psi$  is

$$\mu(\mathbf{H}, \Psi) = \sqrt{n} \max_{1 \leq k, 1 \leq n} |\langle h_k, \psi_j \rangle|, \quad (2.42)$$

which defines coherence as a measure of the largest correlation between any two columns of  $\mathbf{H}$  and  $\Psi$ .

Ideally, one would like to use as less measurements as possible without degrading the reconstructed signal. In compressive sensing, the amount of measurements needed is a function of the sparsity and the coherence. Given a coefficient sequence  $\mathbf{x}$  that is  $K$ -sparse then one needs

$$N_m \geq C \cdot \mu^2(\mathbf{H}, \Psi) \cdot K \cdot \log n \quad (2.43)$$

for a high probability of reconstruction, where  $C$  is just a constant and  $N$  is the dimensionality of the original signal [37].

Equation (2.43) shows the importance of sparsity and coherence in compressive sensing. Lower coherence and sparsity allows one to use less measurements [10]. The more incoherent, and therefore lower correlation, the two bases are, the higher the probability of successful reconstruction of compressive measurements. It turns

out that random matrices have a high probability of being incoherent with any basis [37].

The isometry constant  $\delta_K$  of a matrix  $\mathbf{A}$  is the smallest number such that

$$(1 - \delta_K) \|\mathbf{x}\|_{\ell_2}^2 \leq \|\mathbf{Ax}\|_{\ell_2}^2 \leq (1 + \delta_K) \|\mathbf{x}\|_{\ell_2}^2 \quad (2.44)$$

for all  $K$ -sparse vectors  $\mathbf{x}$ . If  $\delta_K$  is not too close to one then the matrix  $\mathbf{A}$  obeys the *restricted isometry property* (RIP) of order  $K$  [37]. If RIP is satisfied, the matrix  $\mathbf{A}$  approximately preserves the Euclidean length of signals. The RIP is an important theoretical result which allows robust compressive sensing when signals are corrupted by noise. Sensing matrices which have random entries obey the RIP with high probability [37, 10, 35].

All of the concepts I have just discussed can be understood at an intuitive level. Sparsity is the idea that the information content of a signal is relatively small compared to the amount of data which originally described the signal. Coherence extends the concept of how invertible a matrix is, the more linearly independent the system of equations, the easier it is to invert the matrix. The restricted isometry property is basically saying that any matrix with a small isometry constant will keep the distance between signal vectors the same. Why is this important? Think of a geometric picture, imagine noise as a sphere of uncertainty around the signal vectors. When the noise is small, two signal vectors can be mapped to a small part of the measurement space and still fit in that space. When one extracts the signal from the compressed measurements, one can tell them apart. As the noise increases one wants the distance between measured signal vectors to at least stay the same and certainly not dramatically decrease, otherwise it will be difficult to tell the signals apart. The RIP is basically a way of seeing if a measurement matrix will pack the signal vectors with the same distance between them. This is important because one does not want a small amount of noise to result in a large reconstruction error.

### 2.5.3 Solving Inverse Problems For Compressive Sensing

Now that I have discussed what compressive sensing is mathematically, it is time to address how to actually solve the problem of extracting  $\mathbf{x}$  from

$$\mathbf{g} = \mathbf{Ax} + \mathbf{e} \quad (2.45)$$

where  $\mathbf{g}$  is the measurement vector,  $\mathbf{x}$  is the sparse representation of the signal,  $\mathbf{A}$  is the linear mapping from  $\mathbf{x}$  to  $\mathbf{g}$ ,  $\mathbf{e}$  is the noise vector, and the number of

measurements  $N_m$  is much less than the dimensionality of the sparse representation vector  $N$ .

The least squares (LS) estimator attempts to solve this inverse problem by minimizing the objective function

$$\sum_{n=1}^N (\mathbf{g} - \mathbf{Ax})^2 = \|\mathbf{g} - \mathbf{Ax}\|_2^2. \quad (2.46)$$

which is the  $\ell_2$  norm between the given data  $\mathbf{g}$  and the forward model for the data  $\mathbf{Ax}$ . Notice, there are no probabilistic assumptions about the measurement data. It turns out that a closed form version of the LS estimator exists as

$$\hat{\mathbf{x}} = (\mathbf{A}^T \mathbf{A})^{-1} \mathbf{A}^T \mathbf{g}. \quad (2.47)$$

where  $\hat{\mathbf{x}}$  is the estimated value of  $\mathbf{x}$ .<sup>3</sup>

The derivation of the closed form of the least squares estimator is given in Appendix A. Alternatively, if the vector  $\mathbf{x}$  is very large, solving the inverse problem in closed form maybe too computationally intensive. In this case, one may use the gradient descent algorithm or other types of iterative optimization algorithms to solve the least squares problem. While the LS estimator may provide a solution when  $N_m \ll N$ , these solutions tend to overfit the data in these situations, do not take advantage of the prior knowledge of sparsity to reduce the solution space, and  $\mathbf{A}\hat{\mathbf{x}}$  is not unique. Therefore, an unconstrained LS approach do not work well for the compressive sensing problem.

There is a vast number of algorithms that are designed for compressive sensing and new ones are being published constantly. A full discussion of each algorithm is not within the context of this dissertation. The fundamental concept of the ones used by the author will be briefly discussed now and implementation details will be provided in the relavent chapters.

Many of the algorithms for compressive sensing are optimization algorithms. Optimization algorithms are problems which serve to minimize (or maximize) an objective function  $F_0$

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x} \in \mathbb{R}^N} F_0(\mathbf{x}). \quad (2.48)$$

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<sup>3</sup>Note that it is important to realize that in practice one should never use the actual inverse of  $\mathbf{A}^T \mathbf{A}$  due to the various numerical computing issues. One should resort to computing the psuedoinverse.

Which is called an unconstrained optimization problem. Similarly, solving the problem

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x} \in \mathbb{R}^N} F_0(\mathbf{x}) \text{ subject to } F_n(\mathbf{x}) \leq b_n \quad \forall n \quad (2.49)$$

is a constrained optimization problem. If  $F_n \forall n$  are convex then the problem is a convex optimization problem. If  $F_n \forall n$  are linear functions, then it is called a linear program (program is synonymous with optimization) [35].

Given measurements  $\mathbf{g}$  and knowledge that  $\mathbf{x}$  is sparse or compressible, solving an optimization problem of the form

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x}} \|\mathbf{x}\|_0 \text{ subject to } \mathbf{Ax} = \mathbf{g} \quad (2.50)$$

where  $\|\mathbf{x}\|_0$  is the  $\ell_0$  norm, which is equal to the number of nonzero entries in vector  $\mathbf{x}$ .<sup>4</sup> Equation (2.50) returns estimate  $\hat{\mathbf{x}}$  that resembles  $\mathbf{x}$  as long as the measurement noise is small. This is referred to as  $\ell_0$ -minimization. The constraint ensures the solution agrees with the observed measurement data. In other words, one wants the sparsest solution possible that agrees with the measurement data.

Unfortunately,  $\ell_0$ -minimization is nonconvex which means that iterative methods may not converge to a solution. This is an important feature for inverse problems. A convex problem has the property that any local minimum is also a global minimum. In fact, it has been shown that for a general matrix  $\mathbf{A}$ ,  $\ell_0$  minimization is intractable [55]. This means that one can do no better than a brute force search for the answer.

Fortunately, one can minimize the  $\ell_1$  norm

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x}} \|\mathbf{x}\|_1 \text{ subject to } \mathbf{Ax} = \mathbf{g} \quad (2.51)$$

where  $\|\mathbf{x}\|_1 = \sum_n |x_n|$ , and get excellent reconstruction in the case where Equation (2.43) and the Equation (2.44) are satisfied. Not only is Equation (2.51) convex, it can be reformulated as a convex quadratic optimization problem which means that it can be solved by standard optimization methods [30, 28, 35]. Equation (2.51) is the problem that much of the theoretical framework of compressive sensing provides guarantees for.

A more practical version of Equation (2.51) is written as

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x}} \|\mathbf{Ax} - \mathbf{g}\|_2^2 + \tau \|\mathbf{x}\|_1 \quad (2.52)$$

where  $\tau$  is a non-negative number.  $\tau$  is called the regularization parameter and serves to change the sparsity level of the solution and can be used to account for

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<sup>4</sup>The  $\ell_0$  norm is not strictly a norm and is actually a quasi-norm.

noise, by setting small noise contributions to zero, which increases the robustness of the optimization.<sup>5</sup> In this form, the problem is called  $\ell_1$  regularized least squares (LS).  $\ell_1$  regularization also appears in the context of basis pursuit denoising [56].

In statistics,  $\ell_1$  regularized LS is often referred to as the *lasso* regression method or the lasso problem. The original paper for lasso describes both the problem and the lasso algorithm. However, there are multiple algorithms for solving the  $\ell_1$  regularized LS problem, such as Least Angle Regression (LAR) [57], truncated Newton interior point methods [58], and Conjugate Gradients algorithm [52].

A related regression technique which is also used to regularize statistical models to prevent overfitting called is *ridge regression*,

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x}} \|\mathbf{Ax} - \mathbf{g}\|_2^2 + \tau \|\mathbf{x}\|_2. \quad (2.53)$$

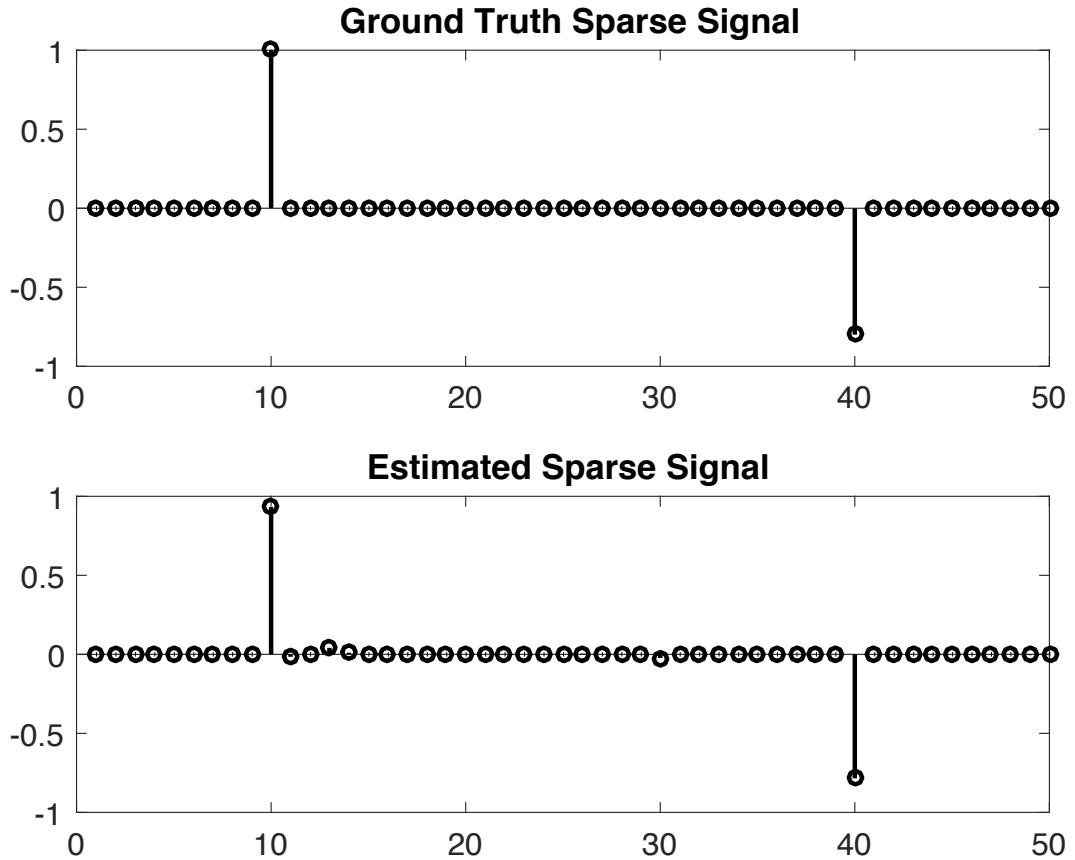
In the context of optimization this is called the Tikhonov regularization problem [58, 59]. As with least squares, ridge regression seeks coefficient estimates that fit the data well. In ridge regression the regularization is performed by using an  $\ell_2$  term, which also tends to shrink the coefficients towards zero as  $\tau$  increases but does not set certain elements to zero like in *lasso* regression.

In Figure 2.4, I show an example of sparse signal recovery using the built-in MATLAB `lasso` function. In this case the signal  $\mathbf{f}$  is sparse in the native basis so the representation basis can be written as the identity matrix  $\Psi = \mathbf{I}$ . The SNR is the ratio of the variance of the signal to the variance of the noise and is set to  $\text{SNR} = 10$ . The top plot shows the ground truth signal  $\mathbf{f}$ . The bottom plot shows the estimated signal  $\hat{\mathbf{f}}$ . The regularization parameter is set to  $\tau = 0.02$ . The sensing matrix  $\mathbf{H}$  is shown in Figure 2.5. The number of measurements  $N_m = 10$ . The dimensionality of the signal  $N = 50$ .

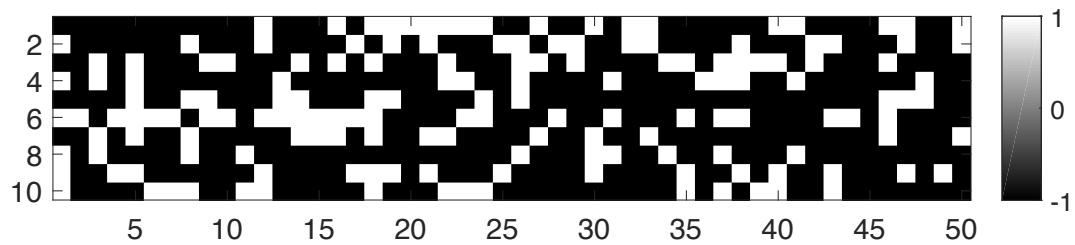
One can gain some geometric intuition of why the  $\ell_1$  regularized least squares produces sparse solutions by looking at Figure 2.6(a). The dot indicates the unconstrained LS solution. The contours represent equal values of the objective function:  $\|\mathbf{Ax} - \mathbf{g}\|_2^2$ . The solution is when the  $\ell_1$  constraint intersects one of the contours. Because of the shape of the  $\ell_1$  ball, this tends to occur along one of the coordinate axes. Figure 2.6(b) represents the situation with  $\ell_2$  regularized LS, ridge regression, because of the shape of the  $\ell_2$  ball the solutions may or may not occur along the

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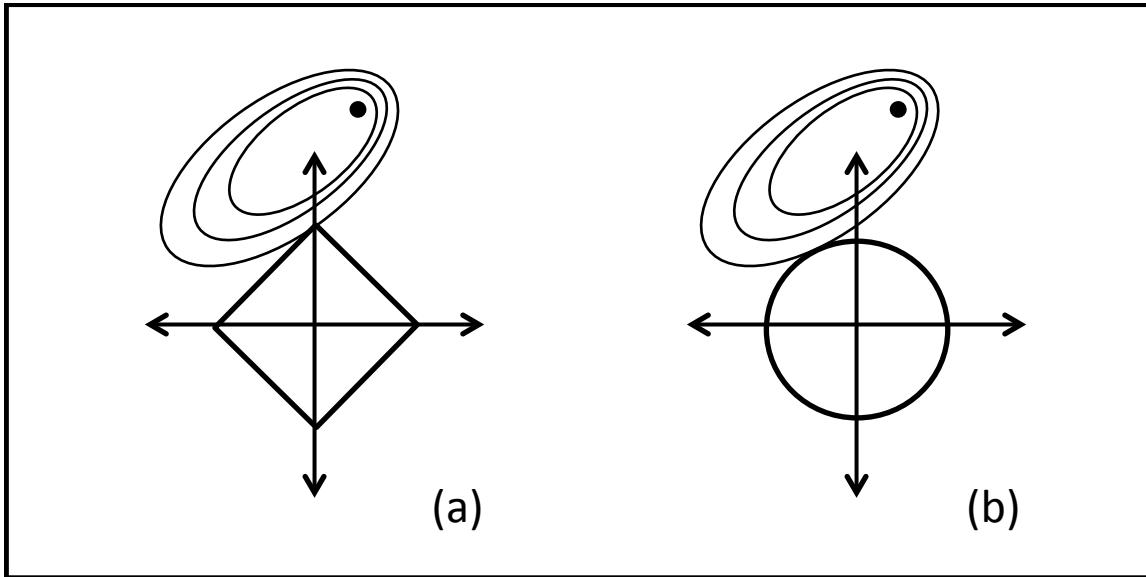
<sup>5</sup>Most papers in compressive sensing use  $\lambda$  to denote the regularization parameter. I choose to use  $\tau$  to prevent confusing it with wavelength since I will be discussing spectral compressive sensing later on.



**Figure 2.4:** Example of sparse vector recovery using  $\ell_1$  regularized least squares algorithms. SNR = 100. The top plot shows the ground truth signal  $\mathbf{x}$ . The bottom plot shows the estimated signal  $\hat{\mathbf{x}}$  and  $\tau = 0.02$ . The number of measurements is  $N_m = 10$ . The dimensionality of the signal is  $N = 50$ .



**Figure 2.5:** The sensing matrix  $\mathbf{H}$  used for Figure 2.4. Since the signal was already sparse, the representation basis can be written as the identity matrix  $\Psi = \mathbf{I}$ . The number of rows correspond to the number of measurements  $N_m$  and the number of columns correspond to the number of elements in the signal vector  $\mathbf{f}$ .



**Figure 2.6:** (a)  $\ell_1$  regularized least squares which is called lasso regression. (b)  $\ell_2$  regularized least squares which is called ridge regression.

coordinate axes.

The lasso regression technique in statistics is a way to perform variable selection without overfitting the data [60, 61]. In simple terms, overfitting means that given some seemingly complicated data, overfitting occurs when the model attempts to fit all of the data producing a model with very low error with the given data but will tend to have poor prediction results when new data is obtained. By regularizing the objective function, the model will tend to have better prediction accuracy by producing simpler models even though it may have a larger error trying to fit the current data.

Algorithms for solving the lasso improve the accuracy of the estimate by selecting only a subset of the columns of the matrix  $A$  which we denote as the  $A_s$ . An example of the LAR algorithm which is often used to solve the lasso problem is provided in [57]. By forcing the sum of the absolute value to be less than some fixed value,  $\ell_1$  regularized least squares forces certain values of  $x_n = 0$ , effectively choosing a simpler model out of all the possible solutions provided by LS.

## 2.6 Conclusion

I used this chapter to cover several important mathematical concepts which are required for the reader to understand the advantages and disadvantages of computational sensing. I first discussed the advantages that Hadamard and S-Matrix multiplexing provided compared to the isomorphic sensor which provided a context

for the discussion of the Fellgett advantage. Then I discussed Principal Component Analysis (PCA), a useful technique for finding useful discriminating features from seemingly complicated data. I also covered the fundamentals of Bayesian statistics and how it can be used to update estimates of statistical parameters given new data. Then I covered important topics in compressive sensing: sparsity, coherence, and the restricted isometry property (RIP) and discussed the  $\ell_1$  regularized LS problem which is used to promoted sparsity and has a multitude of algorithms which can be used to solve it.

## Chapter 3

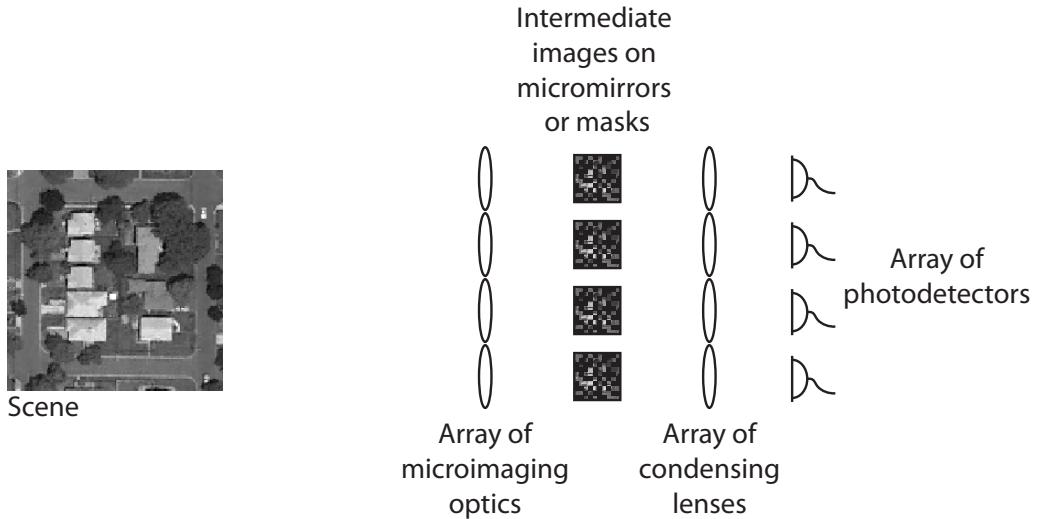
### Static Computational Optical Undersampled Tracker

#### 3.1 Motivation for the Static Computational Undersampled Tracker

In large-area persistent surveillance, traditional isomorphic sensing systems must acquire, process, store, and transmit large amounts of data to achieve high spatial and temporal resolution. These sensors are typically on airborne platforms or orbiting satellites which leads to a large size, weight and power-cost (SWAP-C). However, if one is interested in estimating the location of moving objects (tracking) rather than reconstructing the entire object scene, the information content in the signal-of-interest is relatively low. One can significantly lower the SWAP-C by using a task-specific approach. To address the challenges of traditional target tracking, several colleagues and I designed, built, and demonstrated such a device called the Static Computational Optical Undersampled Tracker (SCOUT) [11, 62]. This chapter will provide details in to how we developed the SCOUT.

Most of the current experimental demonstrations of compressive imaging try to reconstruct the entire object scene or spatial-temporal datacube. For example, the Coded Aperture Compressive Temporal Imaging (CACTI) sensor uses a temporally varying psuedo-random coded aperture during a single FPA exposure and attempts to reconstruct a spatial-temporal datacube [15]. In another experimental compressive imager, a rotating cylindrical lens measures scene data using an optical Radon transform and then reconstructs a static object scene [63]. While these architectures demonstrate the rapid progress that researchers have made towards compressive imaging, they emphasize reconstructing high dimensional data and require another post-processing step to extract task-specific information. Furthermore, this data will then need to be compressed again for storage or transmission. If one is concerned with only tasks, then reconstructing the entire scene as an intermediate step is unnecessary and even wasteful.

