



Designation: D2783 – 21

Standard Test Method for Measurement of Extreme-Pressure Properties of Lubricating Fluids (Four-Ball Method)¹

This standard is issued under the fixed designation D2783; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ϵ) indicates an editorial change since the last revision or reapproval.

1. Scope*

1.1 This test method covers the determination of the load-carrying properties of lubricating fluids. The following two determinations are made:

1.1.1 Load-wear index (formerly Mean-Hertz load).

1.1.2 Weld point by means of the four-ball extreme-pressure (EP) tester.

1.2 For the determination of the load-carrying properties of lubricating greases, see Test Method [D2596](#).

1.3 The values stated in SI units are to be regarded as standard. The values given in parentheses after SI units are provided for information only and are not considered standard.

1.4 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety, health, and environmental practices and determine the applicability of regulatory limitations prior to use.*

1.5 *This international standard was developed in accordance with internationally recognized principles on standardization established in the Decision on Principles for the Development of International Standards, Guides and Recommendations issued by the World Trade Organization Technical Barriers to Trade (TBT) Committee.*

2. Referenced Documents

2.1 *ASTM Standards:*²

[D2596](#) Test Method for Measurement of Extreme-Pressure Properties of Lubricating Grease (Four-Ball Method)

[G40](#) Terminology Relating to Wear and Erosion

¹ This test method is under the jurisdiction of ASTM Committee [D02](#) on Petroleum Products, Liquid Fuels, and Lubricants and is the direct responsibility of Subcommittee [D02.L0.11](#) on Tribological Properties of Industrial Fluids and Lubricates.

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This method was prepared under the joint sponsorship of the American Society of Lubrication Engineers. Accepted by ASLE January 1969.

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

2.2 *ANSI/ABMA/ISO Standard:*

[3290-1-2014](#) Rolling Bearings – Balls – Part 1: Steel Balls³

3. Terminology

3.1 *Definitions:*

3.1.1 *compensation line, n*—a line of plot on logarithmic paper, as shown in [Fig. 1](#), where the coordinates are scar diameter in millimetres and applied load in kilograms-force (or newtons), obtained under dynamic conditions.

3.1.1.1 *Discussion*—Coordinates for the compensation line are found in [Table 1](#), Columns 1 and 3.

3.1.1.2 *Discussion*—Some lubricants give coordinates which are above the compensation line. Known examples of such fluids are methyl phenyl silicone, chlorinated methyl phenyl silicone, silphenylene, phenyl ether, and some mixtures of petroleum oil and chlorinated paraffins.

3.1.2 *compensation scar diameter, n*—the average diameter, in millimetres, of the wear scar on the stationary balls caused by the rotating ball under an applied load in the presence of a lubricant, but without causing either seizure or welding.

3.1.2.1 *Discussion*—The wear scar obtained shall be within 5 % of the values noted in [Table 1](#), Column 3.

3.1.3 *corrected load, n*—the load in kilograms-force (or newtons) for each run obtained by multiplying the applied load by the ratio of the Hertz scar diameter to the measured scar diameter at that load.

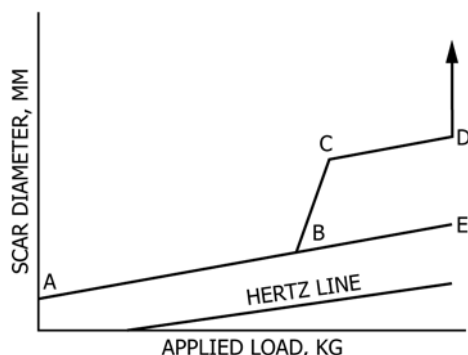
3.1.4 *extreme pressure (EP) additives, n*—tribologically reactive species that prevent mating metallic surfaces from adhering to each other under concentrated contact conditions with high PV values [PV product, [G40](#)].

3.1.4.1 *Discussion*—The PV value is the product of the contact pressure (MPa) and sliding velocity (m/s).

3.1.5 *extreme pressure (EP) lubricants, n*—formulations whose effects may become observable at different operating conditions, preventing adhesive wear under mixed or boundary lubrication regimes and are characterized by an increased load carrying capacity or increased tribofilm strength.

³ Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036, <http://www.ansi.org>.

*A Summary of Changes section appears at the end of this standard



ABE—Compensation line.
B—Point of last nonseizure load.
BC—Region of incipient seizure.
CD—Region of immediate seizure.
D—Weld point.

