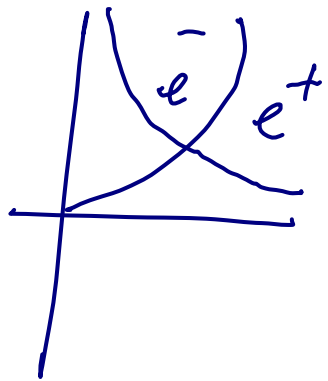


BJT small-signal Analysis

การวิเคราะห์ของ Diode สามารถทำได้ทั้งในสภาวะ
นำและใน Forward และ Reverse bias region
โดยได้สมการ



$$I_D = I_S (e^{k V_D / T_k} - 1)$$

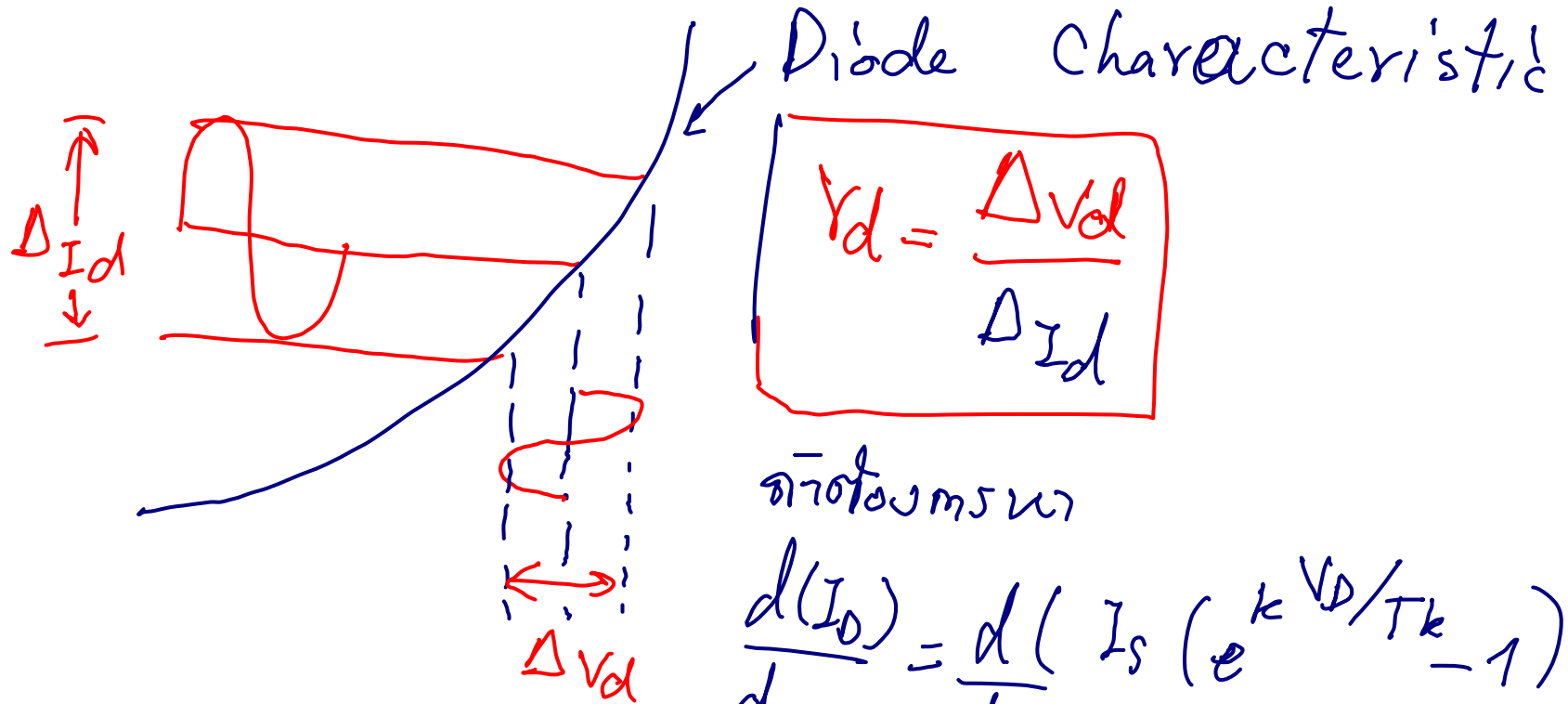
I_S = reverse saturation current

$$k = 11,600 / n \rightarrow n = \begin{cases} 1 & \text{สำหรับ Ge} \\ 2 & \text{" Si} \end{cases}$$

$$T_k = T_c + 273^\circ \text{ (kelvin)}$$

$$V_D = 115 \text{ mV ที่ } I_D = 1 \text{ mA ใน Diode}$$

AC and Dynamic Resistance



$$\frac{d(I_D)}{dV_D} = \frac{d(I_S (e^{kV_D/Tk} - 1))}{dV_D}$$

$$\text{ie, } \frac{dI_D}{dV_D} = \frac{k}{T_k} (I_D + I_S) \text{ if } I_D \gg I_S$$

$$\frac{dI_D}{dV_D} = \frac{k}{T_k} I_D$$

สมมติให้ Diode เป็น Ge จงหา

$$k = \frac{11,600}{1} = \frac{11,600}{1} = 11,600$$

ที่อุณหภูมิห้อง 25°C จงหา

$$T_k = 25^\circ + 273^\circ = 298^\circ$$

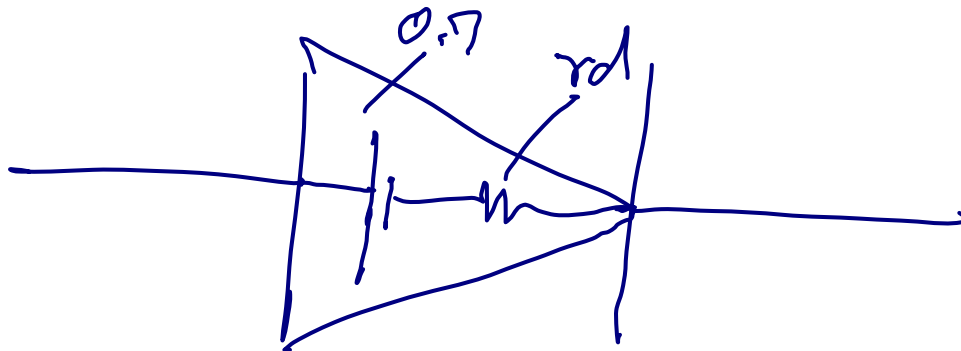
หา k/T_k จงหา

$$\frac{k}{T_k} = \frac{11,600}{298} = 38.93$$

$$\frac{dI_D}{dv_D} = 38.93 I_D$$

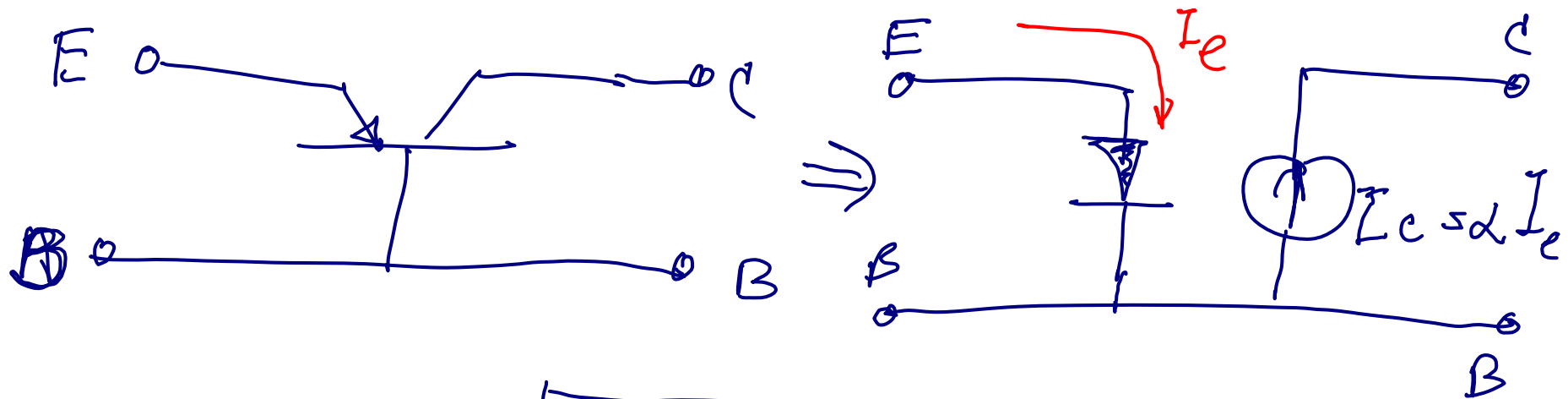
$$\frac{dv_D}{dI_D} = \frac{1}{38.93 I_D} = \frac{0.026 V}{I_D}$$