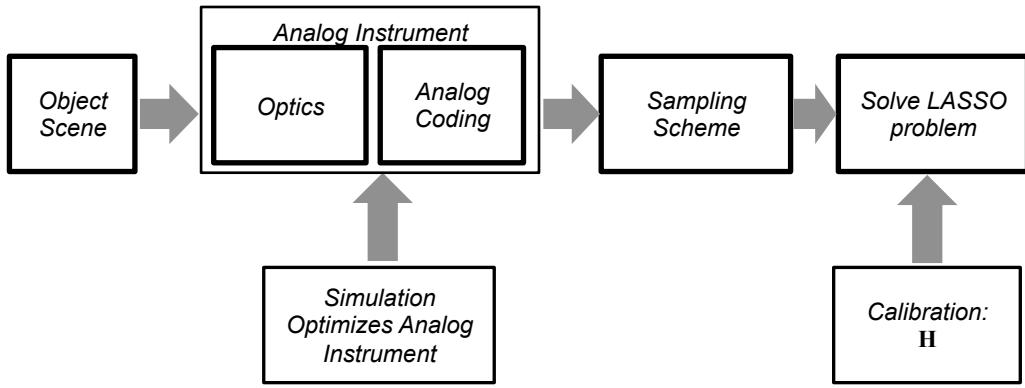
Another example of compressive imaging is the single pixel camera, discussed in Section 1.6. This sensor uses a Digital Micro-Mirror Display (DMD) to measure in any arbitrary basis, but must do so over many time-sequential measurements [10]. Each measurement is an integrated point-by-point multiplication of the scene



**Figure 3.1:** An example of a typical parallel optical CS architecture. Capturing  $N_m$  simultaneous projections requires using  $N_m$  spatial light modulators or masks and  $N_m$  detector elements.

locations with the DMD array values. For temporally static scenes, this architecture allows an arbitrarily long exposure time (within the limit of detector saturation) to increase the SNR for each measurement. However, with temporally varying scenes it needs to record all the projections for each frame before the object moves. Increasing the rate at which projections are made is possible, but this reduces exposure time and SNR. One way to overcome this is by implementing a parallel architecture of single pixel cameras, each with a different projection, see Figure 3.1. Clearly this will significantly increase the SWAP-C of the architecture. Another issue with a fully parallel architecture, is that each camera will have a different entrance pupil location, producing parallax. One issue many computational sensor designs must deal with is “over multiplexing”. All real optical ADC devices have a certain amount of dynamic range, in which linearity is valid. As the amount of light that is recorded increases, the amount of dynamic range being used fills up. Architectures which only use a single pixel are at greater risk for over multiplexing.

A computational sensing architecture dedicated to target tracking rather than full object scene reconstruction, can significantly ameliorate these design trade-offs. We developed the Static Computational Optical Undersampled Tracker (SCOUT) with the goal that measurements must be acquired “single-shot” using a conventional FPA [11, 64]. The SCOUT system is an important step toward practical low-cost computational sensing for optical imaging. The system enables parallel “single-shot” acquisition of compressed, task-specific sensing oriented data, using a static



**Figure 3.2:** A systems level flowchart of the SCOUT system. Light from the object scene propagates to the optical instrument which consists of a coded aperture (mask 1), an objective lens, and another coded aperture (mask 2), a focal-plane array (FPA) then undersamples the coded object scene, measurement data is used to solve a lasso problem. The parameters of the optical instrument is optimized using simulations to minimize the probability of tracking error. Calibration provides accurate measurement of the system matrix  $\mathbf{H}$  to lasso optimization algorithm.

(no moving parts) architecture.

A related static approach uses optical Radon projections [65]. This instrument relies on a several cylindrical lenses to integrate the optical intensity from the object plane onto lines on the FPA. The number of detector elements is much less than the native dimensionality of the object scene. For a single moving point in the field-of-view, two perpendicular Radon projections is enough to compute the change from frame to frame. However, the researchers found heuristically that four cylindrical lens are better for reconstructing the change information for a scene that included up to ten moving objects, called movers.

A systems level flowchart of the SCOUT is shown in Figure 3.2. Like many computational sensors, it relies on the coding of the analog signal-of-interest prior to the ADC step and processes the measurement data using prior information and calibration data. The analog instrument was optimized using a custom ray-based simulation which evaluates a metric based on the simulated system matrix. In this chapter, I will discuss the SCOUT architecture in detail in Section 3.2, which uses a defocused imaging system with two binary amplitude masks. The FPA samples at a much lower resolution than the native resolution of the object scene. While other compressive imaging systems have to reconstruct entire images, the SCOUT only reconstructs frame-to-frame differences. As a result the SCOUT requires sig-

nificantly less bandwidth to transmit to a base station where the post-processing step can occur.

### 3.2 SCOUT Architecture

The goal of the SCOUT was to demonstrate a low SWAP-C compressive target tracking sensor. The SCOUT architecture is designed to avoid the hardware scaling issues of the single-pixel camera. The trade-off for the ability to measure parallel projections is the loss of flexibility to implement arbitrary projections i.e. by using a Spatial Light Modulator (SLM). However, rather than fully designing the projections themselves, I describe a process for optimizing the optical instrument in Section 3.3. Previous prototypes of the SCOUT architecture are described in [62, 66].

The SCOUT system takes measurements that are both compressive and multiplexed: The number of measurements is less than the number of scene locations  $N_m \ll N$ , and each measurement must contain information about many scene locations. In this architecture, the number of measurements is the number of pixels in the FPA. Intuitively this means that the system matrix must exhibit a many-to-few mapping from scene locations to FPA elements.

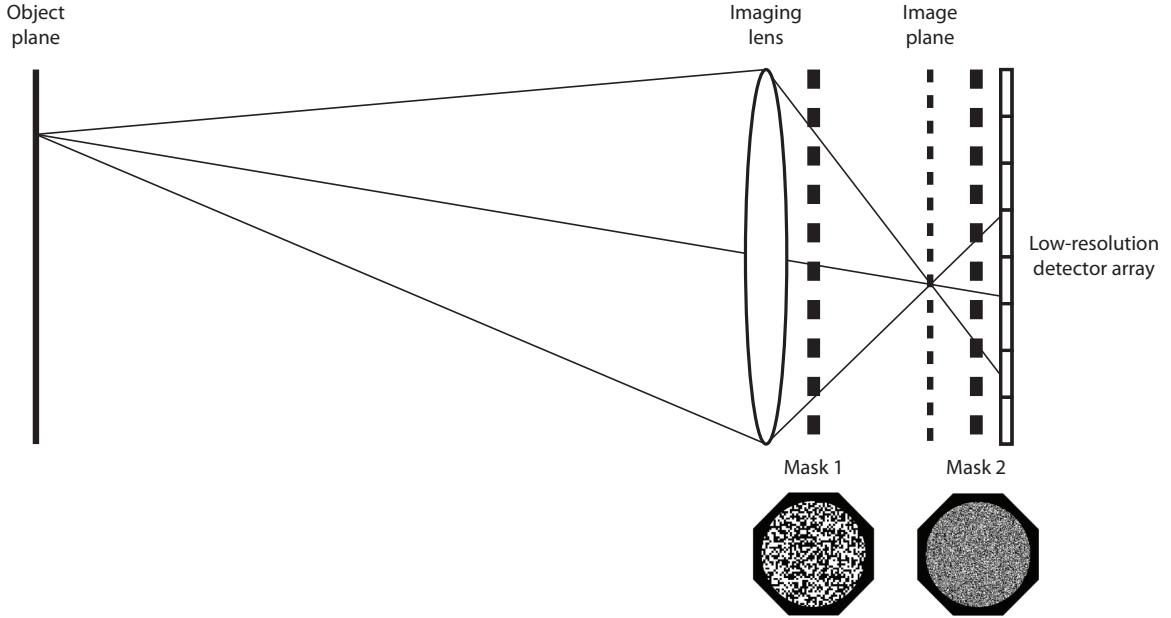
The SCOUT architecture is shown in Figure 3.3. In this architecture the multiplexing occurs in the spatial domain by mapping multiple object scene locations to only a few detector pixels. To accomplish this, we created a structured blur. This blur allows the light from a single object point to be spread to several pixels on the FPA. The most straightforward way to achieve a blur is by defocusing the image so that the PSF is broad, spanning many FPA pixels. Since the number of FPA pixels are less than the object scene resolution, the measurement is compressive.

Like any aberration, defocus significantly reduces contrast of high spatial frequencies, so the measurements will be poorly conditioned for reconstruction. Therefore, we created high-frequency structure in the PSF by using two pseudo-random binary occlusion masks. Each mask is placed at different positions between the lens and the sensor. The separation between masks results in a spatially varying point-spread function.

As with many linear computational sensing architectures, the forward model is written in the form

$$\mathbf{g} = \mathbf{Hf} + \mathbf{e} \quad (3.1)$$

where  $\mathbf{f}$  is the discrete representation of the object signal-of-interest,  $\mathbf{g}$  is the mea-



**Figure 3.3:** A diagram of the SCOUT architecture. A lens projects light through a pair of binary occlusion masks onto a low-resolution sensor which is defocused from the nominal image plane. This creates a spatially multiplexed shift-variant PSF incident on the FPA.

surement,  $\mathbf{H}$  is the matrix which describes mapping of the object to the measurement, and  $\mathbf{e}$  is the noise at each measurement. In this situation the signal-of-interest is actually the difference between two subsequent object scenes (frames)  $\Delta\mathbf{f}$ :

$$\begin{aligned}\mathbf{g}_k &= \mathbf{H}\mathbf{f}_k + \mathbf{e}_k \\ \mathbf{g}_{k+1} &= \mathbf{H}\mathbf{f}_{k+1} + \mathbf{e}_{k+1}\end{aligned}\tag{3.2}$$

Where the subscripts represent the  $k^{th}$  readout from the FPA.

$$\Delta\mathbf{g} = \mathbf{g}_{k+1} - \mathbf{g}_k = \mathbf{H}(\mathbf{f}_{k+1} - \mathbf{f}_k) + \mathbf{e}_{k+1} - \mathbf{e}_k\tag{3.3}$$

so the forward model can be written as

$$\Delta\mathbf{g} = \mathbf{H}\Delta\mathbf{f} + \Delta\mathbf{e}\tag{3.4}$$

In this equation, the 2-dimensional difference frame and object scene have a resolution of  $R_x \times R_y$  elements, and are lexicography reordered into a  $N \times 1$  column vector,  $\Delta\mathbf{f}$  and  $\mathbf{f}$ . Similarly, the difference measurement and measurement  $\Delta\mathbf{g}$  and  $\mathbf{g}$  are  $N_m \times 1$  vectors representing a 2-dimensional FPA readout with a  $r_x \times r_y$  matrix which represents the low resolution measurement. The detector noise is represented by the  $N_m \times 1$  vector  $\mathbf{e}$ . The system matrix  $\mathbf{H}$  is thus an  $N_m \times N$  matrix, where  $N_m \ll N$  in order for the system to be considered compressive. The  $n^{th}$  column of the matrix is the PSF of the  $n^{th}$  location in the object scene. The resulting system

matrix  $\mathbf{H}$  demonstrates that the SCOUT is a spatially variant optical system and presents a block structure, as seen in the example shown in Figure 3.4.

Referring back to the diagram of the SCOUT architecture shown in Figure 3.3. The object distance is much larger than the focal length of the lens so image of the scene occurs approximately one focal length from the lens  $f_E$ . The FPA is placed some distance  $d_{im}$  from the focal plane thus the total distance from the lens to the FPA is  $f_E + d_{im}$ . Two binary occlusion masks, mask 1 and mask 2, are placed at distances  $d_1$  and  $d_2$  from the sensor. Mask 1 and 2 have associated fill factors  $F_1$  and  $F_2$  and pitch  $p_1$  and  $p_2$ , respectively.

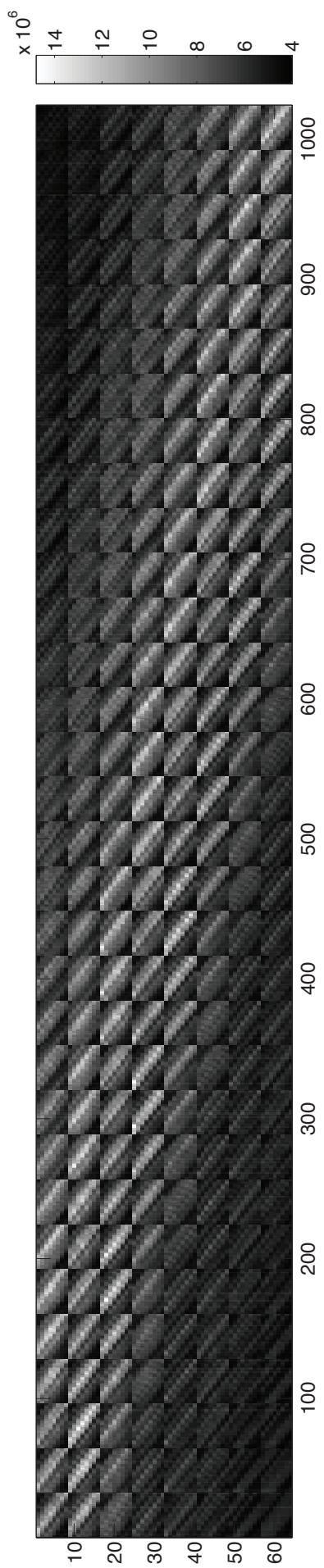
### 3.3 Optimizing the SCOUT

While the SCOUT lacks the ability to implement arbitrary measurement codes, we are able to adjust various physical parameters of the system such as defocus distance and mask fill factor to minimize reconstruction error. Adjusting each parameter in the actual prototype requires too much time, a more practical approach is to simulate the SCOUT architecture. In this section, I will discuss the simulation and define a metric that we used to evaluate different design parameters of the SCOUT without the need to reconstruct the difference frames.

#### 3.3.1 Simulating a SCOUT System

We developed a paraxial ray based simulation for the SCOUT. The simulation allows us to model the effects on the measurement as light travels through the lens and two masks and onto the detector plane. The lens is modeled as a single thin lens with transmittance function  $t_f$  and the two masks have transmittance functions  $t_1$  and  $t_2$ . From calibration measurements, the mask has a transmittances of 0 where the mask is black and 0.88 where the mask is clear. The lateral magnification of the scene and the two masks is calculated using similar triangles.

A simulated calibration occurs, in other words the simulation records the  $r_x \times r_y$  PSF from each scene location in order to obtain the system matrix  $\mathbf{H}$ . Once  $\mathbf{H}$  is known, we use it to simulate the low resolution measurements,  $\mathbf{g}$ , of the higher resolution scenes,  $\mathbf{f}$ . Subsequent simulated measurements are subtracted to find  $\Delta\mathbf{g}$ . We also did not add any noise. I have attached the simulation code in Appendix D.



**Figure 3.4:** An example of an experimentally measured of the system matrix of the SCOUT system. The approximate block-Toeplitz structure is clearly evident, as is the deviation from the Bernoulli or Gaussian ensembles typically considered in CS treatments.

### 3.3.2 Quantifying Reconstruction Error

The MSE error metric is not suitable for our application because it weights all errors equally. For the task of motion tracking we classify errors into three types. A false positive occurs when the estimate shows an object where there is none. A false negative occurs when the estimate fails to show an object where one exists. As shift error occurs when an object is being tracked but appears in the wrong location. We developed a custom tracking error metric that weighs false negatives and false positives more than shift errors. This is because false negatives and false positives indicate a serious failure in the motion tracking task, while shift errors are less serious. We define tracking error as

$$P = \frac{|\mathbf{a} \otimes \epsilon|}{2N_{mv}} \quad (3.5)$$

where

$$\mathbf{a} = \begin{bmatrix} 1/9 & 1/9 & 1/9 \\ 1/9 & 1/9 & 1/9 \\ 1/9 & 1/9 & 1/9 \end{bmatrix} \quad (3.6)$$

where the error  $\epsilon$  is the difference between the true and reconstructed difference frames

$$\epsilon = \Delta\mathbf{f} - \hat{\Delta\mathbf{f}} \quad (3.7)$$

and  $N_{mv}$  is the number of movers in the scene. To reduce the penalty for one-pixel shift errors, the error frame is convolved with a three pixel averaging kernel  $\mathbf{a}$ . The absolute value is taken in order to count positive and negative errors equally, and the error is divided by  $2N_{mv}$  to make the metric independent of the number of movers.

### 3.3.3 Optimizing Optical System Parameters

Now that I have explained the simulation and the custom error metric for tracking, I can finally begin to discuss how we optimized some of the parameters to reduce the reconstruction error. Both the simulation and experimental study demonstrates a relationship between mask position and pitch: the tracking error is very sensitive to the *projected* mask pitch on the FPA. Furthermore, increasing the mask separation reduced tracking error, generating a highly space-variant PSF. With these observations in mind, we focus our study on the mask pitches ( $p_1, p_2$ ) as well as the defocus distance  $d_{im}$ .

A brute force search, using the lasso solver at each step is computationally intensive. We wanted a simple to compute metric which can predict tracking error. So we developed a custom metric inspired by the coherence parameter from the compressive sensing community, see Equation (2.42). We created a customized coherence parameter  $\mu$ ,

$$\mu = \max |\langle h_i, h_j \rangle|; \quad i \neq j \quad (3.8)$$

which is the maximum absolute value of the inner product between unique columns  $h_i$  and  $h_j$  of  $\mathbf{H}$ . The columns are unnormalized because their relative magnitude is related to the physical light throughput.

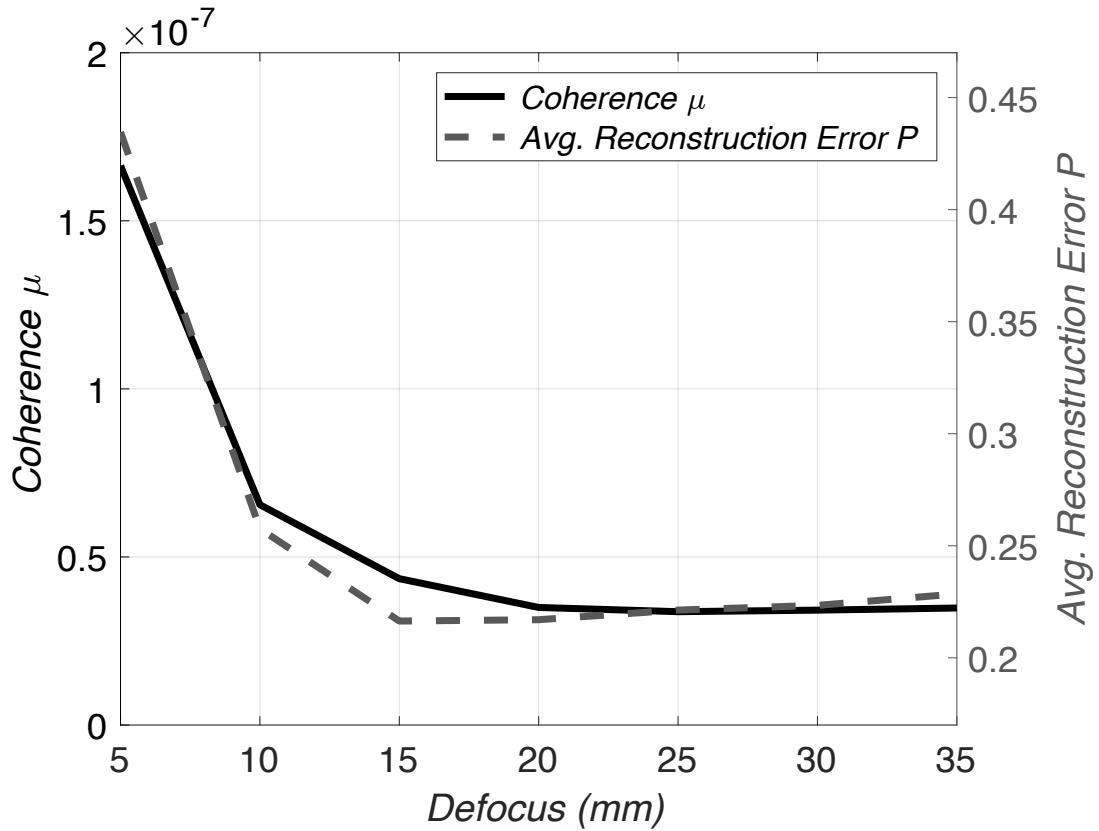
Notice that although system matrices with nearly pairwise orthogonal columns will result in small coherence values, system matrices with numerically small entries can accomplish the same. Optimizing  $\mathbf{H}$  for minimum coherence would drive total system throughput down. To eliminate this effect we normalized  $\mathbf{H}$ :

$$\mathbf{H}_{norm} = \frac{\mathbf{H}}{\sum_{m=1}^{N_m} \sum_{n=1}^N h_{m,n}} \quad (3.9)$$

where  $N_m$  and  $N$  are the total number of rows and columns in the system matrix. Physically, this normalization represents division by the sum of each PSF's light throughput. The coherence of a system matrix normalized in this way cannot be biased by reducing throughput. One consequence of this normalization is that mask fill factor cannot be optimized.

To demonstrate the effectiveness of the modified coherence parameter as a predictor of reconstruction error trends, I ran several simulations with complete reconstructions in order to compare reconstruction error to coherence. Figure 3.5 shows that reconstruction error and the coherence parameter follow similar trends for different defocus distances when all other parameters are held constant. Figure 3.6 shows similar agreement when varying values of mask pitch  $p_2$ .

The simulations demonstrate the viability of the architecture and provide an efficient way to optimize most architecture parameter values using the simulated system matrix coherence. Mask throughput cannot currently be optimized because the custom coherence metric is normalized by full system throughput. The problem of finding optimal mask throughput warrants further investigation.



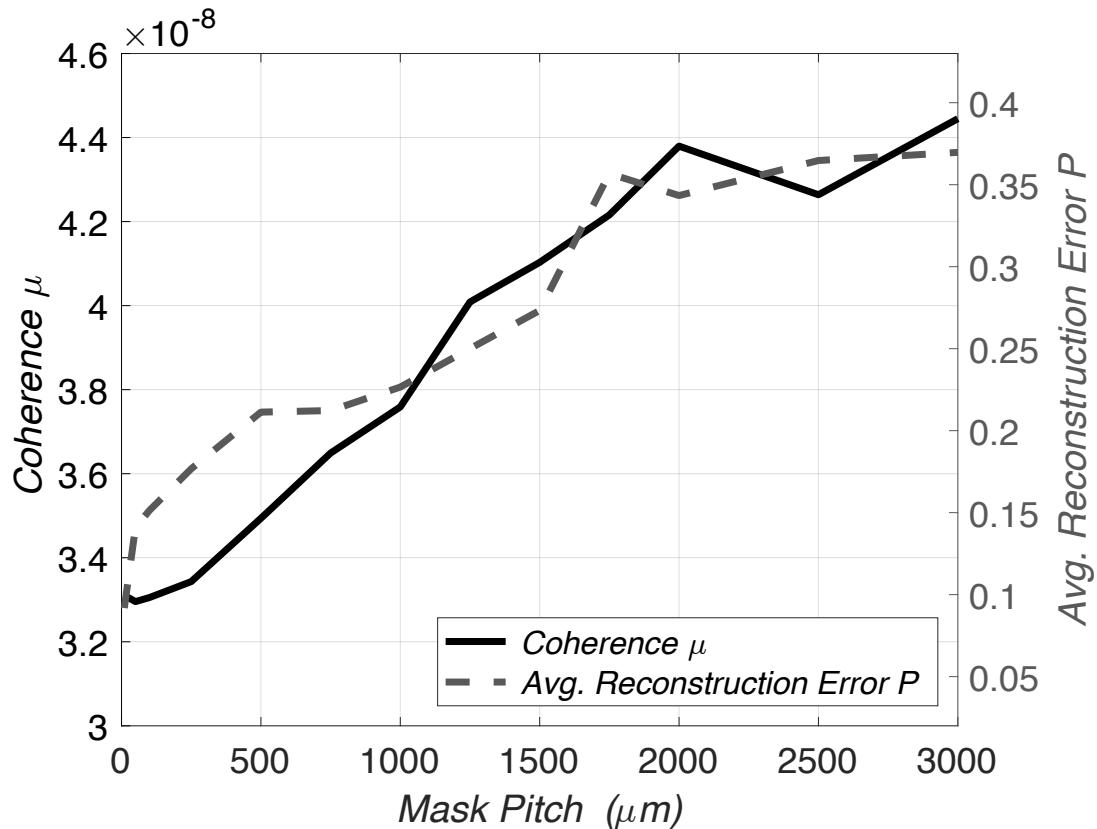
**Figure 3.5:** The coherence  $\mu$  (left vertical axis - black) and reconstruction error  $P$  (right vertical axis - dashed gray) plotted as a function of defocus distance  $d_{im}$ .

