

Problem 1

Given the LTI system

$$\begin{cases} \dot{x}(t) = \begin{bmatrix} -0.2 & -1 \\ 1 & 0 \end{bmatrix}x(t) + \begin{bmatrix} 0.5 \\ 0 \end{bmatrix}u(t), \\ y(t) = \begin{bmatrix} 0 & 1 \end{bmatrix}x(t) \end{cases}, x(0) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

- Suppose that the system state can be measured. Design, if possible, a state feedback controller of the form

$$u(t) = -Kx(t) + Nr(t)$$

to meet the following requirements:

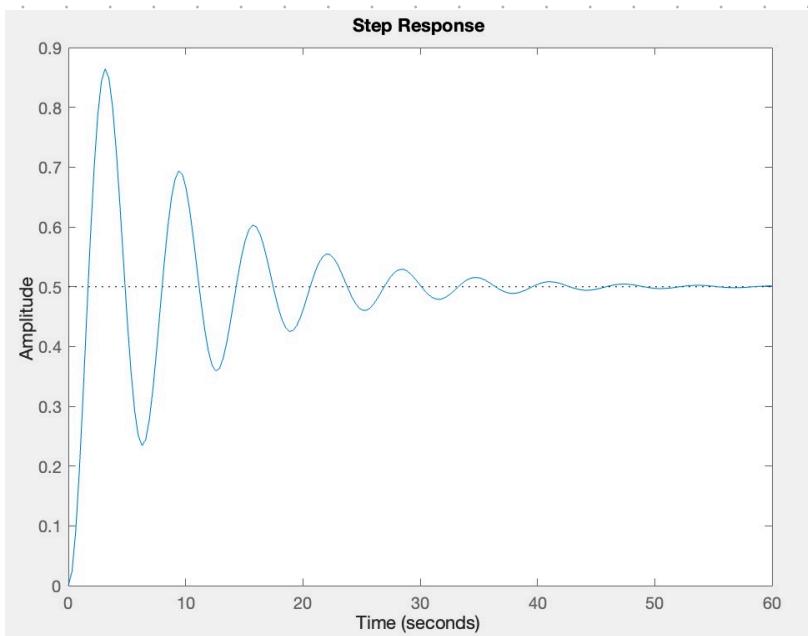
1. unitary dc-gain for the controlled system

2. $\hat{s} \leq 6\%$

3. $t_{s,2\%} \leq 2$ s

- Compute the analytical expression of the output response $y(t)$ of the controlled system in the presence of a step reference input, i.e., $r(t) = \varepsilon(t)$.

first lets examine the asymptotic behavior!



it is asymptotically stable
as $t \rightarrow \infty$ goes to 0!
Converges!

Secondly let's examine the reachability!

$$M_R = \begin{bmatrix} 0.5 & -0.1 \\ 0 & 0.5 \end{bmatrix} \Rightarrow g(M_R) = 2 ; \text{ since } R^{n,n} ; n=2$$

and $g(M_R) = n$
system is reachable!

$$\hat{s} = e^{\frac{-\pi \zeta}{\sqrt{1-s^2}}} \Rightarrow g = \frac{|\log(\hat{s})|}{\sqrt{\pi^2 + \log^2(\hat{s})}} = 0.15$$

$$t_{s,12} = \frac{\log(0.02)^{-1}}{\omega_n g} \Rightarrow \omega_n = \frac{3 \cdot g}{t_{s,12} g} = 13.03$$

$$\lambda_{1,2} = \bar{\omega}_0 \pm J\omega_0 = -g\omega_n \pm J\omega_n \sqrt{1-g^2}$$

