# Forward Kinematics of Delta Robot

Ajou. Univ. Mechnical Engineering
Kim Yun Beom

 $L_i$ : length of active leg  $(\overline{B_iA_i})$ 

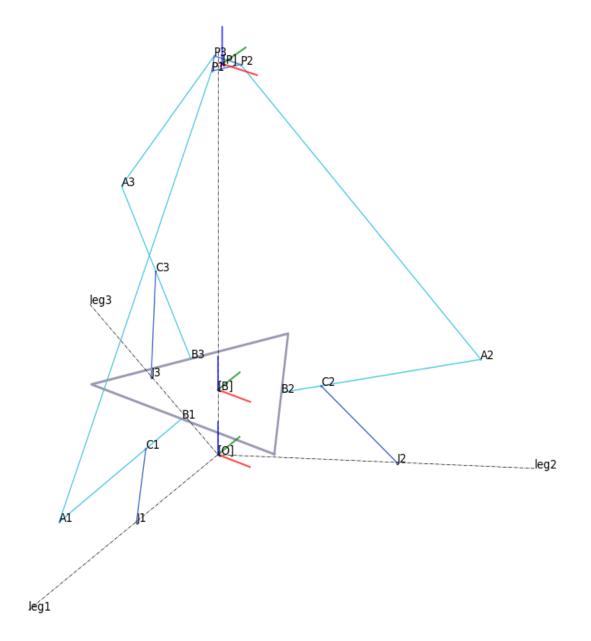
 $l_i$ : Length of passive leg  $(\overline{A_iP_i})$ 

 $B_i$ : Hips (Revolute Joint)

 $A_i$ : Knees (Universal Joint)

 $P_i$ : Ankles (Universal Joint)

i = 1, 2, 3



[B]: Base Reference Frame

 $B_0$ : Origin of Base Reference Frame

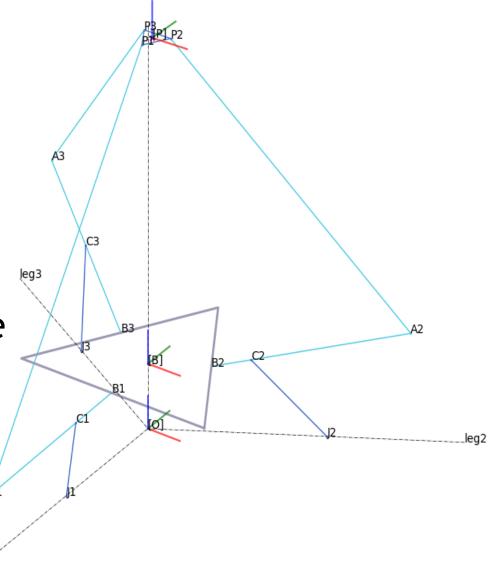
 $h_B$ : Z-axis height between [O] and [B]

[P]: Platform Reference Frame

 $P_0$ : Origin of Platform Reference Frame

[0]: Reference Frame

*O*: Origin of Reference Frame



 $C_i$ : One end of the linear actuator

 $J_i$ : Another end of the linear actuator

 $D_i$ : Length of linear actuator

 $t_i$ : Ratio of  $C_i$  ( $\overline{B_iC_i}/\overline{B_iA_i}$ ),  $(0 \le t_i \le 1)$ 

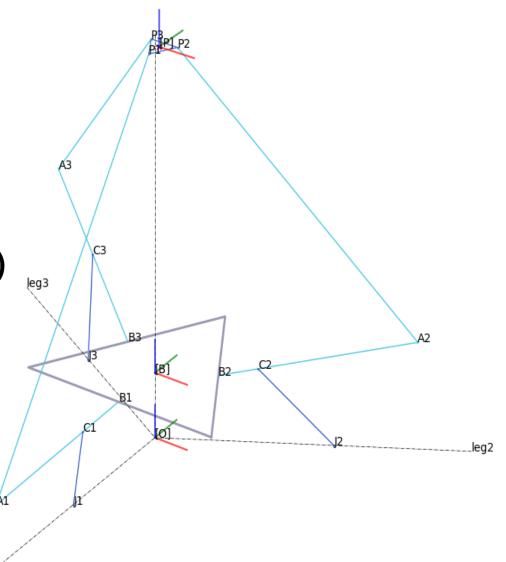
 $B'_i$ : xy-plane projection of  $\boldsymbol{B}_i$ 