### 3.4 Experiment

#### 3.4.1 Experimental Setup

For the experiment, the captured image resolution  $r_x \times r_y$  is  $8 \times 8$ , while the ground-truth and reconstructed frame differences have a resolution  $R_x \times R_y$  of  $32 \times 32$ . To simulate a low-resolution detector, the camera captures the scenes at  $128 \times 128$  sensor pixels and the images are binned down to  $8 \times 8$  before being used in reconstruction.

We used a SBIG Model ST-7XMEI CCD camera with modified optics. The object scenes were displayed on a plasma television monitor. Figures 3.7 and 3.8 shows a photograph of the experimental setup. The optical system of the camera includes a 35 mm focal length lens and two random amplitude binary masks. Each mask was printed on transparencies using a high resolution laser printer. Mask 1 has pitch  $p_1 = 30$  microns and fill factor  $F_1 = 0.4$  and is located at a distance  $d_{m1} = 14mm$  from the sensor. Mask 2 has pitch  $p_2 = 500$  microns and fill factor  $F_2 = 0.2$  and is located at a distance  $d_{m2} = 57mm$  from the sensor. These parameters were chosen based on the aforementioned optimization process. A plasma monitor



**Figure 3.6:** The coherence  $\mu$  (left vertical axis - black) and the reconstruction error  $P$  (right vertical axis - dashed gray) is plotted as a function of the pitch of mask 2

was used because it provides a higher contrast compared to the traditional liquid crystal displays (LCD). However, the black background of the plasma monitor still produced a small amount of irradiance, which is a source of systematic error and potentially reduces the usable amount of dynamic range.

### 3.4.2 Calibration

Instruments based on compressive sensing rely heavily on accurate calibration. Especially important is the knowledge of the system matrix  $\mathbf{H}$  to prevent reconstruction or task-specific sensing errors. The SCOUT architecture is no different. Inaccurate calibration dramatically affects the tracking error. Furthermore, because of the non-isomorphic nature of compressive sensing, it is difficult to look at the system matrix and intuitively tell whether it will lead to good results. In this section, I will describe the calibration procedure for the SCOUT architecture.

Conceptually the calibration procedure is a straightforward. The goal is to experimentally determine the system matrix  $\mathbf{H}$ . Each column of the matrix is the point-spread function (PSF) due to a “point” at the  $n^{\text{th}}$  location in the object scene.



**Figure 3.7:** The camera captures images of scenes displayed on a plasma television approximately 2 meters away..



**Figure 3.8:** The camera disassembled to show the camera body, the optical tube and the custom fabricated lens holder which goes inside the lens tube.

All one needs to do is display the point at each location and store the measurement in the respective column of  $\mathbf{H}$ .

There are several practical issues in the calibration process for the SCOUT. Calibration itself is a measurement process, noise is present in each measurement. To mitigate the effects of noise, we cooled the CCD in the camera to 0 degrees Celsius

using the built-in thermoelectric cooling (TEC). We also increased the exposure time to 1.0 seconds. While it is possible to continue increasing the exposure time, we found that increasing the exposure time past this did not significantly reduce the tracking error metric.

To eliminate any systematic error due to light pollution, we constructed a light-tight box using 80/20 aluminum framing, black poster board, and black gaffer tape. This box enclosed the entire SCOUT and the plasma monitor. We also found that the plasma monitor emitted a certain amount of light even though it is set to zero. To mitigate this, we take several dark frame measurements, which is a measurement with the plasma monitor set to all zero and then averaged. This averaged dark frame measurement is subtracted from each PSF measurement.

Another issue with the plamsa is that the intensity varies after a few minutes. Therefore, every 60 seconds we pause the calibration procedure and set the entire screen to all white. This resets the intensity levels and a new set of dark frame measurements is recorded. The calibration sequence is then allowed to continue.

Another issue with the plamsa monitor is that when a particular pixel is illuminated, the intensity of the adjacent pixels change. So when the next pixel is illuminated, that intensity is different compared to the intensity we measure if the adjacent pixel had not been turned on. In other words, turning on pixel  $n$  changes the intensity at pixel  $n + 1$  when it is turned on. In order to mitigate this effect, we created a psuedo-random sequence so that after a certain amount of time, the effect of a neighboring pixels activity is reduced. The total time to calibrate the SCOUT is approximately 20 minutes.

Remember that an isomorphic sensor is represented by the identity matrix. In comparison, in the SCOUT, the spatially varying blurred PSF leads to an approximate block-Toeplitz structure for the system matrix, with approximate Toeplitz structure within individual blocks due to the shifting PSF. This circulant structure is modified by random variations corresponding to the differing projections created by the two masks. Psuedo-case describing the calibration is given in Appendix C.

### 3.4.3 Reconstruction: $\ell_1$ regularized Least Squares Minimization

Given  $\Delta\mathbf{g}$  and  $\mathbf{H}$ , reconstructing the difference frame  $\Delta\mathbf{f}$ , is a highly underdetermined problem given no other prior knowledge. As discussed in Section 2.5, several important theoretical results show that it is possible to accurately recover  $\Delta\mathbf{f}$  if

the sparsity  $K$  is low relative to the number of measurements  $N_m$  and the RIP is satisfied. Inspired by these results, we turn to algorithms designed to solve the  $\ell_1$  regularized LS (lasso) problem:

$$\hat{\Delta f} = \arg \min_{\Delta f} \|\mathbf{H}\Delta f - \Delta g\|_2^2 + \tau \|\Delta f\|_1 \quad (3.10)$$

Given  $\Delta g$  and  $\mathbf{H}$ , the reconstruction algorithm finds a solution  $\hat{\Delta f}$  that minimizes this objective function.

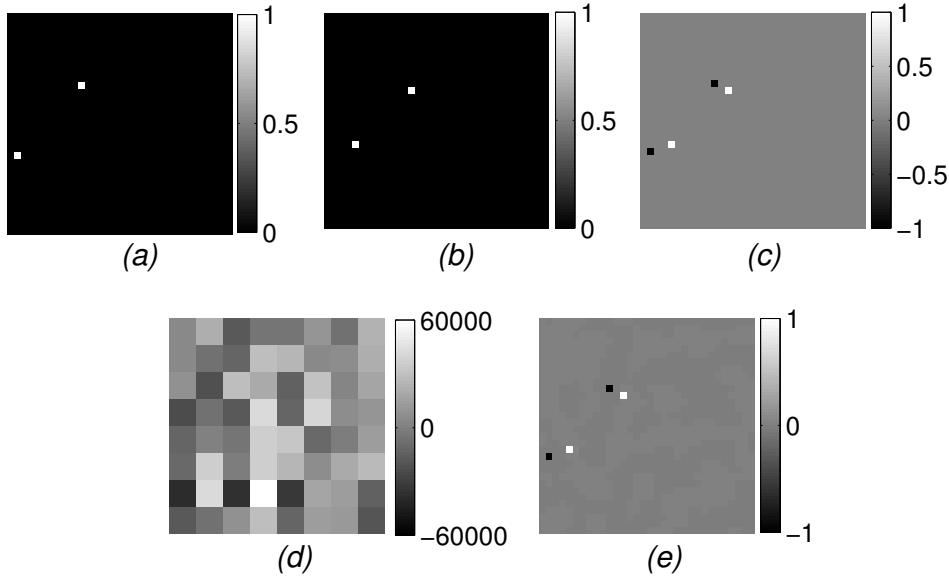
We used the `l1_ls` toolbox for MATLAB which implements an optimization technique based on Interior-Point methods [58]. The `l1_ls` function requires several input arguments:  $\Delta g$ ,  $\mathbf{H}$ ,  $\tau$  the regularization parameter, and a parameter called the relative tolerance, `rel_tol`. As I discussed in Section 2.5,  $\tau$  is a tuning parameter that is used to tell the optimization algorithm how much to weight the sparsity of the solution. Large  $\tau$  tend to drive the solutions towards lower values of sparsity,  $K$ . The `rel_tol` controls how well the solution should agree with the data. Low values of `rel_tol` tend to force the `l1_ls` to run many iterations until the a threshold has been reached. While large values of `rel_tol` tend to produce poorer reconstruction results but less optimization iterations.

We found that a regularization parameter of  $\tau = (1 \times 10^{-9}) \|2 \mathbf{H}_{cal}^T \Delta g\|_\infty$  works well for experimental reconstruction. Where  $\mathbf{H}_{cal}$  is the system matrix measured from calibration and  $\|\cdot\|_\infty$  is the infinity norm. The `rel_tol` is set to  $1 \times 10^{-4}$ .

Finding the correct regularization parameter is one of the major issues for many algorithms designed for compressive sensing. In our experiment, we had to run the reconstruction over many iterations with varying  $\tau$  in order to find the appropriate value. Unfortunately this also depends on the sparsity of the signal-of-interest. Therefore, large numbers of movers may have a different optimal value for  $\tau$ . The value of  $\tau$ , we reported works well from one to ten movers in our experiment.

#### 3.4.4 Experimental Results

Experimental results for a ten difference frame sequence is shown in Appendix B. The object scenes contains two dots (movers) changing position on a black background. Difference frame 1 of this sequence is shown in Figure 3.9. The top row shows two consecutive, before and after,  $f_1$  and  $f_2$ , frames of the scene and the ground-truth difference frame  $\Delta f$ , all at  $32 \times 32$  resolution. The bottom row shows the difference of corresponding  $8 \times 8$  measurement frames,  $\Delta g$ . Finally, the  $32 \times 32$  reconstructed difference frame is shown at the bottom right,  $\hat{\Delta f}$ .



**Figure 3.9:** A reconstruction of a  $32 \times 32$  scene with two movers of equal amplitude on a black background. (a) ground-truth scene 1 (b) ground-truth scene 2 (c) ground-truth frame difference and (d) measured  $8 \times 8$  frame difference, scaled so that it is discernible (e) reconstructed  $32 \times 32$  difference frame

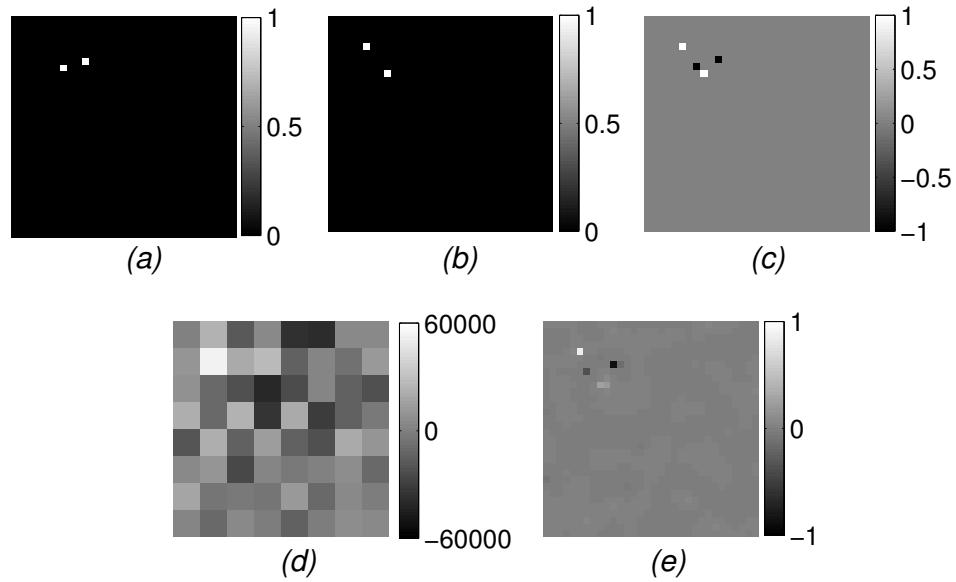
Initially, the amplitude of the movers in the estimated difference frame did not agree qualitatively with the amplitude of the ground truth difference frame. We realized that this was due to the fact that the exposure time during calibration was not the same as the exposure time during the actual experiment. By normalizing the system matrix obtained during calibration by the ratio of exposure times, we were able to demonstrate quantitative agreement with the ground-truth:

$$\mathbf{H}_{recon} = \frac{t_{exp}}{t_{cal}} \mathbf{H}_{cal} \quad (3.11)$$

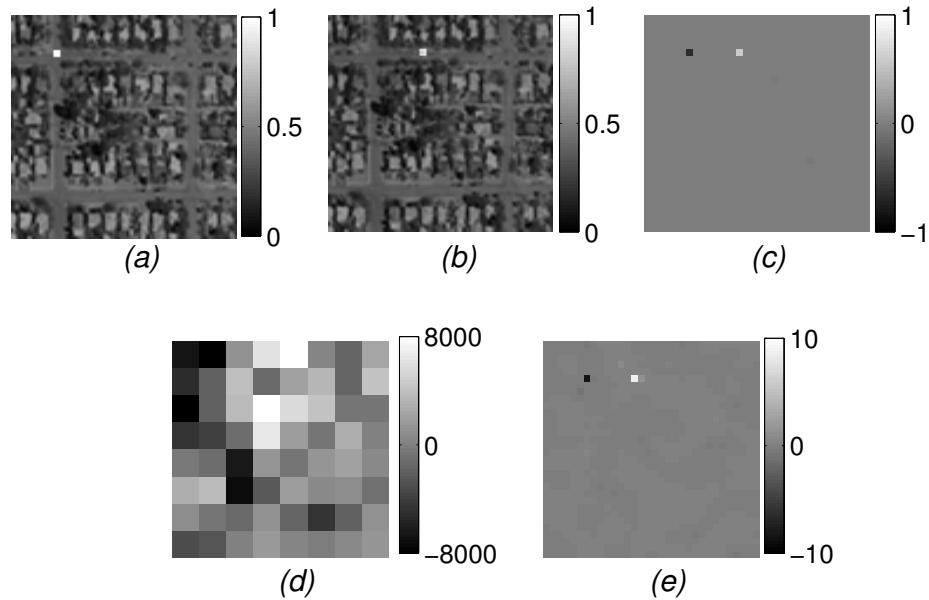
where  $t_{exp}$  and  $t_{cal}$  are the experiment and calibration exposure times, respectively. This scaling accounts for the physical effect of increased photon collection (and hence photodetector counts) as a function of increased exposure time. The resulting peaks are easily identified against background noise.

In the reconstruction of the ninth difference frame, the amplitude of one the movers had a lower amplitude, shown in Figure 3.10. Poor reconstruction tends to occur when two movers are located adjacent to each other in the ground-truth difference scene. This is an issue that can be traced to the system response matrix  $\mathbf{H}$ , locations next to each other have are more likely to have larger correlations in their respective PSF.

We also performed a more realistic experiment in which a mover simulates a



**Figure 3.10:** A reconstruction of  $32 \times 32$  scene with two movers of equal amplitude on a black background. This frame shows the results when the past and present mover locations are adjacent in the difference frame. (a) ground-truth scene 1 (b) ground-truth scene 2 (c) ground-truth frame difference and (d) measured  $8 \times 8$  frame difference, scaled so that it is discernible (e) reconstructed  $32 \times 32$  difference frame



**Figure 3.11:** Difference frame 1 of a video demonstration of compressive tracking of a  $32 \times 32$  difference scene with a non-zero background. Scene background ©2012 Google. (a) ground- truth scene 1 (b) ground-truth scene 2 (c) ground-truth frame difference and (d) measured  $8 \times 8$  frame difference, scaled so that it is discernible (e) reconstructed  $32 \times 32$  difference frame

vehicle driving on a street. This demonstrates that the SCOUT works well in situations with non-zero backgrounds. This sequence with the results for a single mover is also shown in Appendix B. The first difference frame of this sequence is shown in Figure 3.11. As seen in ground truth difference fram  $\Delta f$  shown in Figure 3.11(c), the amplitude of the past and present mover locations in the ground-truth are lower than the zero background case. Therefore there is also less contrast in  $\Delta g$  the difference measurements in Figure 3.11(d), which makes this case more sensitive to noise.

The most notable feature in the non-zero background results is less quantitative agreement with the ground-truth, even when the calibration matrix is scaled according to Equation (3.11). There are several reasons for this: Nonlinearities in the overall system response that result from a nonlinear monitor “gamma” (mapping from pixel value to output brightness) and inter-pixel interactions that effect brightness. These effects are not captured during calibration as that is performed point-by-point (thus reducing inter-pixel effects) and with pixels that are fully-on or -off (thus avoiding effects from monitor gamma). Another possible reason is over-multiplexing, since the total light from each frame is increased, there is less dynamic range in the FPA, and therefore detector non-linearity may be a source of error. Despite the lack of quantitative agreement, qualitative agreement is excellent and the movers are clearly identifiable againts the background in Figure 3.11(e).

### 3.5 Conclusion

While the SCOUT architecture is well-suited for tracking applications, it does have limitations which make it less useful for general imaging applications. Without sparse scene motion, the priors used in reconstruction will lead to incorrect results. Reconstructions only show the locations of moving objects, and the sensing platform must be stationary relative to the scene so that frame differences are sparse. However, more sophisticated techniques could potentially estimate platform motion. Despite the limits of the SCOUT, the architecture is well-suited for applications such as fixed-camera wide-area surveillance where bandwidth, data volume, and cost are key concerns.

Many of the theoretical guarantees for compressive sensing is not specialized or tuned for the block-circulant system matrix. As I mentioned in Chapter 2, random coding has several theoretical properties that make them useful for compressive

sensing. There has been some research work to investigate system matrices with Toeplitz and circulant structure [67, 68, 69], however there has been relatively little work published discussing the approximately block-Toeplitz structure that naturally arises in optical systems such as SCOUT and theoretical guarantees like the ones force random coding. Two exceptions are [70, 71], which provide both theoretical evidence for the viability of CS system matrices with block-Toeplitz structure.

A completely parallel compressive imager would require as many encoding optical elements as simultaneous measurements. The SCOUT architecture eliminates this scaling issue by giving up the ability to implement arbitrary projections. Using a pair of masks at different distances to create a block-circulant system matrix, the system makes compressive measurements and reconstructs frame differences. The system can be optimized by adjusting system parameters such as mask pitch and defocus distance. Simulations demonstrated the use of the a modified coherence parameter as an efficient predictor of system matrix performance to optimize these parameters. An experimental system based on the SCOUT architecture successfully performed compressive motion tracking on scenes with zero and nonzero backgrounds in most instances. However, the reconstruction of difference scenes with adjacent mover locations caused issues due to the design or calibration of the system matrix. The system showed promising results using a general  $\ell_1$ -norm minimization algorithm and we believe that further research on sparse reconstruction with block-circulant system matrices may decrease reconstruction error. We also believe that non-isomorphic calibration techniques and adding further degrees of freedom in the design parameters could result in significant performance gains.

## Chapter 4

### Adaptive Feature Specific Spectral Imaging-Classifier

#### 4.1 Motivation

As I discussed in Chapter 1, the spectrometer is one most of the widely used sensors in the history of mankind. This is because materials have unique spectra, by measuring the spectrum of a material and then comparing it to a database of known spectra one can quickly identify the test material. Spectrometers have become the main tool used for identifying materials for defense [72, 73], security [74, 75], and medicine [76, 77].

By combining the spectrometer with the camera, the spectral imager produces a spectral datacube, a three dimensional representation of the scene consisting of two spatial dimensions and a spectral dimension [78, 79]. By measuring both spatial and spectral information from an object scene, spectral imaging allows for improved discrimination of objects in a scene [80, 81, 82]. In this chapter, I will introduce the Adaptive Feature Specific Spectral Imaging-Classifier (AFSSI-C), a computational imaging system which directly computes the spectral classification at each spatial location in a scene.

One of the major design trade-offs of an isomorphic spectral imaging sensor is that one must acquire a three-dimensional spectral datacube using a two-dimensional FPA [78]. Traditional isomorphic systems rely on a point-by-point acquisition technique to acquire the entire spectral datacube. A spotlight or whiskbroom technique simultaneously measures the entire spectrum from a single spatial location. This is repeated for each location until the spectral datacube is completely acquired [83]. A pushbroom technique uses measures the spectrum of a spatial row (or column) in a two dimensional object scene at a time. This is repeated until all the rows (or columns) in the spectral datacube is acquired [84, 83]. A tunable filter technique, such as the Fabry-Perot interferometric filter [85, 86, 87], simultaneously measures a single spectral channel but over the entire field-of-view, scanning through the spectral dimension [88] .

A typical spectral datacube has a significant amount of measurement samples, for example, an airborne spectral imaging instrument called the Airborne Visible /

Infrared Imaging Spectrometer (AVIRIS) system, acquires  $R_x \times R_y = 677$  spatial locations and  $N_\lambda = 224$  spectral channels [89], producing a spectral datacube with  $N \approx 10^9$  measurement samples in 10 minutes.

Just like with the traditional spectrometer and camera, researchers have turned computational sensing for spectral imaging. These architectures use the Fellgett advantage (multiplexing) and *Jacquinot advantage* (open aperture) to improve the SNR and use a computational step to reconstruct the spectral datacube  $\mathcal{F}$  from non-isomorphic measurements. Some spectral imaging architectures also leverage compressive sensing.

One of the early examples of computational sensing in spectral imaging is the Computed tomography imaging spectrometer (CTIS) [90]. The CTIS can reconstruct the spectral datacube  $\mathcal{F}$  from a single FPA exposure by take multiple measurements of the spectral datacube simultaneously. The CTIS uses several gratings to create two-dimensional projections of the three-dimensional hyperspectral datacube. According to the central slice theorem, the two-dimensional Fourier Transform of each projection is a plane through the three-dimensional frequency space representing the spectral datacube. Ideally, one must collect enough projections to fully reconstruct the three dimensional frequency representation of the spectral datacube. The three-dimensional real-space distribution of the spectral datacube is then recovered through an inverse 3D Fourier transform. However, in practice only a finite subset of projections are recorded and missing information is must be inferred. In the CTIS, the missing information is recovered by maximizing the likelihood of the measurement data using the expectation-maximization algorithm [91, 92]. The CTIS maybe considered compressive in that the number of measurement samples is less than the object dimensionality of the spectral datacube according to the practical definition of compressive sensing. However, it does not make any assumptions of sparsity or incoherence.

In another example of a computational sensing spectral imaging is the Coded Aperture Snapshot Spectral Imaging (CASSI) sensor. In the CASSI, a coded aperture and spatially codes the spectral datacube  $\mathcal{F}$ . The dispersive element then creates a projection of the spectral datacube that maps three-dimensional information into a two-dimensional image at the FPA. Unlike the CTIS, only one two-dimensional projection is recorded per FPA readout which allows for higher spatial resolution for the same detector array. Using calibration data and prior knowledge of sparsity, the post-processing step solves the lasso problem to reconstruct the spectral

datacube [31, 93]. Often a total-variation regularization is also invoked to improve reconstruction of the spatially varying image [94, 95].

The task for most spectral imaging is material classification [80, ?, ?]. However the CTIS, the CASSI, and all other computational spectral imaging architectures use the post-processing step to reconstruct the spectral datacube [96]. Just like the traditional spectral imaging architectures, they produce a significant amount of data. Once the spectral datacube is reconstructed, the spectrum at each spatial location is compared to known spectra to make a classification.

