

Líneas de Transmisión y Antenas

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Radio Observatorio de Jicamarca

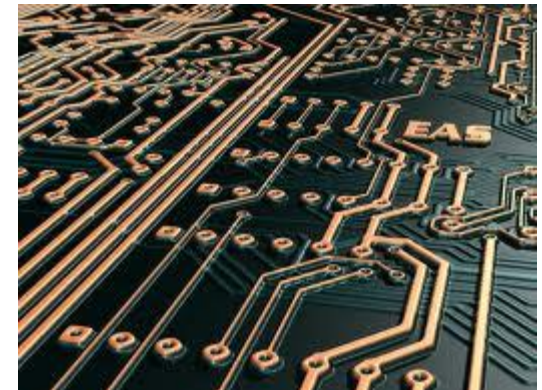
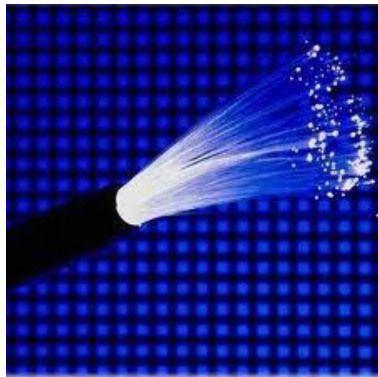


Línea de transmisión (1)

- Definición: Dispositivo para transmitir o guiar energía de un punto a otro



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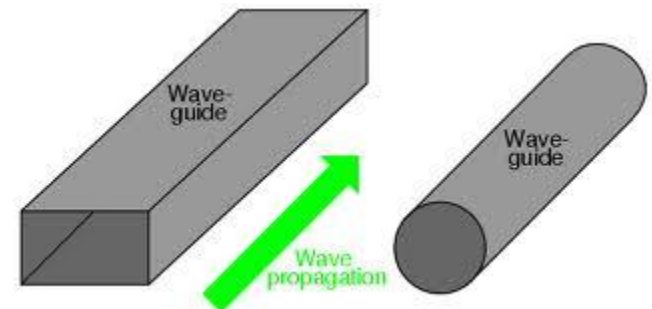
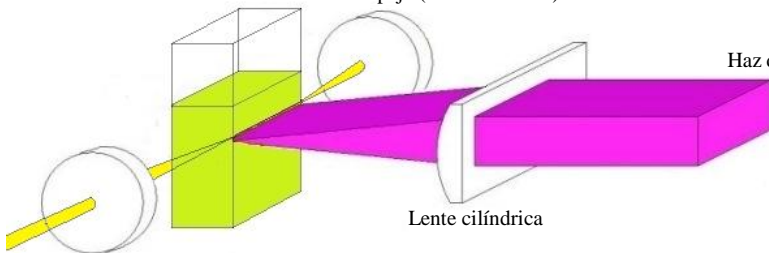
Cubeta que contiene la solución del colorante

Espejo (100% reflector)

Haz de bombeo

Lente cilíndrica

Acoplador de salida



Línea de transmisión. Ecuaciones de Maxwell (1)

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon_0}$$

$$\nabla \cdot \mathbf{B} = 0$$

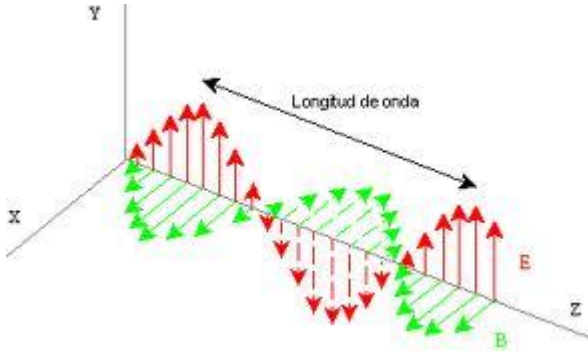
$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \times \mathbf{B} = \mu_0 \mathbf{J} + \mu_0 \epsilon_0 \frac{\partial \mathbf{E}}{\partial t}$$

$$\nabla \times \mathbf{H} = \frac{d\mathbf{D}}{dt} \quad \text{Ley de Ampere}$$

$$\nabla \times \mathbf{E} = -\frac{d\mathbf{B}}{dt} \quad \text{Ley de Faraday}$$

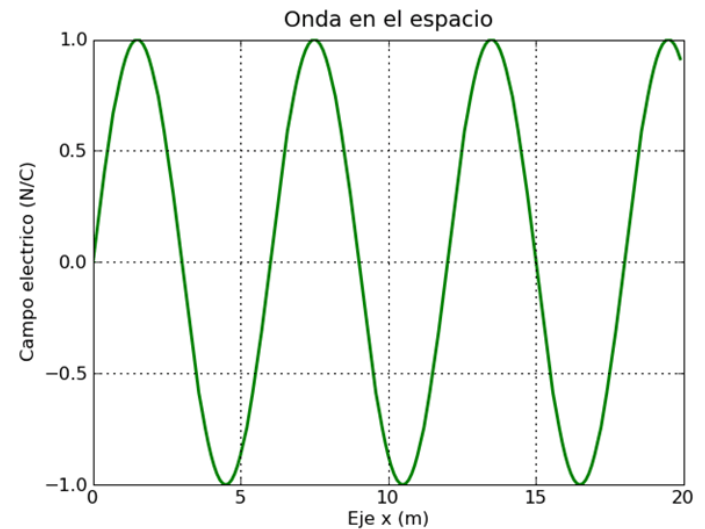
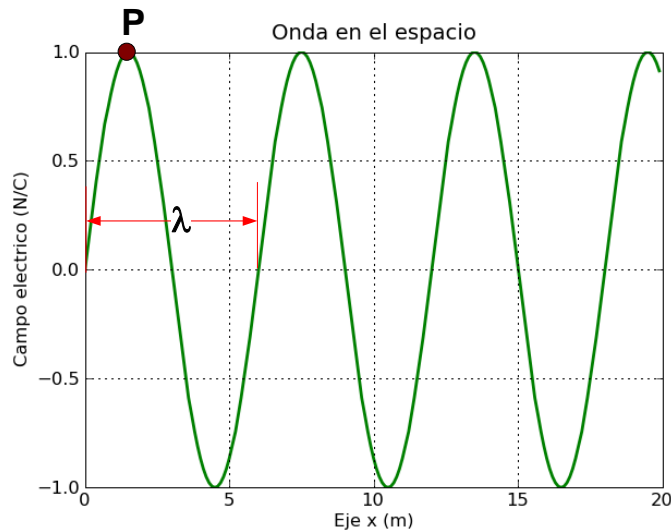
Línea de transmisión. Ecuaciones de Maxwell



$$\frac{\partial^2 H_x}{\partial t^2} = \frac{1}{\mu\epsilon} \frac{\partial^2 H_x}{\partial t^2}$$

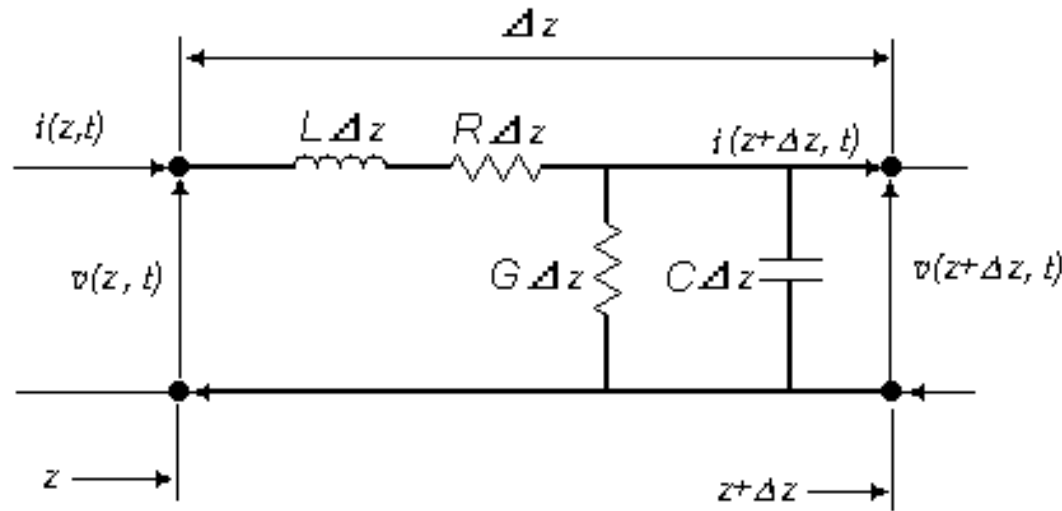
$$\frac{\partial^2 E_y}{\partial t^2} = \frac{1}{\mu\epsilon} \frac{\partial^2 E_y}{\partial t^2}$$