$$\lambda_1 = -1.36 + 12.03J$$

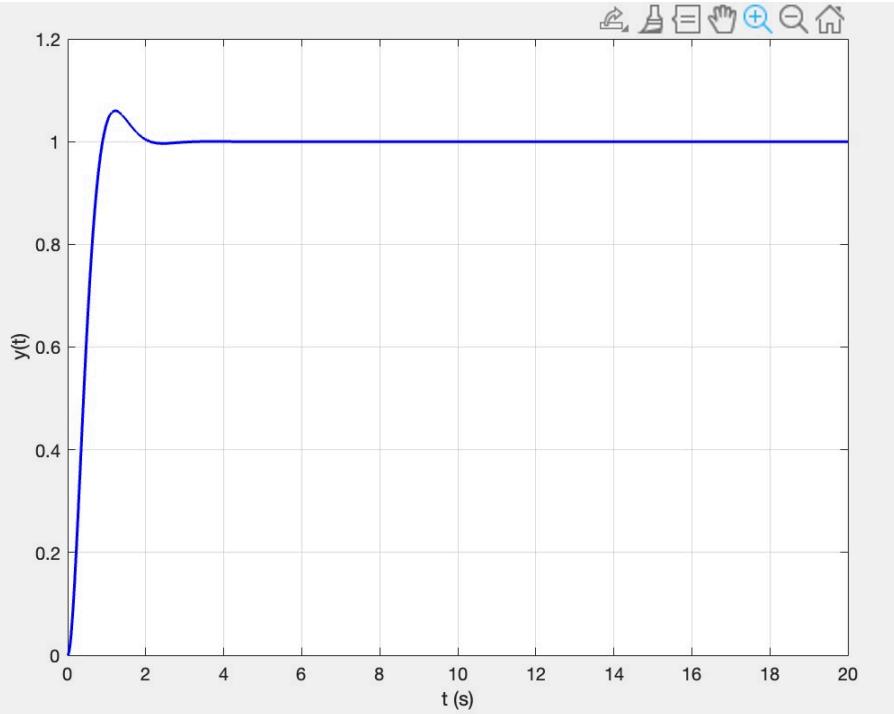
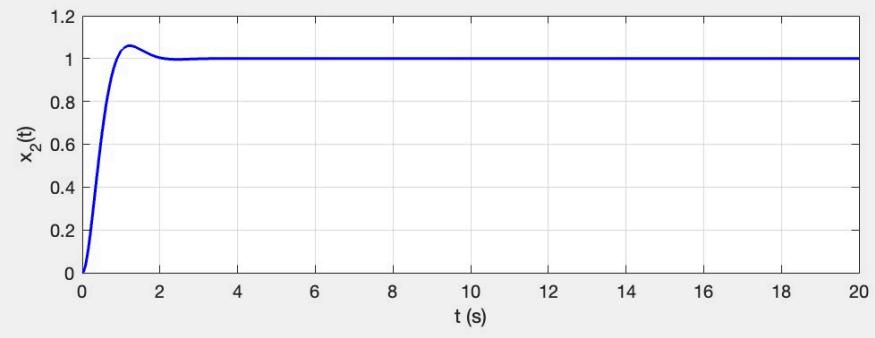
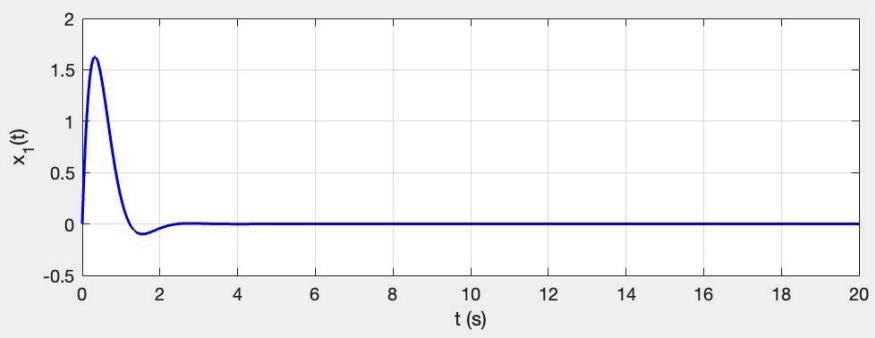
$$\lambda_2 = -1.36 - 12.03J$$

$$k = \begin{bmatrix} 7.4240 & 295.07 \end{bmatrix}$$

$$u = -k \times (+) + N u (+)$$

\curvearrowleft

$$N = 295.07$$



$$t_{Si/2} \leq 2\text{ s}$$

$$\zeta \leq 1.6$$

Problem 2

Given the LTI system

$$\begin{cases} \dot{x}(t) = \begin{bmatrix} -0.2 & -1 \\ 1 & 0 \end{bmatrix}x(t) + \begin{bmatrix} 0.5 \\ 0 \end{bmatrix}u(t), \\ y(t) = \begin{bmatrix} 0 & 1 \end{bmatrix}x(t) \end{cases}, x(0) = \begin{bmatrix} 0.1 \\ 0.1 \end{bmatrix}$$

- Suppose that the system state cannot be measured. Design, if possible, a state feedback controller of the form

$$u(t) = -K\hat{x}(t) + N r(t)$$

to account for the following requirements:

- unitary dc-gain for the controlled system
- controlled system eigenvalues characterized by $\zeta = 0.66$ and $\omega_n = 2.93$ rad/s

- Evaluate the maximum overshoot of the output unitary step response in the presence of the given initial condition.