The Adaptive Feature Specific Spectrometer (AFSS) was the earliest known spectrometers to use the techniques of computational sensing for direct spectral classification [48].

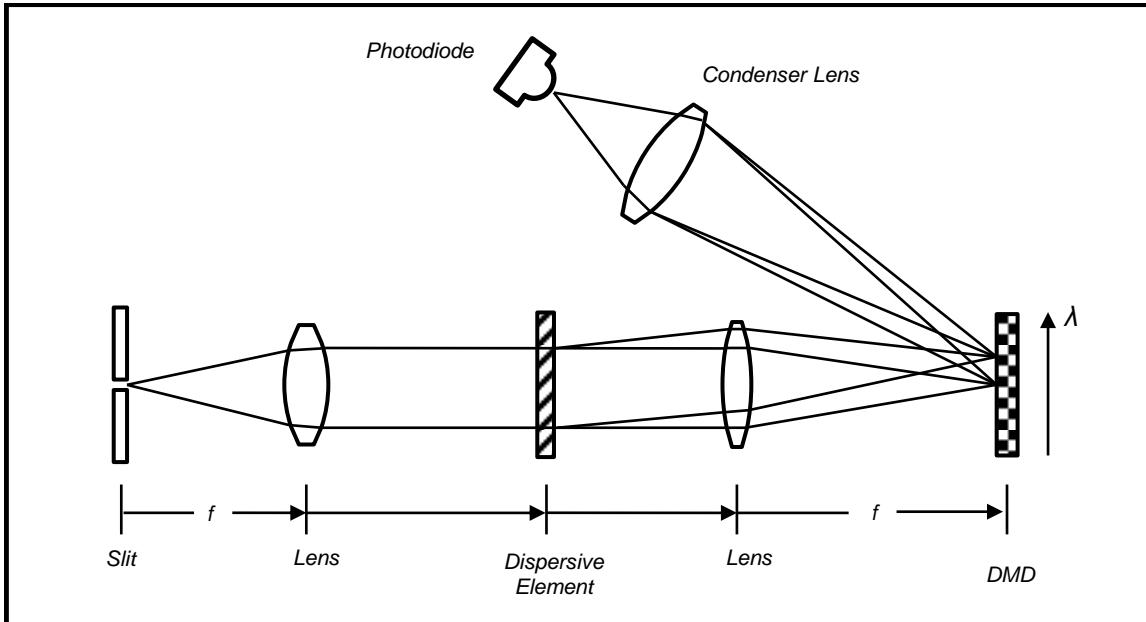
By utilizing adaptive spectral features and a sequential Bayesian update for hypothesis testing, the AFSS significantly improves spectroscopic classification accuracy over traditional slit spectrometers without reconstructing the spectrum.

The AFSSI-C extends this concept first demonstrated by the AFSS to spectral imaging. The AFSSI-C directly classifies the spectrum at each spatial location with the reconstruction of the spectral datacube. By adopting a task-specific sensing approach, the AFSSI-C greatly improves classification accuracy and simultaneous reducing transmission and storage requirements. Further more, the architecture of the AFSSI-C leverages both the Fellgett and Jacquinot advantage like many other computational spectral imaging architectures utilizing significantly more light than the traditional systems mentioned above.

## 4.2 Architecture

Before discussing the architecture of the AFSSI-C I want to quickly review the architecture of the AFSS, is shown in Figure 4.1. Unlike the traditional slit spectrometer, the AFSS images the dispersed slit onto a DMD. The mirrors of the DMD can then be adjusted to selectively reflect certain wavelengths towards the condenser lens, which then focuses light onto a single detector element [48].

In order to create an imaging version of the AFSS, one may attempt to extend the AFSS architecture by simply forming an parallel array of AFSS sensors to achieve classification across a spatial scene. However, like the proposed parallel single-pixel camera design in Chapter 3, this approach would significantly increases the SWAP-C of the design. The AFSSI-C provides a similar feature-based measurement approach



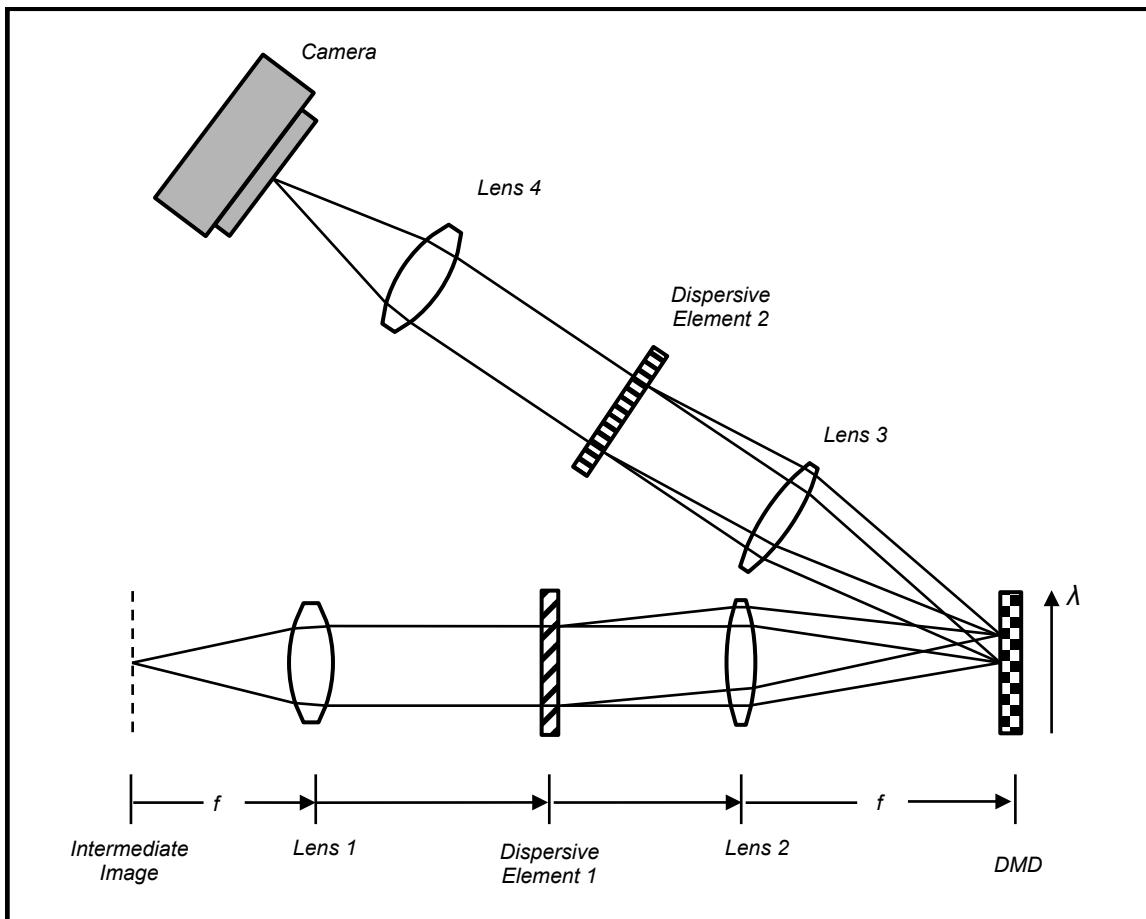
**Figure 4.1:** Blah blah blah.

and Bayesian framework but with a more compact architecture.

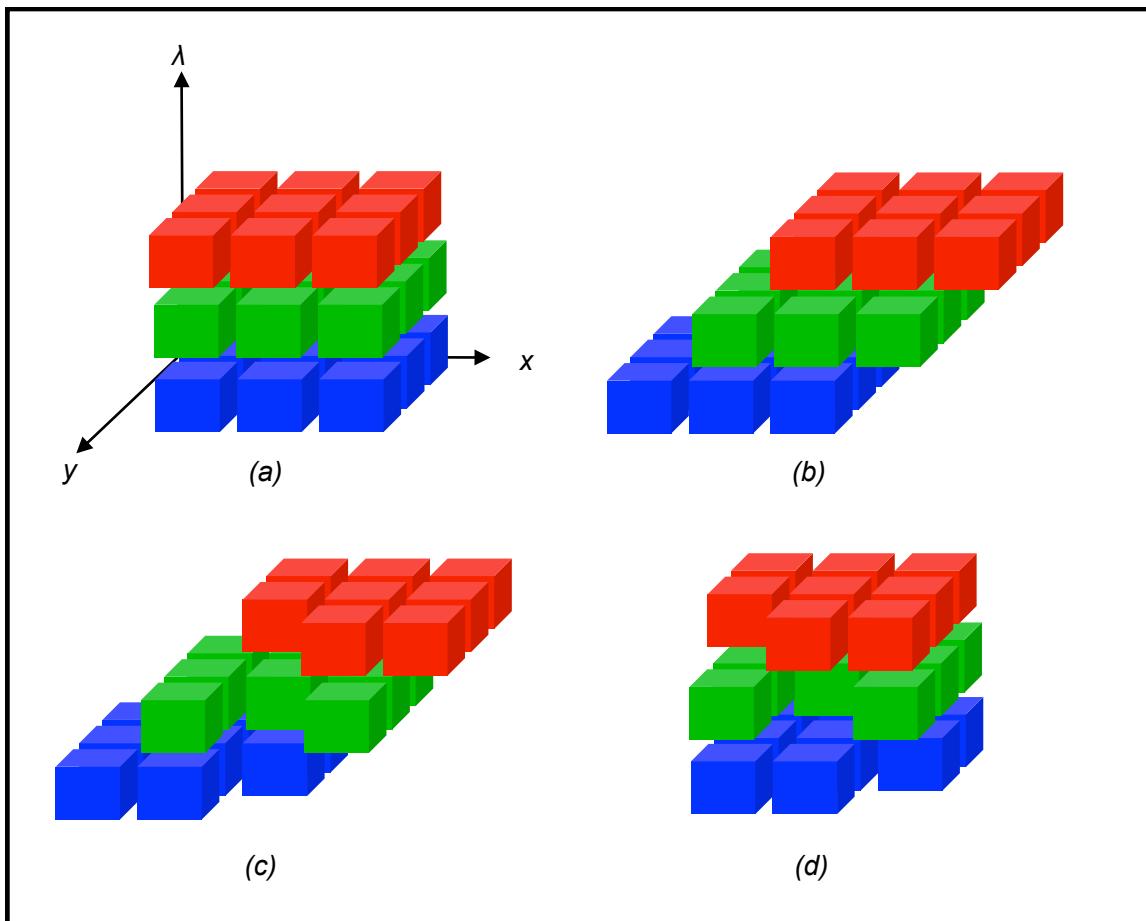
Rather than a fully parallel version of the AFSS, the optical design of the AFSSI-C uses a single DMD and a single set of lenses and dispersive elements. Not only does this approach share resources across multiple spatial locations, it avoids the expense of pixel-specific components.

The design of the AFSSI-C is essentially two  $4f$  open-aperture monochromators back-to-back, shown in Fig. 4.2. A DMD divides the two halves. An objective lens (not shown) creates an intermediate image at the input plane of the instrument. At this point in the system one can imagine the source spectral datacube as depicted in Figure 4.3(a), where  $x$  and  $y$  are the spatial axes, and  $\lambda$  the spectral axis. The first lens of the system collimates the light. The first grating disperses the light. The second lens then images spectrally dispersed copies of the intermediate image at the DMD. Just prior to being reflected from the DMD, one can imagine the spectral datacube as being sheared at an angle in the direction of the dispersion, see Figure 4.3(b). We implement mirror patterns on the dense array of micromirrors at the DMD which either allow the light to continue to the rest of the system, or block it by sending it to a beam dump, on a mirror-by-mirror basis. This pattern encodes the datacube, portrayed in Figure 4.3(c) as holes punched through the sheared cube.

The now-encoded signal is once again collimated before hitting the second grating, which is identical to the first, but with the dispersion direction flipped so as to undo the applied dispersion. This removes the shear in the encoded spectral data-



**Figure 4.2:** An objective lens forms the intermediate image of the object scene at the input plane of the instrument. The first lens collimates the light and a diffraction grating disperses the light. A second lens images spectrally dispersed versions of the image of the object scene onto the DMD. The DMD directs light to a beam dump or reflects the light towards the third lens on a mirror-by-mirror basis. Collimated light from third lens is sent through a second grating, and finally imaged onto the detector by the fourth lens.



**Figure 4.3:** (a) The input cube is (b) sheared by the first grating, (c) encoded at the DMD, and finally (d) spatially re-registered by the second grating.

acube, as depicted in Figure 4.3(d). The final lens in the system focuses that result onto the detector array, which integrates the cube through the spectral dimension. The result at each pixel is the inner product of the source spectrum at that location in the scene with a spectral filter—the implemented feature vector—imposed on that location by the mirror pattern on the DMD.

We chose to use a dual-disperser (DD) architecture rather than the single-disperser architecture such as the one in the CASSI since the mirror patterns on the DMD acts as spectral filters for each spatial location. In the single-disperser design the spatially-varying spectral encoding is more appropriate for parallel direct classification, as the measurements can be mapped one-to-one with the spatial locations in the scene, allowing for parallel operation of the Bayesian inference approach, rather than having to solve a single larger joint inference problem.

The mirror pattern at the DMD gives rise to the spectral filters that act at each spatial location in the scene. We turn to a system model to understand this relationship. The system model, and the relationship between the pixelation of the detector and the pixel size at the DMD. We start with this model, and extend it to provide the restriction imposed on the feature design.

#### 4.2.1 Forward Model

If we consider a source spectral density of  $S_0(x, y; \lambda)$  at the input aperture and assume unit magnification throughout the optical system, we can write the measurements at location  $(n, l)$  on the detector array as

$$\begin{aligned} \Gamma_{nl} = & \sum_{n'l'} \iiint \text{rect}\left(\frac{x}{\Delta} - l, \frac{y}{\Delta} - n\right) \text{rect}\left(\frac{x - \alpha(\lambda - \lambda_c)}{\Delta} - l', \frac{y}{\Delta} - n'\right) \\ & \times T_{n'l'} S_0(x, y; \lambda) dx dy d\lambda. \end{aligned} \quad (4.1)$$

where  $\Delta$  is the pixel (mirror) size on the DMD and the FPA,  $T$  is an array that describes the pixelated mirror pattern on the DMD,  $\alpha$  is the linear dispersion of the gratings, and  $\lambda_c$  is the center wavelength of the system. The first rectangular function represents the finite pixel size of the FPA at pixel coordinates  $(n, l)$ . The second rectangular function represents how the spectral density is sheared: each value of  $x$  is shifted the amount corresponding the distance  $\alpha(\lambda - \lambda_c)$ .

As will be shown later, the system relies on calibration which accommodates deviations from these assumptions.

If we analyze two constrained cases, we can gain an understanding of how the spectral filter influences the measured intensity. We first consider a monochromatic source  $S_0(x, y, \lambda) = I_0(x, y) \delta(\lambda - \lambda_c)$ , where  $I_0$  is the intensity distribution of the monochromatic scene. In this case, Eq.(4.1) simplifies to

$$\begin{aligned} \Gamma_{nl}(\lambda = \lambda_c) &= \sum_{n'l'} \iiint \text{rect}\left(\frac{x}{\Delta} - l, \frac{y}{\Delta} - n\right) \text{rect}\left(\frac{x}{\Delta} - l', \frac{y}{\Delta} - n'\right) \\ &\quad \times T_{n'l'} I_0(x, y) \delta(\lambda - \lambda_c) dx dy d\lambda \\ &= \sum_{n'l'} \delta_{ll'} \delta_{nn'} T_{n'l'} I_{nl} \\ &= T_{nl} I_{nl}, \end{aligned} \quad (4.2)$$

where  $I_{nl}$  is a spatially pixelated version of the monochromatic source with intensity distribution  $I_0(x, y)$

Now we consider a case with the monochromatic source is shifted by a spectral channel  $\Delta\lambda = \Delta/\alpha$ . Then,

$$\begin{aligned} \Gamma_{nl}(\lambda = \lambda_c + \Delta\lambda) &= \sum_{n'l'} \iiint \text{rect}\left(\frac{x}{\Delta} - l, \frac{y}{\Delta} - n\right) \text{rect}\left(\frac{x}{\Delta} - (l' + 1), \frac{y}{\Delta} - n'\right) \\ &\quad \times T_{n'l'} I_0(x, y) \delta(\lambda - (\lambda_c + \Delta\lambda)) dx dy d\lambda \\ &= \sum_{n'l'} \delta_{ll'} \delta_{nn'} T_{n'(l'+1)} I_{nl} \\ &= T_{n(l-1)} I_{nl} \end{aligned} \quad (4.3)$$

where we find that a shift by a spectral channel results in a shift in the mirror pattern.

For a natural scene with content spanning the spectral range, we can consider spectral channel index  $\kappa$  out of  $C$  total spectral channels. We can also define a discretized source spectral datacube  $S_{nl\kappa}$ , and then the detector signal  $\Gamma_{nl}$  as a result of mirror pattern  $T$  acting on the pixelated source is

$$\Gamma_{nl} = \sum_{\kappa=0}^{C-1} T_{n(l+\kappa)} S_{nl\kappa}, \quad (4.4)$$

which shows the measurement at each pixel being the inner product of the source spectrum and the feature vector which results from the mirror pattern. If we look at an adjacent pixel on the detector,  $\Gamma_{n(l+1)}$  we find that

$$\Gamma_{n(l-1)} = \sum_{\kappa=0}^{C-1} T_{n(l+1+\kappa)} S_{n(l+1)\kappa}. \quad (4.5)$$

The spatial location  $(n, l)$  sees the effect of the pattern in mirror locations  $T_{nl}$  to  $T_{n(l+C-1)}$ , while the neighboring spatial location at  $n, (l + 1)$  is encoded by the mirror pattern from  $T_{n(l+1)}$  to  $T_{n(l+C)}$ . What we notice is that the mirror pattern for neighboring pixels overlap, and have the mirror pattern from  $T_{n(l+1)}$  to  $T_{n(l+C-1)}$  in common. Essentially what each source location sees is a spectral filter formed by a length  $C$  segment of a mirror pattern which spans the entire row, with the neighboring location seeing a length  $C$  segment of that underlying pattern offset by 1.

#### 4.2.1.1 Simple Example

Imagine a spectral datacube with dimensions  $R_x \times R_Y \times R_\lambda = 2 \times 2 \times 2$ . Thus the spectral datacube has two discrete spatial locations in the  $x$  and  $y$  direction. Also imagine that the FPA has a readout resolution of  $r_x \times r_y = 2 \times 2$

The overlap of the spatial and spectral information at the DMD disallows independent feature vectors for each spatial location. The spectral filters imposed by the DMD pattern are unique for every spatial location, but *cannot* be implemented independently, requiring the features to be designed *jointly* for spatial locations along a row.

### 4.3 Adaptive Classification Algorithm

The AFSSI-C uses adaptive features designed from information in previous measurements to make a classification decision from hypothesis spectra in a spectral library. This library is common to all spatial locations, and it is helpful to first look at the process of feature design and classification decision for a single spatial location. We can then expand the analysis to include the entire scene, building from the single-location tool set.

The measurement at each detector pixel is compared to the spectral library, subject to the spectral filter implemented at that spatial location. A probability is assigned to each hypothesis in the library using Bayes' theorem. The conditional probability of hypothesis  $\mathbf{h}_i$  given the measurement history up to the  $k^{th}$  measurement  $\{m\}_k$ , can be written as:

$$P(\mathbf{h}_i | \{m\}_k) = \frac{P(\{m\}_k | \mathbf{h}_i) P(\mathbf{h}_i)}{P(\{m\}_k)}. \quad (4.6)$$

The probabilities are assigned and updated using a Gaussian noise model and log-likelihood ratios, as implemented by the AFSS in [?]. The probability assignment

is on a per-pixel basis and is independent of the probability assignment of adjacent spatial locations in the AFSSI-C.

Features are designed to yield measurements which discriminate between the hypotheses with the greatest probability. To this end we use a modification of principal component analysis (PCA) that employs the updated probability estimates of each hypothesis as a weighting factor. We consider this an intuitively reasonable approach, keeping in mind that the first principal component (PC) is an eigenvector of the scatter matrix, along the direction of greatest variance in the library spectra [?]. By taking the inner product of the spectra at each location with this first eigenvector, we significantly separate the possible measurement outcomes, facilitating discrimination. Using standard PCA does not allow for informing subsequent measurements with previous results, so we modify PCA as follows.

At each individual pixel we create a scatter matrix with  $R$  spectral hypotheses, with individual spectrum  $\mathbf{s}_r$ , weighted in relation to the prior probability associated with each hypothesis given the measurement history. The individual scatter matrices  $\mathbf{Q}(k)$  at each spatial location with spectral library element hypothesis  $\mathbf{h}_r$  take the form

$$\begin{aligned} \mathbf{Q}(k) &= \sum_{r=1}^R P(\mathbf{h}_r | \{m\}_k) (\mathbf{s}_r - \bar{\mathbf{s}}) (\mathbf{s}_r - \bar{\mathbf{s}})^T \\ &= \mathbf{X}(k) \mathbf{X}^T(k). \end{aligned} \quad (4.7)$$

Here  $\mathbf{X}(k)$  is the matrix of weighted spectral elements, where the row index  $i$  is from 1 to the number of spectral channels  $C$ , with columns  $j$  from 1 to  $R$  as follows,

$$\mathbf{X}_{ij}(k) = \sqrt{P(\mathbf{h}_j | \{m\}_k)} (\mathbf{s}_{ij} - \bar{\mathbf{s}}_i), \quad (4.8)$$

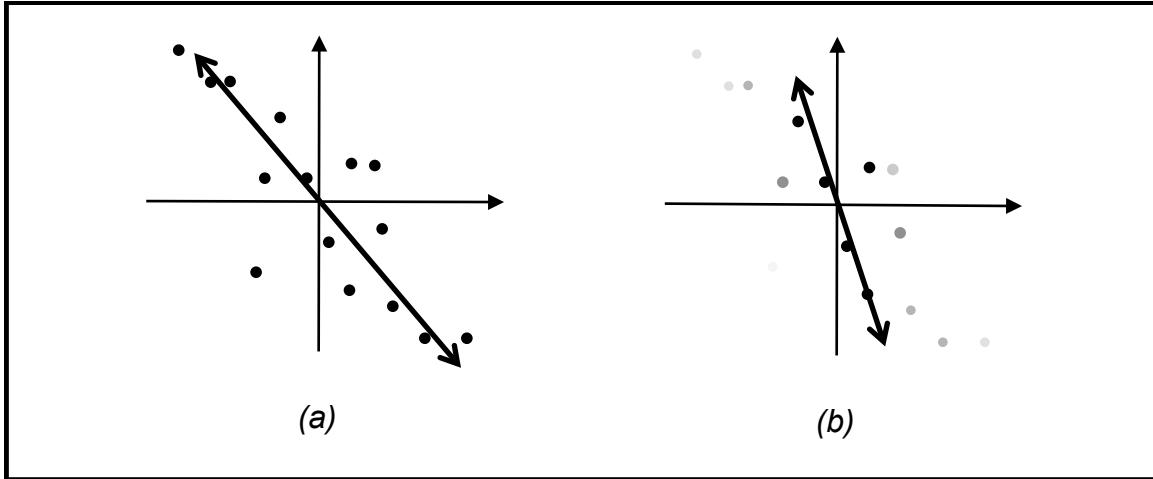
and  $\bar{\mathbf{s}}$  is the probabilistically-weighted sum of the spectral library:

$$\bar{\mathbf{s}} = \sum_{r=1}^R P(\mathbf{h}_r | \{m\}_k) \mathbf{s}_r. \quad (4.9)$$

We can then compute the first eigenvector of  $\mathbf{Q}(k)$ , analogous to PCA. We call this probabilistic-PCA or pPCA, and in the case of the AFSS this eigenvector becomes the feature for the next measurement. The scatter matrix  $\mathbf{Q}(k)$  is then updated with every measurement.