$$E_y = E_0 \sin\left[\frac{2\pi}{\lambda} x + \omega t\right]$$



$$E(x,t) = E_0 \sin\left(\frac{2\pi}{\lambda} x + 2\pi f t\right)$$

Línea de transmisión. Solución para cantidades distribuidas de L,C y G



$$\frac{\partial^2 E_y}{\partial x^2} - j\omega L(G + j\omega C)E_y = 0$$

$$V = E_y * h \Rightarrow E_y = V / h$$

$$\frac{\partial^2 V}{\partial x^2} - j\omega L(G + j\omega C) * V = 0$$

$$\frac{\partial^2 V}{\partial x^2} - Y * Z * V = 0$$

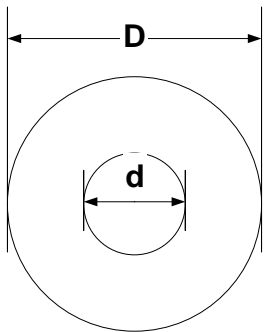
Línea de transmisión, Impedancia Característica

$$\frac{\partial^2 V}{\partial x^2} - Y * Z * V = 0$$

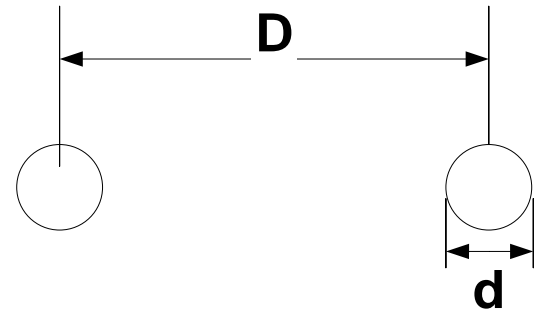
$$V = V_1 e^{j(\omega t + \beta x)} + V_2 e^{j(\omega t - \beta x)}$$

$$I = \frac{V_1}{\sqrt{Z/Y}} e^{j(\omega t + \beta x)} + \frac{V_2}{\sqrt{Z/Y}} e^{j(\omega t - \beta x)}$$

$$Z_0 = \sqrt{\frac{Z}{Y}}$$

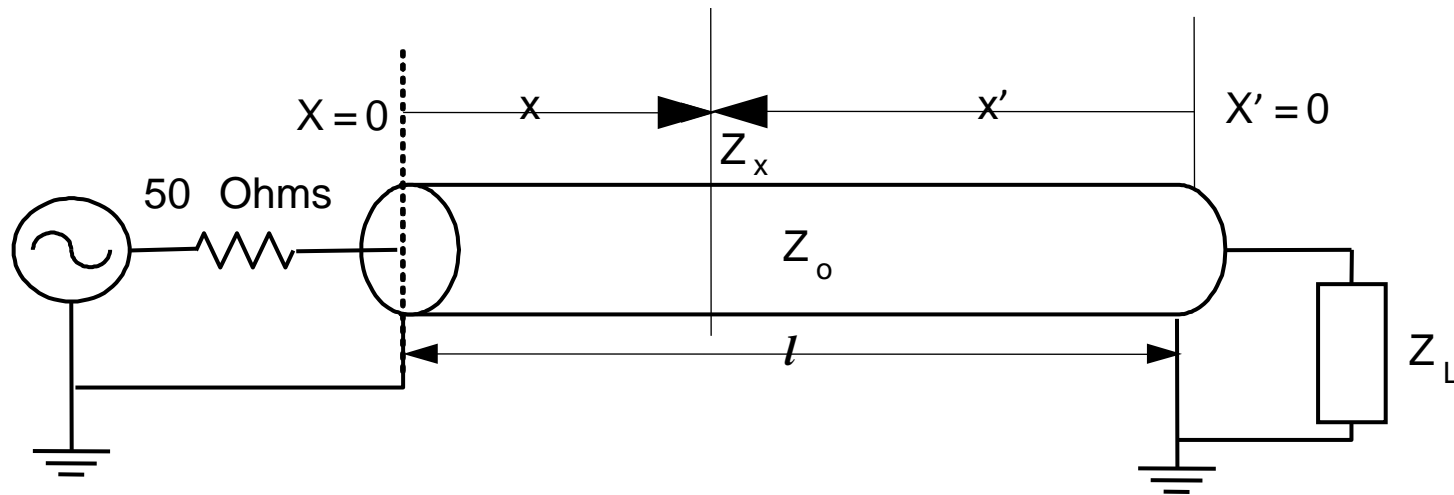


$$Z_o = \frac{138}{\sqrt{\epsilon_r}} \log(D/a)$$



$$Z_o = 276 \log(D/d)$$

Línea de transmisión. Impedancia de la línea

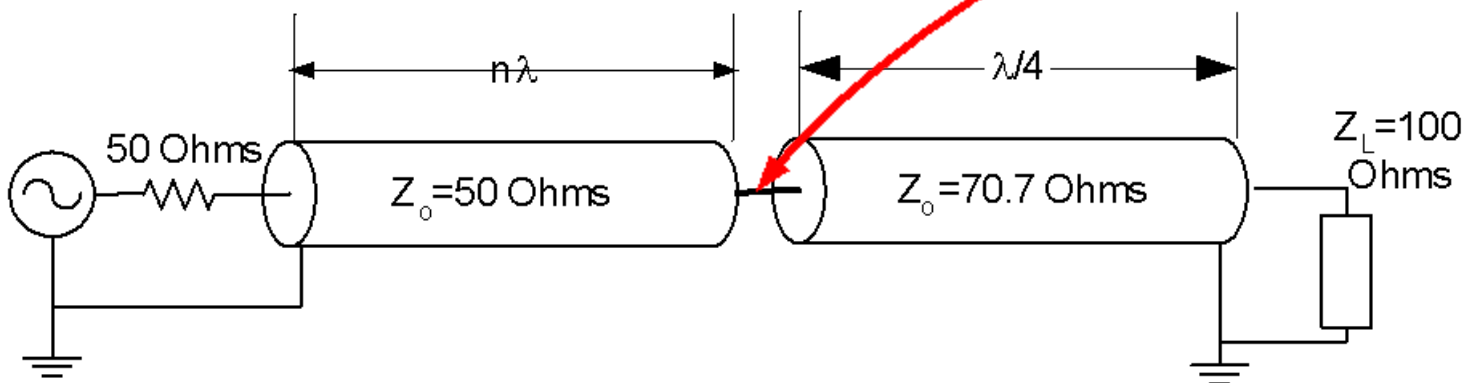


$$Z_x = Z_o * \left(\frac{Z_L + jZ_o \tan \left(\frac{2\pi * (l - x)}{\lambda} \right)}{Z_o + jZ_L \tan \left(\frac{2\pi * (l - x)}{\lambda} \right)} \right)$$

Línea de transmisión. Ecuación del Transformador de $\lambda/4$

$$Z_{\lambda/4} = Z_o * \frac{Z_L + jZ_o \tan\left(\frac{\pi}{2}\right)}{Z_o + jZ_L \tan\left(\frac{\pi}{2}\right)} \Rightarrow Z_{\lambda/4} = \frac{Z_o^2}{Z_L}$$