$$\boxed{\therefore r_d = \frac{26 \text{ mV}}{I_D}} \leftarrow \text{Diode}$$



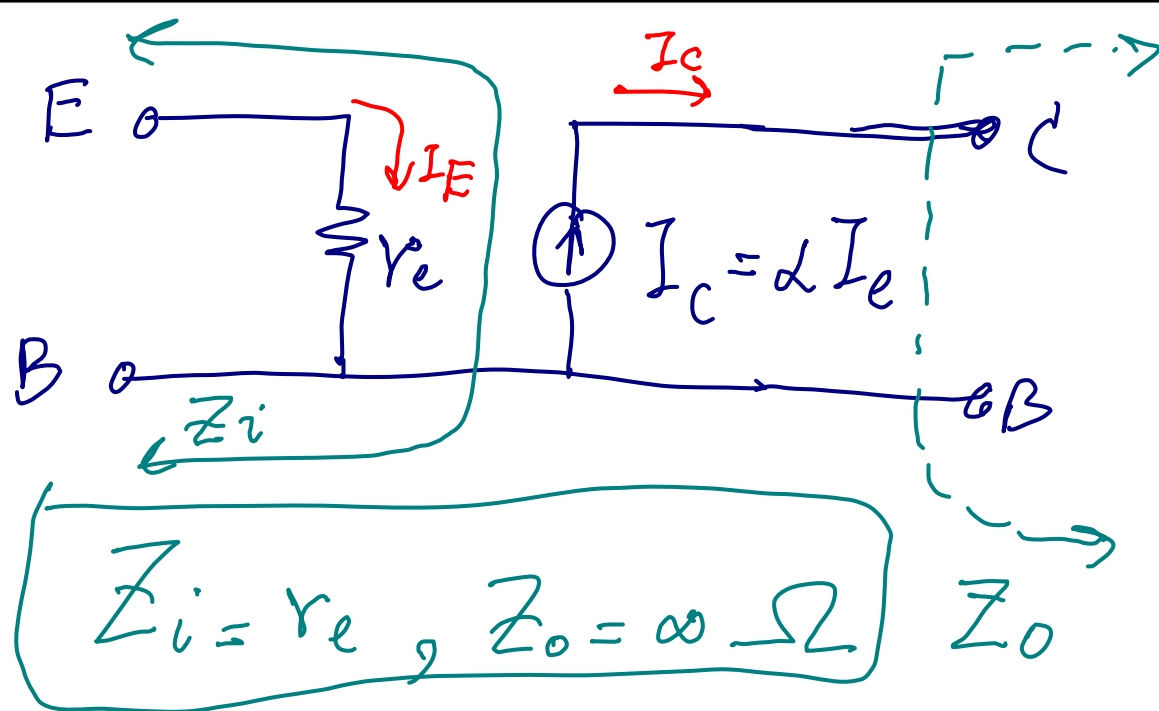
The r_e Transistor Model (Transistor)

= Common base



$$r_e = \frac{26\text{mV}}{I_E}$$

~~I_E~~



$$V_o = -I_o R_L = -(-I_c R_L) = \alpha I_e R_L$$

$$v_i = I_e Z_i = I_e r_e$$

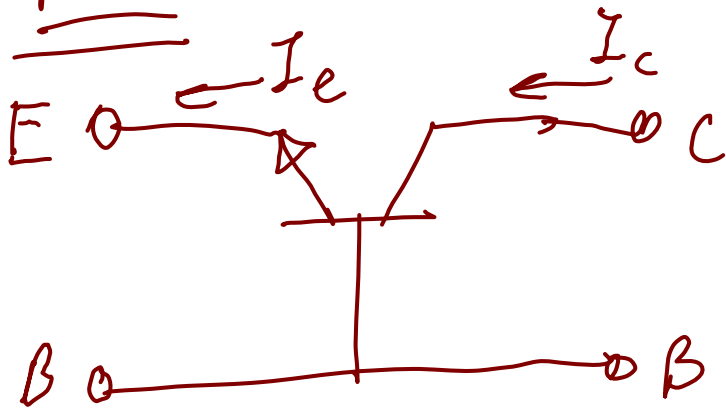
อัตราขยาย
1150 ต่อ 1 $\rightarrow A_v = \frac{V_o}{V_i} = \frac{\cancel{\alpha} \cancel{I_e} R_L}{\cancel{I_e} r_e} = \alpha \frac{R_L}{r_e}$

ถ้า $\alpha \approx 1$
ดังนั้น $A_v \approx \frac{R_L}{r_e}$ #

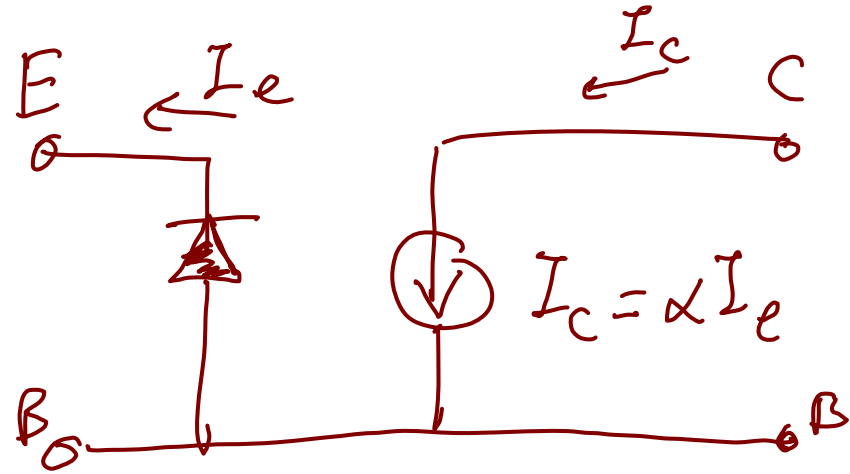
A_i (อัตราขยายกระแส: 1150) $= \frac{I_o}{I_i}$

$A_{i(cB)} = -\frac{I_c}{I_e} = -\frac{\cancel{\alpha} \cancel{I_e}}{\cancel{I_e}} = -\alpha \approx -1$