FIG. 1 Schematic Plot of Scar Diameter Versus Applied Load

TABLE 1 Suggested Form for Recording Test Results

| Column 1 Applied Load, kg ^A (L) | Column 2 Average Scar Diameter, mm (X) | Column 3 Compensation Scar Diameter, mm | Column 4 LD_h Factor | Column 5 Corrected Load, kg ^A (LD_h/X) |
|---|---|--|------------------------------|--|
| 6 | | | 0.95 | |
| 8 | | | 1.40 | |
| 10 | | 0.21 | 1.88 | |
| 13 | | 0.23 | 2.67 | |
| 16 | | 0.25 | 3.52 | |
| 20 | | 0.27 | 4.74 | |
| 24 | | 0.28 | 6.05 | |
| 32 | | 0.31 | 8.87 | |
| 40 | | 0.33 | 11.96 | |
| 50 | | 0.36 | 16.10 | |
| 63 | | 0.39 | 21.86 | |
| 80 | | 0.42 | 30.08 | |
| 100 | | 0.46 | 40.5 | |
| 126 | | 0.50 | 55.2 | |
| 160 | | 0.54 | 75.8 | |
| 200 | | 0.59 | 102.2 | |
| 250 | | | 137.5 | |
| 315 | | | 187.1 | |
| 400 | | | 258 | |
| 500 | | | 347 | |
| 620 | | | 462 | |
| 800 | | | 649 | |

^A To convert from kilograms-force to newtons, multiply by 9.806.

3.1.6 *Hertz line, n*—a line of plot on logarithmic paper, as shown in Fig. 1, where the coordinates are scar diameter in millimetres and applied load in kilograms-force (or newtons), obtained under static conditions.

3.1.7 *Hertz scar diameter, n*—the average diameter, in millimetres, of an indentation caused by the deformation of the balls under static load (prior to test). It may be calculated from the equation

$$D_h = 8.73 \times 10^{-2} (P)^{1/3} \quad (1)$$

where:

D_h = Hertz diameter of the contact area, and
 P = the static applied load.

3.1.8 *immediate seizure region, n*—that region of the scar-load curve characterized by seizure or welding at the startup or by large wear scars. Initial deflection of indicating pen on the optional friction-measuring device is larger than with nonseizure loads. See Fig. 1.

3.1.9 *incipient seizure or initial seizure region, n*—that region at which, with an applied load, there is a momentary breakdown of the lubricating film. This breakdown is noted by a sudden increase in the measured scar diameter and a momentary deflection of the indicating pen of the optional friction-measuring device. See Fig. 1.

3.1.10 *last nonseizure load, n*—the last load at which the measured scar diameter is not more than 5 % above the compensation line at the load. See Fig. 1.

3.1.11 *load carrying capacity, n*—the load carrying capacity of a lubricant is the maximum PV value [PV limit, G40] that can be sustained by the lubricant at a reported temperature without failure of the sliding contact surfaces as evidenced by adhesive wear or localized welding.

3.1.11.1 *Discussion*—The PV value is the product of the contact pressure (MPa) and sliding velocity (m/s).

3.1.12 *load-wear index (or the load-carrying property of a lubricant), n*—an index of the ability of a lubricant to minimize wear at applied loads.

3.1.12.1 *Discussion*—Under the conditions of this test, specific loadings in kilograms-force (or Newtons) having intervals of approximately 0.1 logarithmic units, are applied to the three stationary balls for ten runs prior to welding. The load-wear index is the average of the sum of the corrected loads determined for the ten applied loads immediately preceding the weld point.

3.1.13 *weld point, n*—under the conditions of this test, the lowest applied load in kilograms at which the rotating ball welds to the three stationary balls, indicating the extreme-pressure level of the lubricants-force (or newtons) has been exceeded.

3.1.13.1 *Discussion*—Some lubricants do not allow true welding, and extreme scoring of the three stationary balls results. In such cases, the applied load which produces a maximum scar diameter of 4 mm is reported as the weld point.

4. Summary of Test Method

4.1 The tester is operated with one steel ball under load rotating against three steel balls held stationary in the form of a cradle. Test lubricant covers the lower three balls. The rotating speed is 1760 r/min \pm 40 r/min. The machine and test lubricant are brought to 18 °C to 35 °C (65 °F to 95 °F) and then a series of tests of 10 s duration are made at increasing loads until welding occurs. Ten tests are made below the welding point. If ten loads have not been run when welding occurs and the scars at loads below seizure are within 5 % of the compensation line (AB Fig. 1) no further runs are necessary. The total can be brought to ten by assuming that loads below the last nonseizure load will produce wear scars equal to

the “compensation scar diameter.” Values of these “assumed” scars are given in Table 1. For clarification of “last nonseizure load” and “weld point” see Fig. 1.⁴

5. Significance and Use

5.1 This test method, used for specification purposes, differentiates between lubricating fluids having low, medium, and high level of extreme-pressure properties. The user of this method should determine to his own satisfaction whether results of this test procedure correlate with field performance or other bench test machines.