$$Z_{\lambda/4} = \frac{70.7^2}{100} = 49.98$$



Línea de transmisión. Ejemplos de Transformador de $\lambda/4$

Transformadores de Lambda cuartos ubicados en el módulo



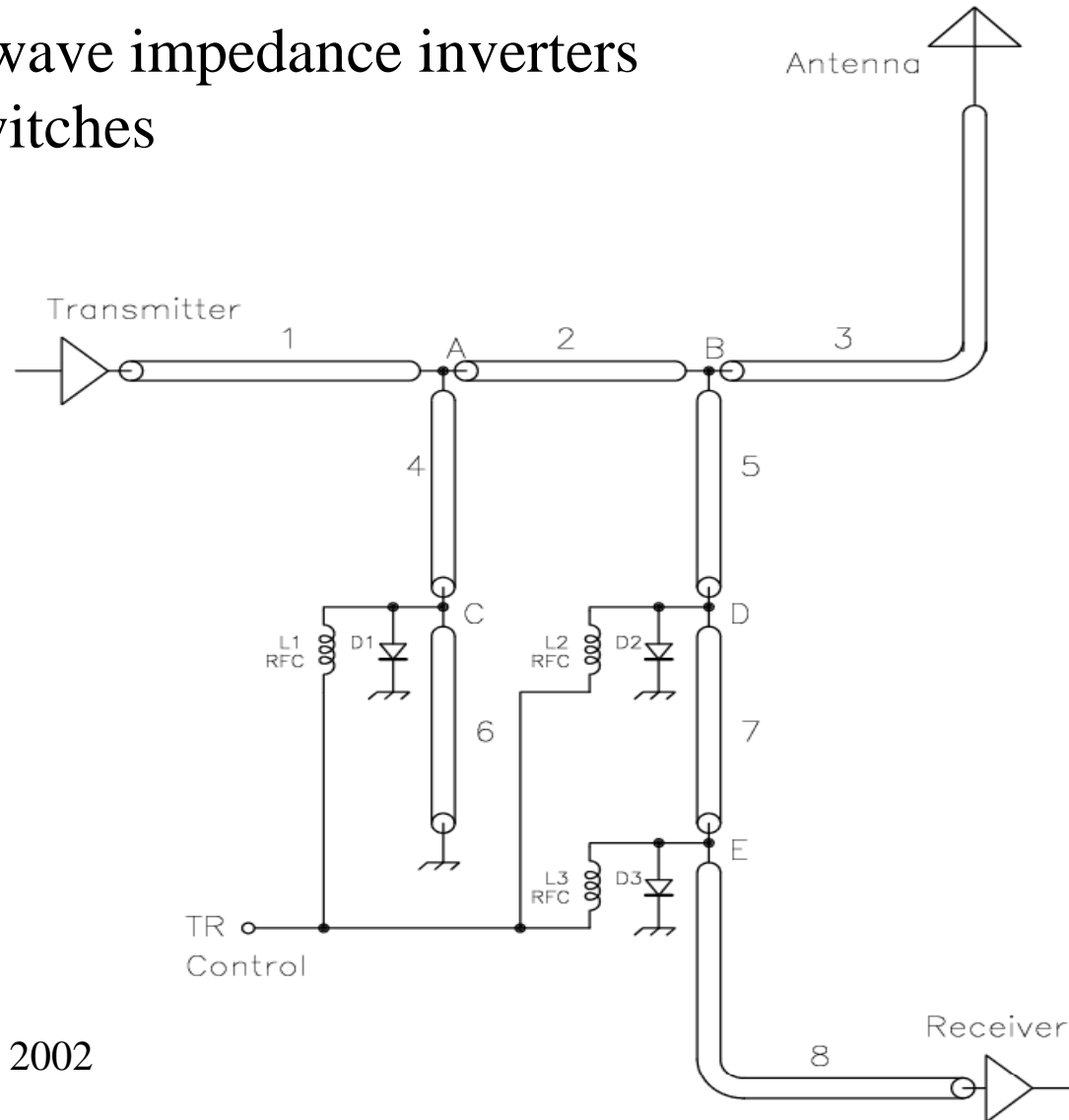
Línea de transmisión. Ecuación del Transformador de $\lambda/4$, caso de corto circuito y circuito abierto

$$Z_{\lambda/4} = \frac{Z_o^2}{Z_L}$$

$$Z_{sc} \rightarrow \infty \qquad Z_{oc} \rightarrow 0$$

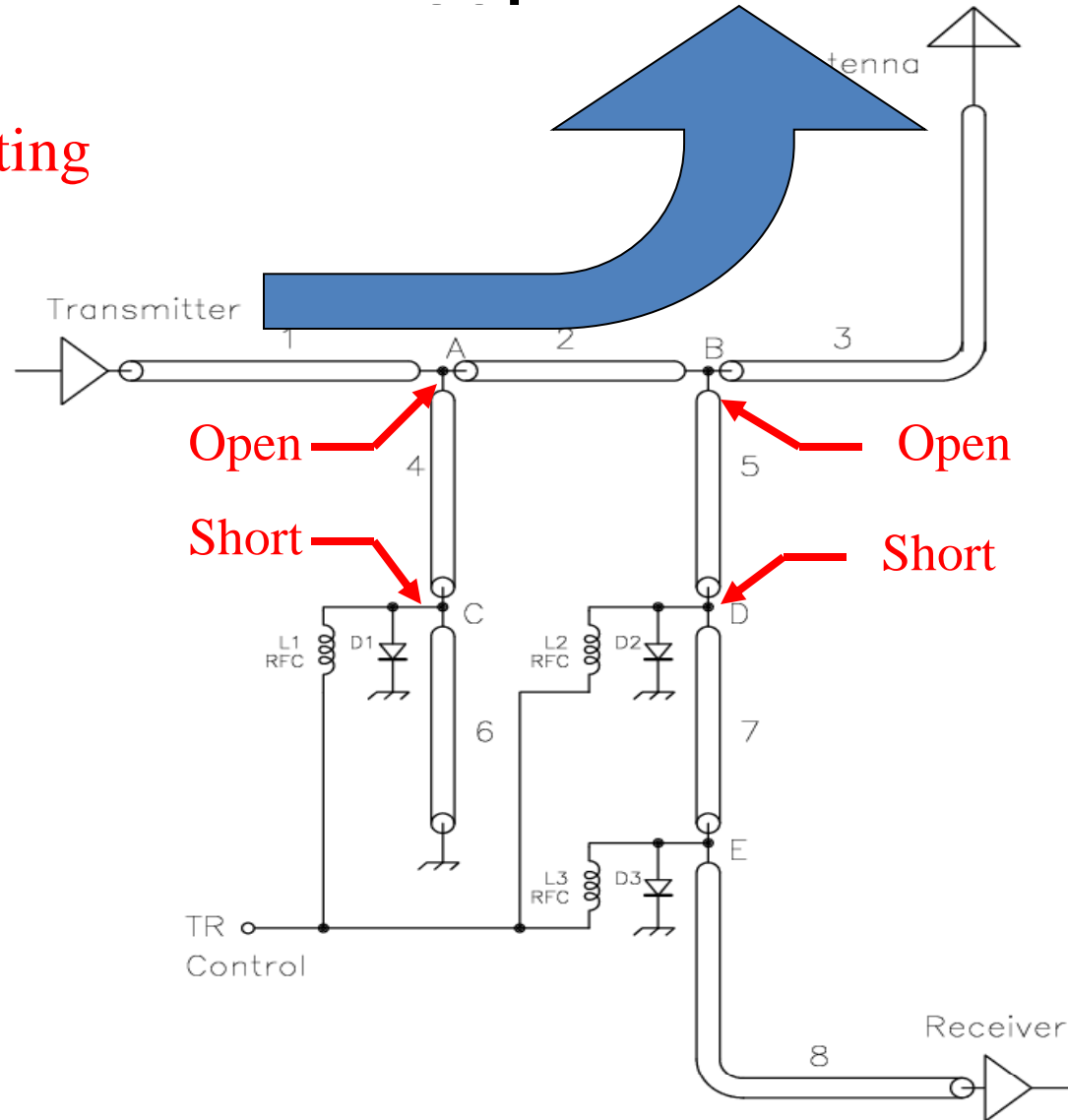
Línea de transmisión. Ejemplos de Transformador de $\lambda/4$