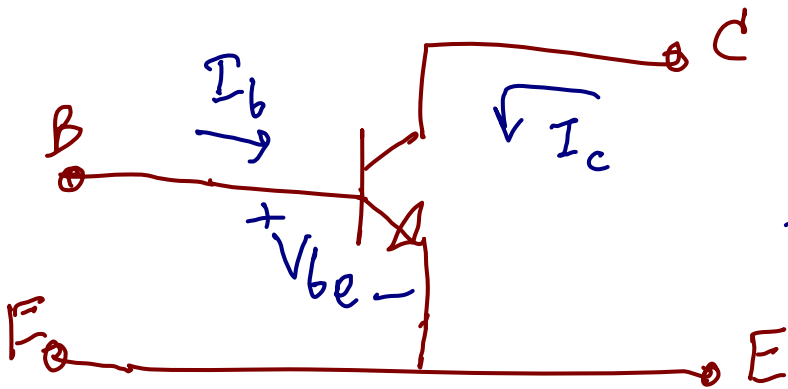
NPN



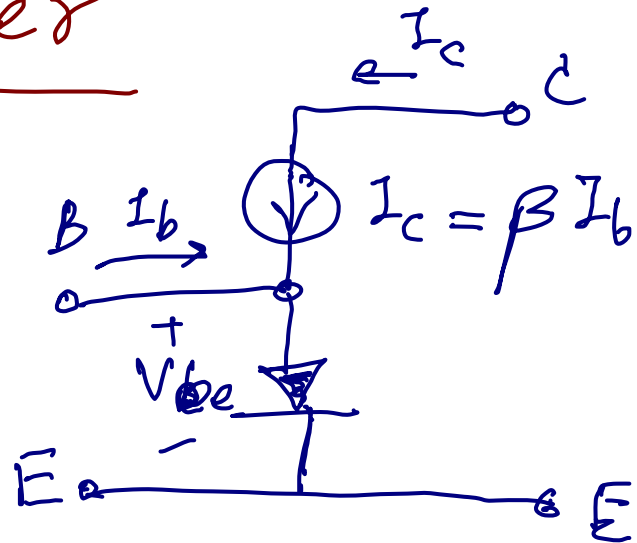
\Rightarrow



Common Emitter



\Rightarrow



$$I_c = \beta I_b$$

$$I_e = I_c + I_b = \beta I_b + I_b = (\beta + 1) I_b$$

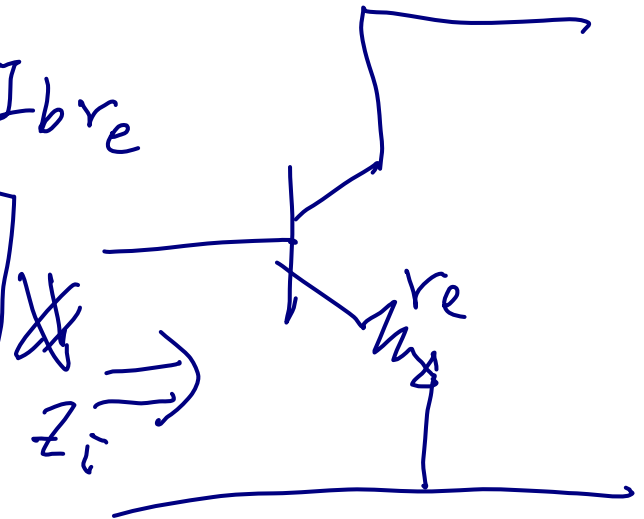
$$I_e \approx \beta I_b$$

on Z_i

$$Z_i = \frac{V_i}{I_i} = \frac{V_{be}}{I_b} \quad \#$$

$$\text{on } V_i = V_{be} = I_e r_e \approx \beta I_b r_e$$

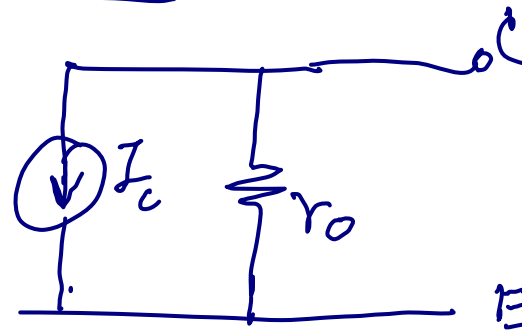
$$Z_i = \frac{\beta I_b r_e}{I_b} = \beta r_e \quad \#$$



สำหรับ CE ของ Z_i มีค่าประมาณ $100\Omega - 7k\Omega$

Z_o (output impedance)

$$Z_o = r_o$$



✓
ถ้าสมมติ $I_c = \infty$ $Z_o = \infty \Omega$ ปรากฏว่า
Voltage gain V_o/V_i หมด



$$V_o = I_c R_L = \beta I_b R_L$$

$$\text{In: } V_i, I_i Z_i = I_b \beta r_e$$

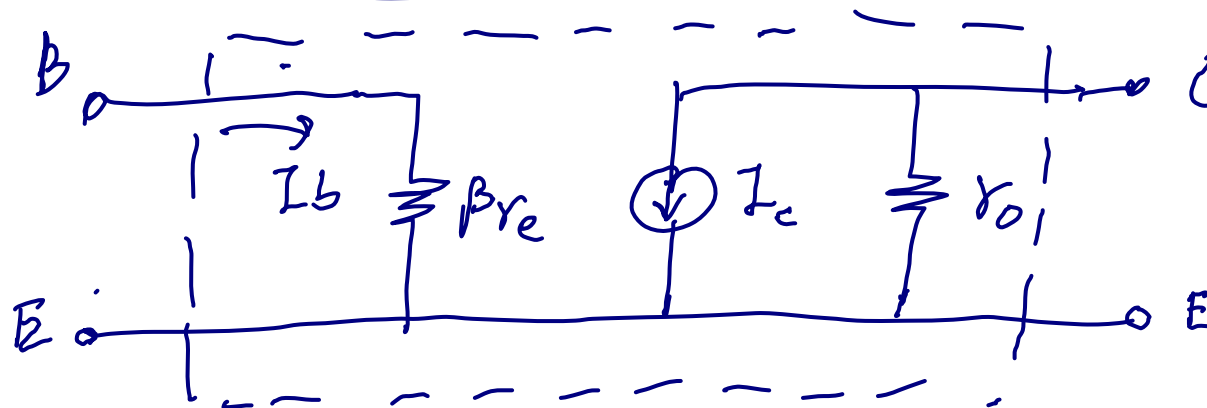
$$\therefore A_v = \frac{V_o}{V_i} = \frac{\beta I_b R_L}{\beta I_b r_e} = \frac{R_L}{r_e}$$

$$\downarrow \text{No } r_o = \infty \Omega$$

อัตราส่วนกระแส (A_i)

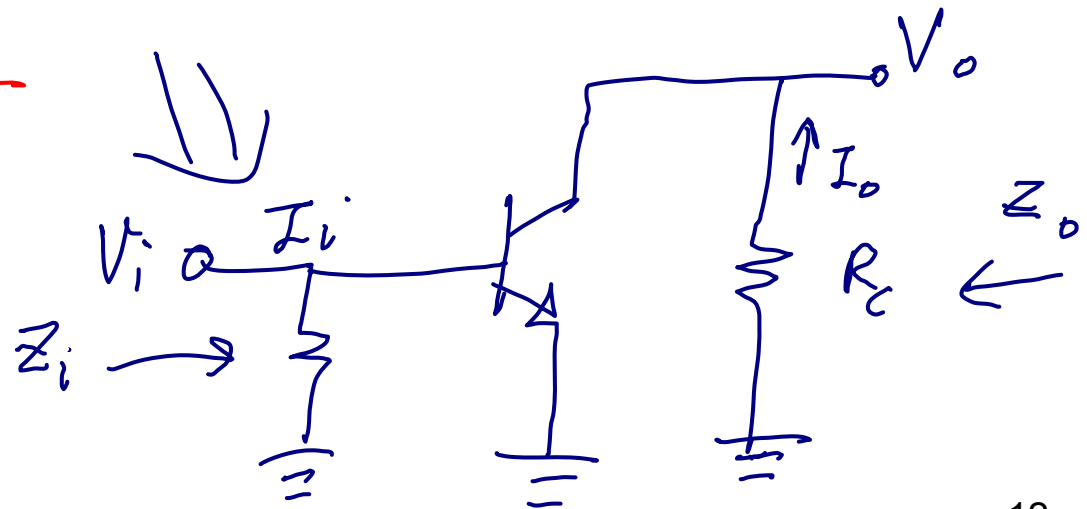
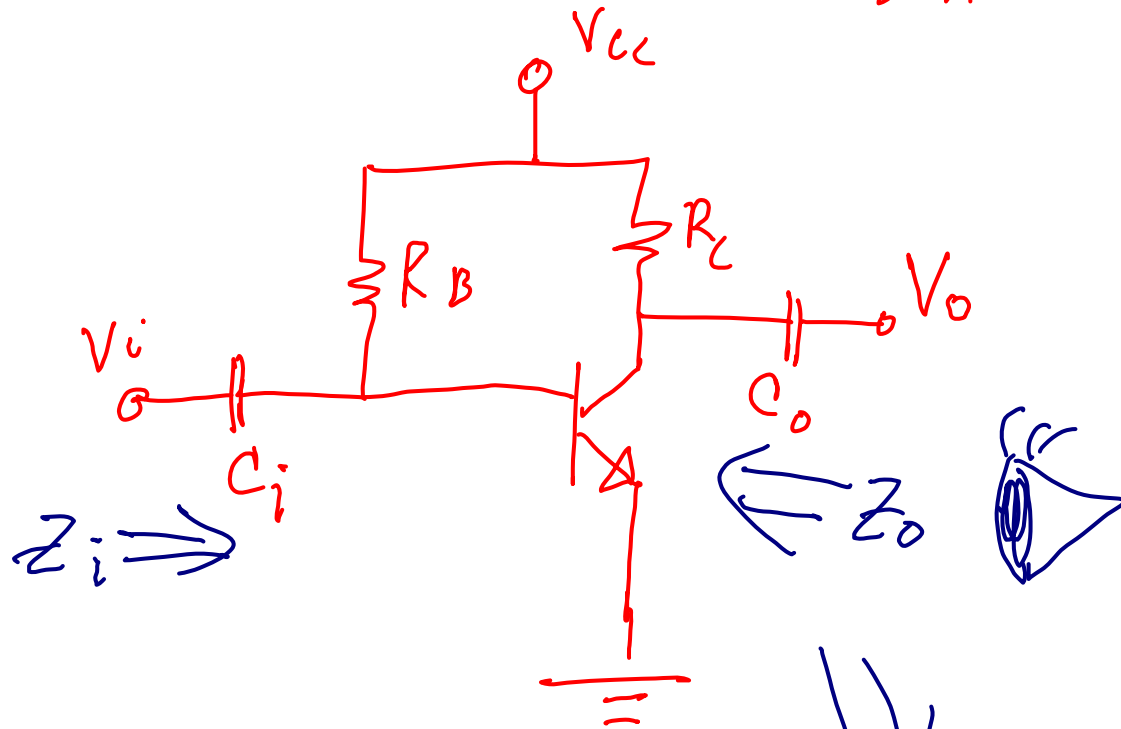
$$A_i = \frac{I_o}{I_i} = \frac{I_c}{I_b} = \frac{\beta I_b}{I_b} = \beta$$