The effect this has on the first PC is illustrated in the two-dimensional (i.e. a spectral library with two spectral channels) example in Fig. 4.4. In Fig. 4.4

(a) each hypothesis is equiprobable, whereas in Fig. 4.4(b) the hypotheses are probabilistically-weighted after the first measurement, showing a new direction for the first PC vector. In the case of the AFSS [?], the features derived from this PC vector allow the system to further discriminate between the most likely library spectra when making a classification decision.



**Figure 4.4:** Depiction of the pPCA (simple 2D example). (a) First principal component before a measurement has been made. All of the hypotheses are equiprobable, depicted here as all points having the same grayscale value. (b) After a measurement has been made: the darker points are more probable hypotheses, with the less probable hypotheses taking on lighter shades of gray. The first principal component has now been shifted to the direction of greatest variation in the weighted data.

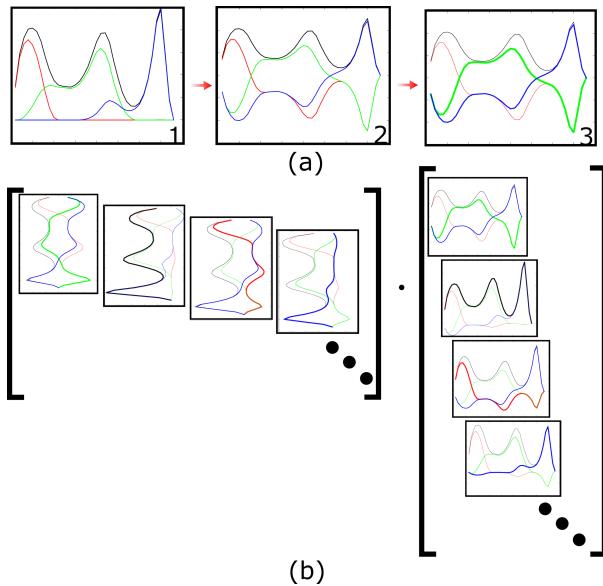
As discussed above, the AFSSI-C system architecture mixes spatial and spectral information at the coding plane in a way that requires joint design of the mirror pattern on each row. Therefore, pPCA is further modified by instead using the matrix  $\tilde{\mathbf{X}}_{uv}(k)$ , constructed from the single-location probabilistically weighted hypothesis matrices  $\mathbf{X}_{ij}(k)$  from each spatial location ( $l'$ ) in a row ( $n'$ ). The individual  $\mathbf{X}_{ij}(k)$  matrices become block elements in this much larger matrix, with each block offset in  $v$  by the appropriate value of  $l'$ . The  $\mathbf{X}_{ij}(k)$  matrices for neighboring spatial locations share  $C - 1$  columns in this larger matrix, which represents the overlap of spatial and spectral information at the DMD as illustrated by the system model discussion. Figure 4.5(b) illustrates the stacking of the elements of the mean-centered, weighted library spectra from Fig. 4.5(a) into a larger array  $\tilde{\mathbf{X}}(k)$ . We arrive at a joint scatter matrix similar in form to Equation (4.7),

$$\tilde{\mathbf{Q}}(k) = \sum_{\tilde{r}=1}^{\tilde{R}} (\tilde{\mathbf{x}}_{\tilde{r}}(k) - \bar{\tilde{\mathbf{x}}}(k)) (\tilde{\mathbf{x}}_{\tilde{r}}(k) - \bar{\tilde{\mathbf{x}}}(k))^T, \quad (4.10)$$

where  $\bar{\tilde{\mathbf{x}}}$  is the mean of each column in  $\tilde{\mathbf{X}}$ , and the sum is over the library elements

$\tilde{r}$  from all of the row locations. The first PC of  $\tilde{\mathbf{Q}}(k)$  is a vector pointing in the direction of greatest variation in the probability-weighted data for the entire row. We repeat this process for all of the rows in the datacube to arrive at the features to be implemented for the subsequent measurement. We refer to this feature design method as joint-pPCA.

With the system able to take advantage of prior information to adapt features for the subsequent measurement, the AFSSI-C is able to accurately and rapidly determine pixel-level classification. For this work, the classification decision after each measurement is given by the maximum a-posteriori probability (MAP) estimate (the mode of the probability mass function)[?] of the hypothesis spectra at each location. We now look at the components and design of the experimental system.



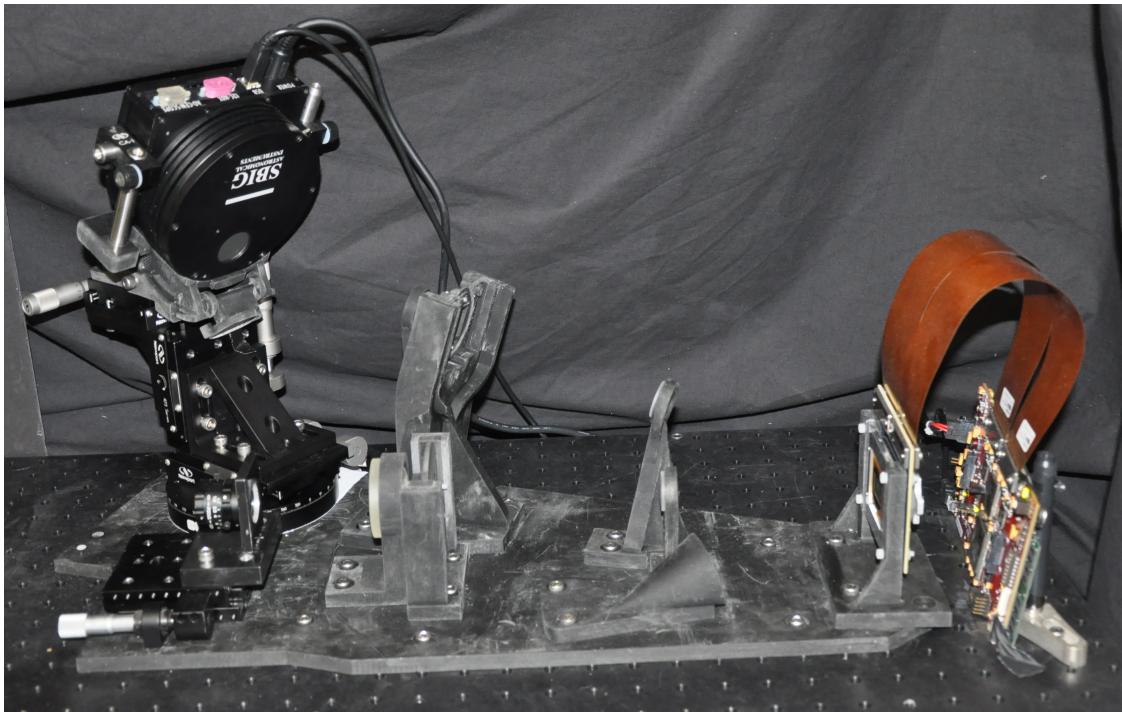
**Figure 4.5:** Joint-pPCA schematic. (a) The pictorial illustration of the formation of  $\mathbf{X}(k)$  from Equation(4.7). The hypothesis spectra (1) are centered around the mean (2), and given a weight based on their probabilities (3). (b) The joint-pPCA calculation involves the stacking of the  $1, \dots, C - 1$  elements of  $\mathbf{X}_{i,j}(k)$  for each location  $(n', l')$  along a row into a larger matrix  $\tilde{\mathbf{X}}_{uv}(k)$ . The final joint-pPCA scatter matrix is formed from  $\tilde{\mathbf{X}}(k)$  multiplied by its mean-centered transpose, to arrive at scatter matrix  $\tilde{\mathbf{Q}}(k)$ . The first principal component of this much larger scatter matrix is then in the direction of greatest variation in the joint-position data.

#### 4.4 Experiments

The goal of the AFSSI-C effort was to design and build a system that would yield direct classification and outperform traditional spectral imaging systems in classification accuracy. This comparison is to be performed via simulation, so we must

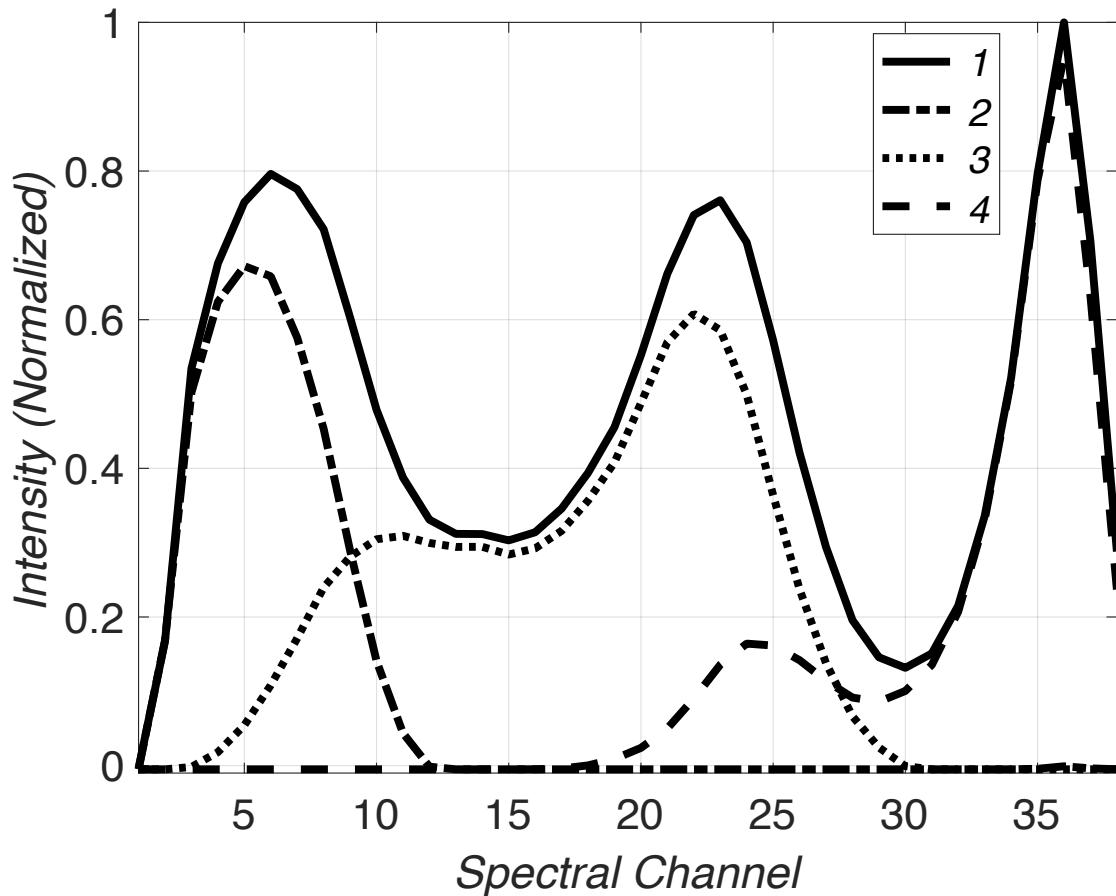
validate our ability to simulate the real world performance of such a system. Thus, we first compare the experimental results of the AFSSI-C system (Fig. 5) with simulation. This allows for confident comparison to the conventional approaches.

To be convinced in our experimental corroboration of the simulation results, we need to be able to claim agreement for different levels of classification difficulty. To this end, we corrupt the experimental measurements in software with white Gaussian noise, and hence we manipulate the difficulty of classification. As in [32], the experimental results reported here are for a 4-class problem, with an input spectral datacube of  $64 \times 64$  spatial pixels and 38 spectral channels. Figure 6 is an illustration of the spectral source used, with the associated 4-class spectral library.



**Figure 4.6:** Photo of AFSSI-C

While this spectral datacube is small compared to those used in remote sensing, the implemented size was driven by practical considerations regarding the source, DMD and detector on hand. The dual-disperser architecture, in general, places no significant limitation on possible datacube sizes. Similarly, the processing involved in the Bayesian inference and feature design are computationally lightweight and do not create a computational limit on datacube size.



**Figure 4.7:** The spectral library consists of four spectral classes: the white, red, green, and blue of the LED monitor.

#### 4.4.1 Hardware

Certain considerations were made before fabrication and assembly of the experimental AFSSI-C system. Here we outline some of the design decisions and consequences of those decisions.

Lenses are off-the-shelf achromatic doublets to avoid the need for custom fabrication. This also limited the degrees of freedom in the optical design, requiring the design focal lengths to match available lenses. A compact, fixed focal length, lens (Edmund Optics Stock No. 58-001,  $f = 12\text{mm}$ ) is used as an objective lens, relaying the object onto an intermediate image plane. A fast entrance optic is needed to meet the layout and magnification requirements. Referring to Fig. 1, lenses 1 and 4 are 75 mm focal length achromatic doublets with a 50 mm diameter (Edmund Optics Stock No. 49-291), and lenses 2 and 3 are 150 mm focal length achromatic doublets with 25 mm diameter (Edmund Optics Stock No. 47-643).

For a repeatable, updatable synthetic datacube source, we use an LED display



**Figure 4.8:** Four class spectral source used for the AFSSI-C experiment.

(Dell P2311H LED monitor with  $248\mu m$  pixel pitch). Though this limits the spectra we are able to generate, it still allows for programmable spectra at every spatial location. The center  $1080 \times 1080$  pixels are used to generate the source spectral datacubes. Spectra consist of combinations of the RGB monitor colors.

The design spectral range is 425-625nm; filters were placed in the collimated space to attenuate light outside of this range. The system is designed for 38 spectral channels, resulting in roughly 5nm/spectral channel. The system magnification to the DMD, which then dictates the lateral spread allowed per spectral channel, requires custom  $0.10$  lines  $\mu m$  holographic blaze gratings as the dispersive elements, fabricated by Wasatch Photonics. The gratings are designed to minimize diffraction in all the orders except the first order.

The DMD is a Texas Instruments DLP Discovery 4100 DMD development kit, with the DLP9500 0.95" 1080p DMD chipset. The DMD has  $1080 \times 1920$   $10.8\mu m$  mirrors on the array, and the mirrors pivot 12 degrees on a diagonal axis. The DMD is oriented such that the bottom of the array is parallel to the optical table, which forces the second arm of the AFSSI-C to rise off the optical table at an angle of 17.5 degrees; this orientation was chosen so that the mirrors would be oriented as squares

rather than diamonds. While the periodic structure of the DMD can produce strong diffraction for certain types of illumination, no diffraction effects are observed in the AFSSI-C as the light striking the DMD is highly incoherent.

An SBIG ST-10XME detector with a  $2184 \times 1472$ ,  $6.8 \mu\text{m}$  pitch CCD array is used as the detector array. Because of the angle of the optical axis at the detector, a goniometer was constructed using a rapid prototyping 3D printer to facilitate easy alignment of the CCD array.

Because we are interested in a quantitative system analysis, we compare measurements on the discretized detector to what was projected by our discretized source. The layout dimensions, component pixel size, and lens design were tuned to yield pixel groups—referred to here as system pixels—at each component that are an integer number of the component pixel, or in the case of the DMD, integer number of mirrors. We therefore have the following system pixel dimensions:  $16 \times 16$  pixels on the source,  $8 \times 8$  DMD mirrors, and  $12 \times 12$  pixels at the detector.

Once the optical layout was finalized, the physical system was designed in SolidWorks. The lens mounts, detector mount, DMD mount, beam dump, and locating plates were then fabricated on a Eden 350 rapid prototyping 3D printer.

Light baffling is utilized to shield the system from ambient light as well as stray light within the system. A baffling structure was designed and printed to surround the detector, with smaller baffling elements to attenuate stray light around the optical paths.

#### 4.4.2 Calibration

As previously mentioned in [?], calibration is fundamental for the functioning of a computational imaging system as the AFSSI-C. Here we will elaborate on the derived challenges.

A measurement at the detector must be compared to the source to assess system performance, but the DMD geometry creates a tilted object plane for the second arm of the AFSSI-C. The DMD plane is normal to the optical axis of the first arm, but it is at an angle (equal to twice the tilt of the mirrors on the diagonal) to the second arm. We can think of the DMD plane as the object for the second arm of the system. This object is extended along the optical axis of the second arm, which causes keystone distortion at the detector as explained by the Scheimpflug condition [?]. The distortion is rectified by a mapping routine which creates fiducial markers

on the source. The points are registered to the corresponding image on the detector, and a lookup table can then be used to map detector pixels to the source locations.

The optical system has aberrations, and there are intensity variations across the measured ROI of the source. The system is therefore calibrated for spectral response. This is done any time physical adjustments to the system have been made. System calibration involves activating each of the available colors on the source, and then sweeping a single column of ‘on’ system pixels (i.e., angled to send light to the detector) across the DMD. A datacube consisting of the spectral response at each spatial location is compiled from the measurements. Knowledge of the spectral response of the system is used to accommodate aberrations and imperfect recombination of the spectral signal at the second grating.

Finally, a map of the source brightness is determined at the beginning of each experiment to account for spatial variations in the spectral throughput. This map is created by turning the entire DMD to ‘on’ and measuring the intensity at each spatial location from a white source. Subsequent measurements rely on this flat field measurement to accommodate for the spatially varying illumination response of the system.

#### 4.4.2.1 Spatial Calibration

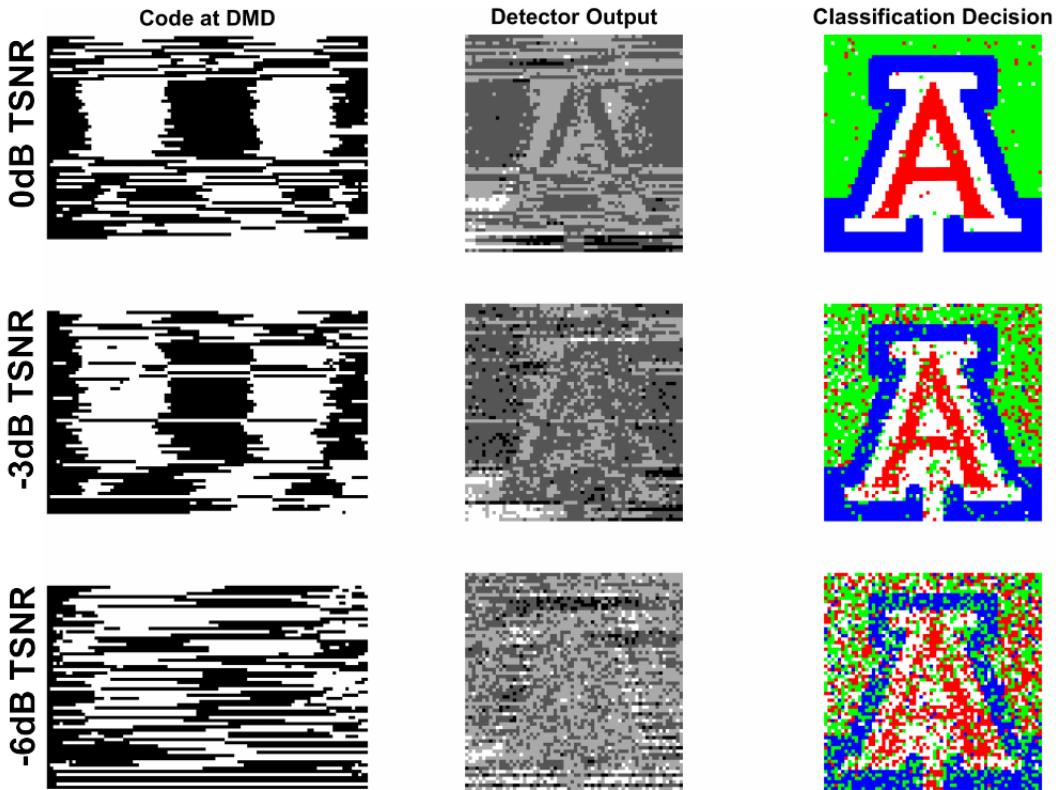
#### 4.4.2.2 Spectral Calibration

#### 4.4.2.3 Noise Model Calibration

### 4.5 Experimental Results

Figure 4.9 presents a snapshot of a video (see **Visualization 1**) comparing system performance at different TSNR levels. As the classification difficulty increases, the system takes longer to correctly classify. However, the AFSSI-C feature-design process intelligently adjusts the codes to focus attention on uncertain spatial locations

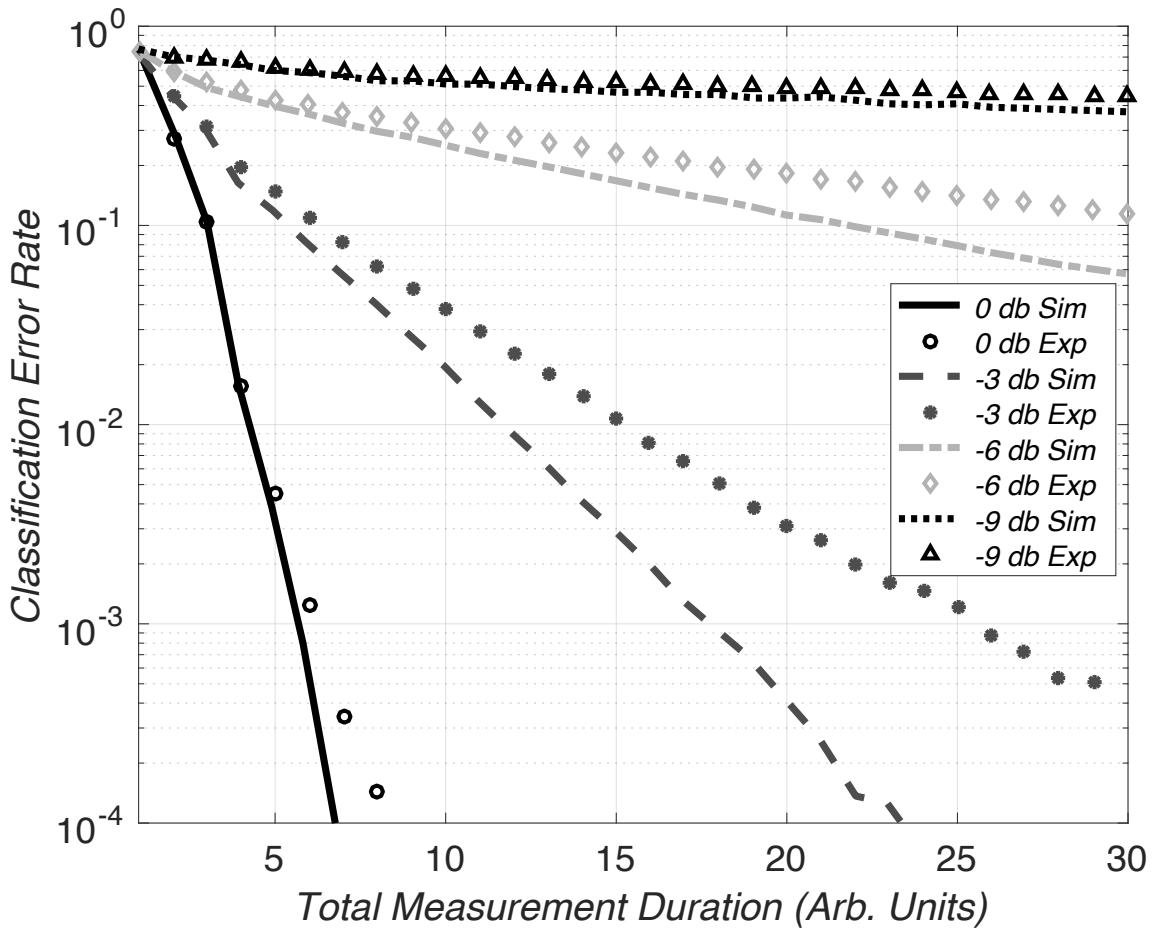
Figure 4.10 shows the comparison between the AFSSI-C system experiment results and the simulated values. The simulated and experimental data are the average of multiple runs, i.e., 30 simulations and 10 experiments, for each of the four TSNR values representing octaves of classification difficulty (0, -3, -6, and -9dB TSNR). Figure 4.10 shows good agreement between the simulated and measured classification accuracy. This agreement allows us to compare the performance of the AFSSI-C with traditional systems via simulation. We can then assess the gain in performance over these traditional scanning systems.