M_r =

$$\begin{bmatrix} 0.5000 & -0.1000 \\ 0 & 0.5000 \end{bmatrix}$$

rho_M =

2

✓

the system is reachable

M_0 =

$$\begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}$$

rho_M_0 =

2

✓

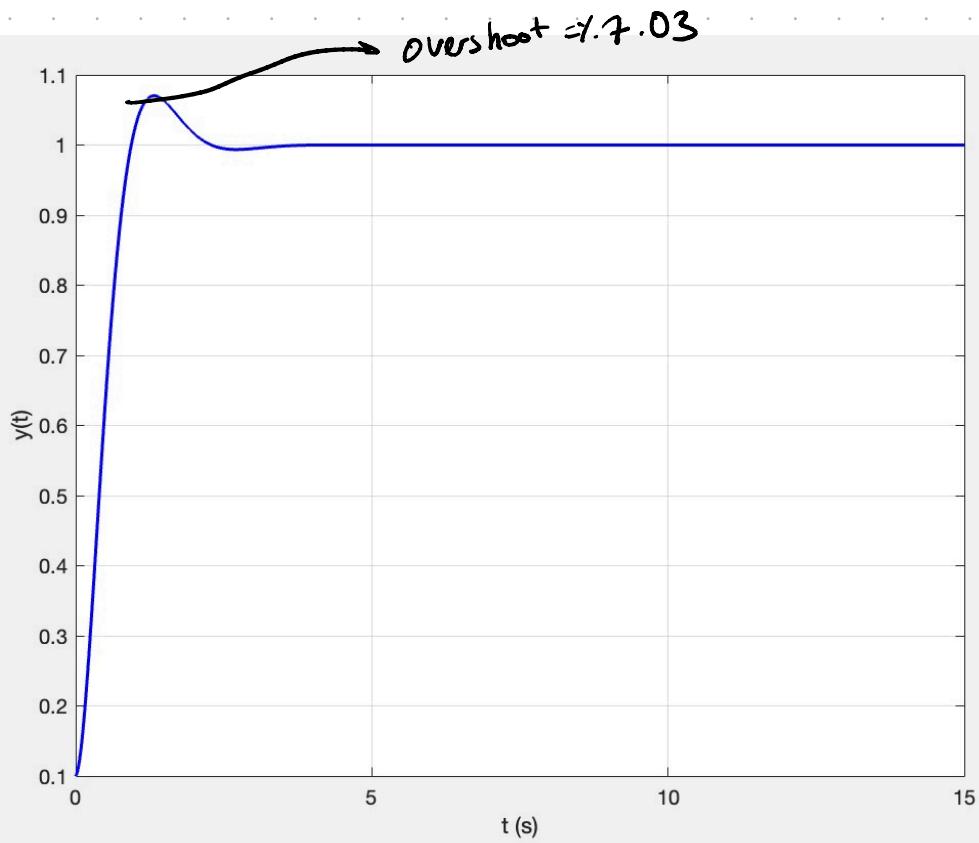
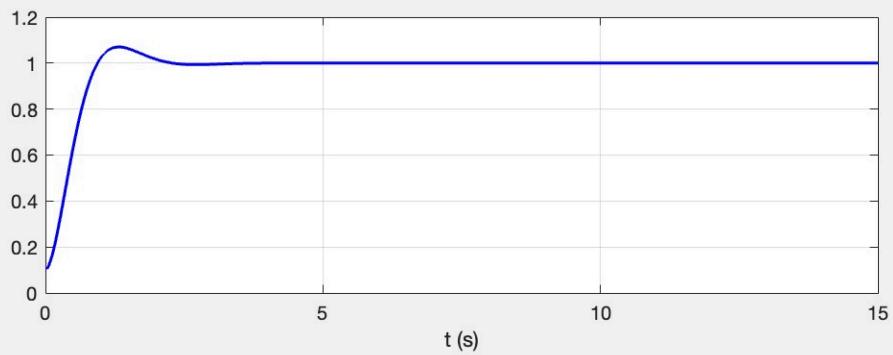
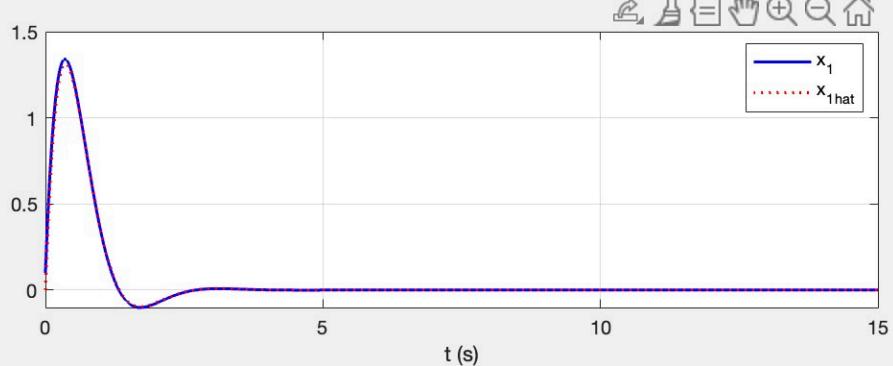
$$\lambda_1 = -1.33 + 2.25$$