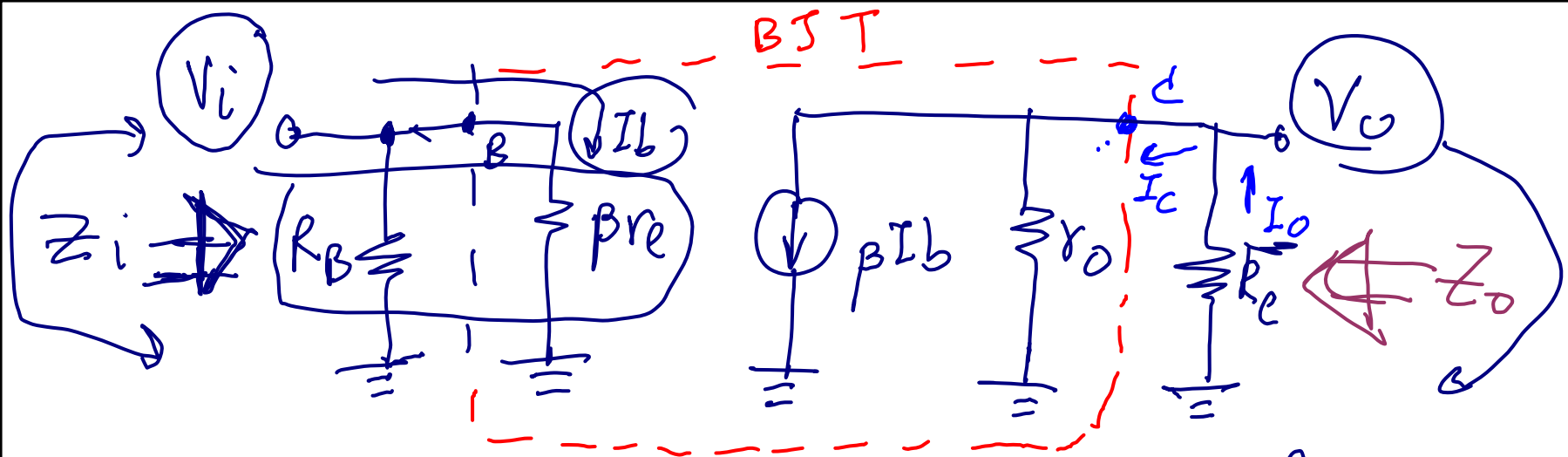
$$\downarrow \text{No } r_o = \infty \Omega$$



COMMON EMITTER FIXED-BIAS

out send





u1 Zi

$Z_i = R_B \parallel \beta r_e$
(tot)

$R_B \gg 10 \beta r_e \quad a = \frac{V_o}{V_i}$

$Z_i = \beta r_e$

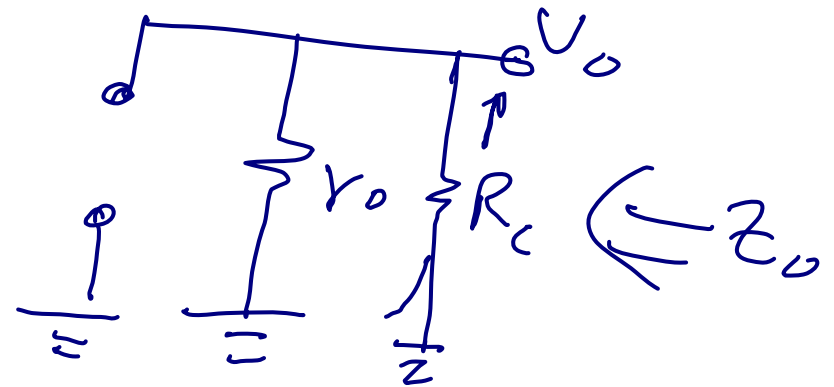
u1 Zo

$Z_o = R_C \parallel r_o$

$\frac{R_B \times \beta r_e}{R_B + \beta r_e}$

જો $r_o \gg 10 R_c$ તો:

$$Z_o = R_c$$



ક, A_v

$$V_o = -\beta \overbrace{I_b}^{I_c} (R_c \parallel r_o)$$

તેથી $I_b = \frac{V_i}{\beta r_e}$

અથવા I_b થી

$$V_o = -\beta \left(\frac{V_i}{\beta r_e} \right) (R_c \parallel r_o) =$$

$$A_v = \frac{V_o}{V_i} = - \frac{(R_c \parallel r_o)}{r_e}$$

12/0 $r_o \gg 10 R_c$ $\Rightarrow \gamma \approx 1$

$$A_v = -\frac{R_c}{r_e} \quad \#$$

หา A_v \Rightarrow หา I_o ก่อน

$$I_o = \frac{r_o \beta I_b}{r_o + R_c}$$

$$\parallel \Rightarrow \frac{I_o}{I_b} = \frac{r_o \beta}{r_o + R_c}$$

หา I_b ก่อน

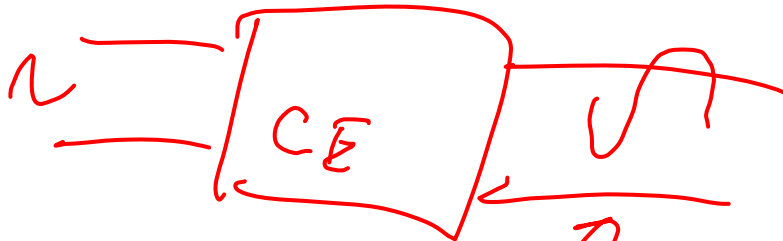
$$I_b = \frac{R_B I_i}{\beta r_e + R_B}$$

$$\text{หา } I_i = \frac{(\beta r_e + R_B) I_b}{R_B}$$

$$\text{ดังนั้น } A_v = \frac{I_o}{I_i} = \frac{r_o \beta \cancel{I_b}}{r_o + R_c} \cdot \frac{R_B}{(\beta r_e + R_B) \cancel{I_b}} = \frac{R_B r_o \beta}{(r_o + R_c)(\beta r_e + R_B)}$$

$$\beta r_o \gg 10 R_L \quad \text{and} \quad R_B \gg 10 \beta r_e \quad \Rightarrow \quad \gamma = 100\%$$

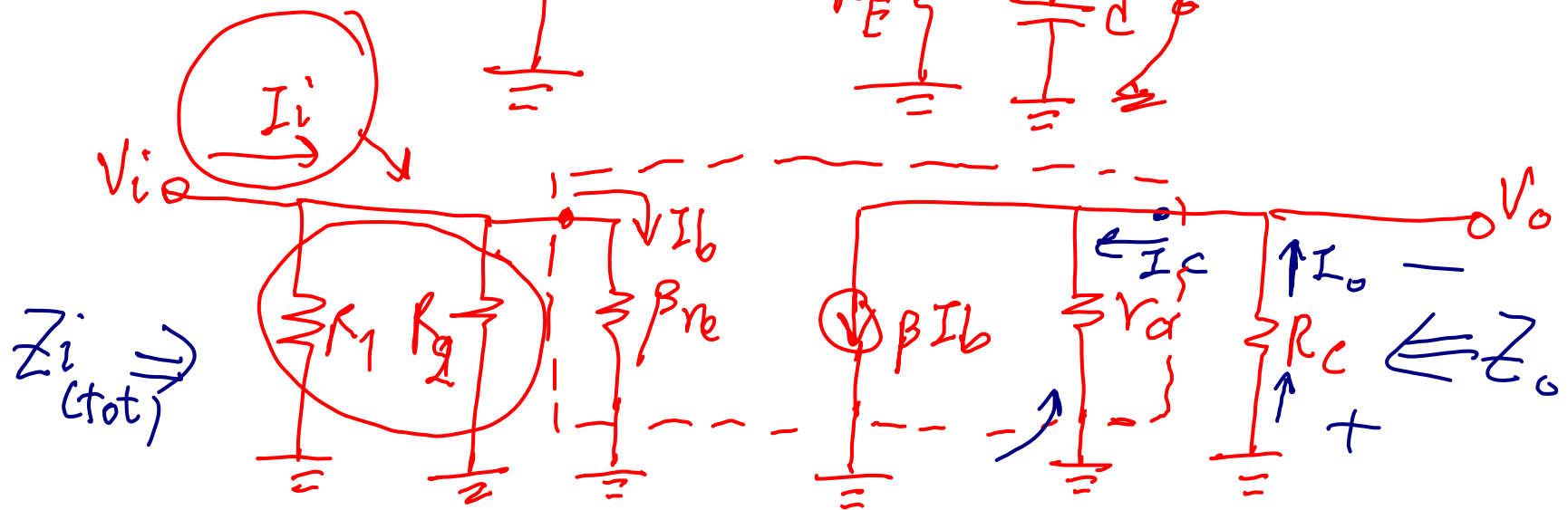
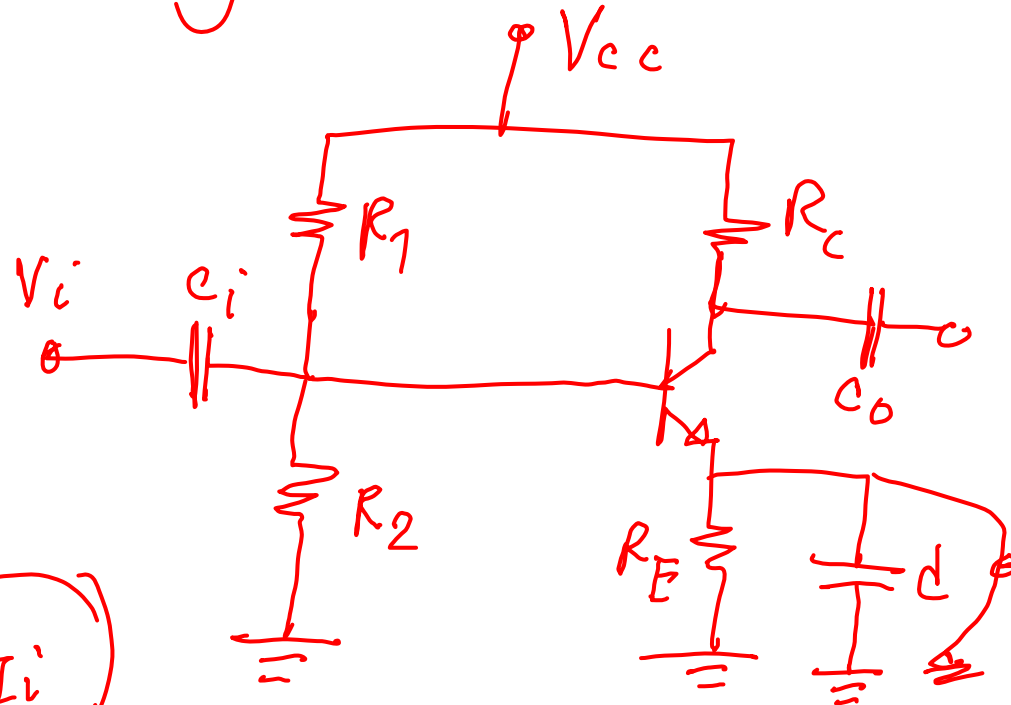
$$A_i = \frac{\beta \cancel{R_B} \cancel{r_o}}{\cancel{r_o} \cancel{R_B}} = \beta$$