**Figure 4.9:** Frame from a movie (see **Visualization 1**) showing experimental results for three different levels of TSNR, over the course of 30 measurements. The left column is a depiction of the DMD code, center is the output from the detector, and the right is the classification decision at the current measurement.

Figure ?? compares the AFSSI-C to traditional scanning spectral imaging systems. It also compares different feature design modalities. To test feature designs, the adaptive, joint-pPCA designed features are compared to static, pseudo-random features. The traditional systems that were investigated as simulations are the pushbroom, whiskbroom, and tunable filter systems. The performance of the simulated traditional systems follows intuition—a whiskbroom system has to sweep over all 4096 spatial locations, while the pushbroom and tunable filter system only make 64 and 38 scanning steps, respectively. This explains the greater SNR and hence greater classification accuracy of the tunable filter system, with the whiskbroom system being least accurate of the three. Note that the sequential nature of the measurements in the AFSSI-C limits its applicability to those scenes which are slowly varying with respect to the time needed to achieve a desired classification accuracy.

In this manuscript, we are explicitly considering the case where the spectral library is completely known—there are no ‘nuisance parameters’ such as amplitude variations of the spectra—and we are investigating the performance of the AFSSI-C

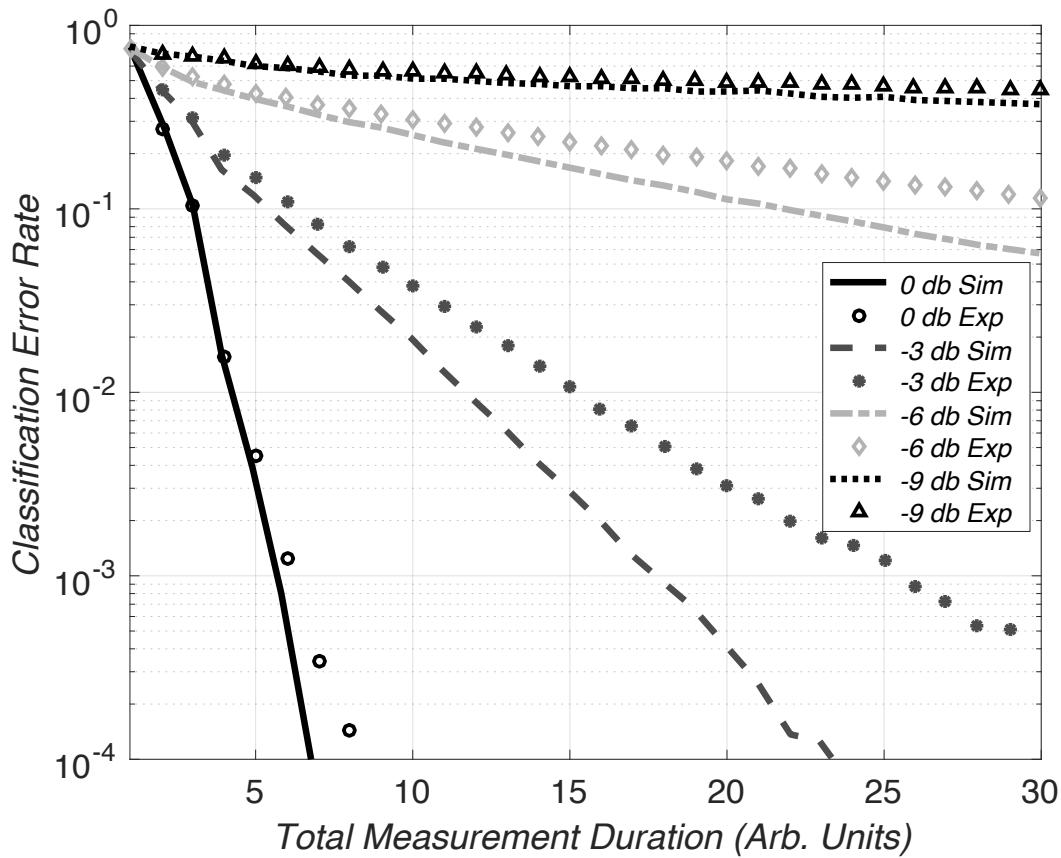


**Figure 4.10:** Comparison of the AFSSI-C experimental system results to the simulation results for multiple TSNR levels by plotting the classification error versus measurement. Shown are repeated experiments of a  $64 \times 64 \times 38$  spectral datacube and a 4-class library.

in this baseline scenario. However, there do exist methods for addressing nuisance parameters in Bayesian inference schemes [?, ?], which could be incorporated into the design and inference framework of the AFSSI-C. Alternatively, a single uncoded measurement would capture the total signal energy at each spatial location and the library could be locally normalized to the appropriate value prior to proceeding with the algorithm described here.

There are a number of phenomena which give the AFSSI-C an advantage over traditional systems. When comparing the AFSSI-C system with joint-pPCA designed features to traditional systems at the 5<sup>th</sup> measurement in Fig. 4.11, we see that the classification accuracy improves by  $250 \times$ . This improvement in performance is attributed to a combination of factors such as the open aperture architecture of the AFSSI-C design, lack of scanning, and adaptivity.

Figure 4.11 also demonstrates the benefit of using joint-pPCA to design spectral



**Figure 4.11:** Simulation comparing the classification performance for different measurements at  $\text{TSNR} = 0$  for different systems: the AFSSI-C with designed features (joint pPCA), the AFSSI-C with random features, the traditional pushbroom imager, the traditional tunable filter imager, and the traditional whiskbroom imager. The input is a  $64 \times 64 \times 38$  spectral datacube with a 4-class library.

features that discriminate between the possible hypothesis spectra. Looking again at the 5th measurement, we see a  $100 \times$  performance gain relative to static, pseudo-random coding. The performance curve for the random coding case is generated by directly classifying from the acquired measurements using an identical Bayesian inference framework. The information processing inequality of information theory [3] guarantees us that the alternative approach of classifying after datacube reconstructions can do no better than direct classification. Thus, the separation of these two curves represents the true performance improvement arising from adaptive measurement, while the separation between the static-coded curve and the traditional systems represents the performance improvement arising from the increased open aperture. Moreover, we expect further improvement in classification accuracy for larger systems as the traditional systems become even more starved for light, having to sweep through even larger spatial arrays. In all, these simulated results indicate

that there is great potential for the AFSSI-C system to outperform traditional systems where classification is the desired result of the analysis.

#### 4.6 Conclusion

In this chapter, I discussed the practical considerations of direct spectral classification using the AFSSI-C, a spectral imager classifier that utilizes adaptive spectral features in a resource-lean configuration. We are able to show multiple order-of-magnitude improvement in classification accuracy compared to traditional spectral imaging systems when the noise in the system is equal to the minimum separation between the library spectra, by employing a robust system simulation corroborated with experimental results. By taking advantage of its adaptiveness, the AFSSI-C performance with designed features also achieves multiple order-of-magnitude improvement over a random feature implementation. These adaptive features are designed via Bayesian inference and a novel joint-probabilistic PCA approach, which drives the measurement decision evolution to boost the discrimination ability between spectra candidates at every spatial location.

Direct classification is a useful modality for many of the applications of spectral imaging. By making measurements of an encoded datacube instead of explicit measurement of every element, huge performance gains are realized. It is reasonable to imagine the AFSSI-C system being of great benefit to a number of industries that rely on *in situ* material classification. Further work is underway to test the system with larger spectral libraries, as well as a second generation system based on a transmissive spatial light modulator (SLM). Using a transmissive SLM will reduce keystone distortion, and simplify the optical path.

## Chapter 5

### Computational Spectral Unmixing

This chapter introduces the reader the computational spectral unmixer.

## Chapter 6

### Conclusion

This chapter concludes the dissertation.

## Appendix A

### Derivation of the Least Squares Estimator

Suppose

$$\mathbf{g} = \mathbf{Ax} \quad (\text{A.1})$$

Given  $\mathbf{g}$  and  $\mathbf{A}$  we want to solve for  $\mathbf{x}$ . If the matrix is full rank then we can simply multiply both sides of equation A.1 by  $\mathbf{A}^{-1}$

$$\mathbf{A}^{-1}\mathbf{g} = \mathbf{A}^{-1}\mathbf{Ax} = \mathbf{Ix} = \mathbf{x} \quad (\text{A.2})$$

where  $\mathbf{I}$  is the identity matrix.

If  $\mathbf{A}$  is not full rank then its inverse does not exist. However we can try to find a solution  $\hat{\mathbf{x}}$  that minimizes the squared error. This is called the *Least Squares Solution* also known as the *Least Squares Estimator*, *Ordinary Least Squares* and by many other names. We define the squared error as

$$\|\epsilon\|^2 = \|\mathbf{Ax} - \mathbf{g}\|^2 \quad (\text{A.3})$$

To minimize the error, we take the derivative of equation A.3 with respect to  $\mathbf{x}$  and set it equal to zero and solve for  $\mathbf{x}$ . Note that the equation A.3 can be expanded in terms of an inner product

$$\|\epsilon\|^2 = \|\mathbf{Ax} - \mathbf{g}\|^2 = \sum_{i=1}^N \epsilon_i^2 = \epsilon^T \epsilon = (\mathbf{Ax} - \mathbf{g})^T (\mathbf{Ax} - \mathbf{g}) \quad (\text{A.4})$$

The transpose is distributive

$$(\mathbf{Ax} - \mathbf{g})^T = (\mathbf{Ax})^T - \mathbf{g}^T \quad (\text{A.5})$$

The transpose of a product of matrices equals the product of their transposes in reverse order

$$(\mathbf{Ax})^T = \mathbf{x}^T \mathbf{A}^T \quad (\text{A.6})$$

So equation A.4 becomes

$$\begin{aligned}\|\epsilon\|^2 &= (\mathbf{x}^T \mathbf{A}^T - \mathbf{g}^T)(\mathbf{Ax} - \mathbf{g}) \\ &= \mathbf{x}^T \mathbf{A}^T \mathbf{Ax} - \mathbf{x}^T \mathbf{A}^T \mathbf{g} - \mathbf{g}^T \mathbf{Ax} + \mathbf{g}^T \mathbf{g}\end{aligned}\tag{A.7}$$

We can see that the two middle terms  $\mathbf{x}^T \mathbf{A}^T \mathbf{x} = \mathbf{g}^T \mathbf{Ax}$  because they are just scalars.

$$\|\epsilon\|^2 = \mathbf{x}^T \mathbf{A}^T \mathbf{Ax} - 2\mathbf{g}^T \mathbf{Ax} + \mathbf{g}^T \mathbf{g}\tag{A.8}$$

To find the least squares solution, take the gradient with respect to  $\mathbf{x}$  and set it equal to zero.

It should be noted that there are two different notations for writing the derivative of a vector with respect to a vector  $\frac{\partial \mathbf{y}}{\partial \mathbf{x}}$ . If the numerator  $\mathbf{y}$  is of size  $m$  and the denominator  $\mathbf{x}$  of size  $n$ , then the result can be laid out as either an  $m \times n$  matrix or  $n \times m$  matrix, i.e. the elements of  $\mathbf{y}$  laid out in columns and the elements of  $\mathbf{x}$  laid out in rows, or vice versa. They are both correct and equal, which leads to confusion when switching back and forth. I will write both to reduce confusion.

Clearly the gradient of the third term in equation A.8 w.r.t  $\mathbf{x}$  is 0, so it goes away. We first tackle the first term on the right hand side in equation A.8

$$\frac{\partial}{\partial \mathbf{x}} \mathbf{x}^T \mathbf{A}^T \mathbf{Ax}\tag{A.9}$$

Let  $\mathbf{K} = \mathbf{A}^T \mathbf{A}$ . Since  $\mathbf{K}$  is symmetric, we can use the identity

$$\frac{\partial}{\partial \mathbf{x}} \mathbf{x}^T \mathbf{K} \mathbf{x} = 2\mathbf{x}^T \mathbf{K} = 2\mathbf{K}^T \mathbf{x}\tag{A.10}$$

since  $\mathbf{K} = \mathbf{K}^T$  then

$$\frac{\partial}{\partial \mathbf{x}} \mathbf{x}^T \mathbf{A}^T \mathbf{Ax} = 2\mathbf{x}^T \mathbf{A}^T \mathbf{A} = 2\mathbf{A}^T \mathbf{Ax}\tag{A.11}$$

and the gradient of the middle term in equation A.8 is simply  $-2\mathbf{A}^T \mathbf{g}$  so

$$\frac{\partial}{\partial \mathbf{x}} \|\epsilon\|^2 = 2\mathbf{A}^T \mathbf{Ax} - 2\mathbf{g}^T \mathbf{A}\tag{A.12}$$

setting it equal to zero and solving for  $\mathbf{x}$  gives the least squares estimate

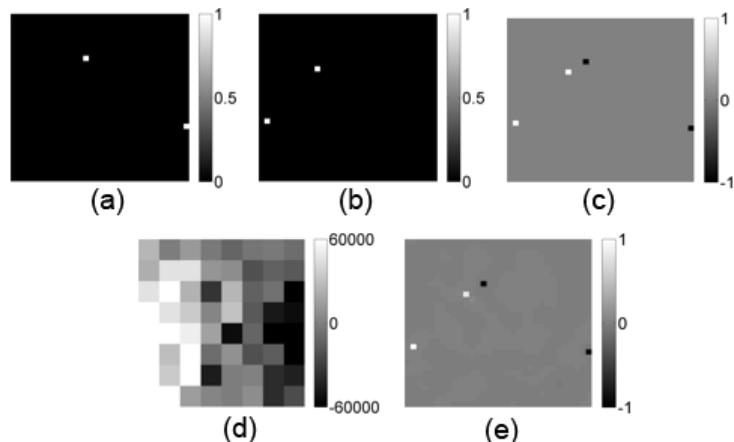
$$\hat{\mathbf{x}} = (\mathbf{A}^T \mathbf{A})^{-1} \mathbf{A}^T \mathbf{g}\tag{A.13}$$

## Appendix B

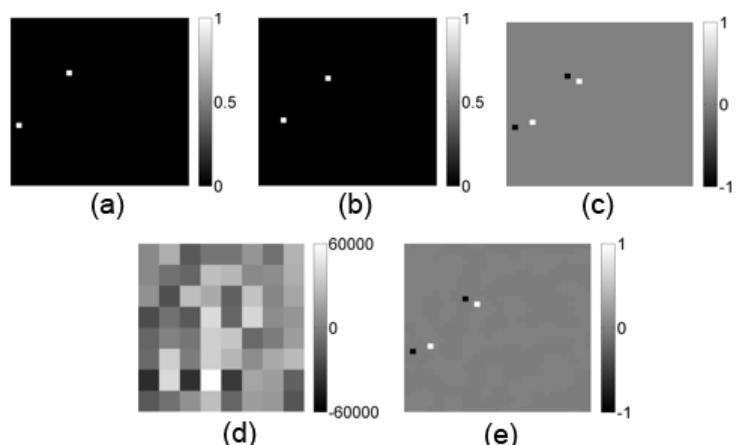
### SCOUT Experimental Results

This appendix contains the experimental reconstruction results of two movers in 10 difference frames from the zero (black) background SCOUT data. It also contains the experimental reconstruction results of one mover in 10 difference frames from non-zero (black) background.

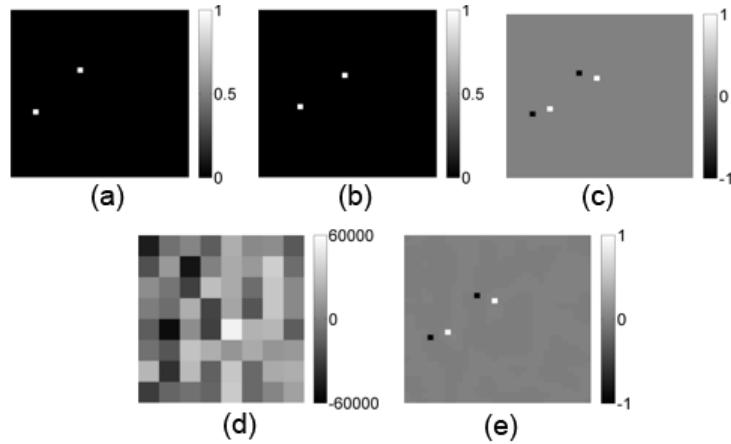
#### B.1 Zero Background Difference Frames



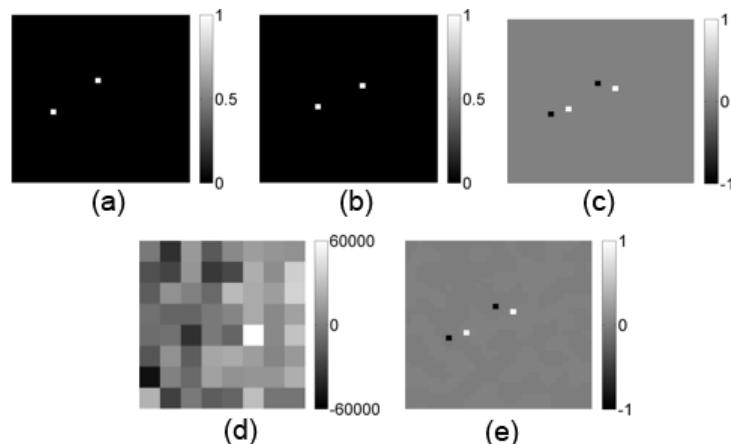
**Figure B.1:** Difference frame 1 of a sequence of one mover on a black background.



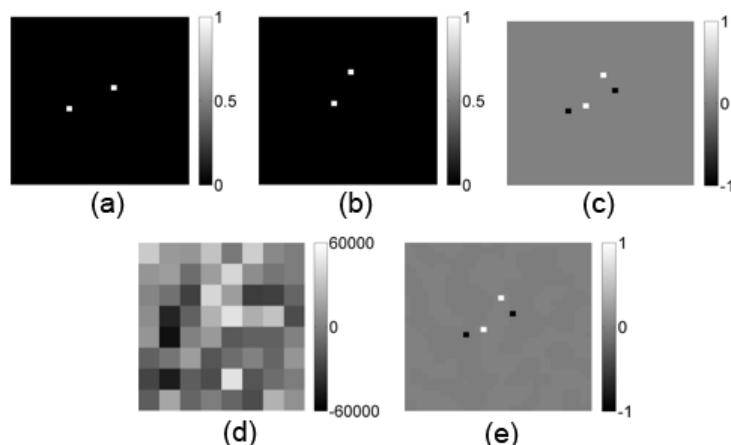
**Figure B.2:** Difference frame 2 of a sequence of one mover on a black background.



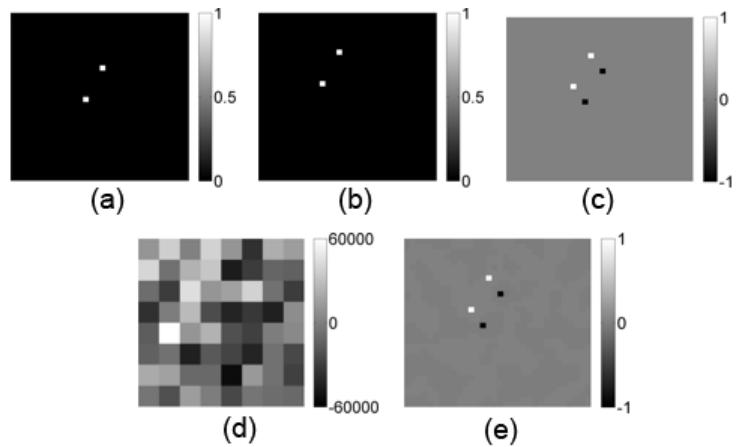
**Figure B.3:** Difference frame 3 of a sequence of one mover on a black background.



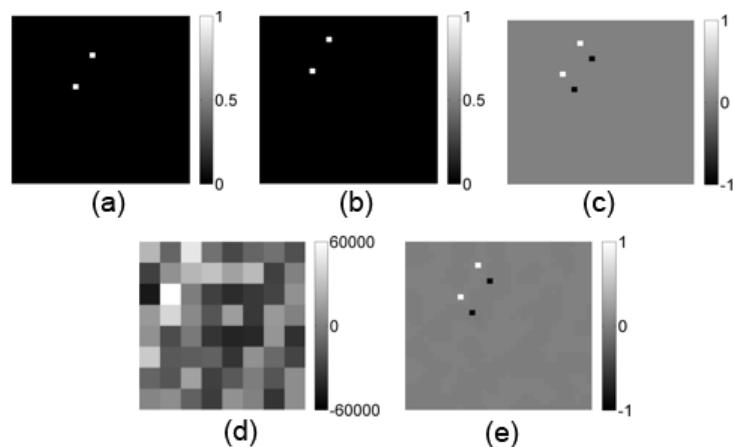
**Figure B.4:** Difference frame 4 of a sequence of one mover on a black background.



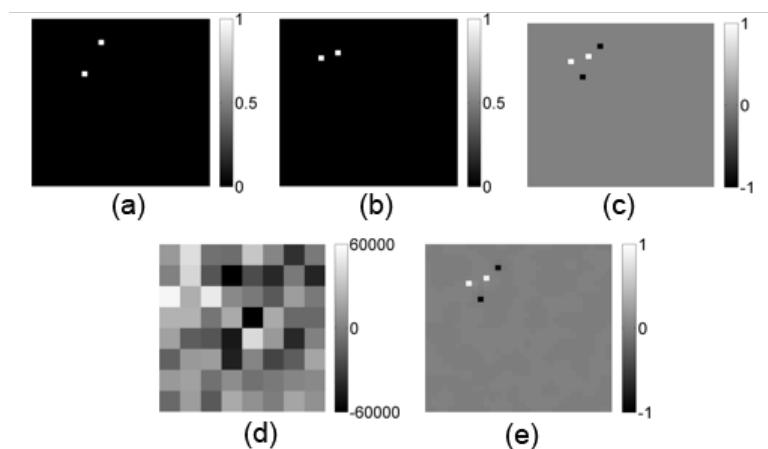
**Figure B.5:** Difference frame 5 of a sequence of one mover on a black background.