- Quarter-wave impedance inverters
- Diode switches



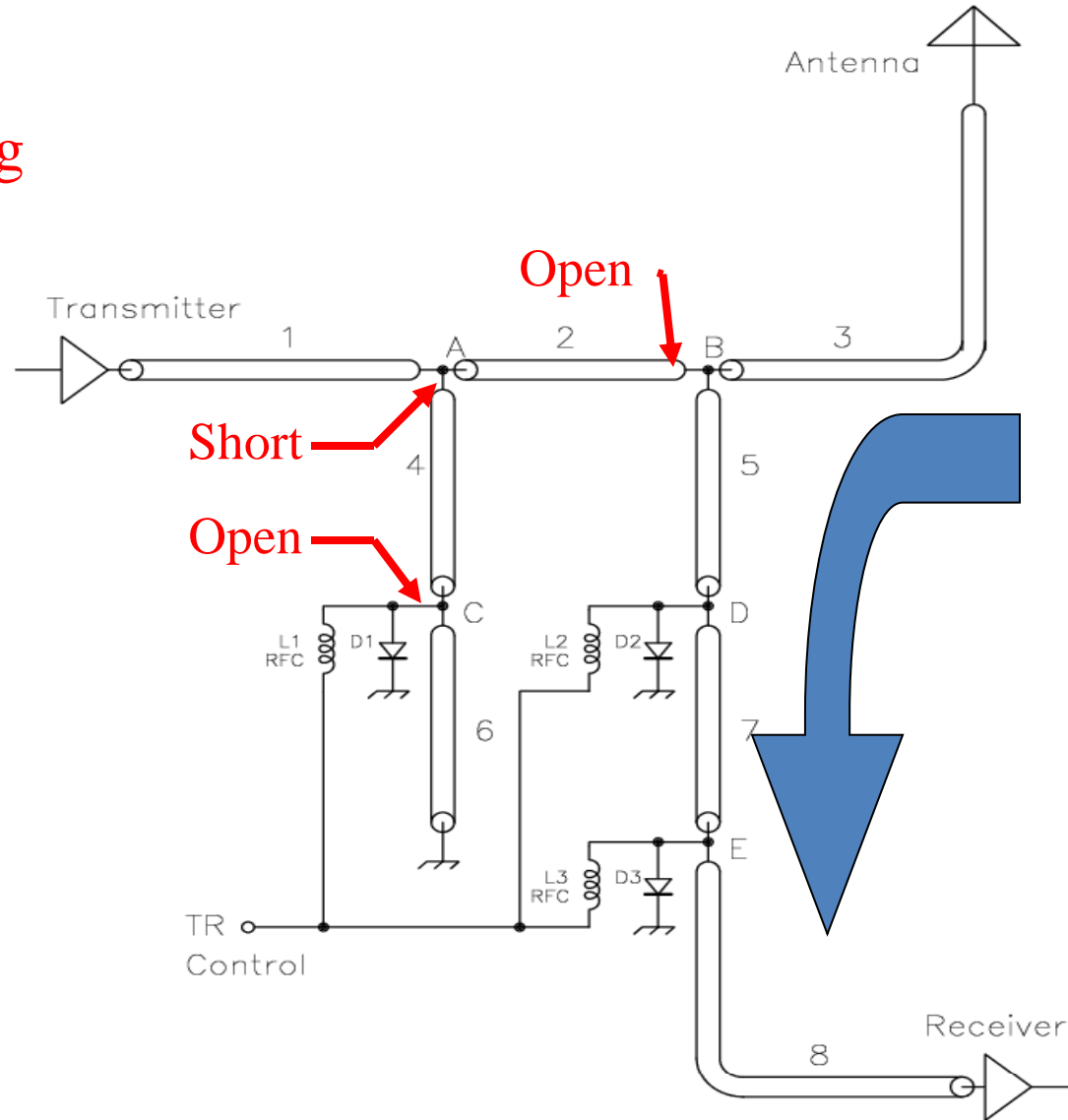
Línea de transmisión. Ejemplos de Transformador de $\lambda/4$

- Transmitting

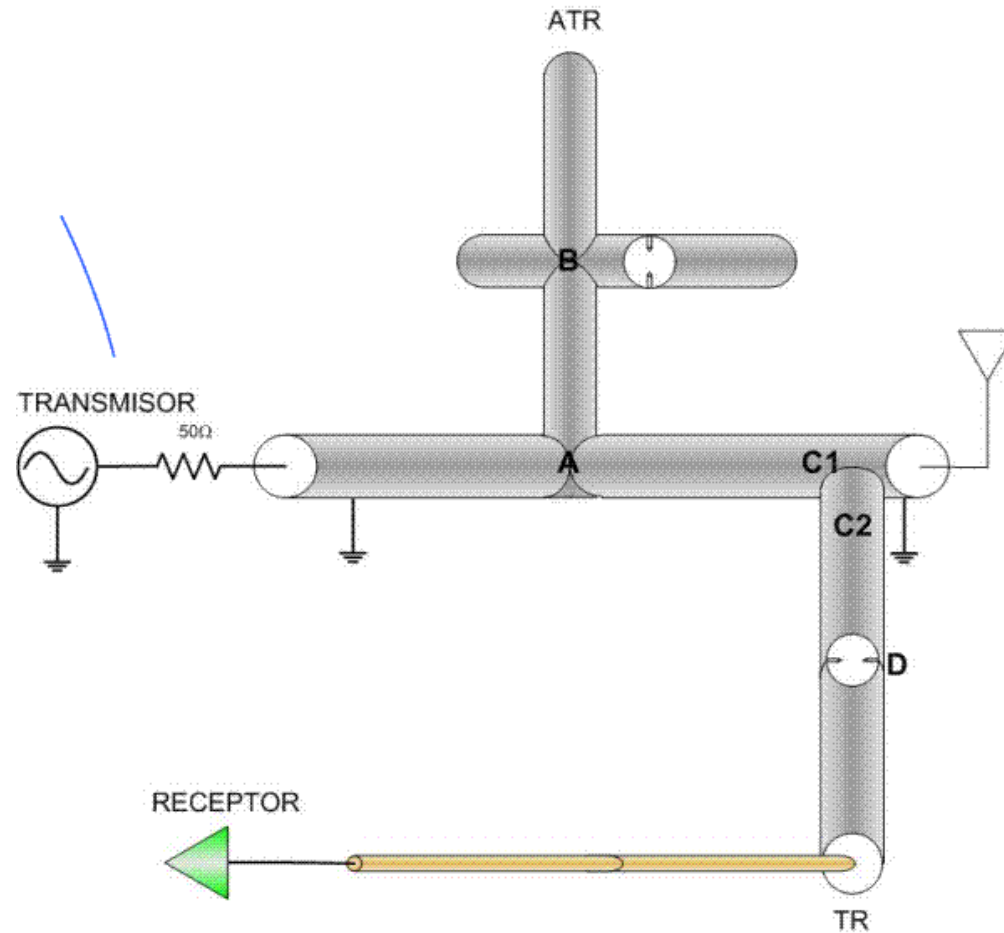


Línea de transmisión. Ejemplos de Transformador de $\lambda/4$

- Receiving



Línea de transmisión. Ejemplos de Transformador de $\lambda/4$



Pregunta 1

Se quiere adaptar 3 líneas de antenas de 50 Ohm a una línea de transmisión de 50 Ohm. ¿Cual debe ser la impedancia característica del adaptador?

- (a) 37 Ohms
- (b) 50 Ohms
- (c) 28 Ohms
- (d) 100 Ohms

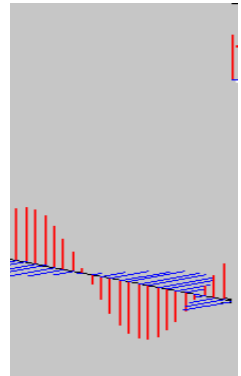
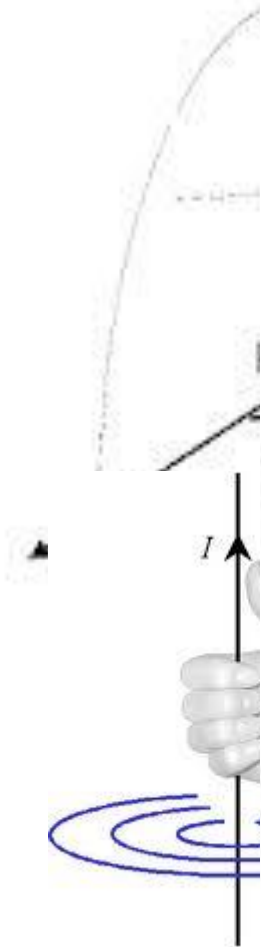
Introducción a antenas. Algunos conceptos