$$A_i = \beta \quad \text{inverse}$$

$$A_v = \frac{-R_L}{r_e}$$

Voltage-Divider bias



$$Z_i = R_1 \parallel R_2 \parallel \beta r_e \quad *$$

$$Z_o = r_o \parallel R_c$$

if $r_o \gg R_c$ then $Z_o = R_c$

$$V_o = -(R_c \parallel r_o) \beta I_b$$

$$I_b = \frac{V_i}{\beta r_e}$$

$$V_o = -(R_c \parallel r_o) \beta \left(\frac{V_i}{\beta r_e} \right) = \frac{(R_c \parallel r_o) \cdot V_i}{r_e}$$

$$A_v = \frac{V_o}{V_i} = - \frac{R_c \parallel r_o}{r_e} \quad \text{if } r_o \gg R_c \Rightarrow A_v = - \frac{R_c}{r_e} \quad *$$

$$A_i \approx \frac{I_o}{I_i}$$

$$I_o = \frac{r_o \beta I_b}{r_o + R_c}$$

$$I_b = \frac{(R_1 \parallel R_2) I_i}{(R_1 \parallel R_2) + \beta r_e}$$

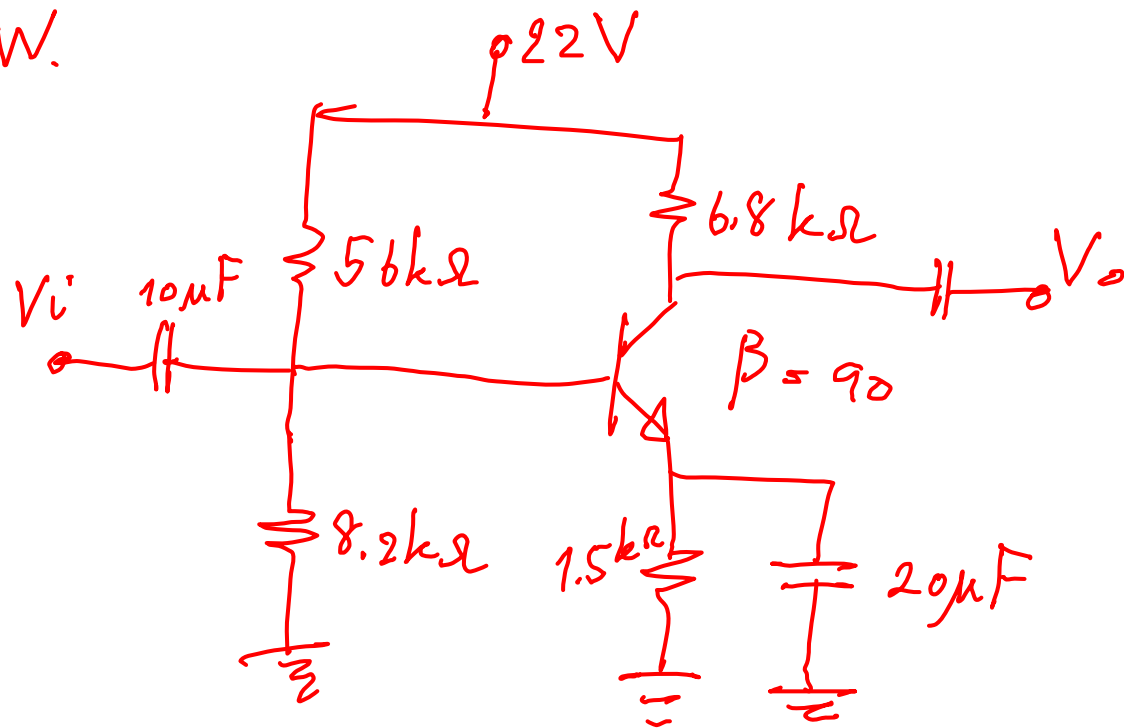
$$I_i = \frac{[(R_1 \parallel R_2) + \beta r_e] I_b}{(R_1 \parallel R_2)}$$

$$\beta r_o \gg 10 R_c \Rightarrow \beta r_o \approx 10 R_c$$

$$A_i = \frac{\beta (R_1 \parallel R_2)}{(R_1 \parallel R_2) + \beta r_e}$$

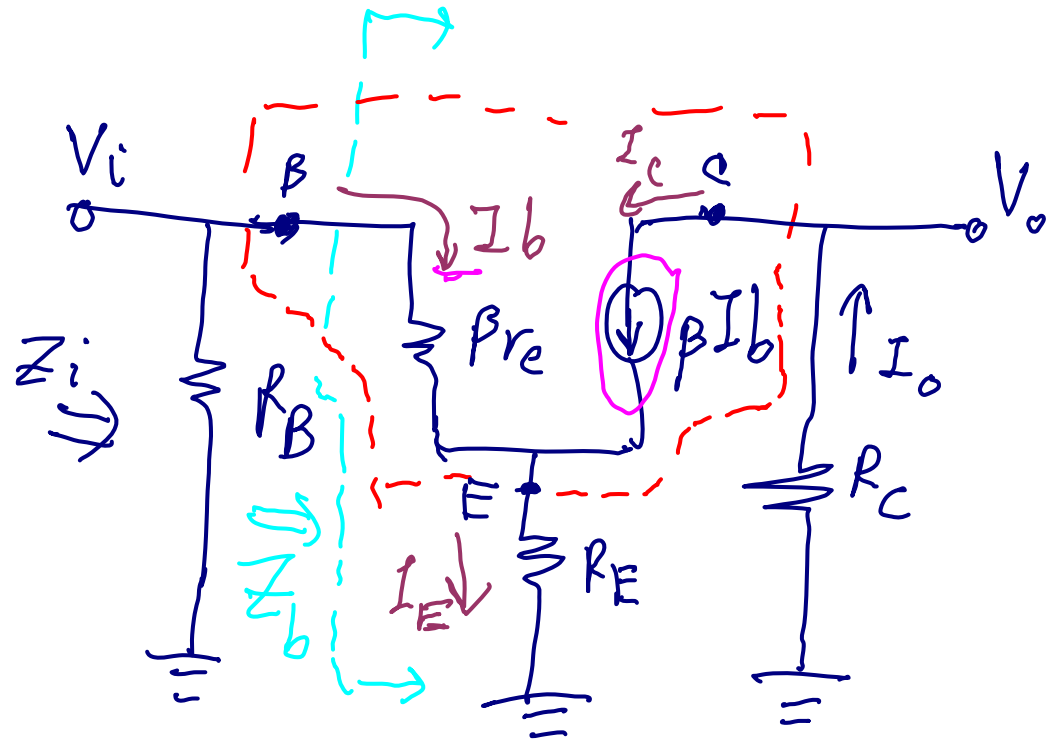
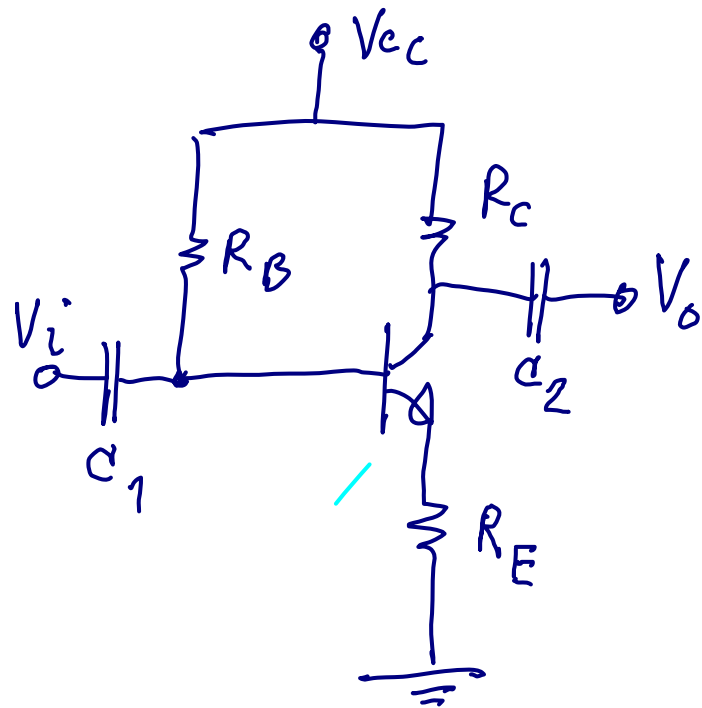
$$\therefore A_i = \frac{r_o \beta \cancel{I_b}}{r_o + R_c} \cdot \frac{(R_1 \parallel R_2)}{[(R_1 \parallel R_2) + \beta r_e] \cancel{I_b}} = \frac{r_o \beta (R_1 \parallel R_2)}{(r_o + R_c) [(R_1 \parallel R_2) + \beta r_e]}$$