$$\lambda_2 = -1.33 - 2.25$$

$$K = [7.34, 15.17] \quad \left. \right\} \text{state feedback design}$$

$$N = 17.17$$

$$L = [2.01, 3.67] \quad \left. \right\} \text{Observer design}$$



Problem 3

Consider the LTI system

$$\begin{cases} \dot{x}(t) = \begin{bmatrix} -1 & 0 \\ 0 & 10 \end{bmatrix}x(t) + \begin{bmatrix} 1 \\ 1 \end{bmatrix}u(t) \\ y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix}x(t) \end{cases}$$

1. Study the stability properties of the given system.
2. Supposing that the system state can be measured, is it possible to compute a state feedback controller of the form $u(t) = -Kx(t) + Nr(t)$ to stabilize the given system? Motivate your answer.
3. Supposing that the system state cannot be measured, is it possible to compute a state feedback controller of the form $u(t) = -K\dot{x}(t) + Nr(t)$ to stabilize the given system? Motivate your answer.

1. $\text{eig}(A) = \begin{bmatrix} -1 \\ 10 \end{bmatrix}$ $\lambda_1 = -1 ; \lambda_2 = 10$
 (convergent) (Divergent)

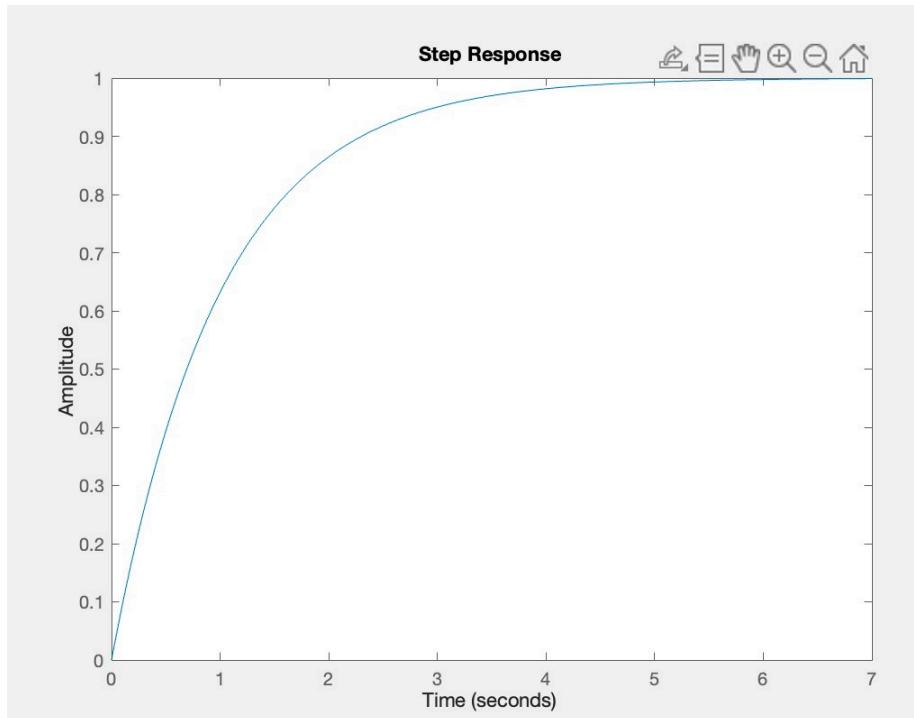
 $H(s) = \frac{1}{(s+1)}$
 Since $y(t) = e^{\lambda_1 t} + e^{\lambda_2 t}$
 conv Divergent

