# UHARD/VUHARD subroutines

User subroutine to define the yield surface size and hardening parameters for isotropic plasticity or combined hardening models

User subroutine to define the yield surface size and hardening parameters **UHARD:** for isotropic plasticity or combined hardening models.

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### From the ABAQUS documentation:

### ABAQUS/standard



### User subroutine **UHARD**:

- is called at all material calculation points of elements for which the material definition includes user-defined isotropic hardening or cyclic hardening for metal plasticity;
- can be used to define a material's isotropic yield behavior;
- can be used to define the size of the yield surface in a combined hardening model;
- can include material behavior dependent on field variables or state variables; and
- requires, when appropriate, that the values of the derivatives of the yield stress (or yield surface size in combined hardening models) be defined with respect to the strain, strain rate, and temperature.

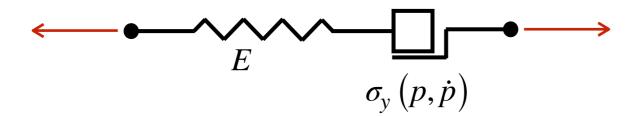
### ABAQUS/explicit



### User subroutine **VUHARD**:

- is called at all material points of elements for which the material definition includes user-defined isotropic hardening or cyclic hardening for metal plasticity;
- can be used to define a material's isotropic yield behavior;
- can be used to define the size of the yield surface in a combined hardening model;
- can include material behavior dependent on field variables or state variables; and
- requires that the derivatives of the yield stress (or yield surface size in combined hardening models) be defined with respect to the appropriate independent variables, such as strain, strain rate, and temperature.

In this example, we want to develop an elasto-visco-plastic model.



Hypo-elasticity:

$$\hat{\mathbf{D}} = \hat{\mathbf{D}}_e + \hat{\mathbf{D}}_p$$

Isotropic elastic:

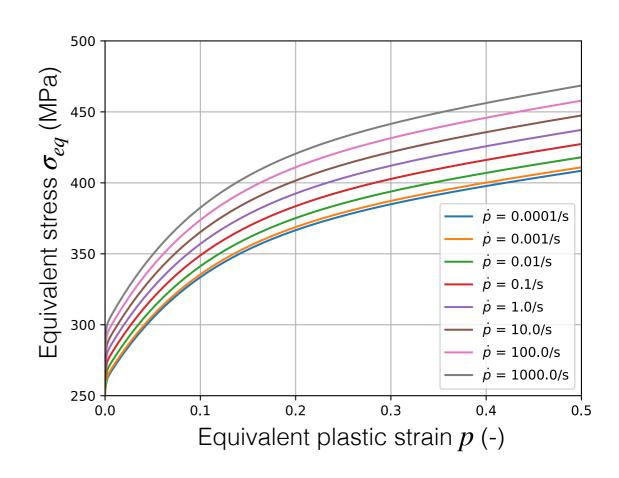
$$\dot{\hat{\boldsymbol{\sigma}}} = \frac{E}{1+\nu}\hat{\mathbf{D}}_{e}' + \frac{E}{3(1-2\nu)} \text{tr}\hat{\mathbf{D}}_{e}\mathbf{I}$$

Isotropic hardening:

$$\sigma_{y} = \sigma_{0} + \sum_{i=1}^{3} Q_{i} \left( 1 - \exp\left(-\frac{\theta_{i}}{Q_{i}}p\right) \right)$$

Visco-plasticity:

$$\dot{p} = \dot{p}_0 \left\langle \left( \frac{\sigma_{eq}}{\sigma_y} \right)^{1/C} - 1 \right\rangle$$



Overall goal of UHARD/VUHARD:

$$p, \dot{p}, T \longrightarrow$$
 UHARD/VUHARD  $\longrightarrow \sigma_y \left( p, \dot{p}, T \right), \frac{\partial \sigma_y}{\partial p}, \frac{\partial \sigma_y}{\partial \dot{p}}, \frac{\partial \sigma_y}{\partial T}$ 