H.W.



- W. a) r_e ($7.15 k\Omega$)
 b) Z_i ($1.35 k\Omega$)
 c) Z_o ($r_o = \infty \Omega$) ($6.8 k\Omega$)
 d) A_v ($r_o = \infty \Omega$) (-367.97)
 e) A_i ($r_o = \infty \Omega$) (73.04)

CE EMITTER-BIAS



u1 Zi

analysis

$$V_i = I_b r_{be} + I_E R_E$$

$$V_i = I_b r_{be} + (\beta + 1) I_b R_E$$

$$V_i = \cancel{I_b} [\beta r_e + (\beta + 1) R_E]$$

$$Z_b = \frac{V_i}{I_b} = \frac{\cancel{I_b} [\beta r_e + (\beta + 1) R_E]}{\cancel{I_b}}$$

$$Z_b = \beta r_e + (\beta + 1) R_E$$

$$\text{if } (\beta + 1) \approx \beta$$

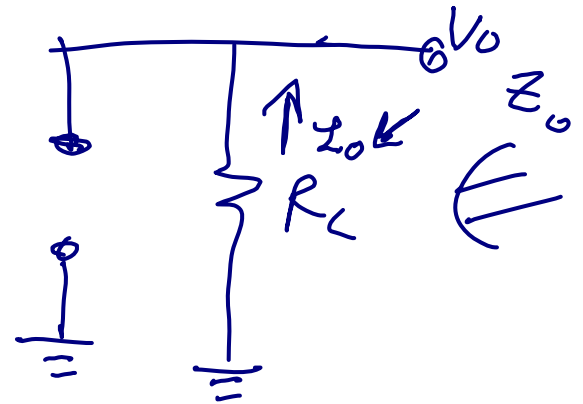
$$\therefore Z_b = \beta (r_e + R_E)$$

$$\text{if } R_E \gg r_e$$

$$\therefore \boxed{Z_b = \beta R_E}$$

$$\boxed{Z_i = Z_b \parallel R_B = \beta R_E \parallel R_B} \quad \#$$

$$\therefore Z_o = R_c \quad | \quad \text{open } \beta I_b$$



u1 A_v

$$V_o = -\beta I_b R_c$$

$$I_b = \frac{V_i}{Z_b} = \frac{V_i}{\beta R_E}$$

$$V_i = \beta R_E I_b$$

$$\therefore A_v = \frac{V_o}{V_i} = \frac{-\cancel{\beta I_b R_c}}{\cancel{\beta R_E I_b}} = -\frac{R_c}{R_E} \quad \#$$

$$A_i = \frac{I_o}{I_i}$$

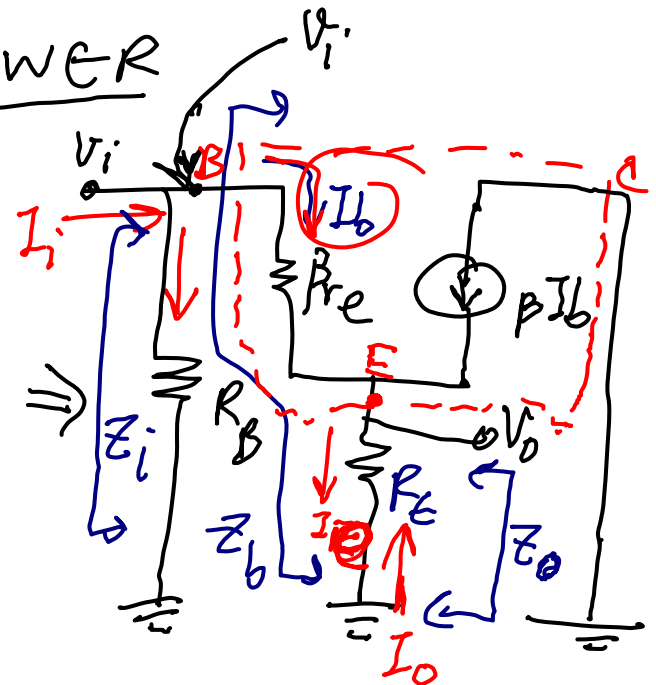
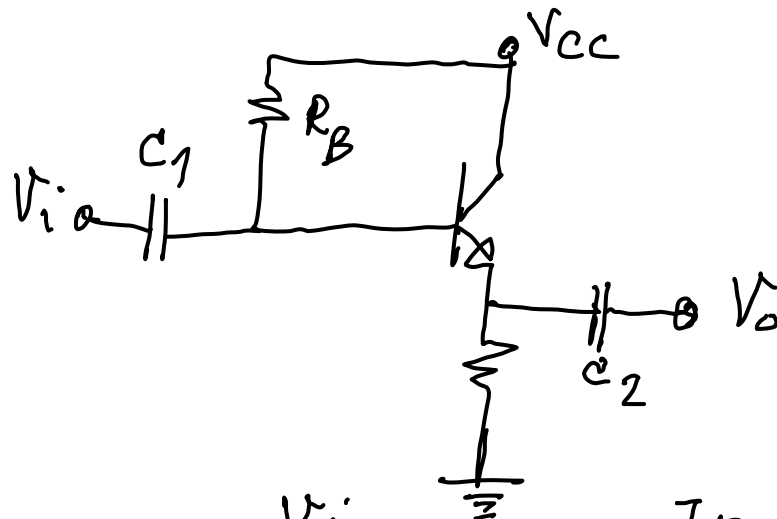
$$I_o = \frac{-V_o}{R_c} = -\beta \frac{I_b R_c}{R_c} = -\beta I_b = -I_c$$

Then $I_b = \frac{R_B I_i}{R_B + Z_b}$ (Current divider)

$$I_i = \frac{(R_B + Z_b) I_b}{R_B}$$

∴ $A_i = \frac{I_o}{I_i} = \frac{-\beta I_b}{(R_B + Z_b) I_b} \cdot R_B = \frac{-\beta R_B}{R_B + Z_b}$ ✗