 $s_i$ : Length of  $\overline{{\pmb B}'_i {\pmb J}_i}$ 

 $\theta_i$ : Angle of Active Leg

= Angle between xy-plane and  $\overline{B_i A_i}$ 

= Angle between  $\overline{\boldsymbol{B}_{i}\boldsymbol{A}_{i}}$  and  $\overline{\boldsymbol{B}'_{i}\boldsymbol{J}_{i}}$ 



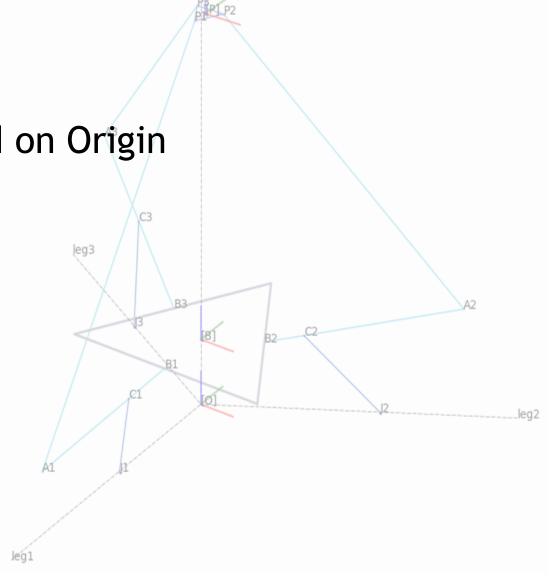
B, A, P, C: Bold Alphabet

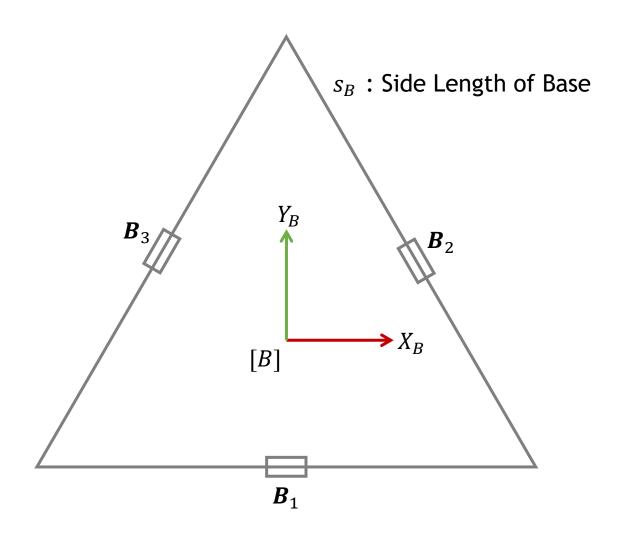
: Row vector or Point based on Origin

 ${}^{B}\boldsymbol{B}_{i}$ : Row Vector based on [B]

 $\underline{B}, \underline{A}, \underline{P}, \underline{C}$ : Alphabet with underbar

: Matrix





 $P_3$   $P_2$   $X_P$   $S_P$ : Side Length of Platform  $P_1$ 

Base Reference Frame

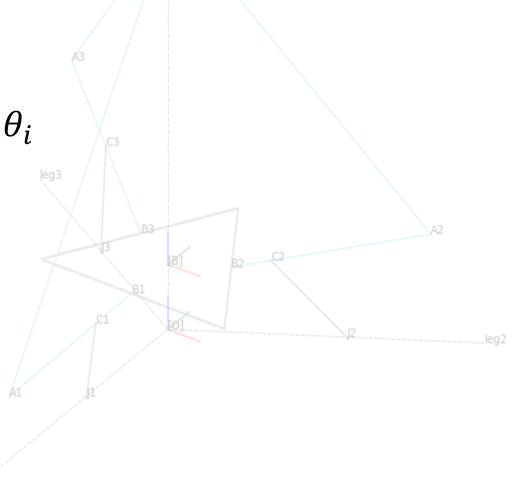
Platform Reference Frame

 $Y_P$ 

#### Forward Kinematics - Points

Forward Kinematics: Find  ${}^{B}\boldsymbol{P}_{0}$  or  ${}^{O}\boldsymbol{P}_{0}$ 