Where p is the equivalent plastic strain,  $\dot{p}$  is the equivalent plastic strain rate, T is the temperature and  $\sigma_{\rm v}$  is the current yield stress

Description of the arguments for UHARD/VUHARD:

ABAQUS/standard

# $\sigma_{y}\left(p,\dot{p},T\right) \qquad \frac{\partial\sigma_{y}}{\partial p}, \frac{\partial\sigma_{y}}{\partial\dot{p}}, \frac{\partial\sigma_{y}}{\partial T} \qquad p \qquad \dot{p}$ $SUBROUTINE \ UHARD (SYIELD, HARD, EQPLAS, EQPLASRT, \\ + \ TIME, DTIME, TEMP, DTEMP, \\ + \ NOEL, NPT, LAYER, KSPT, KSTEP, KINC, CMNAME, NSTATV, \\ + \ STATEV, NUMFIELDV, PREDEF, DPRED, NUMPROPS, PROPS) <math display="block">T$ $SUBROUTINE \ VUHARD (NBLOCK, JELEM, KINTPT, KLAYER, KSECPT, \\ LANNEAL, STEPTIME, TOTALTIME, DT, CMNAME, \\ NSTATEUV, NFIELDV, NPROPS, \\ PROPS, TEMPOLD, TEMPNEW, FIELDOLD, FIELDNEW, \\ STATEOLD, TEMPOLD, TEMPNEW, FIELDOLD, TEMPNEW, PIELDOLD, PIELDOLD, TEMPNEW, PIELDOLD, TEMPNEW, PIELDOLD, PIE$

ABAQUS/explicit

### ABAQUS/standard

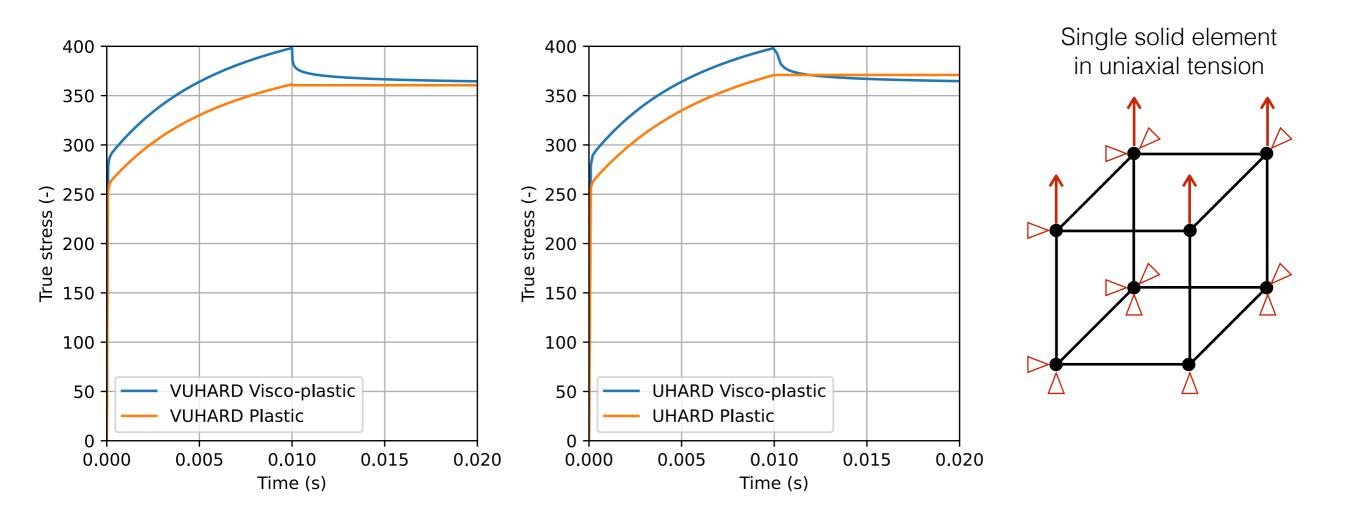
```
Compute yield stress and derivatives
      SYIELD = (SIGMA0+Q1*(1.0-exp(-T1oQ1*EQPLAS)))
                        +Q2*(1.0-exp(-T2oQ2*EQPLAS))
                        +Q3*(1.0-exp(-T3oQ3*EQPLAS)))
      Compute yield stress derivatives
      Derivative with respect to equivalent plastic strain
\partial \sigma_y \rightarrow HARD(1) = (T1*exp(-T1oQ1*EQPLAS)
                +T2*exp(-T2oQ2*EQPLAS)
\partial p
                +T3*exp(-T3oQ3*EQPLAS))
      Derivative with respect to equivalent plastic strain rate
    → HARD(2) =(SIGMA0+Q1*(1.0-exp(-T1oQ1*EQPLAS))
                        +02*(1.0-exp(-T2oQ2*EQPLAS))
\partial \dot{p}
                        +03*(1.0-exp(-T3oQ3*EQPLAS)))
      Derivative with respect to temperature
C
      HARD(3) = 0.0
```