6. Apparatus

6.1 *Four-Ball Extreme-Pressure Tester*,⁵ illustrated in Figs. 2 and 3.

NOTE 1—It is important to distinguish between the four-ball EP tester and the four-ball wear tester. The four-ball EP tester is designed for testing under more severe conditions and lacks the sensitivity necessary for the four-ball wear test.

6.2 *Microscope*, equipped with a calibrated measuring scale and readable to an accuracy of 0.01 mm.

6.3 *Timer*, graduated in tenths of a second.

NOTE 2—Optional equipment with four-ball apparatus consists of a friction-measuring device electrically driven and conveniently graduated in 10 s markings.

7. Materials

7.1 *Cleaning Solvent*, safe, non-film forming, nonchlorinated. (**Warning**—Flammable. Harmful if inhaled. See A1.1.)

NOTE 3—Certain petroleum distillates, formerly used as solvents, have been eliminated due to possible toxic effects. Each user should select a solvent that can meet applicable safety requirements and thoroughly clean

machine parts. Reagent Grade Stoddard solvent is an example of a solvent that has been found suitable.

7.2 *Rinse Solvent*, same as in 7.1, but with higher volatility. ASTM *n*-Heptane is an example of one such rinse solvent that has been found suitable. (**Warning**—Flammable. Harmful if inhaled. See A1.2.)

7.3 *Test Balls*⁶—Test balls shall be chrome alloy steel, made from AISI standard steel No. E-52100, with diameter of 12.7 mm (0.5 in.), Grade 25 EP (Extra Polish). Such balls are described in B3.12, for Metal Balls. The Extra-Polish finish is not described in that specification. The Rockwell C hardness shall be 64 to 66, a closer limit than is found in the ANSI requirement.

8. Preparation of Apparatus

8.1 Thoroughly clean four new test balls, test-lubricant cup, and chuck assemblies by first washing with cleaning solvent (see 7.1) and then rinse solvent (see 7.2).

NOTE 4—Do not use solvents such as carbon tetrachloride or other solvents that may inherently possess load-carrying properties which may affect the results.

8.2 Lower the crosshead by raising the lever arm. Lock the lever arm in the raised position by means of a locking arrangement for that purpose.

9. Procedure

9.1 Place the three test balls in the test-lubricant cup. Place the lock ring over the test balls and screw down the nut securely (Note 5). Pour the lubricating fluid to be tested over the three test balls until they are covered.

NOTE 5—Subsequent independent investigations reported in 1971 by several laboratories indicate that optimum test repeatability is obtained when the force on the lock-down nut is maintained within the range 68 N·m ± 7 N·m (50 ft·lb ± 5 ft·lb), applied, and measured by means of

⁴ Further details applicable to this method may be found in: Sayles, F. S., et al., “The Four-Ball E. P. Tester, An ASTM Method of Test,” *National Lubricating Grease Institute*, NLGIA, Vol 32, No. 5, August 1968, pp. 162–167.

⁵ Satisfactory sources of supply for this instrument are Falex Corp., 1020 Airpark Dr., Sugar Grove, IL 60554–9585 and Stanhope-Seta Ltd., Park Close, Egham, Englefield Green, Surrey, England TW20 OXD.

⁶ Steel balls meeting this description were used in developing the precision of the test. They are available from the manufacturer of the test machine. All balls used in one test should be taken from one carton (of 500 balls) as received from the supplier.

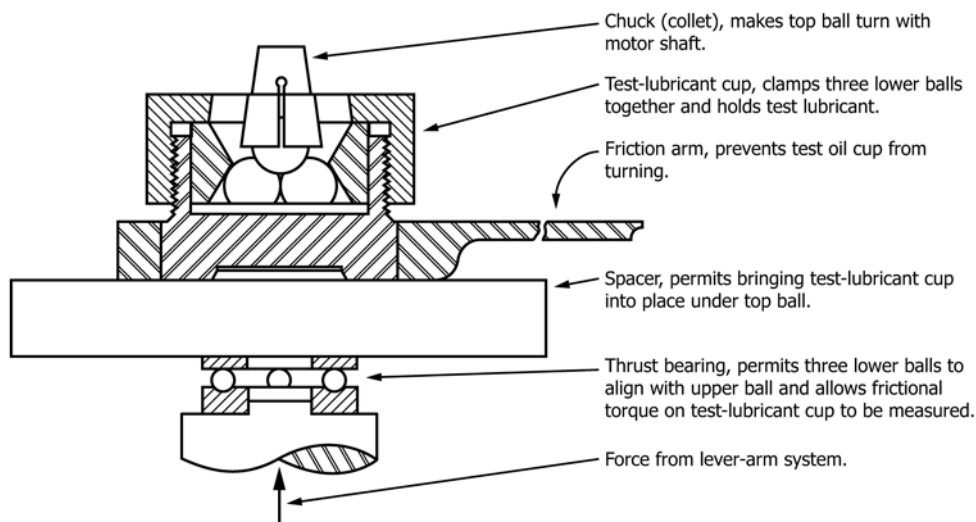


FIG. 2 Sectional View of Four-Ball Tester



FIG. 3 Four-Ball EP Test Machine

a torque wrench. Significantly lower weld points were obtained when the force applied was approximately 136 N·m (100 ft·lb).