EMITTER-FOLLOWER



$$Z_b = \frac{V_i}{I_b} = \frac{V_i}{I_b} = \frac{I_b r_e + I_b (\beta + 1) R_E}{I_b} = \beta r_e + (\beta + 1) R_E \approx \beta (r_e + R_E)$$

$$Z_i = R_B \parallel Z_b = R_B \parallel \beta (r_e + R_E)$$

$$Z_o = ?$$

$$\text{then } I_b = V_i / z_b \quad \text{---} (*)$$

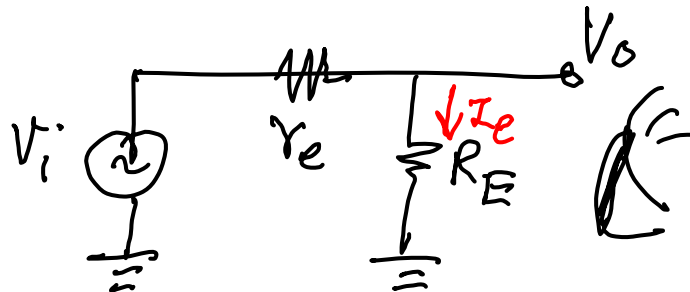
ถ้า $(\beta+1)$ ใหญ่มาก $(*)$ แล้ว $V_o \approx V_i$

$$(\beta+1) I_b = (\beta+1) V_i / z_b$$

$$I_e = \frac{(\beta+1) V_i}{r_e + (\beta+1) R_E}$$

$$Q_{w}(\beta+1) \approx \beta$$

$$\text{so } I_e = \frac{V_i}{r_e + R_E}$$



ถ้า $R_E \gg r_e$ หรือ

$$z_o = r_e$$

$$z_o = R_E \parallel r_e \quad V_i = 0$$

u) A_v

$$V_o = \frac{R_E V_i}{R_E + r_e}$$

$$A_v = \frac{V_o}{V_i} = \frac{R_E}{R_E + r_e}$$

if $R_E \gg r_e$ then $A_v \approx 1$

$$A_v = \frac{R_E}{R_E} = 1$$

u) A_i $A_i = I_o / I_i$

$$I_b = \frac{R_B I_i}{R_B + Z_b}$$

$$I_i = \frac{I_b (R_B + Z_b)}{R_B}$$

$$I_o = -I_e = -(\beta + 1)I_b$$

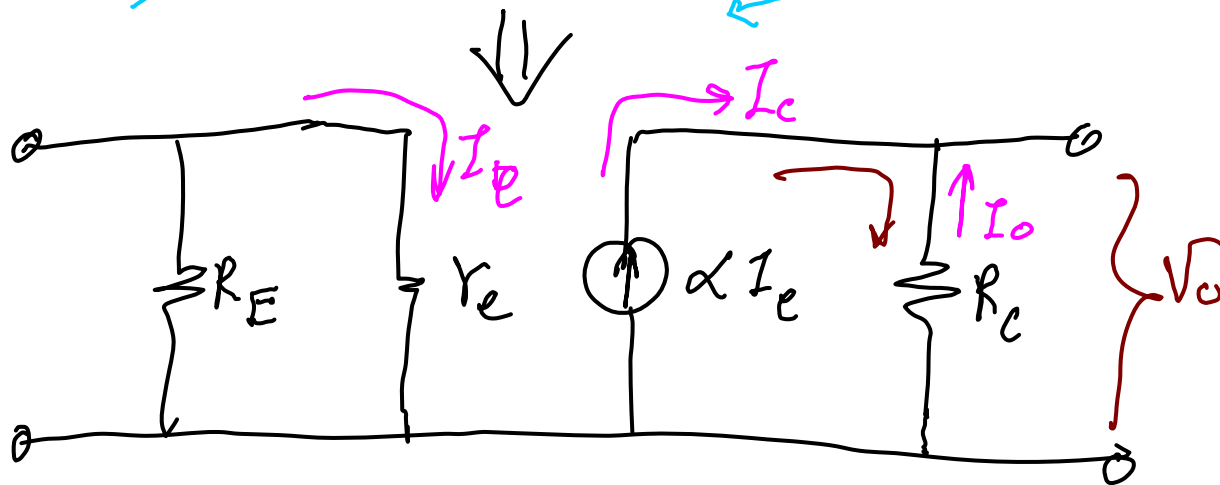
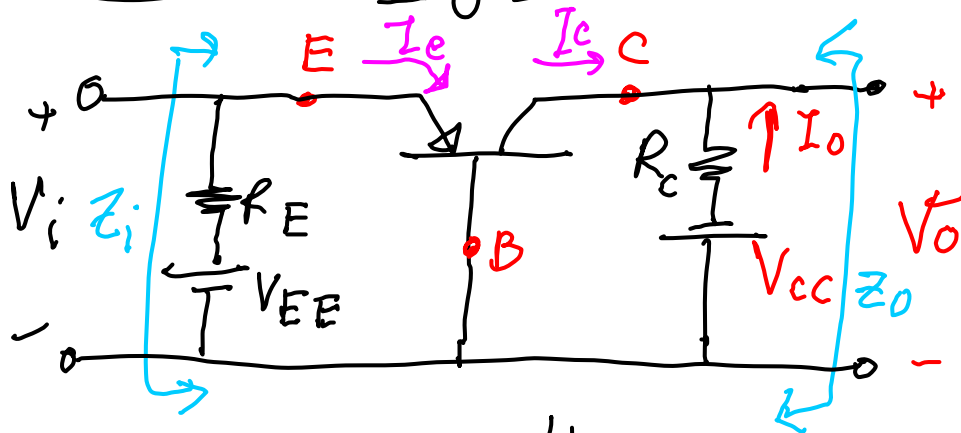
$$\therefore A_i = \frac{I_o}{I_i} = \frac{-(\beta + 1)I_b \cdot R_B}{(R_B + Z_b)I_b}$$

$$= \frac{-(\beta + 1)R_B}{R_B + Z_b}$$

$$\text{if } \beta \gg 1 \approx \beta$$

$$\therefore A_i = \frac{-\beta R_B}{R_B + Z_b}$$

C-B configuration



$$Z_i = R_E \parallel r_e$$

$$Z_o = R_C$$

$$V_o = -I_o R_C = -(-I_c) R_C = \alpha I_e R_C$$

$$V_i = I_e r_e \rightarrow I_i$$

$$I_e = V_i / r_e$$

$$\text{Then } V_o = \alpha I_e R_c = \alpha \left(\frac{V_i}{r_e} \right) R_c$$

$$A_v = \frac{V_o}{V_i} = \alpha R_c / r_e$$

$\alpha \approx 1$

$$\therefore A_v = R_c / r_e \mid \alpha \approx 1$$

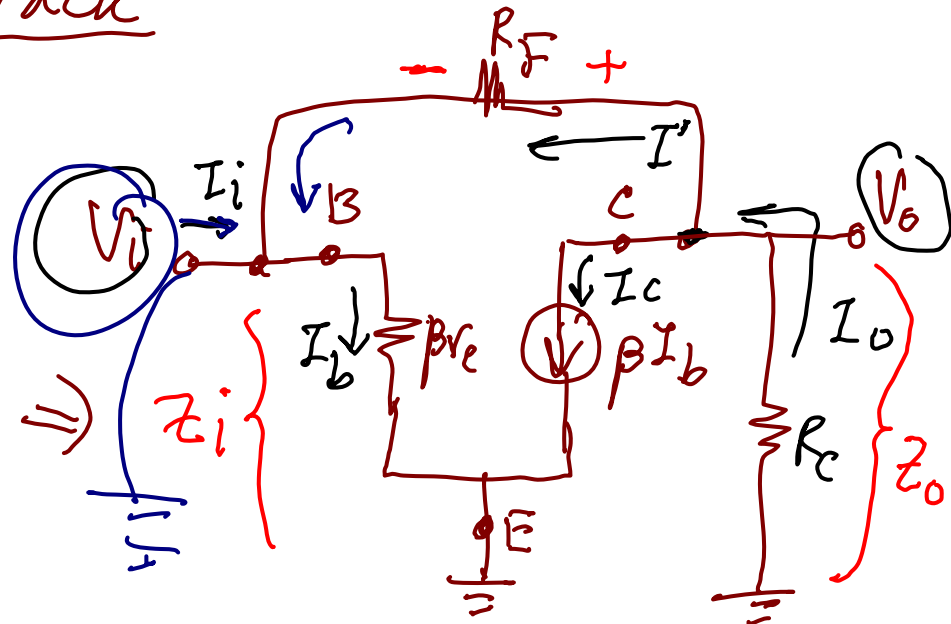
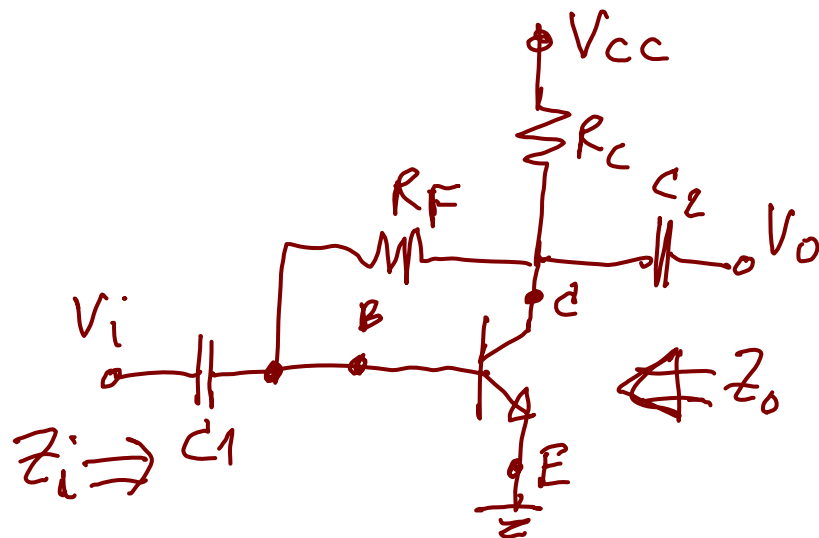
$$\text{Wt } A_i = \frac{I_o}{I_i}$$

$$\text{Then } I_o = -\alpha I_e = -\alpha I_i$$

$$A_i = \frac{I_o}{I_i} = -\alpha$$

$$A_i \approx -1$$

Collector Feedback



$$I' = \frac{V_o - V_i}{R_F} \quad (1)$$

also $V_o = -I_o R_c$

$$I_o = I' + \beta I_b$$

Since βI_b is much larger than I'

$$I_o \approx \beta I_b$$

$$V_o = -\beta I_b R_c \quad \text{--- (2)}$$

$I_b = \frac{V_i'}{\beta r_e}$

Substituting (2)

$$V_o = -\beta \frac{V_i'}{\beta r_e} R_c \quad \text{--- (3)}$$

$$A_v = \frac{V_o}{V_i} = -\cancel{\beta} R_c / \cancel{\beta} r_e = -R_c / r_e$$

