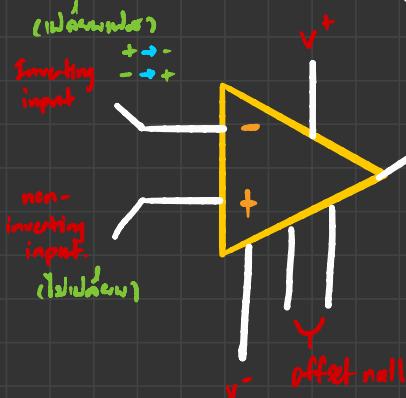
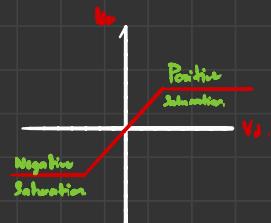
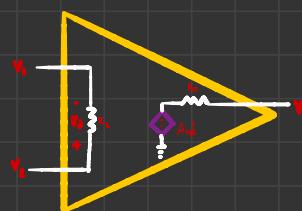


# Operational Amplifier (Op-Amp)

→ behave like "V<sub>C</sub>V<sub>S</sub>" , use in analog system (active circuit element)



## ① [Equivalent Circuit.]



$$V_d = V_2 - V_1 = V_o = A V_d = A(v_2 - v_1)$$

typical range.

Amplifier.

## ② [Ideal Op-Amp Laws].

1. Infinite open loop ,  $A \approx \infty$
2. Infinite input resistance ,  $R_i \approx \infty$
3. 0 output resistance ,  $R_o \approx 0$

→ input resistance ( $R_i$ ) =  $\infty \Omega$  (ideal)  
→ output resistance ( $R_o$ ) =  $0 \Omega$  (ideal)

$$i_1 = 0, i_2 = 0$$

$$V_d = V_2 - V_1 = 0 \rightarrow \therefore V_2 = V_1$$

$$V_d = \frac{V_o}{A}$$

L law ①

L law ② and ③.

## ③ [Configuration of Op-Amp].

### 1. inverting amplifiers.



$$V_o = -\frac{R_f}{R_i} (V_i)$$

$$\text{proof. } \frac{V_i - V_1}{R_i} = \frac{V_1 - V_o}{R_f} \quad \text{Law } V_1 = V_2 = 0!$$

$$\therefore \frac{V_i}{R_i} = -\frac{V_o}{R_f} \quad \therefore V_o = -\frac{R_f}{R_i} (V_i)$$

$R_i$  much  $\gg$  op-Amp.

## 2. non-inverting amplifier.

For obtain  $V_o = A \cdot V_i$  - op Amp.



$$V_o = \left(1 + \frac{R_f}{R_1}\right) V_i$$

proef: at Loop  $i_1$  (KVL)  $i_1 = 0$

$$-V_i + V_d + i/R_1 + i_f R_1 = 0 \rightarrow -V_i + V_d + i_f R_1 \quad : \quad i_f = \frac{V_i - V_d}{R_1}$$

at Loop  $i_f$  (KVL)  $i_f = 0$

$$-V_o + i_f R_f + i_f R_1 + i/R_1 = 0 \rightarrow V_o = i_f (R_f + R_1)$$

an if ennu. loop if.

$$\therefore V_o = \left(\frac{V_i - V_d}{R_1}\right) (R_f + R_1) \quad V_d = \frac{V_o}{A}$$

$$; V_o = \left(\frac{V_i}{R_1}\right) (R_f + R_1) - \left(\frac{V_o}{R_1}\right) (R_f + R_1)$$

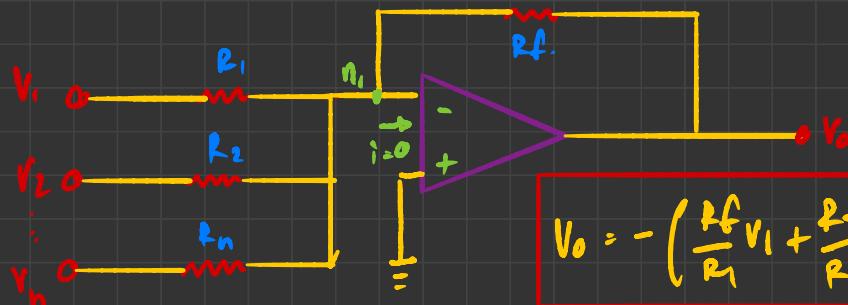
$$; V_o = \left(\frac{V_i}{R_1}\right) (R_f + R_1) - \left(\frac{V_o}{A}\right) \frac{(R_f + R_1)}{(R_1)}$$

$$; V_o + \left(\frac{V_o}{A R_1}\right) (R_f + R_1) = \left(\frac{V_i}{R_1}\right) (R_f + R_1) \quad (\text{inversie})$$

$$; V_o \left(1 + \frac{R_f + R_1}{A R_1}\right) = V_i \left(\frac{R_f}{R_1} + 1\right) \quad \lim_{A \rightarrow \infty}$$

$$\therefore \frac{V_o}{V_i} = \frac{R_f}{R_1} + 1 \quad \therefore V_o = \left(\frac{R_f}{R_1} + 1\right) V_i \quad \#$$