Divergent \Rightarrow internally unstable

Nodal Analysis $y(t) = e^{-t} + e^{10t}$

$\frac{1}{s+1} \Rightarrow$ converges to 0; BIBO stable

2. System state can be measured!



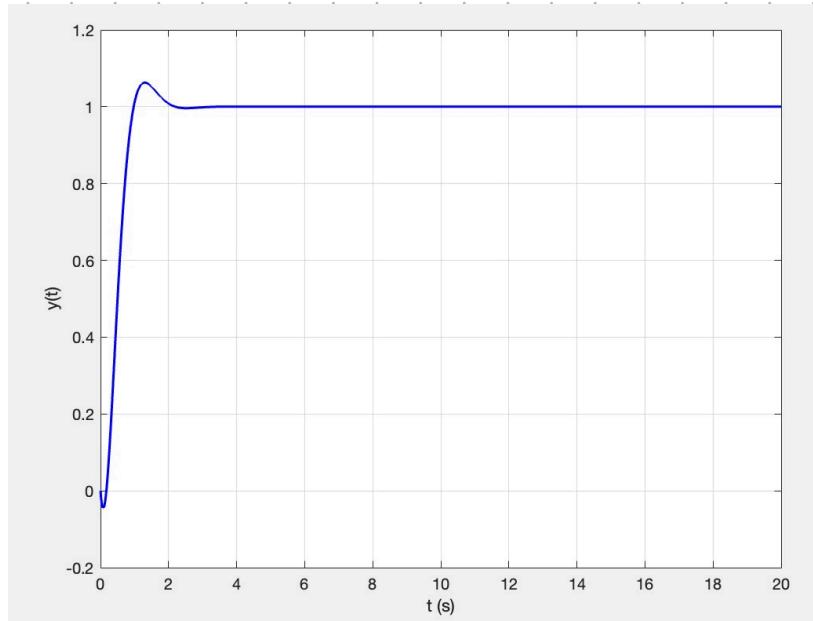
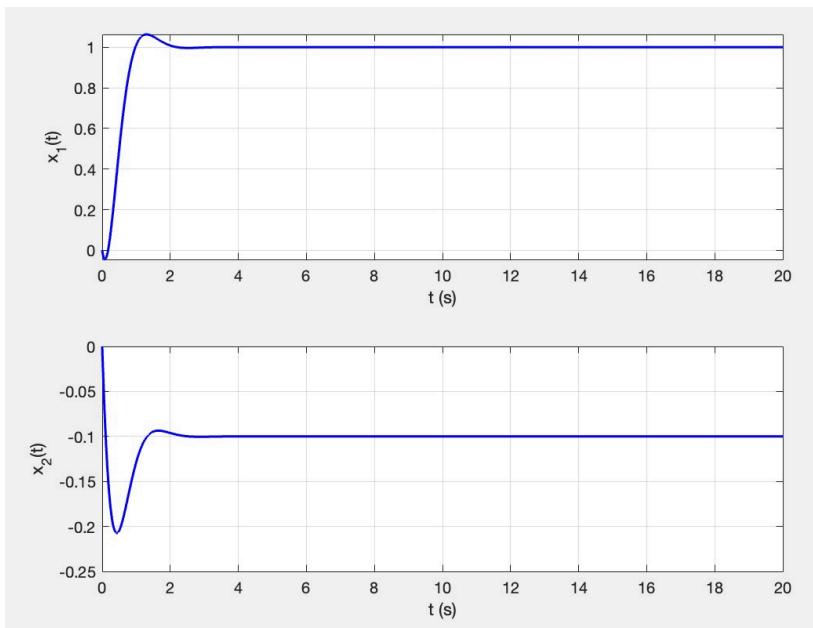
the step response
is converging to 1

$$M_R = \begin{pmatrix} 1 & -1 \\ 1 & 10 \end{pmatrix} \quad \text{and} \quad \boxed{\rho(M_R) = 2}$$

hence the system is reachable

Since the system is reachable hence it can be stabilized.

Example for the conditions in question 1:



3. if cannot be measured ; we have to use an observer. And for that the system needs to be observable

$$M_0 = \begin{pmatrix} 1 & 0 \\ -1 & 0 \end{pmatrix} \quad ; g(M_0) = 1$$

Hence not observable hence we cannot stabilize it 