Substituting (3) into (1)

$$I' = \left(-\frac{V_i R_c}{r_e} - V_i \right) / R_F = \frac{-V_i}{R_F} \left(\frac{R_c}{r_e} + 1 \right)$$

$$\text{on } V_i = I_b \beta r_e$$

$$\text{Ans } I_b = I_i + I'$$

$$\therefore V_i = (I_i + I') \beta r_e = \left[I_i + \overbrace{\left[-\frac{V_i'}{R_F} \left(\frac{R_c}{r_e} + 1 \right) \right]}^{I'} \right] \beta r_e$$

$$\textcircled{V_i} = I_i \beta r_e - \frac{V_i' \beta r_e}{R_F} \left(\frac{R_c}{r_e} + 1 \right)$$

$$I_i \beta r_e = V_i + \frac{V_i' \beta r_e}{R_F} \left(\frac{R_c}{r_e} + 1 \right)$$

$$I_i \beta r_e = V_i \left[\textcircled{1} + \frac{\beta r_e}{R_F} \left(\frac{R_c}{r_e} + 1 \right) \right] = V_i \left[\frac{R_F + \beta r_e \left(\frac{R_c}{r_e} + 1 \right)}{R_F} \right]$$

$$Z_i = \frac{V_i}{I_i} = \frac{\beta r_e}{\left[1 + \left(\frac{\beta r_e}{R_F} \left(\frac{R_c}{r_e} + 1 \right) \right) \right]}$$

$$Z_i = \frac{V_i}{I_i} = \frac{\beta r_e R_F}{R_F + \beta(R_C + r_e)}$$

$$\beta R_C \gg r_e$$

$$\therefore Z_i = \frac{\beta r_e R_F}{R_F + \beta R_C}$$

u) Z_o

$$Z_o = R_C \parallel R_F \big|_{V_i=0}$$

u) A_i 9u 95 kVL 9u Loop σ78260170052]

$$V_i + V_{R_F} - V_o = 0$$

$$\text{στη } V_i = I_b \beta r_e$$

$$V_{R_F} = I' R_F = (I_b - I_i) R_F$$

$$V_o = -I_o R_C \approx -\beta I_b R_C$$

Ημ4 V_i, V_{R_F}, V_o δι1οτ

$$I_b \beta r_e + (I_b - I_i) R_F + \beta I_b R_C = 0$$
$$I_b (\beta r_e + R_F + \beta R_C) = I_i R_F$$

thn $I_0 = \beta I_b$ do đó $I_b = \frac{I_0}{\beta}$

$$\frac{I_0}{\beta} (\beta r_e + R_F + \beta R_C) = I_i R_F$$

thì $\beta \otimes$ nó 2 lần

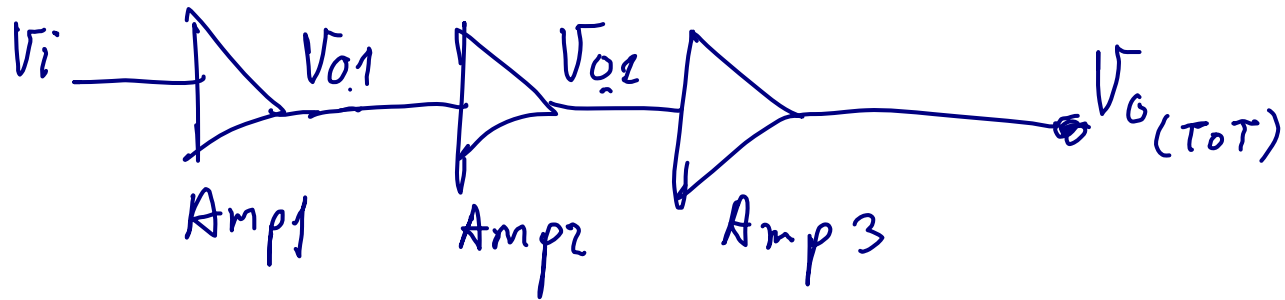
$$I_0 (\beta r_e + R_F + \beta R_C) = I_i \beta R_F$$

$$A_i = \frac{I_0}{I_i} = \frac{\beta R_F}{\beta r_e + R_F + \beta R_C}$$

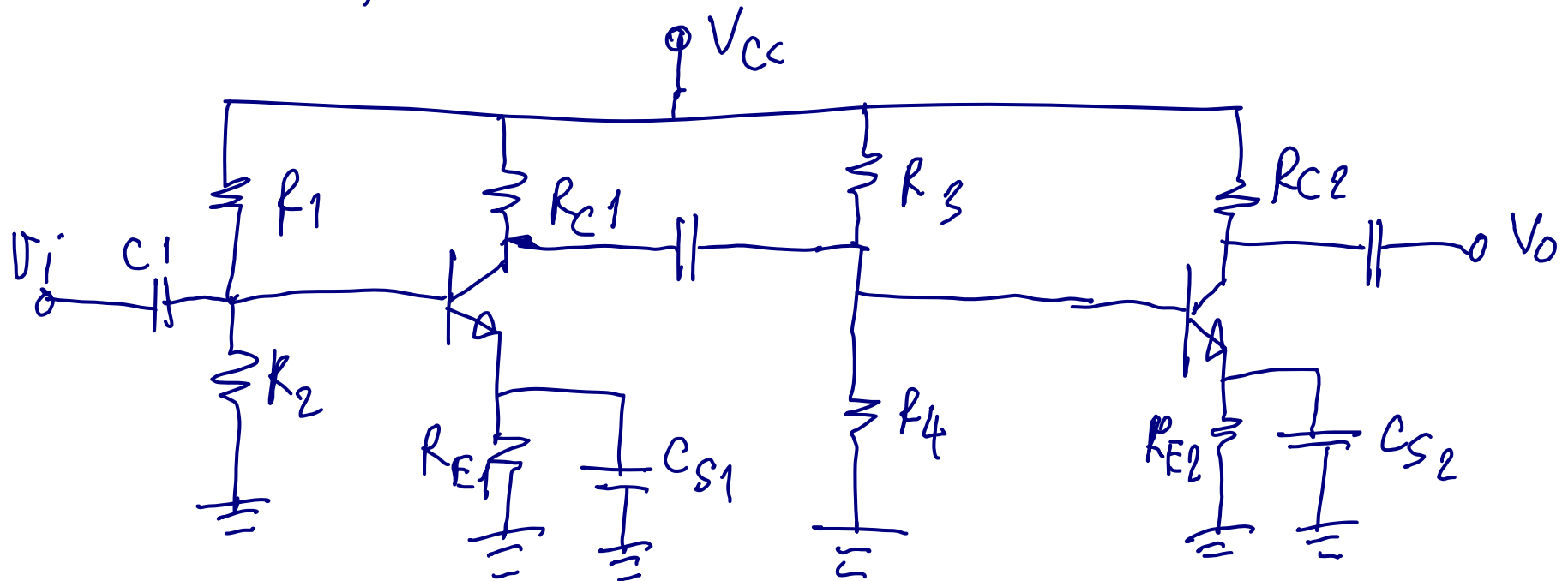
thì $\beta r_e \leq R_F \leq \beta R_C$

$$A_i = \frac{\beta R_F}{\beta R_C} = R_F / R_C$$

BJT cascade Amplifier



$$A_{V(tot)} = A_{V1} \times A_{V2} \times A_{V3}$$



$$Z_i = R_1 \parallel R_2 \parallel \beta r_e$$

$$Z_o = r_{o2} \parallel R_c$$

$$A_{v1} = \frac{R_{c1} \parallel R_3 \parallel R_4 \parallel \beta r_{e2}}{r_{e1}}$$

$$A_{v2} = \frac{R_{c2}}{r_{e2}}$$

$$\therefore A_v = A_{v1} \times A_{v2}$$

~~$$A_i \quad V_o = A_v \times V_i \quad \#$$~~