### ABAQUS/explicit

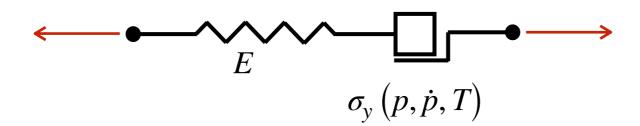
```
Compute yield stress and its derivatives
        do i=1,nblock
  \sigma_{v} \longrightarrow \text{yield(i)} = (SIGMA0+Q1*(1.0-exp(-T1oQ1*eqps(i))))
                                  +02*(1.0-exp(-T2oQ2*eqps(i)))
                                  +03*(1.0-exp(-T3oQ3*eqps(i))))
            Derivative with respect to equivalent plastic strain
 ^{\mathsf{c}}\partial\sigma_{\mathsf{v}}
          dyieldDeqps(i,1) =(T1*exp(-T1oQ1*eqps(i))
                                    +T2*exp(-T2oQ2*eqps(i))
                                    +T3*exp(-T3oQ3*eqps(i)))
            Derivative with respect to equivalent plastic strain rate
 c \partial \sigma_{v}
          \rightarrow dyieldDeqps(i,2) = 0.0
^{f ackslash}_{f c} \partial \dot{ar p}
            Derivative with respect to temperature
            dyieldDtemp(i) = 0.0
        enddo
         \partial \sigma_{y}
```

```
*material, name=EXAMPLE UHARD RATE
                    *elastic
                    210000.0, 0.3
                    *plastic, hardening=user, properties=16
ABAQUS/standard
                    ** SIGMA0, / T1, Q1, T2, Q2, T3, Q3, BLANK
                       250, 10000.0, 10.0, 1000.0, 100.0, 100.0, 1000.0, 0.0
                        C, PDOTO, BLANK, BLANK, BLANK, BLANK, BLANK
                        0.01, 0.001, 0.0, 0.0, 0.0, 0.0, 0.0
   Call to VUHARD/
  UHARD subroutine
                    *material, name=EXAMPLE_VUHARD_RATE
                    *density
                    7.8e-9
                    *elastic
                    210000.0, 0.3
ABAQUS/explicit
                    *plastic, hardening=user, properties=16
                    ** SIGMA0, T1, Q1, T2, Q2, T3, Q3, BLANK
                       250.0, 10000.0, 10.0, 1000.0, 100.0, 100.0, 1000.0, 0.0
                    ** C, PDOTO, BLANK, BLANK, BLANK, BLANK, BLANK, BLANK
                        0.01, 0.001, 0.0, 0.0, 0.0, 0.0, 0.0
```

Results from the UHARD\_V1 and VUHARD\_V1 subroutines



In this example, we want to develop an elasto-visco-thermo-plastic model.