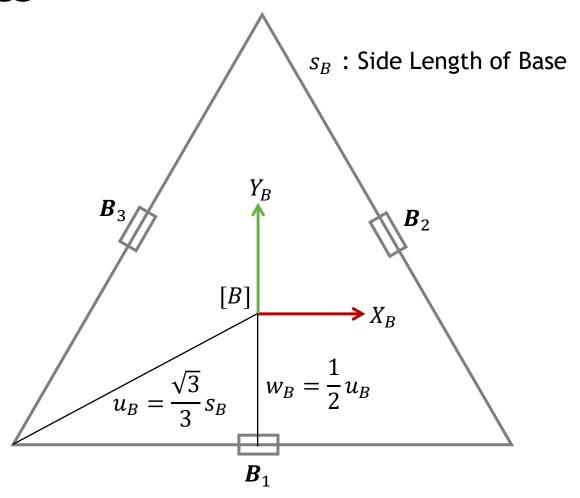
- 1. Find Point Coordinates depends on  $\theta_i$
- 2. Find  ${}^{B}\mathbf{P}_{0}$  depends on  $\theta_{i}$
- 3. Find  $\theta_i$  depends on  $D_i$



$${}^{B}\boldsymbol{B}_{1} = \begin{bmatrix} 0 & -w_{B} & 0 \end{bmatrix} = \begin{bmatrix} 0 & -\frac{\sqrt{3}}{6}s_{B} & 0 \end{bmatrix}$$

$${}^{B}\mathbf{B}_{1} = [w_{B}\cos 30^{\circ} \quad w_{B}\sin 30^{\circ} \quad 0] = \begin{bmatrix} s_{B} & \sqrt{3} \\ 4 & 12 \end{bmatrix} s_{B} \quad 0$$

$${}^{B}\mathbf{B}_{1} = [w_{B}\cos 30^{\circ} - w_{B}\sin 30^{\circ} \ 0] = \begin{bmatrix} s_{B} \\ 4 \end{bmatrix} - \frac{\sqrt{3}}{12}s_{B} \ 0$$

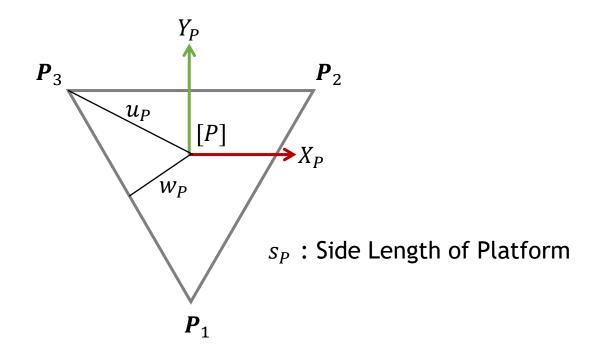


Base Reference Frame

$${}^{P}\boldsymbol{P}_{1} = \begin{bmatrix} 0 & -u_{P} & 0 \end{bmatrix} = \begin{bmatrix} 0 & -\frac{\sqrt{3}}{3}s_{P} & 0 \end{bmatrix}$$

$${}^{P}\mathbf{P}_{2} = [u_{P}\cos 30^{\circ} \quad u_{P}\sin 30^{\circ} \quad 0] = \begin{bmatrix} s_{P} & \sqrt{3} \\ 2 & 6 \end{bmatrix}$$

$${}^{P}\mathbf{P}_{3} = [u_{P}\cos 30^{\circ} - u_{P}\sin 30^{\circ} \ 0] = \begin{bmatrix} \underline{s}_{B} \\ 2 \end{bmatrix} - \frac{\sqrt{3}}{6}s_{B} \ 0$$

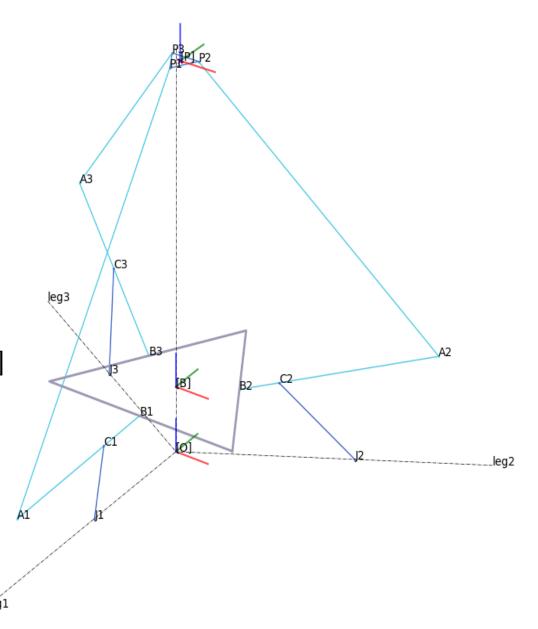


Platform Reference Frame

$${}^{B}A_{1} = \begin{bmatrix} 0 & -L_{1}\cos\theta_{1} & L_{1}\sin\theta_{1} \end{bmatrix}$$