9.2 Bring the lubricant and cup to 18 °C to 35 °C (65 °F to 95 °F).

9.3 Press one ball into the ball chuck (Note 6) and mount the chuck into the chuck-holder.

NOTE 6—Examine the chuck and top ball after each run. If the ball shows signs of movement in the chuck, even though welding of the four-balls did not occur, the chuck should be replaced. When welding occurs slippage between ball and chuck nearly always occurs. If the chuck has metal from the top ball adhering to it, the metal must be removed or the chuck replaced.

9.4 Install the test-lubricant cup assembly on the test apparatus in contact with the fourth ball. Place the spacer between cup and thrust bearing.

9.5 Place the weight tray and sufficient weights on the horizontal arm in the correct notch for a base test load of 784 N (80 kg). Release the lever arm and gently apply (Note 7) the test load to the balls, making certain the cup assembly and spacer are centered. If the optional friction-measuring device is used, connect the calibrated arm on the test-lubricant cup to the indicator spring by means of the clip and wire.

NOTE 7—Shock-loading should be avoided as it may deform the balls permanently.

9.6 Start the motor and run for 10 s ± 0.2 s.

NOTE 8—The time for the apparatus to “coast” to a stop is not considered.

9.7 Remove the test-lubricant cup assembly; remove the chuck and discard the ball.

9.8 Measure the scar diameter of test balls as follows:

9.8.1 *Option A*—Remove the test balls. Clean the balls with cleaning solvent (see 7.1) and then rinse solvent (see 7.2). Wipe dry with a soft cloth. Place the individual balls on a suitable holder and by means of a microscope, measure to the nearest 0.01 mm the scar diameters both parallel (horizontal) and normal (vertical) to the striations in the scar surface of one of the three test balls (Note 9).

9.8.2 *Option B*—Leave the balls clamped in the cup. Pour out the lubricating fluid. Wash the ball surfaces with cleaning solvent (see 7.1) and then the rinse solvent (see 7.2). Using a microscope, measure to the nearest 0.01 mm the scar diameters both parallel (horizontal) and normal (vertical) to the striations in the scar surface of one of the three test balls (Note 9).

9.8.3 Measurements by microscope of the scar diameters on all three balls, rather than one ball as outlined in Options A or B, may be made if the operator so desires.

NOTE 9—It is recommended that prior to selection of Option A or B, the operator examines visually the test balls to ascertain no gross discrepancy in the wear scars formed on the test balls; if discrepancy is noted, then wear scar measurements on all three test balls must be made.

9.9 Record (Table 1, Column 2) for the 784 N (80 kg) load the average scar diameter by any one of the three techniques described in 9.8. Compare this average scar diameter with the compensation scar diameter (Table 1, Column 3).

9.10 Make additional runs at consecutively higher test loads (Table 1, Column 1), recording the measured scar diameter(s) (Note 10) and discarding test balls, until welding occurs (Note 11). Make a check run at this point. If welding does not occur on the check run, repeat the test at the next higher load until welding is verified.

NOTE 10—Measuring the scar diameter(s) of test balls in the incipient and immediate seizure region is sometimes difficult due to the flow of metal obliterating the full contact area formed by the rotating ball. In such cases the metal flow can generally be removed or peeled off with a suitable instrument. See Figs. 4 and 5. If the scar periphery is obscure or not well defined an estimate of the scar diameter is made. See Figs. 6 and 7.

NOTE 11—Shut off the motor immediately to prevent damage to the tester. Excessive seizure between the ball and ball chuck may result if caution is not observed. Welding may be detected by any or all of the following: (1) If friction-measuring device is used, a sharp transverse movement of the indicating pen, (2) increased noise level of motor, (3) smoking from test-oil cup, (4) a sudden drop in the lever arm.

9.11 If the measured scar diameter for the 784 N (80 kg) load is more than 5 % from the compensation scar diameter, make the next run at the next lower load (Table 1, Column 1). Continue this procedure until the last nonseizure load is determined.

NOTE 12—When the optional friction-measuring device is used, the last nonseizure load is detected by a gradual transverse movement of the indicating pen.