$$\sigma_{y} = (\sigma_{0} + R) \cdot \left(1 + \frac{\dot{p}}{\dot{p}_{0}}\right)^{C} \cdot \left(1 - \left(\frac{T - T_{r}}{T_{m} - Tr}\right)^{m}\right)$$

Isotropic hardening:

$$R = \sum_{i=1}^{3} Q_i \left( 1 - \exp\left( -\frac{\theta_i}{Q_i} p \right) \right)$$
 Visco-plasticity

Thermo-plasticity

Temperature: 
$$T=T_0+\Delta T$$
 with  $\Delta T=\int_0^p \beta \frac{\sigma_{eq} ap}{\rho C_p}$  Adiabatic heating

### Starting from the VUHARD\_V1.f subroutine:

```
Apply temperature—sensitivity if needed

if((m.gt.0.0).and.(Tm.gt.0.0))then

do i=1,nblock

Compute rate effects and its derivative

Teff = ((min(TEMPNEW(i),0.99*Tm))-Tr)/(Tm-Tr))

tp = (1.0-Teff**m)

dtp =-(m/(Tm-Tr))*(Teff***(m-1.0))

Apply rate effects to the required quantities

dyieldDtemp(i) = yield(i)*dtp

dyieldDeqps(i,2) = dyieldDeqps(i,2)*tp

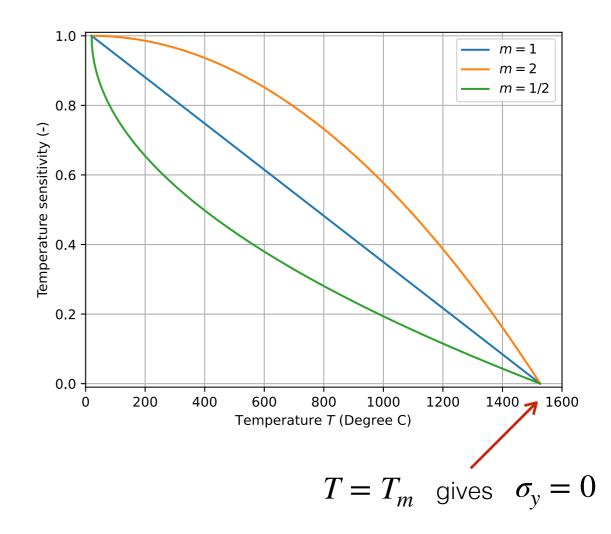
dyieldDeqps(i,1) = dyieldDeqps(i,1)*tp

yield(i) = yield(i)*tp

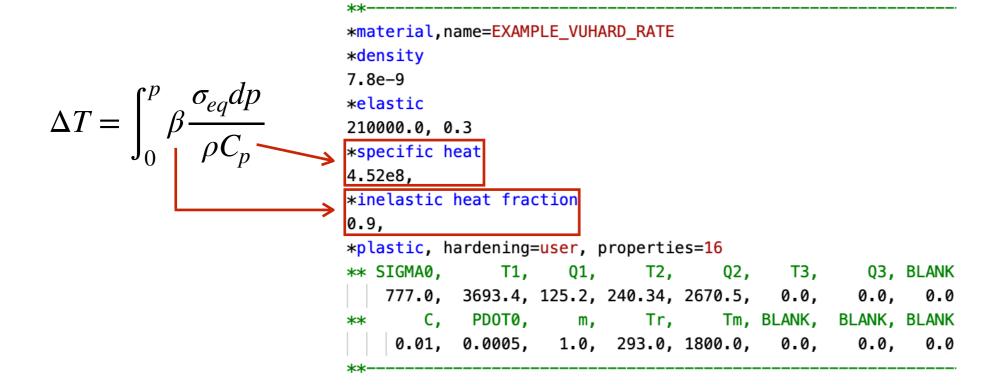
enddo

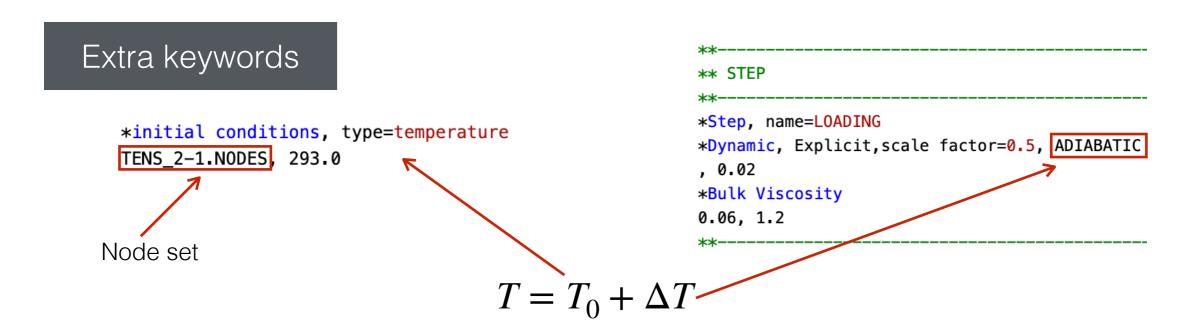
endif
!
```