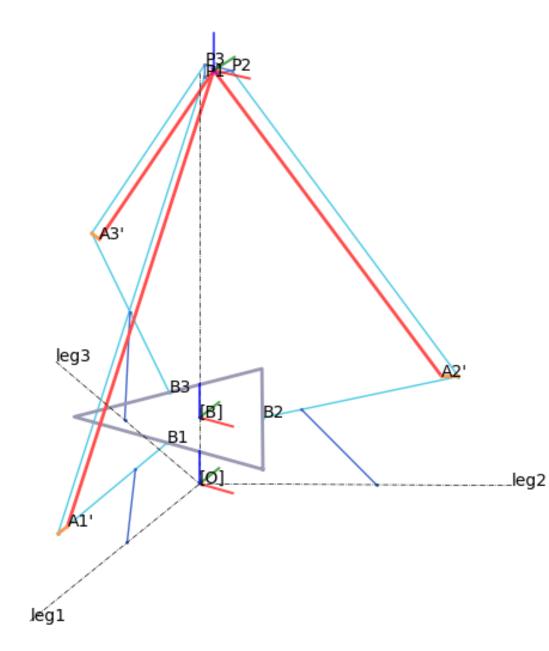
$${}^{B}\mathbf{A}_{2} = [L_{2}\cos\theta_{2}\cos30^{\circ} \quad L_{2}\cos\theta_{2}\sin30^{\circ} \quad L_{2}\sin\theta_{2}]$$

$${}^{B}\mathbf{A}_{3} = \begin{bmatrix} -L_{3}\cos\theta_{3}\cos30^{\circ} & L_{3}\cos\theta_{3}\sin30^{\circ} & L_{3}\sin\theta_{3} \end{bmatrix}$$



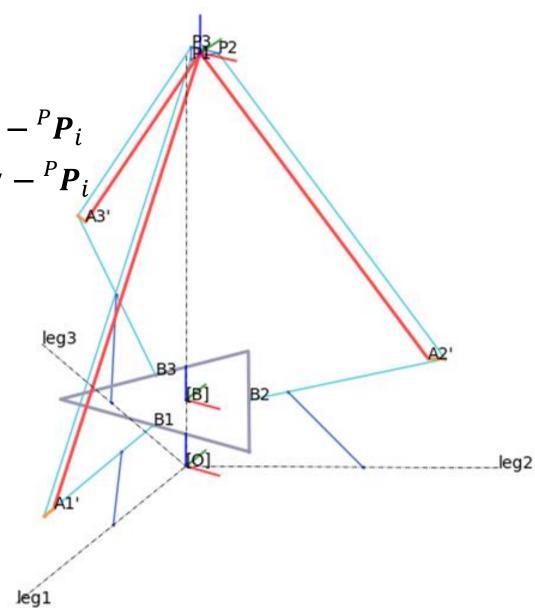
Let  ${}^{B}\mathbf{P'}_{i}$  is the point such that  ${}^{B}\mathbf{P}_{i}$  moves by  $-{}^{P}\mathbf{P}_{i}$ 

Then all  ${}^{B}\mathbf{P'}_{i}$  gather at a point  ${}^{B}\mathbf{P}_{0}$ 



Let  ${}^{B}P'_{i}$  is the point such that  ${}^{B}P_{i}$  moves by  $-{}^{P}P_{i}$ And  ${}^{B}A'_{i}$  is the point such that  ${}^{B}A_{i}$  moves by  $-{}^{P}P_{i}$ 

Then  ${}^{B}\mathbf{P}_{0}$  is the intersection of 3 Spheres with each center is  ${}^{B}\mathbf{A'}_{i}$  and radius is  $l_{i}$ 



In this section, bold alphabet means column vector

Let  $c_j = \{x_j, y_j, z_j\}^T$  is center of the sphere with a radius of  $R_j$ , and  $\mathbf{x} = \{x, y, z\}^T$  is intersection of spheres. (j = 1, 2, 3)