9.12 Alternatively, in instances when the measured wear scars remain more than 5 % above the compensation line, continue this procedure until a total of ten runs below the weld point is recorded.

10. Calculations and Reports

10.1 *Corrected Load*—Calculate and record (Table 1, Column 5) for each applied load between the last nonseizure load and weld point using the equation

$$\text{Corrected load, kgf} = LD_h/X \quad (2)$$

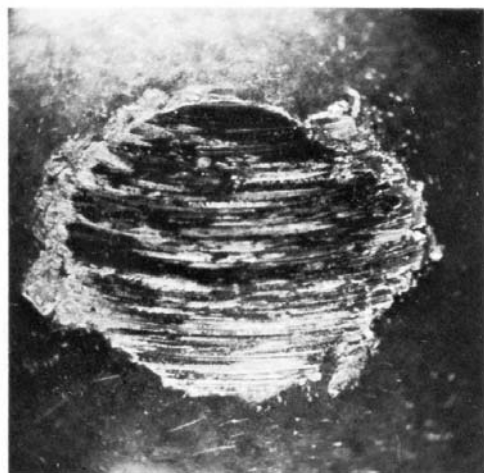


FIG. 4 Typical Test Ball Scars—Before Removal

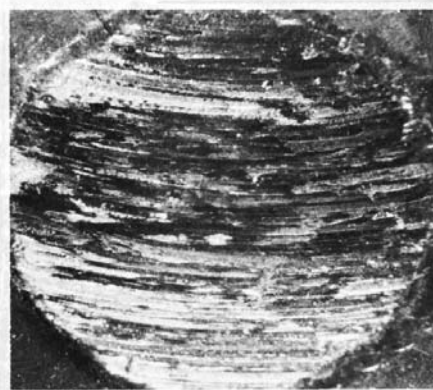


FIG. 5 Typical Test Ball Scars—After Removal

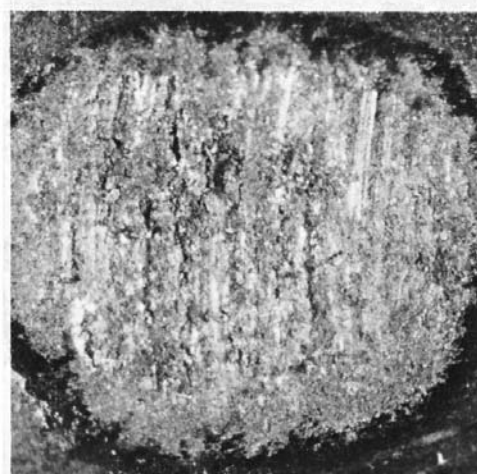


FIG. 6 Typical Test Ball Scars—After Removal



FIG. 7 Typical Test Ball Scars—After Removal

where:

L = applied load, kgf, that is, total weight applied (tray and weights) multiplied by lever arm ratio,
 D_h = Hertz scar diameter, mm, and
 X = average scar diameter, mm.

10.2 *Load-Wear Index*⁷—Calculate and report the load-wear index (formerly Mean-Hertz Load) in kilograms-force using the equation:

$$\text{Load - wear index, kgf} = A/10 \quad (3)$$

where:

A = sum of the corrected loads determined for the ten applied loads immediately preceding the weld point (see

Note 13).

NOTE 13—If tests applied to the lubricant indicate it follows the compensation line, then A may be defined as:

A = sum of corrected loads plus compensation line corrected loads, for the ten applied loads preceding the weld point.

For convenience, Table 2 has been constructed to give the compensation line corrected load for any portion of the compensation line. This value is obtained by noting the intersection of the last nonseizure load and weld load values. For example: the last nonseizure load of a lubricant was found to be 490 N (50 kgf). Subsequent runs in the seizure portion of the curve were made at 618 N, 784 N, 981 N, 1236 N, and 1569 N (63 kgf, 80 kgf, 100 kgf, 126 kgf, and 160 kgf) loads with weld-point found to be 1961 N (200 kgf). Table 2 notes the value at intersection of 490 N and 1961 N (50 kgf and 200 kgf) to be 1456 N (148.6 kgf). This value, the compensation line corrected load, was obtained by correcting loads of 490 N, 392 N, 314 N, 235 N, and 196 N (50 kgf, 40 kgf, 32 kgf, 24 kgf, and 20 kgf) using compensation line scar diameters. This fulfills the definition of load-wear index, that a total of eleven runs be made, the eleventh run causing welding of the test balls. If the tests applied to the lubricant indicate the wear scars do not follow the compensation line, then Table 2 cannot be applied and actual determinations must be made for all ten applied loads preceding the weld point.

10.3 *Weld Point*—Report the verified weld point as found in 9.10.