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon_0}$$

$$\nabla \cdot \mathbf{B} = 0$$

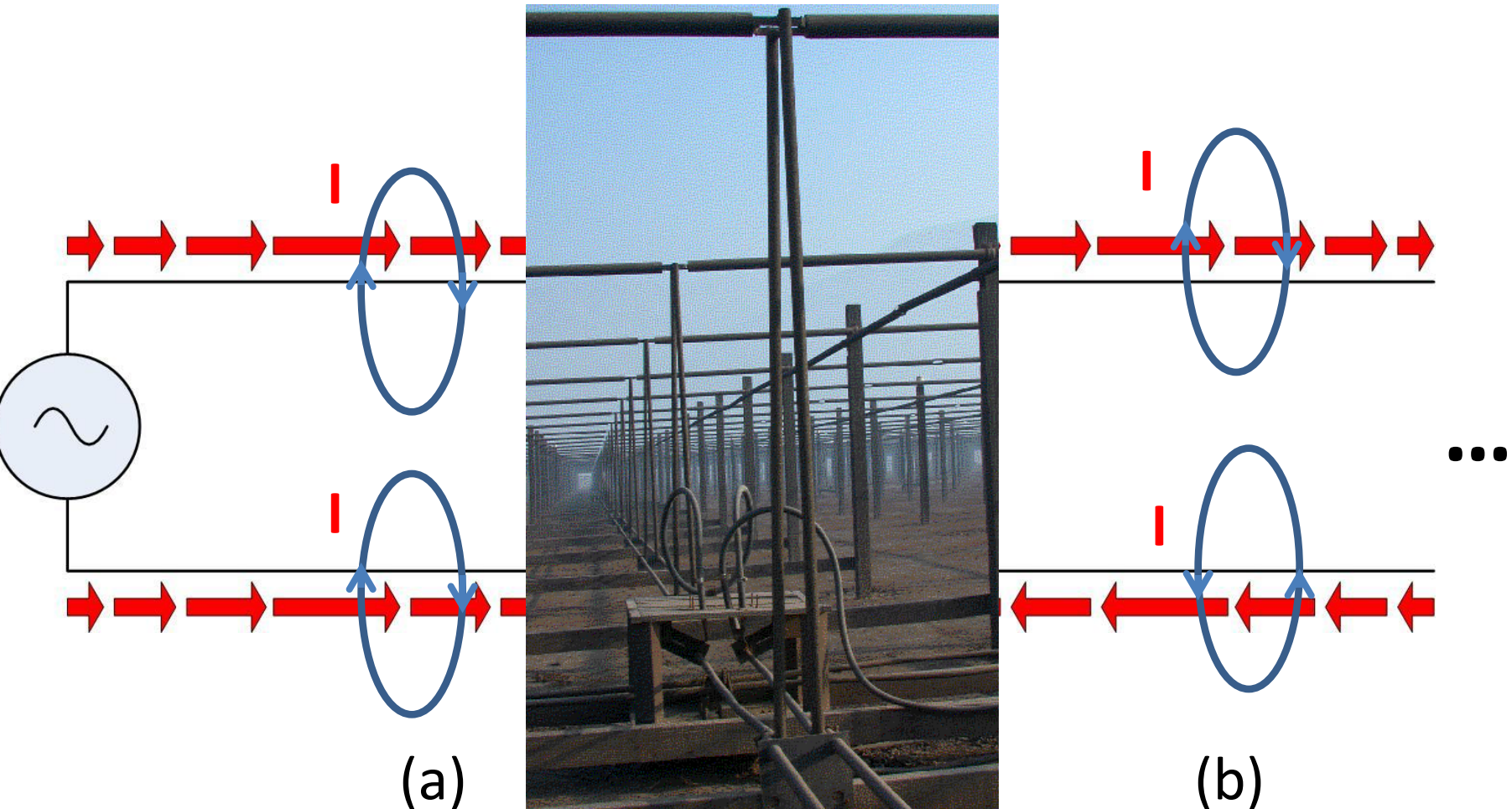
$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \times \mathbf{B} = \mu_0 \mathbf{J} + \mu_0 \epsilon_0 \frac{\partial \mathbf{E}}{\partial t}$$



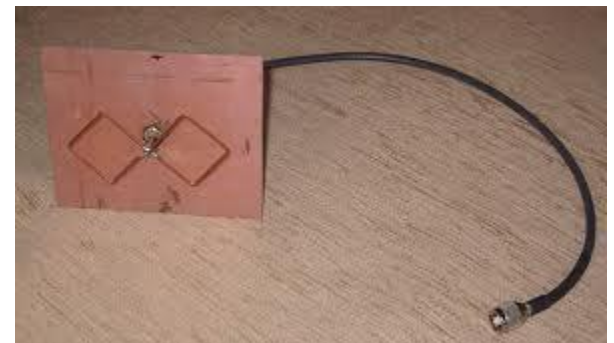
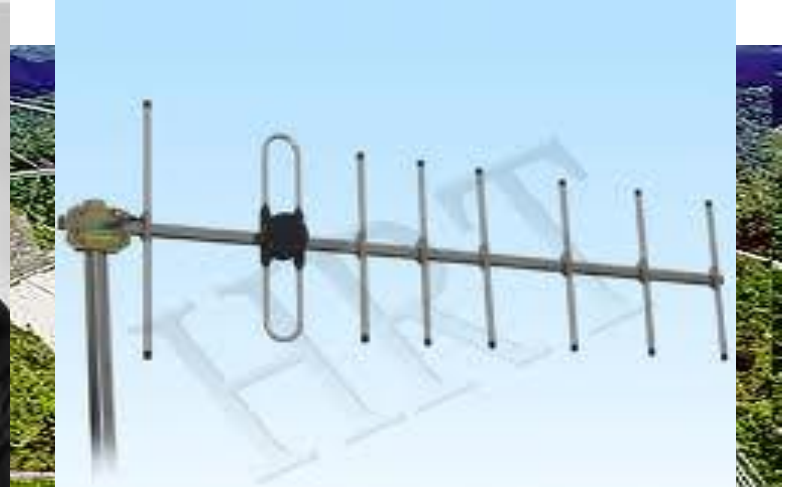
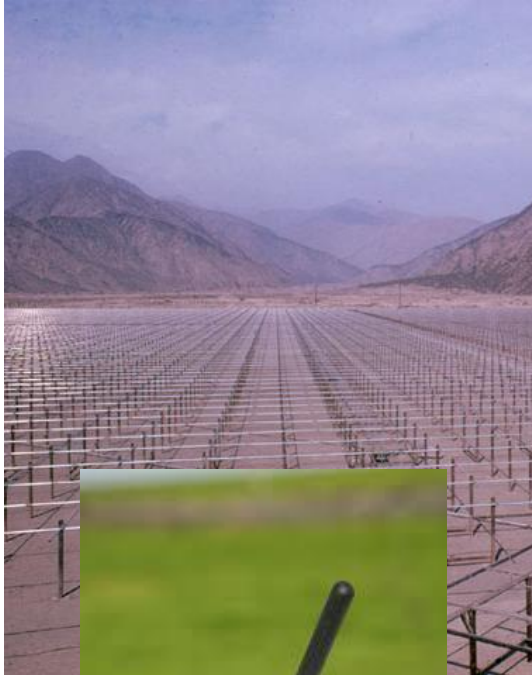
Pregunta 2

Se tiene el circuito (a) y (b). ¿Cual de ellos radiara?

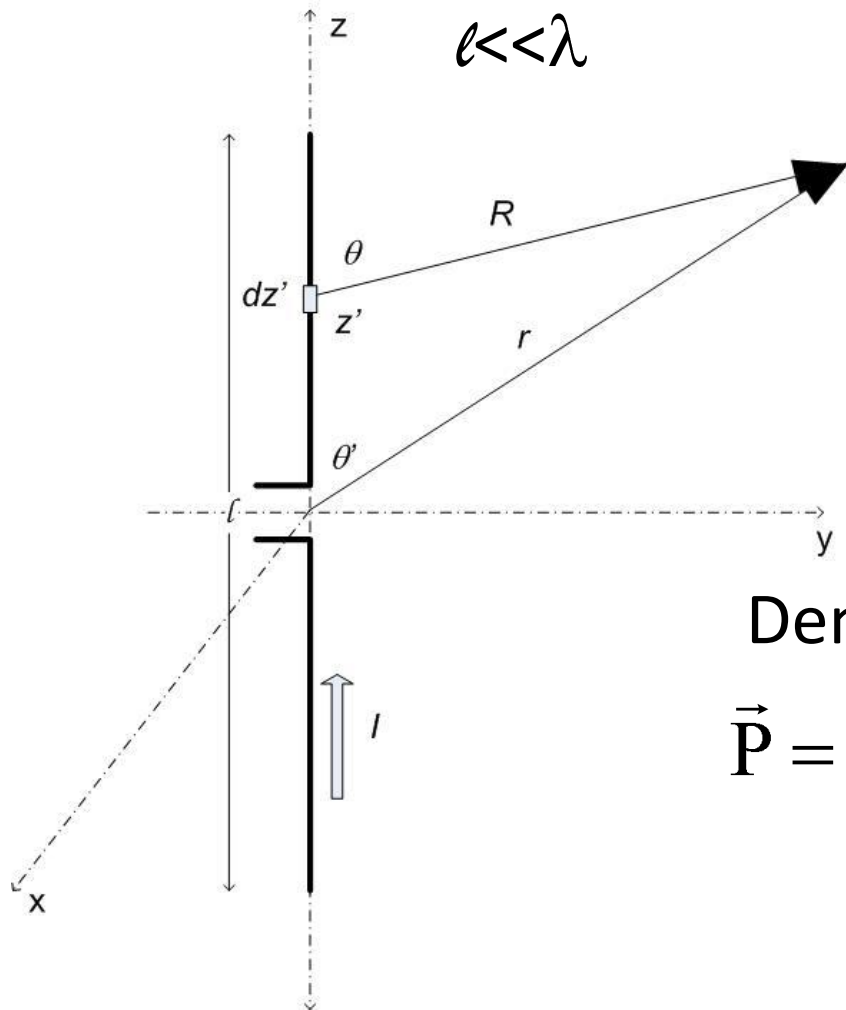


Antenas . ¿Qué es una antena?