Then x satisfying the nonlinear equation

$$\left\|\mathbf{x}-\boldsymbol{c_j}\right\|^2=R_j^2$$

or equivalently,

$$\mathbf{x}^T \mathbf{x} - 2\mathbf{x}^T \mathbf{c_i} + \mathbf{c_i}^T \mathbf{c_i} = R_i^2$$

At equation

$$\mathbf{x}^T \mathbf{x} - 2\mathbf{x}^T \mathbf{c_j} + \mathbf{c_j}^T \mathbf{c_j} = R_j^2$$

Let  $r = \mathbf{x}^T \mathbf{x}$ , and  $b_j = \boldsymbol{c_j^T c_j} - R_j^2$  then equation can rewrite as  $\boldsymbol{c_j^T x} = \frac{r + b_j}{2}$ 

In matrix form, equation

$$\boldsymbol{c}_{\boldsymbol{j}}^{\mathrm{T}}\mathbf{x} = \frac{r + b_{\boldsymbol{j}}}{2}$$

become

$$\begin{bmatrix} x_1 & y_1 & z_1 \\ x_2 & y_2 & z_2 \\ x_3 & y_3 & z_3 \end{bmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix} = \frac{r}{2} + \frac{1}{2} \begin{pmatrix} b_1 \\ b_2 \\ b_3 \end{pmatrix}$$

$$\underline{C}^T \mathbf{x} = \frac{r\mathbf{e} + \mathbf{b}}{2}$$

$$\underline{C} = [\mathbf{c_1} \quad \mathbf{c_2} \quad \mathbf{c_3}], \qquad \mathbf{e} = \{1 \quad 1 \quad 1\}^T, \qquad \mathbf{b} = \{b_1 \quad b_2 \quad b_3\}^T$$

Therefore

$$\mathbf{x} = \underline{C}^{-T} \left( \frac{r\mathbf{e} + \mathbf{b}}{2} \right)$$

$$\mathbf{x} = \frac{r\mathbf{u} + \mathbf{v}}{2}$$

$$\mathbf{u} = \underline{C}^{-T}\mathbf{e}, \qquad \mathbf{v} = \underline{C}^{-T}\mathbf{b}$$

Since,  $r = \mathbf{x}^T \mathbf{x}$ 

$$r = \mathbf{x}^T \mathbf{x} = \frac{1}{4} (r\mathbf{u} + \mathbf{v})^{\mathrm{T}} (r\mathbf{u} + \mathbf{v})$$

Therefore

$$(\mathbf{u}^{\mathrm{T}}\mathbf{u})r^{2} + (2\mathbf{u}^{\mathrm{T}}\mathbf{v} - 4)r + \mathbf{v}^{\mathrm{T}}\mathbf{v} = 0$$

Which is a quadratic equation in the scalar r.

$$r = \frac{-(\mathbf{u}^{\mathrm{T}}\mathbf{v} - 2) + \sigma\sqrt{(\mathbf{u}^{\mathrm{T}}\mathbf{v} - 2)^{2} - (\mathbf{u}^{\mathrm{T}}\mathbf{u})(\mathbf{v}^{\mathrm{T}}\mathbf{v})}}{\mathbf{u}^{\mathrm{T}}\mathbf{u}}, \qquad \sigma = \pm 1$$

## FWD Kinematics - ${}^{B}P_{0}$

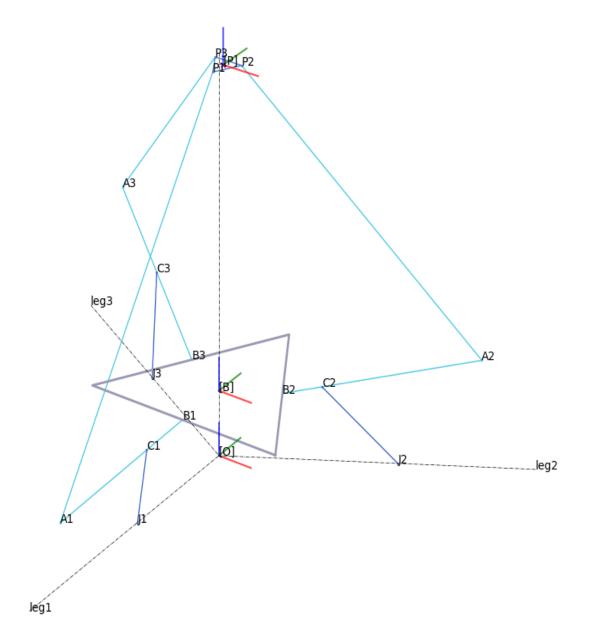
$$^{B}\mathbf{P}_{0}=\mathbf{x}=\frac{r\mathbf{u}+\mathbf{v}}{2}$$