11. Precision and Bias⁸

11.1 *Precision*—The following criteria should be used for judging acceptability of results (95 % probability) for lubricating fluids which follow the compensation line and have weld points of 400 kg or less.

⁷ The method of calculation was amended in 1982. For a lubricant with a weld load of 400 kg or less, the load-wear index is the same with the old and the present method of calculation.

⁸ Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR: RR:D02-1023. Contact ASTM Customer Service at service@astm.org.

11.1.1 *Load-Wear Index*:

11.1.1.1 *Repeatability*—The difference between successive test results, obtained by the same operator with the same apparatus under constant operating conditions on identical test material would, in the long run, and in the normal and correct operation of the test method, exceed the following values only in one case in twenty:

$$17 \% \text{ of the mean value} \quad (4)$$

11.1.1.2 *Reproducibility*—The difference between two, single and independent results, obtained by different operators working in different laboratories on identical test material would, in the long run, and in the normal and correct operation of the test method, exceed the following values only in one case in twenty:

$$44 \% \text{ of the mean value} \quad (5)$$

11.1.2 *Weld Point*:

11.1.2.1 *Repeatability*—The difference between successive test results, obtained by the same operator with the same apparatus under constant operating conditions on identical test material would, in the long run, and in the normal and correct operation of the test method, exceed the following values only in one case in twenty:

$$\text{more than one increment loading} \quad (6)$$

11.1.2.2 *Reproducibility*—The difference between two, single and independent results, obtained by different operators working in different laboratories on identical test material would, in the long run, and in the normal and correct operation of the test method, exceed the following values only in one case in twenty:

$$\text{more than one increment loading} \quad (7)$$

NOTE 14—A round robin with five cooperators has shown that at a 95 % confidence level similar load-wear index and weld point values have been obtained with five lubricants at 1770 r/min (two laboratories) and at 1440 r/min (three laboratories).⁸ Physical properties and composition of the lubricating fluids used and sample data obtained by this round-robin testing are shown in the appendix.

11.2 Precision for lubricants with weld points greater than 400 kg or above the compensation line, or both, has not been established.

TABLE 2 Total of Compensation Line Corrected Loads

| Last Nonseizure Load, kgf ^A | Weld Load, kgf ^A | | | | | | | | | | |
|--|-----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 800 | 620 | 500 | 400 | 315 | 250 | 200 | 160 | 126 | 100 | 80 |
| 200 | 583 | 639 | 684 | 720 | 749 | 770 | | | | | |
| 160 | 410 | 466 | 511 | 547 | 576 | 597 | 615 | | | | |
| 126 | 269.8 | 325.8 | 370.5 | 407 | 435 | 457 | 474 | 489 | | | |
| 100 | 159.7 | 215.8 | 260.5 | 296.7 | 325.3 | 346.9 | 364.4 | 378 | 390 | | |
| 80 | 71.6 | 127.7 | 172.4 | 208.6 | 237.2 | 258.2 | 276.3 | 290 | 302 | 311.0 | |
| 63 | | 56.1 | 100.8 | 137.0 | 165.6 | 187.1 | 204.7 | 218.8 | 230.4 | 239.3 | 246.7 |
| 50 | | | 44.7 | 80.9 | 109.5 | 131.0 | 148.6 | 162.7 | 174.3 | 183.2 | 190.6 |
| 40 | | | | 36.2 | 64.8 | 86.4 | 103.9 | 118.0 | 129.6 | 138.6 | 145.9 |
| 32 | | | | | 28.6 | 50.2 | 67.7 | 81.8 | 93.4 | 102.4 | 109.7 |
| 24 | | | | | | 21.6 | 39.1 | 53.2 | 64.8 | 73.8 | 81.1 |
| 20 | | | | | | | 17.6 | 31.6 | 43.2 | 52.2 | 59.2 |
| 16 | | | | | | | | 14.1 | 25.7 | 34.6 | 42.0 |
| 13 | | | | | | | | | 11.6 | 20.6 | 27.9 |
| 10 | | | | | | | | | | 9.0 | 16.3 |
| 8 | | | | | | | | | | | 7.4 |

^A To convert from kilograms-force to newtons multiply by 9.806.

11.3 *Bias*—Since there is no accepted reference material suitable for determining the bias for the procedure in this Test Method D2783, no statement on bias is being made.

12. Keywords

12.1 extreme pressure properties (in lubricating fluids); load wear index; weldpoint

ANNEX

(Mandatory Information)

A1. PRECAUTIONARY STATEMENTS

A1.1 Stoddard Solvent

Keep away from heat, sparks, and open flame.
Keep container closed.
Use with adequate ventilation.
Avoid breathing vapor or spray mist.
Avoid prolonged or repeated contact with skin.