- Cualquier elemento que radie la potencia que se le suministra, con la direccionalidad adecuada



Antenas . Dipolo Elemental, campos lejanos



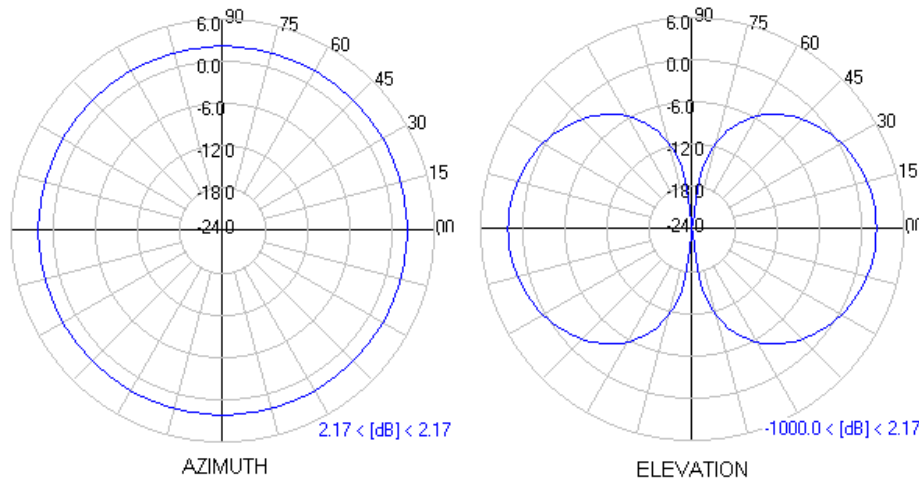
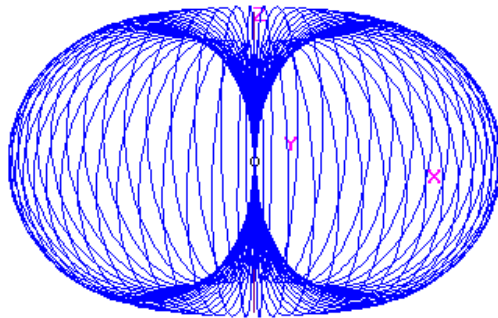
$$\vec{E}_{rad} = j\varpi\mu \frac{Il}{4\pi} \frac{e^{-jkr}}{r} \sin \theta \hat{\theta}$$

$$\vec{H}_{rad} = jk \frac{Il}{4\pi} \frac{e^{-jkr}}{r} \sin \theta \hat{\phi}$$

Densidad de potencia radiada

$$\vec{P} = \text{Re} \left[\vec{E} \times \vec{H}^* \right] = jk \frac{(Il)^2}{16\pi^2} \frac{k\varpi\mu}{r^2} \sin^2 \theta \hat{r}$$

Antenas . Dipolo Elemental, campos lejanos



Potencia radiada

$$P_r = \iint_S \vec{P} \cdot d\vec{s} = I^2 \pi \frac{\sqrt{\frac{\mu}{\epsilon}}}{2} \frac{l^2}{\lambda^2} \frac{4}{3}$$

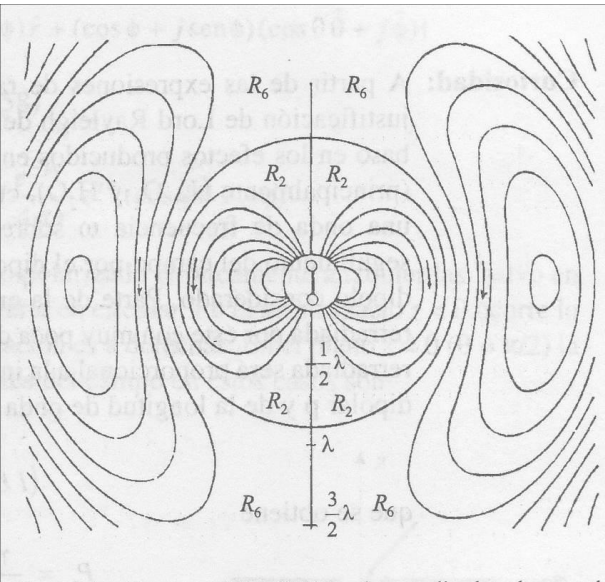
Resistencia de radiación

$$R_r = \frac{P_r}{I^2} \approx 790 \frac{l^2}{\lambda^2}$$

Directividad

$$D(\theta, \phi) = \frac{P}{P_{med}} = 1.5 \sin^2 \theta$$

Antenas . Dipolo Elemental, campos lejanos

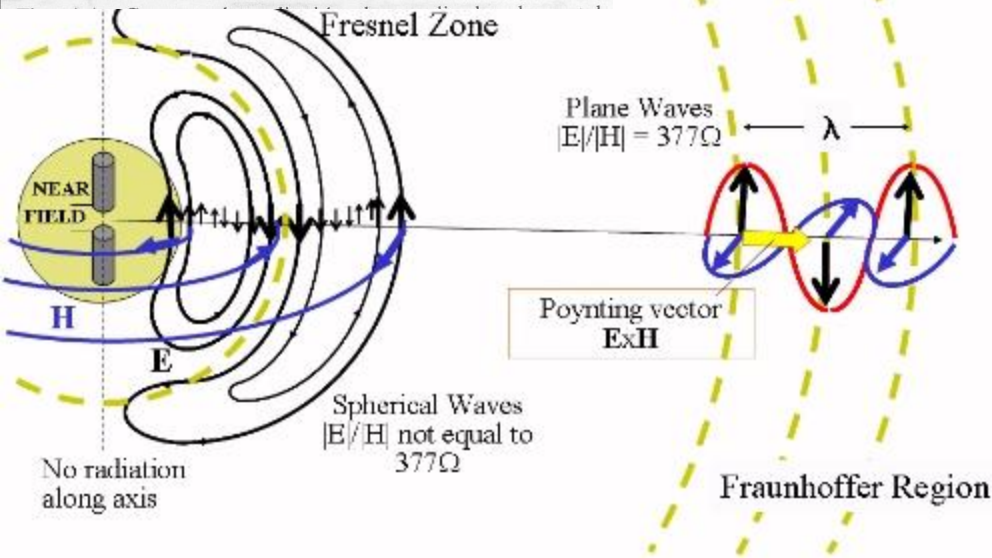


$$\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon_0}$$

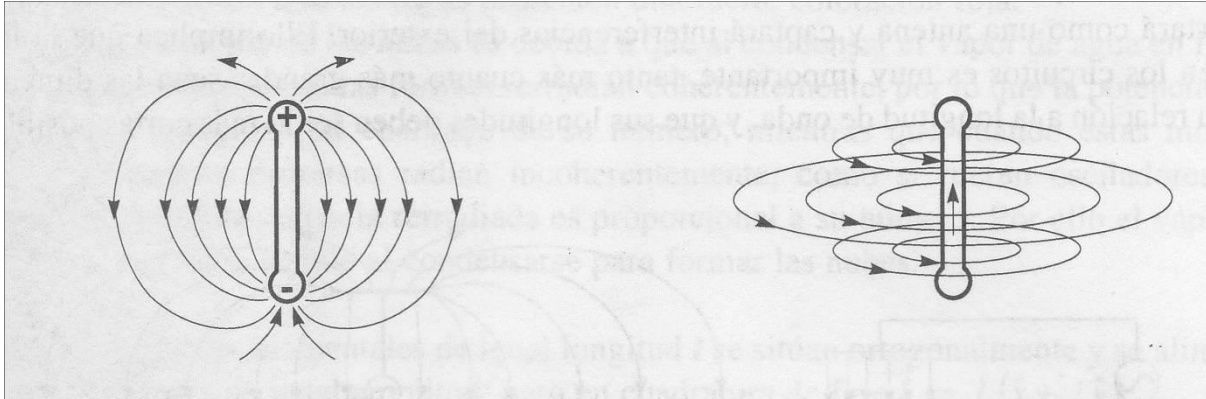
$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \times \mathbf{B} = \mu_0 \mathbf{J} + \mu_0 \epsilon_0 \frac{\partial \mathbf{E}}{\partial t}$$