 $T \le 99 \% T_m$ 

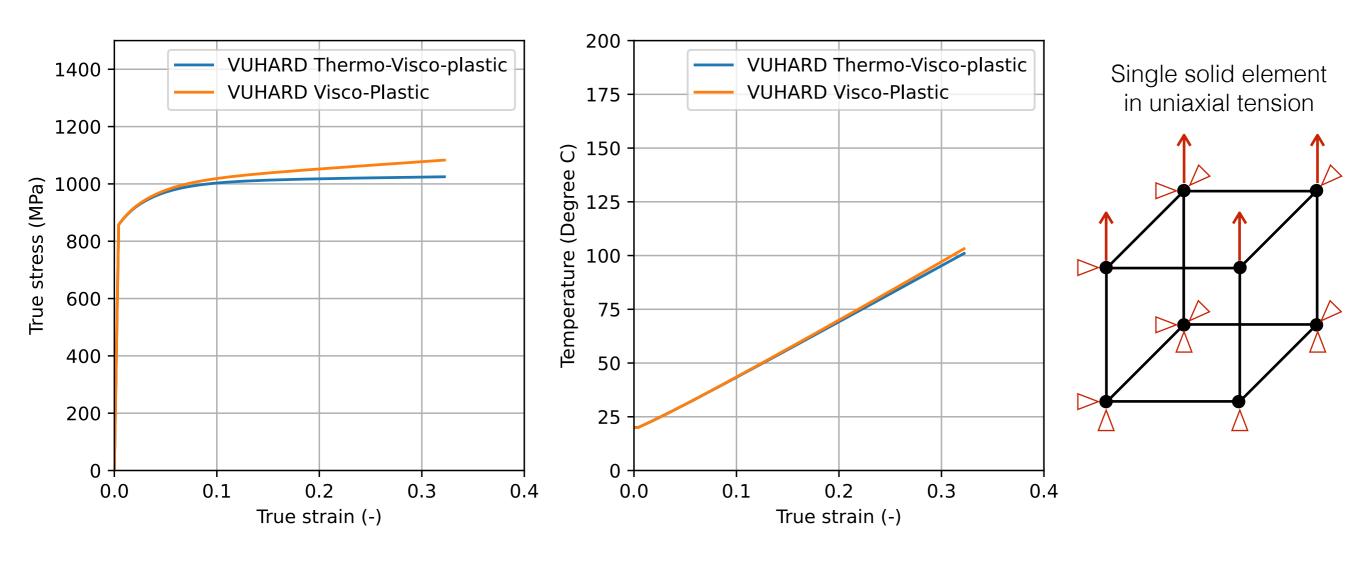


### Material card





### Results from the VUHARD\_V2 subroutine



### Can be used with:

- a von Mises/Hill/Raghava yield surface
- the Gurson model
- A combined isotropic/kinematic hardening model