$${}^{B}\boldsymbol{A'}_{i} = {}^{B}\boldsymbol{A}_{i} - {}^{P}\boldsymbol{P}_{i}, \qquad \underline{\boldsymbol{C}}^{T} = \begin{cases} {}^{B}\boldsymbol{A'}_{1} \\ {}^{B}\boldsymbol{A'}_{2} \\ {}^{B}\boldsymbol{A'}_{3} \end{cases}, \quad \mathbf{u} = \underline{\boldsymbol{C}}^{-T}\mathbf{e}, \quad \mathbf{v} = \underline{\boldsymbol{C}}^{-T}\mathbf{b}$$

$$\mathbf{e} = \{1 \quad 1 \quad 1\}^{T}, \quad \mathbf{b} = \{b_{1} \quad b_{2} \quad b_{3}\}^{T}, \quad b_{i} = {}^{B}\boldsymbol{A'}_{i}{}^{T}{}^{B}\boldsymbol{A'}_{i} - l_{i}^{2}$$

$$r = \frac{-(\mathbf{u}^{T}\mathbf{v} - 2) + \sigma\sqrt{(\mathbf{u}^{T}\mathbf{v} - 2)^{2} - (\mathbf{u}^{T}\mathbf{u})(\mathbf{v}^{T}\mathbf{v})}}{\mathbf{u}^{T}\mathbf{u}}, \quad \sigma = \pm 1$$

# FWD Kinematics - ${}^{B}P_{0}$

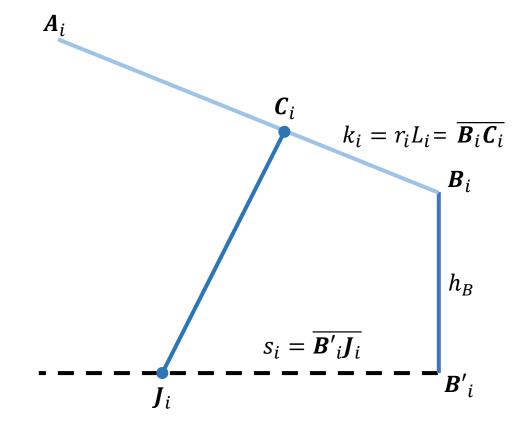


#### FWD Kinematics - $\theta_i(D_i)$

[B] is equilvalent to moving [O] by  $h_B$  following Z-axis

$$\boldsymbol{C}_i = t_i \boldsymbol{A}_i + (1 - t_i) \boldsymbol{B}_i$$

$$\boldsymbol{J}_i = \boldsymbol{B}_i' + \frac{\boldsymbol{B}_i'}{\|\boldsymbol{B}_i'\|} s_i$$



## FWD Kinematics - $\theta_i(D_i)$

$$\phi_i = \angle E_i B_i J_i = \cos^{-1} \left( \frac{S_i}{n_i} \right), \qquad (0 < \phi_i \le 90^\circ)$$
2<sup>nd</sup> Law of Cosine

$$D_{i}^{2} = k_{i}^{2} + n_{i}^{2} - 2n_{i}k_{i}\cos(\theta_{i} + \phi_{i}), \qquad (0 \le \theta_{i} + \phi_{i} \le 180^{\circ}) \xrightarrow{k_{i} = r_{i}L_{i} = \overline{B_{i}C}} B_{i}$$

$$\theta_{i} = \cos^{-1}\left(\frac{D_{i}^{2} - k_{i}^{2} - n_{i}^{2}}{2n_{i}k_{i}}\right) - \cos^{-1}\left(\frac{s_{i}}{n_{i}}\right)$$

$$s_{i} = \overline{B_{i}J_{i}} \qquad h_{B}$$

#### Reference

- [1] Robert L. Williams II, "The Delta Parallel Robot: Kinematics Solutions", 2016
- [2] I.D. Coope, "Reliable computation of the points of intersection of n spheres in n-dimension", 2000