Antenas . Dipolo Elemental, campos cercanos

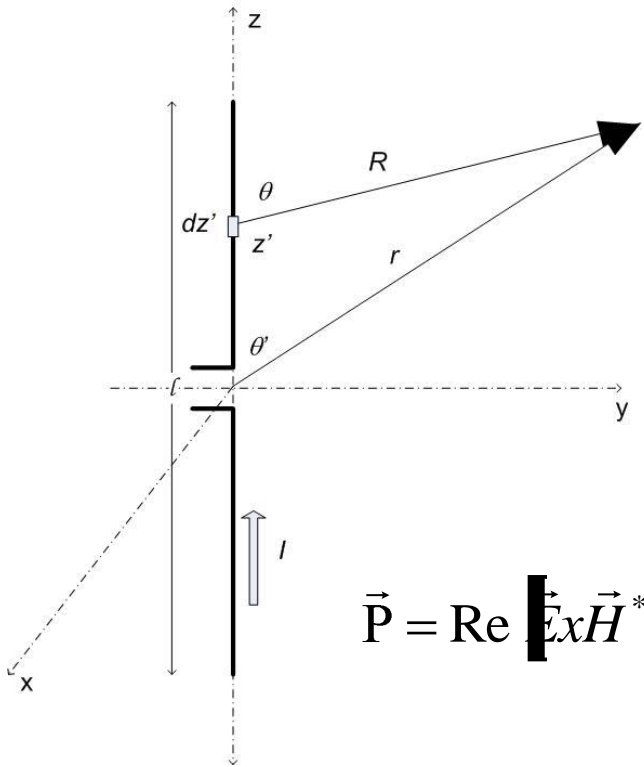


$$H_{\phi}^i = \frac{Il}{4\pi} \frac{\sin \theta}{r^2} e^{-jkr}$$

$$E_r^i = \frac{Il}{4\pi} \frac{2\cos \theta}{j\omega\epsilon^3} e^{-jkr} = \textcircled{Ql} \frac{2\cos \theta}{4\pi\epsilon^3} e^{-jkr}$$

$$E_{\theta}^i = \frac{Il}{4\pi} \frac{\sin \theta}{j\omega\epsilon^3} e^{-jkr} = \textcircled{Ql} \frac{\sin \theta}{4\pi\epsilon^3} e^{-jkr}$$

Antenas. Dipolo cilíndrica



$$E_{\theta} = j \sqrt{\frac{\mu}{\epsilon}} \frac{e^{-jkr}}{2\pi r} \frac{\cos(kH \cos \theta) - \cos kH}{\sin \theta}$$

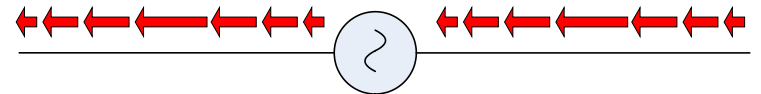
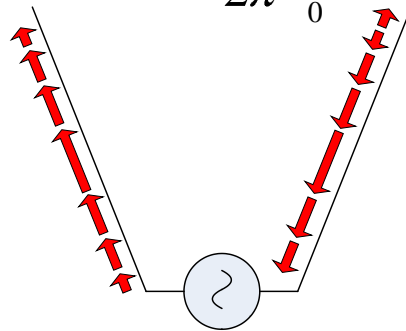
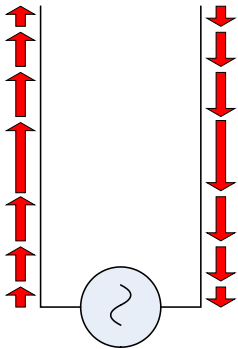
$$E_{\phi} = 0$$

$$H_{\theta} = 0$$


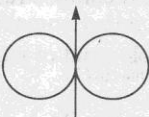
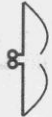
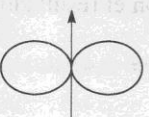

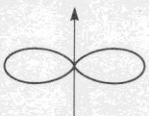

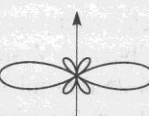



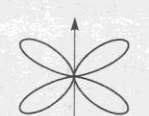
$$H_{\phi} = \frac{E_{\theta}}{\sqrt{\frac{\mu}{\epsilon}}}$$

$$\vec{P} = \text{Re} \left[\vec{E} \times \vec{H}^* \right] = jk \frac{I^2}{4\pi^2 r^2} \left(\frac{\cos(kH \cos \theta) - \cos kH}{\sin \theta} \right)^2$$

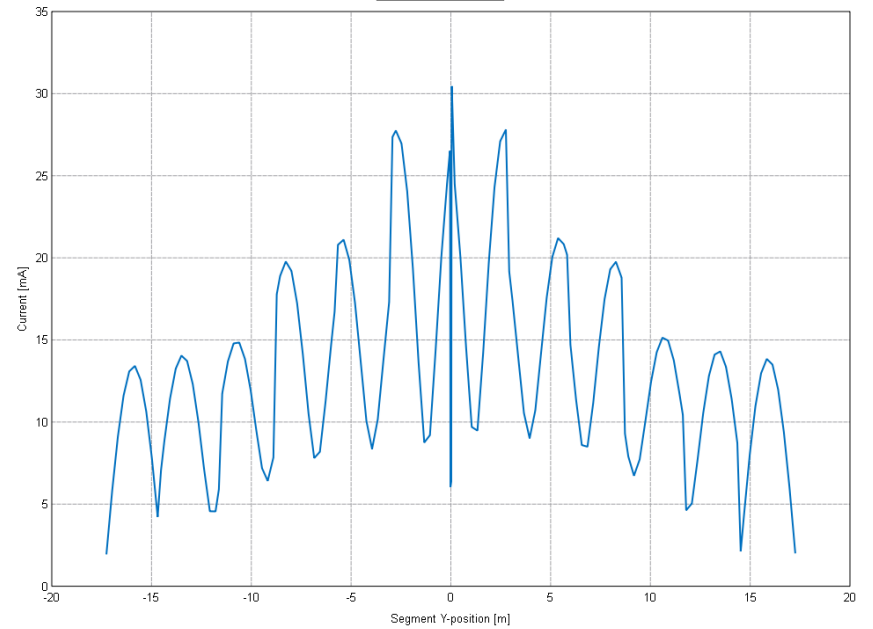
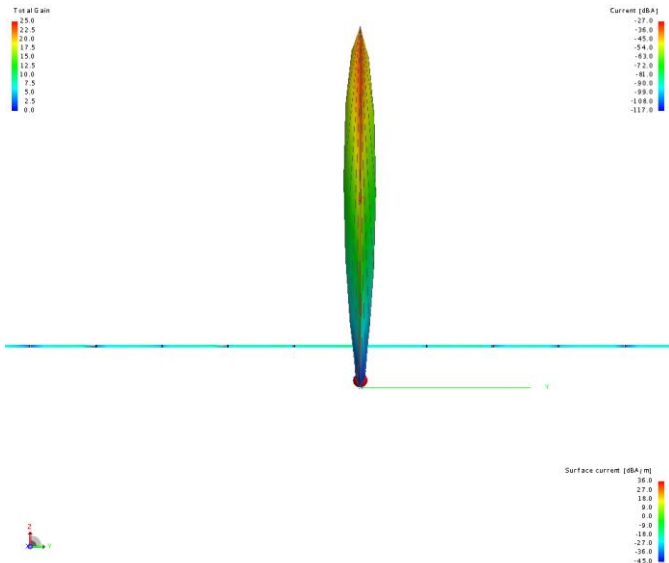
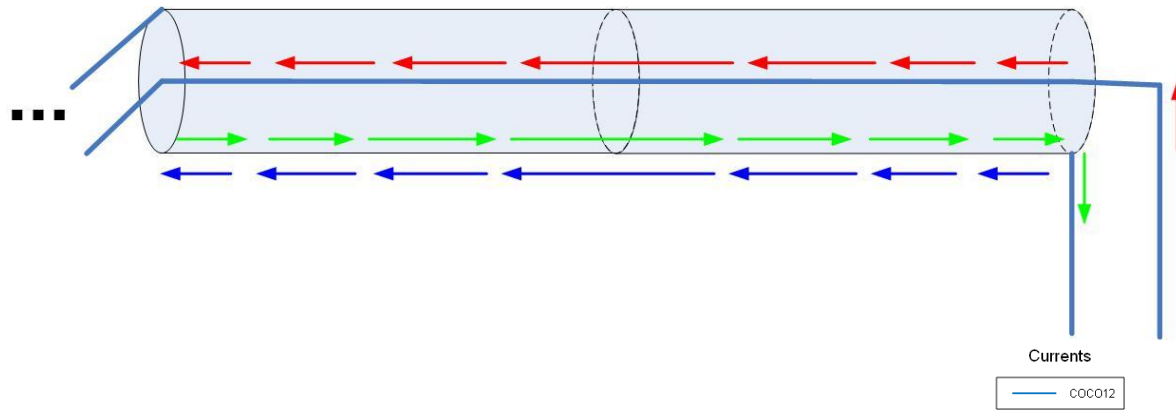
$$P_r = \iint_S \vec{P} \cdot d\vec{s} = I_m^2 \frac{\sqrt{\frac{\mu}{\epsilon}}}{2\pi} \int_0^{\pi} \frac{(\cos(kH \cos \theta) - \cos kH)^2}{\sin \theta} d\theta$$