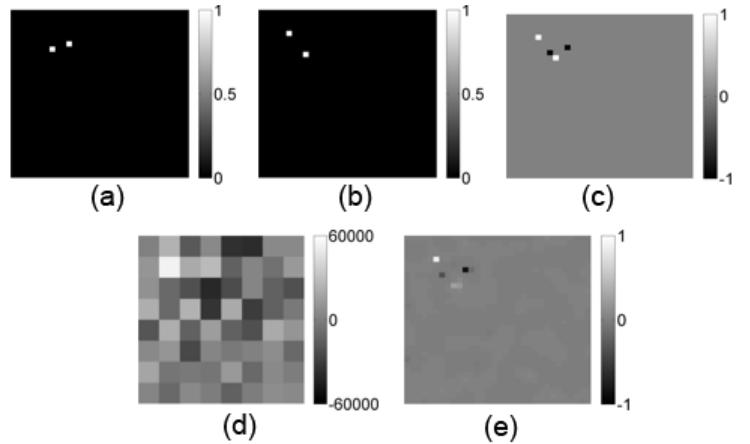
**Figure B.6:** Difference frame 6 of a sequence of one mover on a black background.



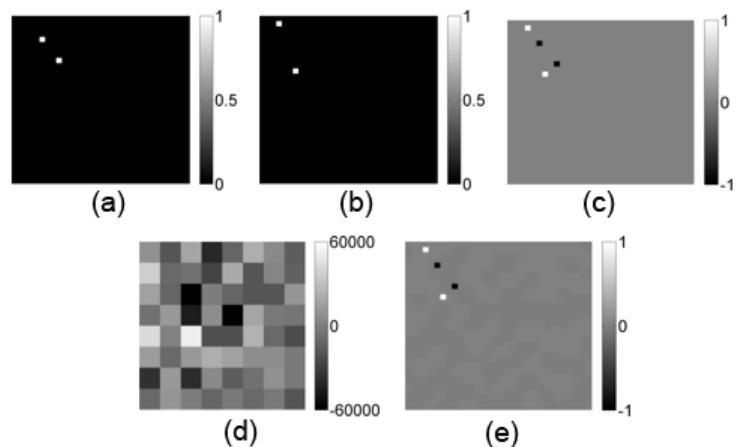
**Figure B.7:** Difference frame 7 of a sequence of one mover on a black background.



**Figure B.8:** Difference frame 8 of a sequence of one mover on a black background.

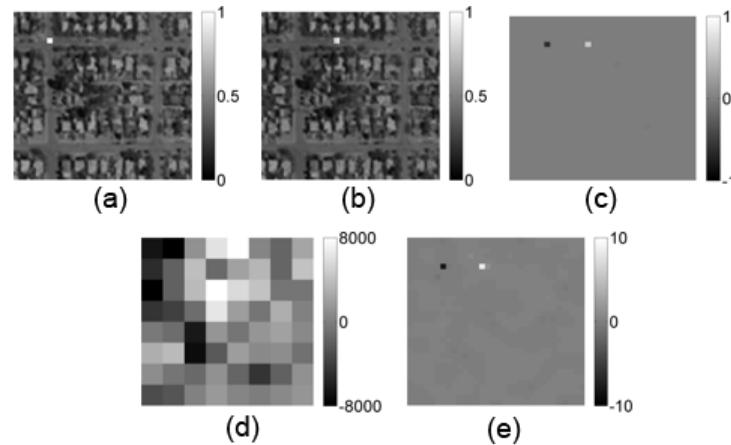


**Figure B.9:** Difference frame 9 of a sequence of one mover on a black background.

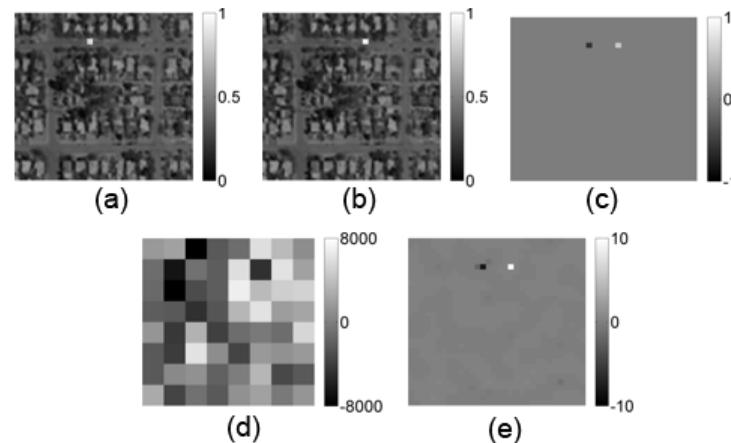


**Figure B.10:** Difference frame 10 of a sequence of one mover on a black background.

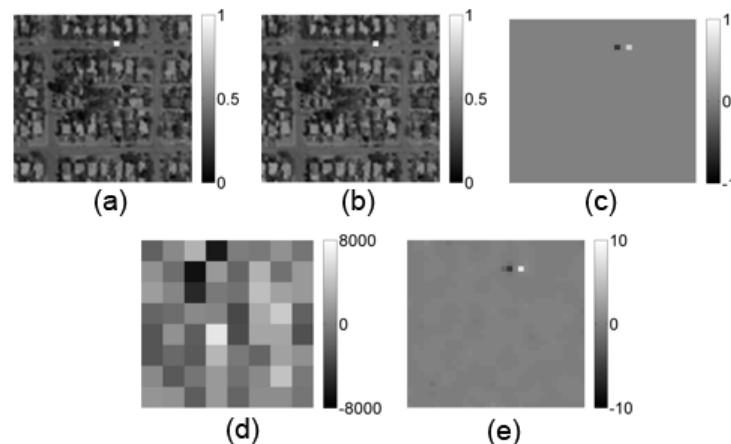
## B.2 Non-Zero Background Difference Frames



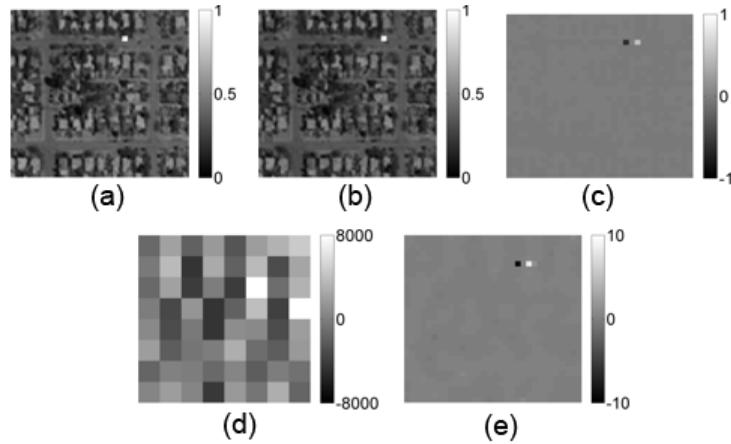
**Figure B.11:** Difference frame 1 of a sequence of one mover on a non-zero background.



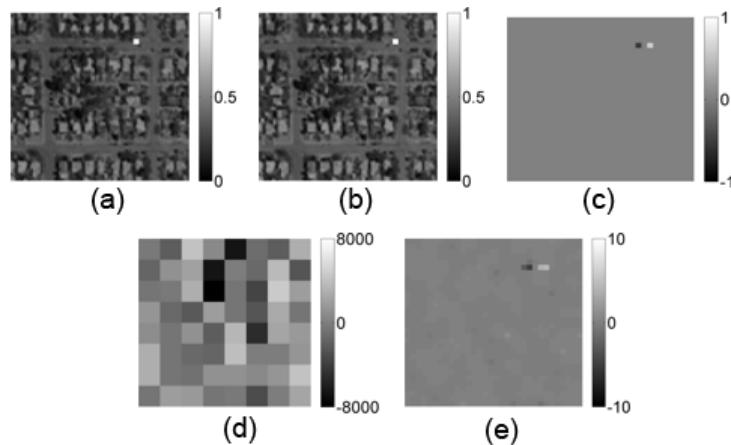
**Figure B.12:** Difference frame 2 of a sequence of one mover on a non-zero background.



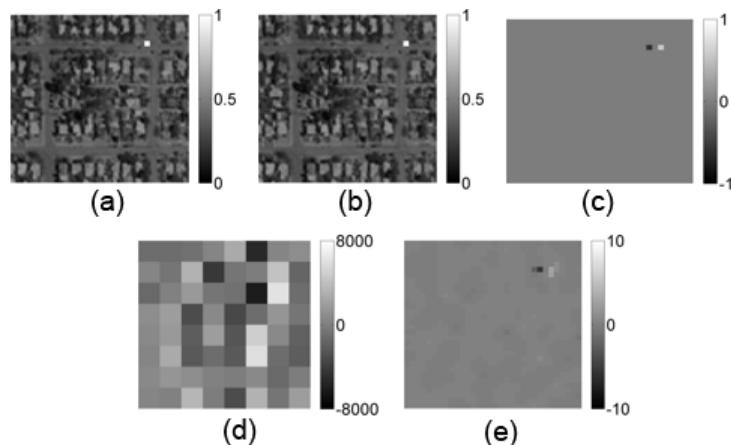
**Figure B.13:** Difference frame 3 of a sequence of one mover on a non-zero background.



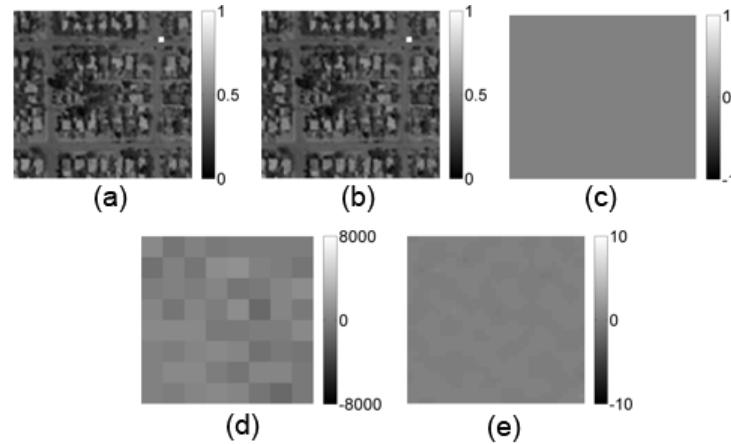
**Figure B.14:** Difference frame 4 of a sequence of one mover on a non-zero background.



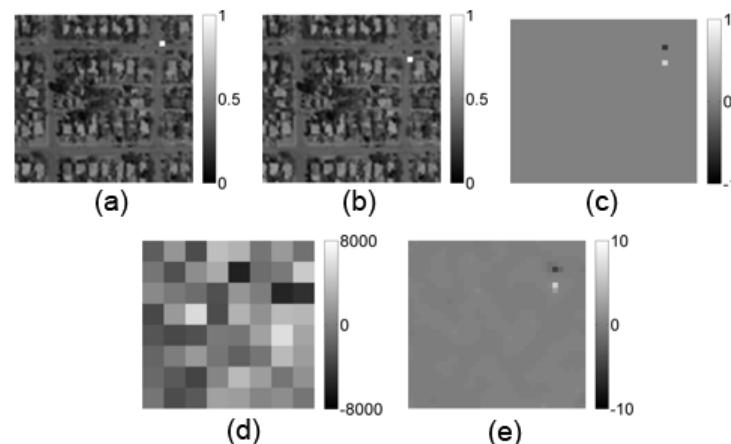
**Figure B.15:** Difference frame 5 of a sequence of one mover on a non-zero background.



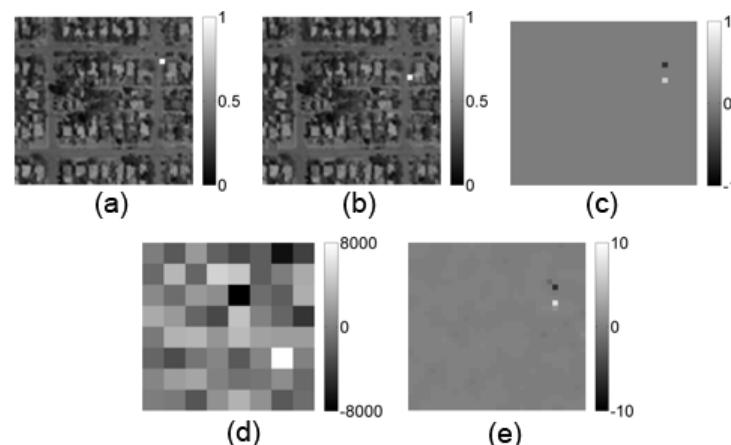
**Figure B.16:** Difference frame 6 of a sequence of one mover on a non-zero background.



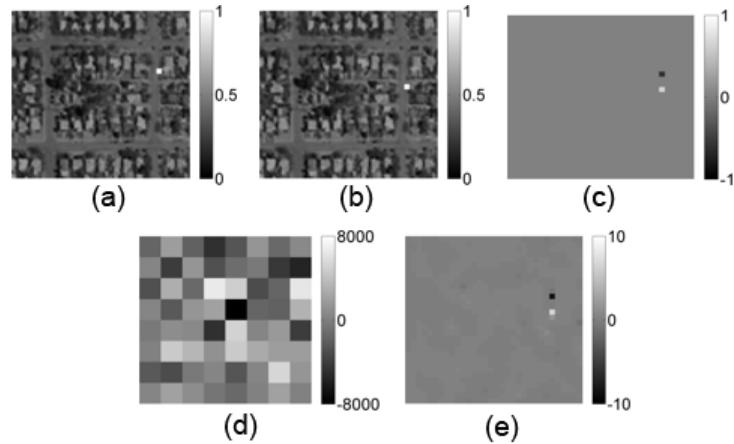
**Figure B.17:** Difference frame 7 of a sequence of one mover on a non-zero background.



**Figure B.18:** Difference frame 8 of a sequence of one mover on a non-zero background.



**Figure B.19:** Difference frame 9 of a sequence of one mover on a non-zero background.



**Figure B.20:** Difference frame 10 of a sequence of one mover on a non-zero background.

## Appendix C

### The Psuedo-Code For SCOUT Experiment

This appendix contains the psuedo-code for running the SCOUT experiment which is described in Chapter 3.

---

**Algorithm 1** Dark Frame Measurement algorithm
 

---

```

1: function getDarkFrame
2: Open Connection to Camera
3: Set camera temperature to 0 degrees Celsius
4: Start a stopwatch timer
5:  $tv := 60$  seconds
6:  $c := 0$ 
7: for  $k = 1$  to numExp do           {Loop takes  $numExp$  camera exposures}
8:   begin
9:      $te :=$  Read the stopwatch timer (units of seconds).
10:    if  $te > c * tv$  then
11:      begin
12:        Display an all white screen on monitor
13:         $c := c + 1$ 
14:      end
15:      Sets the entire plamsa to 0
16:       $df(k) :=$  Camera Readout
17:    end
18:  Close Connection to Camera
19:  average dark frame measurements
20:  Return averaged dark frame measurements
  
```

---

---

**Algorithm 2** SCOUT Calibration algorithm
 

---

```

1: function getHcal
2:  $df := \text{getDarkFrame}$            {Runs the Dark Frame Measurement Function}
3: Open Connection to Camera
4: Set camera temperature to 0 degrees Celsius
5: Start a stopwatch timer
6:  $tv := 60$  seconds
7:  $c := 0$ 
8:  $locList := \text{randomize list of locations } n \text{ to } N$ 
9: for  $n = 1$  to  $N$  do
10:   begin
11:      $te := \text{Read the stopwatch timer (units of seconds).}$ 
12:     if  $te > c * tv$  then
13:       begin
14:         Display an all white screen on monitor
15:          $c := c + 1$ 
16:       end
17:     Sets the entire plamsa to 0
18:     Turn on location  $locList(n)$ 
19:      $p := \text{Camera Readout}$ 
20:     Sets the entire plamsa to 0
21:      $p := p - df$       {Subtract dark frame from the readout of the nth location}
22:     Convert image to vector
23:     Store in the nth column of  $H$ 
24:   end
25: Close Connection to Camera
26: Save H
  
```

---

---

**Algorithm 3** Take Measurements for SCOUT Zero Background
 

---

```

1: function scoutMeasZeroBg
2: Open Connection to Camera
3: Set camera temperature to 0 degrees Celsius
4: Start a stopwatch timer
5:  $tv := 60$  seconds
6:  $c := 0$ 
7: for  $k = 1$  to numFrames do
8:   begin
9:      $te :=$  Read the stopwatch timer (units of seconds).
10:    if  $te > c * tv$  then
11:      begin
12:        Display an all white screen on monitor
13:         $c := c + 1$ 
14:      end
15:      Sets the entire plasma to 0
16:       $movLocList(k) :=$  generate random list of mover locations over all possible
N locations
17:      Create image  $f(k)$  where all zero except the locations from  $movLocList(k)$ .
18:      Display image  $f(k)$                                 {Display the ground truth frame}
19:       $r :=$  Camera Readout
20:       $g(k) :=$  Convert camera readout  $r$  to vector
21:      Sets the entire plasma to 0
22:    end
23:  Close Connection to Camera
24:  Save all measurements and ground truth frames  $g, f$ 
  
```

---

---

**Algorithm 4** Reconstruct SCOUT Experiment Data
 

---

```

1: function reconScoutExp
2: Load all measurements  $g$ 
3: Load  $H$                                      {From the calibration function getHcal}
4: for  $k = 2$  to numFrames do
5:   begin
6:      $\Delta g(k - 1) := g(k) - g(k - 1)$  {Subtract previous measurement from current
one}
7:      $\tau := (1 \times 10^{-9}) (2H^T \Delta g(k - 1))$ 
8:      $reltol := 1 \times 10^{-9}$ 
9:      $\hat{\Delta f}(k - 1) := l1\_ls(H, \Delta g, \tau, reltol, quiet)$       {Reconstruct the difference
frame using the  $l1_ls$  MATLAB code. }
10:    end
11:   Return all reconstructed frame differences  $\hat{\Delta f}$ 
  
```

---

## Appendix D

### SCOUT Simulation Code

**Listing D.1:** Main Simulation Script

```

1 % GENERATING SYSTEM MEASUREMENT MATRIX 'H'
2
3 clc; clearvars; close all
4 rand_trials = 5
5 % lens to camera image sensor defocus in mm
6 defocus_value=35;
7 % pitch (in mm) of mask1 (next to image sensor)
8 p1=0.01;
9 % pitch (in mm) of mask2 (next to lens)
10 p2=0.5;
11 %focal length of lens
12 f=35;
13
14 %% comments about image sensor pitch
15 % reading 288 x 288 part on image sensor and binning
16 % (36x36) to obtain 8x8 pixels
17 % sensor pitch is 9 microns. For binned 8x8, each pixel
18 % is 36*9= 324 microns
19
20 % pitch of image sensor in mm
21 p=0.324;
22
23 for i = 1:rand_trials
24
25 % d1 is distance between Mask 1 and image plane of lens
26 % here 2.04 mm is the spacing between camera sensor
27 % image plane and Mask 1
28 d1=defocus_value -2.04;
29
30 % d2 is distance between Mask 2 and image plane of lens
31 % here 6.35 mm is the spacing between
32 d2=f -6.35;
33
34 % calculating pitch and positions relative to detector
35 % for locating Mask1 away from focus
36 pos1 = (defocus_value -d1)/(f+defocus_value);
37
38 % position of Mask 2
39 pos2=(d2+defocus_value)/(f+defocus_value);
40
41 %calculating pitch values of Masks on detector
42 pd1=(p1*defocus_value)/d1; % for mask1
43 pd2=(p2*defocus_value)/d2; % for mask2
44 pitch1=pd1/p;
45 pitch2=pd2/p;
46
47
48 pitch = [pitch1 pitch2];
49 pos=[pos1 pos2];
50
51 % Mask leakage based on experimental mask transmission
52 % values
53 leakage1=0.12;%masks open part leakage of 12%
54 leakage=0.00;%masks black part no leakage
55
56 % fill factor of mask1 and mask2 , 50%
57 through=[0.5 0.5];
58

```

```

59     lens_defocus=defocus_value;
60
61 %scaling mask patterns, using smaller values speeds up code
62 upsamp=0.25;
63
64 directory=pwd;
65
66 date='feb16'; %date for file names
67
68 name = ...
69 sprintf(['%s/pos_%3g_%3g_through_%3g_%3g',...
70         'pitch_%3g_%3g.mat'],...
71         directory, pos(1), pos(2), through(1), through(2),...
72         pitch(1), pitch(2));
73
74 % choose blur type on masks
75 psfblur='fourierpsf';
76 %psfblur='false' for no blur
77 % for adding blur based on fourier filter
78 %psfblur='fourierpsf'
79
80 varargin={'upsample',upsamp,'mask_pos',...
81           pos,'throughput',through,'maskpitch',...
82           pitch,'defocus',lens_defocus,'psfblur',...
83           psfblur,'leakage',leakage,'leakagel',leakagel};
84
85 N=32;%size of the scene (NxN)
86 K=8;%size of detector (KxK)
87
88 % call function to generate system matrix, with point
89 % by point calibration. Selecting display as 'false'
90 % to prevent figure display while generating matrix
91 H(:,:,i) = struct_projection(N, 'display',false,...
92         'compression', N/K, varargin{:});
93
94
95 save(['condnum_df_ num2str(defocus_value) ...
96         'normalization_on.mat'], 'H', 'rand_trials')
97
98 end
99
100 % use the statement below for locating Mask1 before the focus (i.e. on the same side of focus
101 % as Mask 2)
102 % pos1=(d1+defocus_value)/(f+defocus_value);
103 pos2=(d2+defocus_value)/(f+defocus_value); % position of Mask 2
104
105 %calculating pitch values of Masks on detector
106 pd1=(p1*defocus_value)/d1; % for mask1
107 pd2=(p2*defocus_value)/d2; % for mask2
108 pitch1=pd1/p;
109 pitch2=pd2/p;
110
111
112 pitch = [pitch1 pitch2];
113 pos=[pos1 pos2];
114
115 %Mask leakge based on experimental mask transmission values
116 leakage1=0.12;%masks open part leakage of 12%
117 leakage=0.00;%masks black part no leakage
118
119
120 through=[0.5 0.5]; % fill factor of mask1 and mask2 , 50%
121 lens_defocus=defocus_value;
122 upsamp=0.25; %scaling mask patterns, using smaller values speeds up code
123 directory=pwd;
124 date='feb16'; %date for file names
125
126 name = sprintf('%s/pos_%3g_%3g_through_%3g_%3g_pitch_%3g_%3g.mat',directory,pos(1),pos...
127 (2),through(1),through(2),pitch(1),pitch(2));

```

```

128 %%choose blur type on masks
129 psfblur='fourierpsf';
130 %psfblur='false' for no blur
131 %psfblur='fourierpsf' for adding blur based on fourier filter
132
133
134 varargin={'upsample',upsamp,'mask_pos',pos,'throughput',through,'maskpitch', pitch,'defocus',
135 lens_defocus,'psfblur',psfblur,'leakage',leakage,'leakage1',leakage1};
136
137 N=32;%size of the scene (NxN)
138 K=8;%size of detector (KxK)
139
140 % call function to generate system matrix, with point by point calibration.
141 %selecting display as 'false' to prevent figure display while generating matrix
142 H(:,:,i) = struct_projection(N, 'display',false, ...
143 'compression', N/K, varargin{:});
144
145 % system_mat_name=sprintf('%s_defocus_%d.mat',date,lens_defocus);% file
146 % name to save system matrix 'H'
147
148 % system_mat_name = ['trial' num2str(i) '_default_matrix.mat']
149 save(['condnum_df_' num2str(defocus_value) 'normalization_on.mat'], 'H', 'rand_trials')
150
151 end