A1.2 Heptane

Harmful if inhaled. Vapors may cause flash fire.
Keep away from heat, sparks, and open flame.
Keep container closed.
Use with adequate ventilation.
Avoid build up of vapors and eliminate all sources of ignition especially nonexplosion-proof electrical apparatus and heaters.
Avoid prolonged breathing of vapor or spray mist.
Avoid prolonged or repeated skin contact.

APPENDIX

(Nonmandatory Information)

X1. INFORMATION FROM COOPERATIVE TESTING

TABLE X1.1 Properties of Lubricating Fluids Used in Cooperative Testing

| Sample | L-XI-1-2-A | L-XI-1-2-B | L-XI-1-2-C | L-XI-1-2-D | L-XI-1-2-E | L-XI-1-2-F |
|-------------------------|------------|------------|------------|------------|------------|------------|
| Gravity, deg API | 25.8 | 27.5 | 26.2 | ... | 24.3 | 30.4 |
| Viscosity at 100 °F SUS | 1399.4 | 1392.4 | 950 | 1835 | 359 | 162.4 |
| Viscosity at 210 °F SUS | 100.4 | 99.3 | 86.0 | 101 | 54.5 | 44.0 |
| Viscosity index | 86 | 85 | 95.5 | 58 | 89 | 100 |

TABLE X1.2 Blends (by Weight) Lubricating Fluids Used in Cooperative Testing

| Sample | L-XI-1-2-A | L-XI-1-2-B | L-XI-1-2-C | L-XI-1-2-D | L-XI-1-2-E | L-XI-1-2-F |
|-----------------|------------|--|---|---|---|--|
| Lubricating oil | 100 | 99.5 | SAE 90 | | 80 400 SUS at 100 °F | 96 USP white-oil, heavy |
| Additive | none | L-XI-1-2A 0.5 antimony dialkyl dithiocarbamate (active) | 96 SEMC ^A 90 VI ^B 4 antimony dialkyl phosphorodithioate (active) | 10 mineral seal 90 chlorinated paraffin (40 %) | 90 VI ^B 20 zinc-dialkyl-dithiophosphate | 4 dtertbutyldisulfide (Eastman P-5683) |

^A SEMC = solvent extracted midcontinent.

^B VI = viscosity index.

TABLE X1.3 Representative Data Obtained by Standard Test Method for Extreme-Pressure Properties of Lubricating Fluid (Four-Ball Method)

| Laboratory | Load Wear Index, kgf | | | Weld Point, kgf | | |
|--------------------------|----------------------|------|-------|-----------------|-----|-----|
| | 1 | 3 | 4 | 1 | 3 | 4 |
| <i>Sample L-XI-1-2-A</i> | | | | | | |
| Run 1 | 13.47 | 20.3 | 16.41 | 100 | 126 | 100 |
| Run 2 | 16.43 | 20.3 | 16.37 | 100 | 100 | 100 |
| Run 3 | 11.09 | 20.3 | ... | 100 | 100 | |
| Average | 13.66 | 20.3 | 16.39 | | | |
| <i>Sample L-XI-1-2-B</i> | | | | | | |
| Run 1 | 27.84 | 28.5 | 23.39 | 160 | 160 | 160 |
| Run 2 | 23.59 | 28.0 | 23.41 | 160 | 160 | 160 |
| Run 3 | 27.72 | 29.0 | ... | 160 | 160 | |
| Average | 26.38 | 28.5 | 23.4 | | | |
| <i>Sample L-XI-1-2-C</i> | | | | | | |
| Run 1 | 68.45 | 71.8 | 76.69 | 620 | 500 | 500 |
| Run 2 | 76.39 | 66.9 | 76.25 | 500 | 500 | 500 |
| Run 3 | 78.76 | 69.2 | ... | 500 | 500 | ... |
| Average | 74.58 | 69.3 | 76.46 | | | |

TABLE X1.4 Precision Data for Load Wear Index

| Sample | L-XI-1-2-A | L-XI-1-2-B | L-XI-1-2-C | L-XI-1-2-D ^A | L-XI-1-2-E | L-XI-1-2-F |
|------------------------|------------|------------|------------|-------------------------|------------|------------|
| Number of cooperators | 11 | 11 | 11 | 8 | 8 | 10 |
| Grand average, LWI, kg | 16.08 | 26.87 | 71.23 | 76.8 | 53.7 | 51.25 |
| Number of runs | 30 | 30 | 30 | 19 | 23 | 29 |
| Repeatability, kg | 1.93 | 1.26 | 5.02 | 3.14 | 3.04 | 3.34 |
| Reproducibility, kg | 7.25 | 6.68 | 11.95 | 18.55 | 27.1 | 20.2 |

^A Wear scar values above compensation line.