### 3. Inverting summing amplifier.



$$V_0 = - \left( \frac{R_f}{R_1} V_1 + \frac{R_f}{R_2} V_2 + \dots + \frac{R_f}{R_n} V_n \right)$$

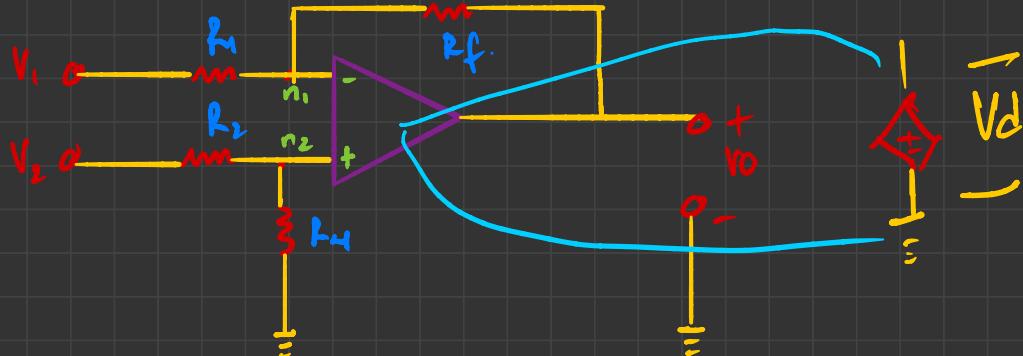
Proof. (KCL) at node 1.  $- \underline{\text{Law}} \quad V_1 = V_2 = 0!$

$$\frac{V_1 - V_{n_1}}{R_1} + \frac{V_2 - V_{n_1}}{R_2} + \frac{V_n - V_{n_1}}{R_n} = \frac{V_{n_1} - V_0}{R_f}$$

$$; \frac{V_1}{R_1} + \frac{V_2}{R_2} + \frac{V_n}{R_n} = - \frac{V_0}{R_f} \quad \therefore V_0 = - R_f \left( \frac{V_1}{R_1} + \frac{V_2}{R_2} + \dots + \frac{V_n}{R_n} \right)$$

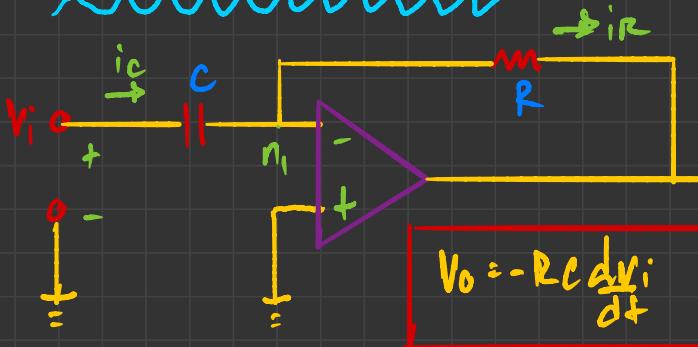
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### 4. Subtracting amplifier.



$$V_0 = V_2 - V_1$$

## 5. Differentiator Amplifier:



$$i_C = C \frac{dV_o}{dt} \quad \text{and} \quad \frac{1}{C} \int i_C dt = V_o$$

proof. KCL at node 1.  $\therefore i_C = i_R$ .

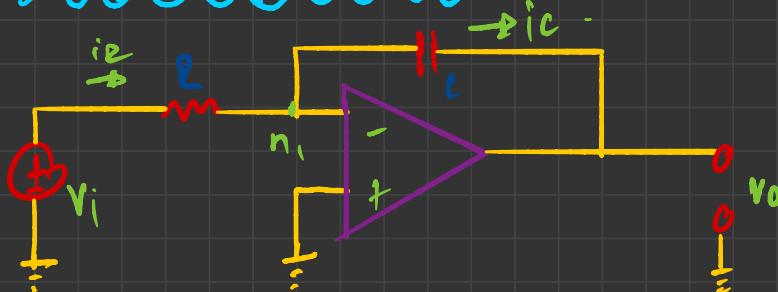
$$; (V_i - V_{n_1}) \frac{1}{RC} = V_{n_1} - V_o$$

$\Rightarrow$  ohne  $R_1 + R_2 + R_{in} \dots$   
 $\therefore$  überzeugend!

diff.  $\uparrow$   $\Rightarrow$  kapazitiver  $\frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3} \dots$

$$; V_i \frac{1}{RC} = -\frac{V_o}{R} \Rightarrow \frac{dV_i}{dt} = -\frac{V_o}{RC} \therefore V_o = -RC \frac{dV_i}{dt}$$

## 6. Integrating Amplifier



proof. (KCL) at node 1

$$\frac{V_i}{R} = i_C ; \frac{V_i}{R} = -\frac{1}{RC} \int V_o dt$$

$$V_o = \frac{-1}{RC} \int V_i dt$$

$$\therefore V_o = -\frac{1}{RC} \int V_i dt$$