```

**Listing D.2:** struct\_projection function

```

1 function H = struct_projection(N,varargin)
2
3 defopt.mask_pos = [.1 .9];
4 defopt.compression = 4;
5 defopt.throughput = 0.5;
6 defopt.defocus = 2;
7 defopt.display = true;
8 defopt.upsample = 4;
9
10 % Sets pitch equal to reconstruction resolution
11 defopt.maskpitch = 1;
12 defopt.psfblur='false';
13 defopt.leakage1=0;%mask clear part
14 defopt.leakage=0;%mask dark part
15
16 opt = matlab_options(varargin, defopt);
17
18 compression = opt.compression;
19 throughput = opt.throughput;
20 dd = opt.defocus;
21 leakage = opt.leakage;
22 leakage1 = opt.leakage1;
23
24 upsample = opt.upsample; % linear upsample factor
25
26 display = opt.display;
27
28 psfblur=opt.psfblur; % read blur type
29
30 % all physical distances are in mm
31
32
33 N=32;% scene size NxN
34
35 % location pitch - desired image-space reconstruction
36 % resolution in mm
37 p = 0.324;
38
39 f = 35; % lens focal length in mm
40 D=25.4; %lens diameter in mm
41
42 maskcount = length(opt.mask_pos);
43

```

```

44 %for locating Mask1 away from focus
45 d1 = dd - opt.mask_pos(1)*(f+dd);
46
47 % use the statement below for locating Mask1 before the
48 % focus (i.e. on the same side of focus as Mask 2)
49
50 %% testing for defocus=1, mask1 behind mask2
51
52 if maskcount>1
53 d2 = opt.mask_pos(2)*(f+dd) - dd; %%edit
54 else
55 d2 = 0;
56 end
57 if maskcount>2
58 d3 = dd+opt.mask_pos(3)*(f+dd); %%edit
59 else
60 d3 = 0;
61 end
62
63 if maskcount>3
64 error('mask_pos is too long, must have length 1-3');
65 end
66
67 throughput = throughput(:);
68 if length(throughput)==1 && maskcount>1
69 throughput=throughput^(1/maskcount)*ones(maskcount,1);
70 end
71 if length(throughput) <3
72 throughput = [throughput;ones(3-length(throughput))];
73 end
74
75 if length(opt.maskpitch) == 1 && maskcount > 1
76 maskpitch=opt.maskpitch*ones(maskcount,1);
77 else
78 maskpitch = opt.maskpitch(:);
79 end
80
81 % Code assumes all masks present even if they aren't,
82 % so pad to length 3
83 maskpitch = [maskpitch ; ones(3 - length(maskpitch),1)];
84
85 % make mask pitch (pd) equal to reconstruction pitch (p)
86 pd = maskpitch * p; % mask pitch in sensor plane
87
88 %% perform geometrical calculations
89
90 p1 = pd(1)*d1/dd; % physical mask pitch----- mm real mask
91 p2 = pd(2)*d2/dd;
92 p3 = pd(3)*d3/dd;
93
94 % this is the pitch of the points in the aperture,
95 % a larger defocus (dd) gives a smaller pitch
96 pL = p*f/dd;
97
98 fprintf('mask 1: d1 = %.1f, p1 = %.3f\n', d1, p1);
99 fprintf('mask 2: d2 = %.1f, p2 = %.3f\n', d2, p2);
100 fprintf('mask 3: d3 = %.1f, p3 = %.3f\n', d3, p3);
101
102 Sf = p * (N-1) / (1 + dd/f); % full "image" width at focus (mm)
103 Sd = Sf * (1 + dd/f); % image width at sensor (at z = dd)
104 S1 = Sf * (1 + d1/f); % at mask 1
105 S2 = Sf * (1 + d2/f); % at mask 2
106
107 S3 = Sf * (1 - d3/f); % at mask 3
108
109 Bd = D * dd/f; % blur width at sensor
110 B1 = D * d1/f;
111 B2 = D * d2/f;
112 B3 = D * d3/f;
113
114 %% define mask structures

```

```

115 m0.z = f; % aperture
116 m0.x = [-D/2:pL:D/2];
117 m0.y = m0.x;
118 [X,Y] = meshgrid(m0.x, m0.y);
119
120 %%## adding gaussian blur to model lens defocus
121
122 % 'blursize' indicates the size of the blur filter which is
123 % computed as per the defocus level above(bigger blur for a larger defocus).
124 blursize=size(X);
125
126 % the standard deviation of 12 is chosen to model lens
127 % defocus with Gaussian blur
128 m0.v=fspecial('gaussian',blursize(1),12);
129
130 m1.z = d1; % first mask
131 m1.x = [-(B1+S1)/2:p1:(B1+S1)/2];
132 m1.y = m1.x;
133 m1.v = double(rand(length(m1.x)) <= throughput(1));
134
135 % including leakage of dark part
136 leak = leakage*ones(length(m1.v));
137
138 % including leakage of clear part
139 leak1 = leakage1*ones(length(m1.v));
140 m1.v = max(m1.v.* (1-leak1), leak);
141 m2.z = d2; % second mask
142 m2.x = [-(B2+S2)/2:p2:(B2+S2)/2];
143 m2.y = m2.x;
144 m2.v = double(rand(length(m2.x)) <= throughput(2));
145
146 % including leakage of dark part
147 leak = leakage*ones(length(m2.v));
148
149 % including leakage of clear part
150 leak1 = leakage1*ones(length(m2.v));
151 m2.v = max(m2.v.* (1-leak1), leak);
152 m3.z = d3; % third mask
153 m3.x = [-(B3+S3)/2:p3:(B3+S3)/2];
154 m3.y = m3.x;
155 m3.v = double(rand(length(m3.x)) <= throughput(3));
156 % including leakage of dark part
157 leak = leakage*ones(length(m3.v));
158 % including leakage of clear part
159 leak1 = leakage1*ones(length(m3.v));
160 m3.v = max(m3.v.* (1-leak1), leak);
161
162 %% perform calculations
163 H = []; Hcrop=[];
164 % range and sampling for masks in sensor plane
165 xx = [-Sd/2:pd/upsample:Sd/2];
166 % range of point locations (mapped to image space)
167 xlist = [-Sd/2:p:Sd/2];
168 progress(1, length(xlist)^2, 1, 1);
169 ind = 1;
170
171 countval=length(xlist);
172
173 for xcount=1:countval
174     for ycount=1:countval
175         x=xlist(xcount);
176         y=xlist(ycount);
177         progress(ind); ind = ind + 1;
178         [mout, ml] = overlay_masks({m0, m1, m2}, ...
179             [x,y], dd, xx, xx,B1,B2,Bd,psfblur,D);
180         full_image = mout.v;
181         scalefac = upsample * p / pd;
182         high_res = imresize(full_image, [N,N], 'bilinear');
183         % default compression of 4 for 32x32 scene to
184         % 8x8 detector
185         low_res = bin_image(high_res, compression);

```

```

186
187     if display
188         if gcf ~= 2; figure(2); end
189         subplot(1,2,1);
190         imagesc(high_res); axis image; colormap gray;
191         subplot(1,2,2);
192         imagesc(low_res); axis image; colormap gray;
193         drawnow;
194     end
195
196     H = [H low_res(:)]; % build the system matrix
197
198 end
199
200 if display
201     figure(3);
202     imagesc(H);
203     colormap jet;
204     colorbar;
205 end

```

Listing D.3: overlay\_masks function

```

1 function [m_out, ml] = overlay_masks(mask_list, origin, ...
2     z, x, y, B1, B2, Bd, psfblur, D)
3 % project a list of masks to given z plane and overlay them
4 % mask_list - list of mask structures
5 % origin - [x, y] coordinates of projection origin
6 % z - z-plane to project to
7 % x, y - x and y coordinate lists to interpolate onto
8
9 if nargin < 4
10     x = ml{1}.x;
11     y = ml{1}.y;
12 end
13
14 % project the masks to common z plane
15 if nargin > 1
16     for ind = 1:length(mask_list)
17         ml{ind} = project_mask(mask_list{ind}, origin, z);
18     end
19 else
20     ml = mask_list;
21 end
22
23 % build the combined mask structure
24 m_out = ml{1};
25 m_out.x = x;
26 m_out.y = y;
27 [X,Y] = meshgrid(x,y); % gridded coordinates for output mask
28 m_out.v = ones(size(X));
29
30 for ind = 1:length(ml)
31     [Xm, Ym] = meshgrid(ml{ind}.x, ml{ind}.y); % native projected coordinates
32     if 0
33         fprintf('ind = %i\n', ind);
34         fprintf('size(Xm) = [%i, %i]\n', size(Xm,1), ...
35             size(Xm,2));
36         fprintf('size(Ym) = [%i, %i]\n', size(Ym,1), ...
37             size(Ym,2));
38         fprintf('size(v) = [%i, %i]\n', ...
39             size(ml{ind}.v,1), size(ml{ind}.v,2));
40         fprintf('size(X) = [%i, %i]\n', size(X,1), ...
41             size(X,2));
42         fprintf('size(Y) = [%i, %i]\n', size(X,1), ...
43             size(X,2));
44     end
45 % interpolate from the native projected coordinates
46 % onto the common coordinates
47

```

```

48     switch (psfblur)
49
50     case 'fourierpsf' % adding blur on masks
51         switch (ind)
52             case 1
53                 m_out.v = m_out.v .* interp2(Xm, Ym, ...
54                     ml{ind}.v, X, Y, '*linear', 0);
55
56             case 2 %blur on mask 1
57                 [sz1,sz2]=size((interp2(Xm, Ym, ...
58                     ml{ind}.v, X, Y, '*linear', 0)));
59
60                 %create filter in fourier domain
61                 blur_radius1=(sz1*((D-B1)/D))/2;
62                 % compute blur radius at chosen defocus
63                 % level
64                 [rr cc] = meshgrid(1:sz1);
65                 blurpsf1 = fftshift(sqrt((rr-round(sz1/2)).^2+(cc-round(sz1/2)).^2)<=
66                     blur_radius1);
67                 blur_filter1 = abs(ifft2(blurpsf1));
68
69                 %apply filter
70
71                 filtered_mask = ...
72                     real(ifft2(blurpsf1.*fft2(interp2(Xm, Ym, ml{ind}
73                         }.v, X, Y, '*linear', 0))));
74
75                 %normalized the filtered mask to it can't amplify
76                 filtered_mask = filtered_mask / max(filtered_mask(:));
77
78                 m_out.v = m_out.v .* filtered_mask;
79                 m_out.v(m_out.v<0)=0;
80
81             case 3 %blur on mask 2
82
83                 [sz1,sz2]=size((interp2(Xm, Ym, ml{ind}.v, X, Y, '*linear', 0)));
84
85                 %create filter in fourier domain
86                 blur_radius2=(sz1*((D-B2)/D))/2; % compute blur radius at chosen defocus
87                 % level
88                 [rr cc] = meshgrid(1:sz1);
89                 blurpsf2 = fftshift(sqrt((rr-round(sz1/2)).^2+(cc-round(sz1/2)).^2)<=
90                     blur_radius2);
91
92                 %apply filter
93                 blur_filter2 = abs(ifft2(blurpsf2));
94
95                 filtered_mask = ...
96                     real(ifft2(blurpsf2.*fft2(interp2(Xm, Ym, ml{ind}
97                         }.v, X, Y, '*linear', 0)));
98
99                 filtered_mask = filtered_mask / max(filtered_mask(:));
100                m_out.v = m_out.v .* filtered_mask;
101                m_out.v(m_out.v<0)=0;
102
103            end
104
105        case 'false' %no blur
106            m_out.v = m_out.v .* interp2(Xm, Ym, ml{ind}.v, X, Y, '*linear', 0);
107
108    end
109
110 end

```

**Listing D.4:** project\_mask function

```

1
2 function m_out = project_mask(m_in, origin, new_z)
3 % project the input mask to a new z plane. The projection is performed
4 % via rays emanating from the provided x-y origin in the z=0 plane
5
6 % mask attributes: z, v, x, y (optional)

```

```

7 % if y is provided , v should be 2d, otherwise 1d
8
9 m_out.z = new_z;
10 m_out.v = m_in.v;
11 x0 = origin(1);
12 m_out.x = (m_in.x - x0) * (m_out.z/m_in.z) + x0;
13 if length(origin) > 1
14     y0 = origin(2);
15     m_out.y = (m_in.y - y0) * (m_out.z/m_in.z) + y0;
16 end
17
18 %calling function to locate the center of the aperture at the point source
19 %co-ordinates
20
21 % call function to center PSF
22 [m_out.x m_out.y]=centering_atlocation(origin,m_out.x,m_out.y);
23
24 end

```

**Listing D.5:** centering\_atlocation function

```

1 function [out1, out2]=centering_atlocation(origin,in1,in2)
2
3 %function to locate the center of the aperture at the point source co-ordinates
4
5 m_out.x=in1;
6 m_out.y=in2;
7
8 #####calculations for x-coordinate#####
9 len_mx=length(m_out.x);
10
11 test_even_odd=mod(len_mx,2);
12 if test_even_odd==0
13     %even length
14     mid_pt=(len_mx/2);
15 elseif test_even_odd==1
16     %odd length
17     mid_pt=((len_mx+1)/2);
18 end
19 % calculating mid point
20 midval=m_out.x(mid_pt);
21 m_out.x=(m_out.x - midval + origin(1));%center the data around origin
22
23
24 #####calculations for y-coordinate#####
25 len_my=length(m_out.y);
26 test_even_odd=mod(len_my,2);
27 if test_even_odd==0
28     %even length
29     mid_pty=(len_my/2);
30 else
31     %odd length
32     mid_pty=((len_my+1)/2);
33 end
34 midvaly=m_out.y(mid_pty);
35 m_out.y=(m_out.y - midvaly + origin(2));%center the data around origin
36
37 out1=m_out.x;
38 out2=m_out.y;
39 %aaaaaaaaaaaaaa

```

**Listing D.6:** bin\_image function

```

1 function imout = bin_image(im, n)
2 % bin images
3 % im - image (or set of images) to be binned
4 % n - number of elements (linearly) to be binned
5 %
6 % n can be a vector of bin sizes in each dimension. If n is a scalar ,

```

```

7 % it is interpreted as
8 % [n, n]      for 2D images,
9 % [n, n, 1]    for 3D images,
10 % [n, n, 1, 1] for 4D images, etc.
11 %
12 % examples:
13 % size(im)      n      -->  size(imout)
14 % [50, 50]       5      -->  [10, 10]
15 % [50, 50, 3]   5      -->  [10, 10, 3]
16 % [50, 50, 100] [5,5,20] --> [10, 10, 5]
17 %
18 % note: if the dimensions of im are not multiples of the elements of n,
19 % then the last few values of im will not be used. That is,
20 % size(im) = [51, 51] and n = 5 --> size(imout) = [10, 10]
21 % and the last row and column of im [im(:,51) and im(51,:)] are unused.
22
23
24
25 % expand n into vector form if necessary
26 if length(n) == 1
27     ntmp = n;
28     n = ones(1, length(size(im)));
29     n(1) = ntmp;
30     n(2) = ntmp;
31 end
32
33 s = floor(size(im)./n); % target size
34 S.type = '()' ; % used in subsref and subsasgn
35 subscell = {} ; %
36 for d = 1:length(s)
37     subscell{d} = ':';
38 end
39
40 for d = 1:length(s) % loop over each dimension
41     if n(d) == 1; % no binning along this dimension - move on
42         continue
43     end
44     S.subs = subscell;
45     ts = size(im);
46     ts(d) = s(d);
47     imout = zeros(ts);
48     for i = 1:s(d)
49         start = (i-1)*n(d)+1;
50         stop = i*n(d);
51         S.subs{d} = [start:stop];
52         M = subsref(im, S);
53         S.subs{d} = i;
54         imout = subsasgn(imout, S, sum(M, d));
55     end
56     if d < length(s) % only need to reassign if we're not done yet
57         im = imout;
58     end
59 end

```

## Glossary

**bandlimited signal** A bandlimited signal is any signal  $g(x)$  that whose Fourier transform  $G(f_x)$  is zero and remains zero past a certain frequency  $|f_x| \geq B$ .

**Coding** In the context of computational sensing, coding is the process of modifying or modulating an analog signal during measurement. Coding is often used to reduce degeneracy in the measurement data. In the context of spectroscopy, the spectral filters act to code the spectrum.

**compressible** Signals with strictly sparse representation vectors are unlikely. Fortunately, it is possible to have approximately sparse representation vectors, which are called compressible. In other words, the sorted magnitudes of the coefficients  $|x_n|$  quickly decay.

**compressive imaging** compressive sensing applied to imaging. Typically the goal is to reconstruct the entire object scene. However some compressive imaging sensors are have a task-specific sensing approach, such as the SCOUT.

**compressive sampling** *See* compressive sensing

**compressive sensing** A sensing technique that attempts to directly a compressive or sparse representation of the signal-of-interest during the measurement. Compressive sensors attempt to uses significantly less measurements than the dimensionality of the signal-of-interest. Compressive sensing relies on non-linear optimization algorithms to perform reconstruction or task-specific sensing from highly underdetermined inverse problems. These algorithms often rely on sparsity to avoid overfitting.

**computational sensing** Any sensing technique in which the sensor uses *indirect-imaging*, *multiplex sensing*, compressive sensing, or *task-specific sensing*.

**computational sensor** *See* computational sensing

**data processing inequality** An theorem from information theory that proves the information of a signal cannot be increased via a local physical operation.

**Fellgett advantage** *See* *multiplex advantage*

**forward model** A numerical model, typically an equation, that explains the mapping of the analog signal-of-interest to the measurement data.

**indirect-imaging** An imaging sensor that attempts to reconstruct an image of an object using non-isomorphic measurements. A computational step is required to reconstruct the object signal-of-interest. X-Ray CT and SAR are examples types of indirect-imaging.

**inverse problem** The problem of taking the measurement data and calculating a reconstruction of the signal-of-interest or task-specific parameters. In computational sensing, computer algorithms are used to solve inverse problems.

**isomorphic** *See* isomorphic sensing

**isomorphic sensing** An isomorphic sensor is any sensor that attempts to produce measurement data that resembles the signal-of-interest. An isomorphic measurement is a measurement that resembles the signal-of-interest. An isomorphic measurement can be described as a one-to-one mapping from the signal-of-interest to the measurement, and is represented in matrix notation with an identity matrix. Isomorphic sensing is synonymous with traditional sensing.

**Jacquinot advantage** This results from the fact that in a dispersive instrument, the traditional spectrometer has entrance and exit slits which restrict the amount of light that passes through it. By removing the slits a spectrometer produces a higher signal-to-noise ratio.

**lasso** The least absolute shrinkage and selection operator (lasso) is a regression analysis method that performs both variable selection and regularization. It refers to an optimization problem, a regression technique, and an algorithm. The lasso problem is the

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x}} \|\mathbf{Ax} - \mathbf{g}\|_2^2 + \tau \|\mathbf{x}\|_1$$

**likelihood** The likelihood is the probability of the data  $g$  assuming that a hypothesis  $h$  or parameter  $\theta$  is true.  $P(g | \theta)$

**measurement** A process that converts a physical phenomena to single datum or a set of data. In the context of this dissertation it used synonymously with the detector readout.

**monochromator** An optical instrument that transmits a selectable narrow wavelength band of light chosen from a wider range of wavelengths available at the input.

**multiplex advantage** The improvement in SNR that is due to multiplexed measurements rather than isomorphic measurements. This is often referred to as the Fellgett advantage since it was first discovered by Peter Fellgett. *See* multiplex sensing

**multiplex sensing** A multiplexing sensor is any sensor that attempts to combine the physical phenomena of the analog signal-of-interest in to a few or one analog-to-digital sample to overcome limits due to signal-to-noise ratio. The measurement data that does resemble the signal-of-interest. A matrix representation of a multiplex measurement will not look like an identity matrix

**multiplexing** *See* multiplex sensing

**pixel pitch** The center to center distance between pixels on a focal-plane array such as a CCD or CMOS image sensor.

**posterior** The posterior probability is the conditional probability of a hypothesis  $h$  or parameter  $\theta$  given some data  $g$ .  $P(\theta | g)$

**prior** The prior probability is the probability of a hypothesis  $h$  or parameter  $\theta$  without any knowledge of the data  $g$ .  $P(\theta)$

**ridge regression** Ridge regression is a regression technique that uses  $\ell_2$  regularization to prevent overfitting of the data. Ridge regression seeks coefficient estimates that fit the data well by making the objective function, the  $\ell_2$  norm between the data and the linear model small, however the shrinkage penalty has the effect of shrinking estimates towards zero.

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x}} \|\mathbf{Ax} - \mathbf{g}\|_2^2 + \tau \|\mathbf{x}\|_2$$

**sample** The process of mapping a continuous signal to a discrete signal.

**sampling** *See sample*

**sparse** *See sparsity*

**sparsity** A set, vector, or matrix which contains an overwhelming majority of zeros relative to the size of the set, vector, or matrix.

**spectral resolution** The smallest difference in wavelength the instrument or sensor can discern.

**task-specific sensing** A sensor that does not attempt to reconstruct the signal-of-interest to perform a signal processing task such as detection, estimation, and classification. The AFSSI-C is an example of a task-specific sensor.

## Acronyms

**ADC** analog-to-digital converter

**AFSS** Adaptive Feature Specific Spectrometer

**AFSSI-C** Adaptive Feature Specific Spectral Imaging-Classifier

**AVIRIS** Airborne Visible / Infrared Imaging Spectrometer

**CACTI** Coded Aperture Compressive Temporal Imaging

**CASSI** Coded Aperture Snapshot Spectral Imaging

**CCD** Charge-Coupled Device

**CMOS** Complementary Metal–Oxide–Semiconductor

**CT** Computed Tomography

**CTIS** Computed tomography imaging spectrometer

**DISP** Duke Imaging and Spectroscopy Program

**DMD** Digital Micro-Mirror Display

**FPA** focal-plane array

**FTS** Fourier Transform Spectrometer

**LAR** Least Angle Regression

**LCOS** Liquid Crystal on Silicon

**LENS** Laboratory for Engineering Non-Traditional Sensors

**LS** least squares

**MAP** Maximum A Posteriori

**MRI** Magnetic Resonance Imaging

**MSE** Mean Squared Error

**OSA** Optical Society of America

**PCA** Principal Component Analysis

**PET** Positron Emission Tomography

**PSF** point-spread function

**RIP** restricted isometry property

**SAR** Synthetic Aperture Radar

**SCOUT** Static Computational Optical Undersampled Tracker

**SLM** Spatial Light Modulator

**SNR** signal-to-noise ratio

**SPECT** Single-Photon Emission Computed Tomography

**SWAP-C** size, weight and power-cost

## Symbols

**A** The product of the sensing matrix and the representation matrix  $\mathbf{A} = \mathbf{H}\Psi$

$\delta_\lambda$  Spectral resolution

**e** Additive noise vector

$\mathcal{F}$  Notation for the spectral datacube.

**f** Object signal-of-interest

$\hat{\mathbf{f}}$  Estimated object

**g** Measurement vector

**H** The system matrix which captures all of the physical phenomena in a measurement. Also called the measurement matrix and sensing matrix.

$\mathbf{H}_N$  A Hadamard matrix of size  $N \times N$

$K$  Notation for sparsity which is defined as the number of non-zero entries in a vector.

$N_\lambda$  Number of spectral channels

$N_m$  Total number of measurements

$\tau$  Notation for a regularization parameter in an objective function for any kind of optimization

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