TABLE X1.5 Laboratory Test Results for Weld Point

| Sample L-XI-1-2-A | | | | | | | | | | | | | |
|----------------------|-----|-----|-----|-----|----------------|-----|-----|-----|-----|-----|-----|-----|-----|
| Laboratory | 1 | 2 | 3 | 4 | 5 ^A | 6 | 7 | 8 | 9 | 10 | 11A | 11B | 12 |
| Run 1 Weld Point, kg | 100 | ... | 126 | 100 | 126 | 100 | 126 | 100 | 126 | 126 | 126 | 126 | 100 |
| Run 2 Weld Point, kg | 100 | ... | 100 | 100 | 126 | 100 | 126 | 100 | 100 | ... | 126 | 126 | 100 |
| Run 3 Weld Point, kg | 100 | ... | 100 | ... | 126 | 100 | 126 | 100 | 100 | ... | 126 | 126 | 100 |
| Sample L-XI-1-2-B | | | | | | | | | | | | | |
| Laboratory | 1 | 2 | 3 | 4 | 5 ^A | 6 | 7 | 8 | 9 | 10 | 11A | 11B | 12 |
| Run 1 Weld Point, kg | 160 | ... | 160 | 160 | 200 | 160 | 200 | 160 | 160 | 160 | 160 | 200 | 160 |
| Run 2 Weld Point, kg | 160 | ... | 160 | 160 | 200 | 160 | 200 | 160 | 160 | ... | 160 | 200 | 160 |
| Run 3 Weld Point, kg | 160 | ... | 160 | ... | 200 | 160 | 200 | 160 | 160 | ... | 160 | 200 | 160 |
| Sample L-XI-1-2-C | | | | | | | | | | | | | |
| Laboratory | 1 | 2 | 3 | 4 | 5 ^A | 6 | 7 | 8 | 9 | 10 | 11A | 11B | 12 |
| Run 1 Weld Point, kg | 620 | ... | 500 | 500 | 620 | 500 | 620 | 500 | 500 | 500 | 500 | 500 | 500 |
| Run 2 Weld Point, kg | 500 | ... | 500 | 500 | 620 | 500 | 620 | 500 | 500 | ... | 500 | 500 | 500 |
| Run 3 Weld Point, kg | 500 | ... | 500 | ... | 620 | 500 | 800 | 500 | 500 | ... | 500 | 500 | 500 |
| Sample L-XI-1-2-D | | | | | | | | | | | | | |
| Laboratory | 1 | 2 | 3 | 4 | 5 ^A | 6 | 7 | 8 | 9 | 10 | 11A | 11B | 12 |
| Run 1 | 500 | ... | ... | 400 | 800 | 400 | ... | 500 | 500 | 500 | 500 | 500 | ... |
| Run 2 | 500 | ... | ... | 400 | 800 | 400 | ... | 400 | 500 | 500 | ... | ... | ... |
| Run 3 | 500 | ... | ... | ... | 800 | 400 | ... | 500 | 500 | 500 | ... | ... | ... |
| Sample L-XI-1-2-E | | | | | | | | | | | | | |
| Laboratory | 1 | 2 | 3 | 4 | 5 ^A | 6 | 7 | 8 | 9 | 10 | 11A | 11B | 12 |
| Run 1 | ... | ... | ... | 250 | 315 | ... | 315 | 250 | 250 | 250 | 250 | 250 | 250 |
| Run 2 | ... | ... | ... | 200 | 315 | ... | 315 | 250 | 200 | 250 | 250 | 250 | 250 |
| Run 3 | ... | ... | ... | ... | 315 | ... | 315 | 250 | 250 | 250 | 250 | 250 | 250 |
| Sample L-XI-1-2-F | | | | | | | | | | | | | |
| Laboratory | 1 | 2 | 3 | 4 | 5 ^A | 6 | 7 | 8 | 9 | 10 | 11A | 11B | 12 |
| Run 1 | 315 | ... | ... | 315 | 315 | 250 | 315 | 250 | 250 | 315 | 315 | 315 | 400 |
| Run 2 | 315 | ... | ... | 250 | 315 | 250 | 400 | 315 | 250 | 315 | 315 | 315 | 315 |
| Run 3 | 315 | ... | ... | ... | 315 | 250 | 400 | 315 | 315 | 315 | 315 | 315 | 315 |

^A Four-ball EP tester run at 1500 r/min.

SUMMARY OF CHANGES

Subcommittee D02.L0 has identified the location of selected changes to this standard since the last issue (D2783 – 19) that may impact the use of this standard. (Approved Nov. 1, 2021.)

(1) Revised referenced document in subsection 2.2.

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