Antenas . Dipolo de varias longitudes

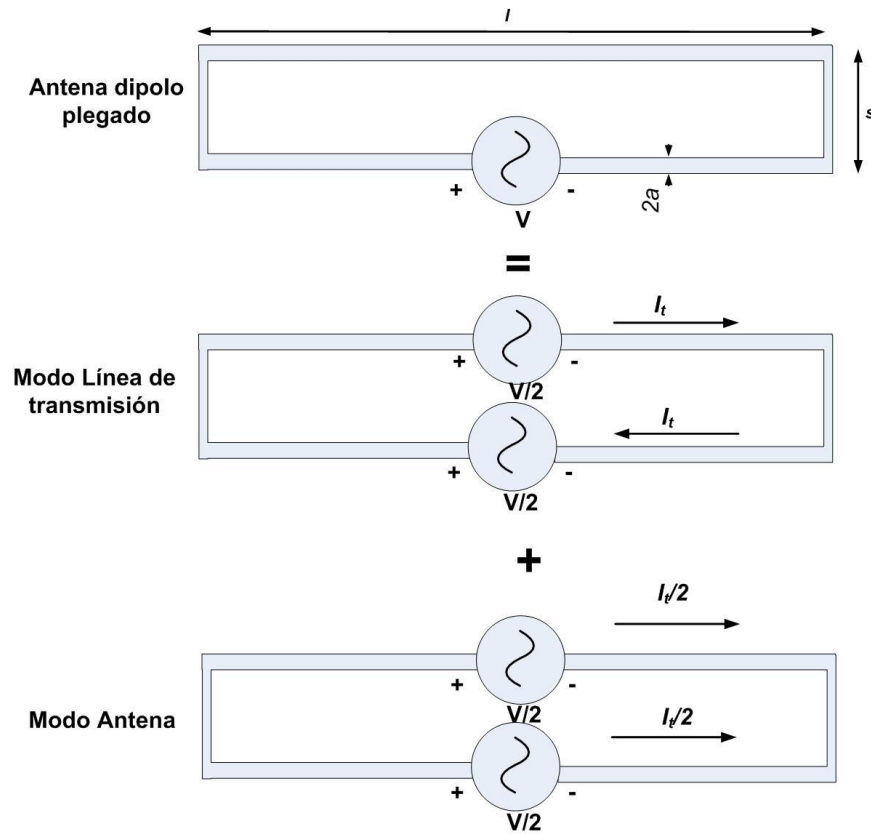
		$H = \lambda/4$ $\Delta\theta_{.3dB} = 78^\circ$	$R_{rm} = 73 \Omega$ $R_{re} = 73 \Omega$ $D = 1,64$
		$H = 3\lambda/8$ $\Delta\theta_{.3dB} = 64^\circ$	$R_{rm} = 180 \Omega$ $R_{re} = 360 \Omega$ $D = 1,94$
		$H = \lambda/2$ $\Delta\theta_{.3dB} = 48^\circ$	$R_{rm} = 199 \Omega$ $R_{re} = \infty \Omega$ $D = 2,41$
		$H = 5\lambda/8$ $\Delta\theta_{.3dB} = 33^\circ$	$R_{rm} = 105 \Omega$ $R_{re} = 210 \Omega$ $D = 3,33$
		$H = 3\lambda/4$ $\Delta\theta_{.3dB} = 33^\circ$ $\theta_{max} = 43^\circ$	$R_{rm} = 99,5 \Omega$ $R_{re} = 99,5 \Omega$ $D = 2,17$
		$H = \lambda$ $\Delta\theta_{.3dB} = 27^\circ$ $\theta_{max} = 57^\circ$	$R_{rm} = 260 \Omega$ $R_{re} = \infty \Omega$ $D = 2,52$

Antenas. COCO

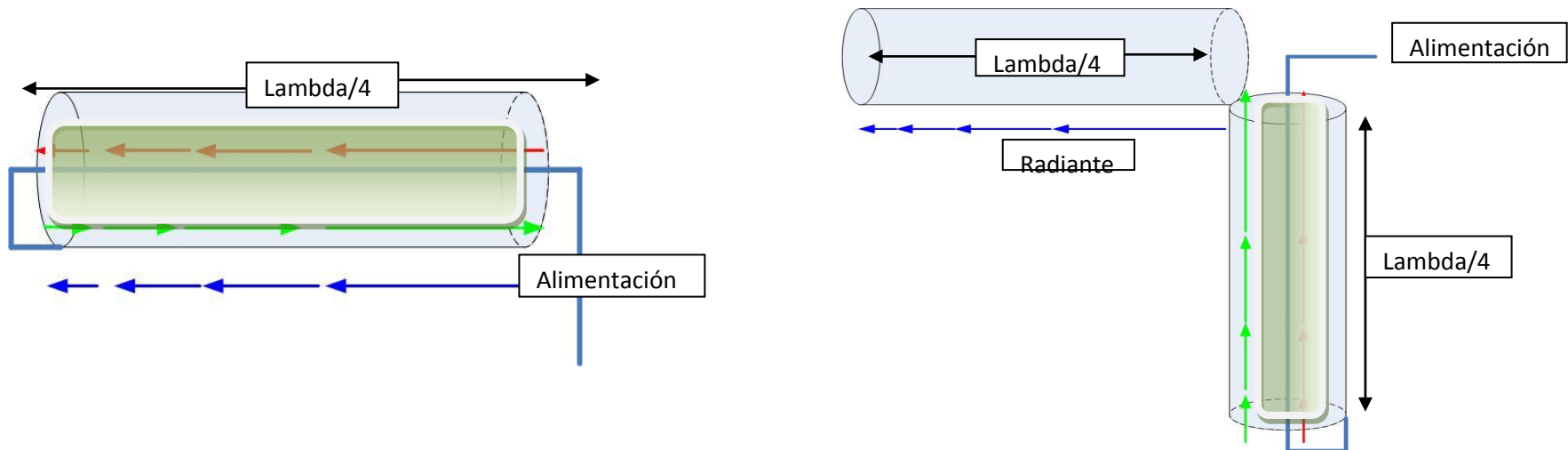
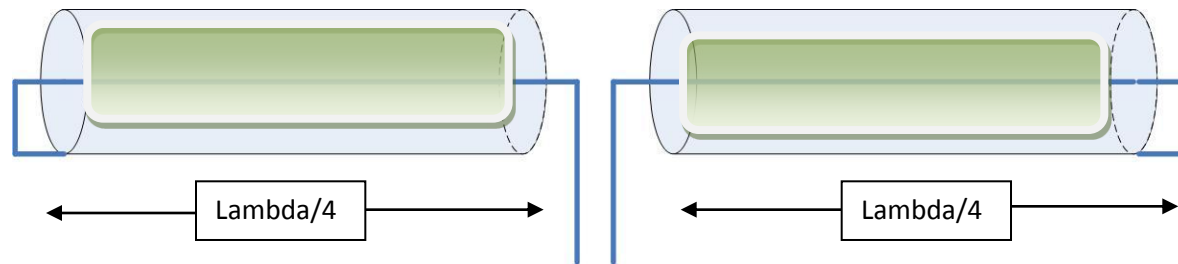


Current Magnitude [mA] (Frequency = 50 MHz) - cocosetiembreg

Antenas. Dipolo plegada



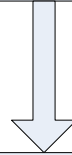
Antenas. Dipolo plegada con coaxial



Antenas. Solución utilizando Métodos numéricos

Calcular el vector potencial $A(z)$ en función de V_i

$$A_z(z) = C_1 \cos(kz) + C_2 \sin(kz) - \frac{jk}{2\omega\mu_0} \left[\sum_{i=2}^n V_i \left[\sin(k|z - z_i|) \right] \right]$$



Resolver $I(z)$ de la ecuación de potencial vector $A(z)$

$$A_z(\vec{r}) = \int_{V'} \frac{\mu \vec{J}(\vec{r}') e^{-jk|\vec{r} - \vec{r}'|}}{4\pi|\vec{r} - \vec{r}'|} dV'$$



La solución de la integral compleja de A se puede resolver por métodos numéricos, mediante la aproximación de la corriente a funciones conocidas

FIN

