DOWNRIGHT LINEARIZED MODEL - NO SPRING

```
K_1 = W_1 \times 1^2 + W_2 \cdot 1^2 + \Gamma_1
                                                        K5 = W2 L1 X2
                                                        K6 = M2 X2 + I2
  K2 = M2 L1 X2
 K3 = KF,1 + Km2/Rm
                                                        K_7 = K_{F_1}2
  K4 = Km/Rm
                                                       K8 = M29 X2
[ K1 01 + k202 + K301 = K4 VIN
 K5 04 + K6 02 + K7 02 + K802 = 0
    01=w1 01=w1
    \dot{\theta}_2 \approx \omega_2 \ddot{\theta}_2 = \dot{\omega}_2
  ( k1 w1+ k2 w2 + k3 w1 = k4 VIN
  | K5 w1 + K6 w2 + K7 w2 + K802 =0
  W1 = - k2 w2 - k3 W1 + k4 VIN
  ks (- k2 ω2 - k3 ω1 + k4 VIN) + k6 ω2 + k7 ω2 + κ8θ2 = 0
Θ1 = ω1
   - 125 12 162 - k5 163 Ws + 125 164 VIN + 126 162 + 127 162 + 16802 = 0
    ( 126 - 125 1/2 ) W2 = 125 1/2 W4 - 127 W2 - 12802 - 125 1/2 VIN
       1116-K5k2
 \dot{\omega}_{2} = \frac{k_{1}}{k_{1}k_{6} - k_{5}k_{2}} \frac{k_{5}}{k_{4}} \frac{k_{3}}{k_{4}} \omega_{1} - \frac{k_{1}k_{7}}{k_{1}k_{6} - k_{5}k_{2}} \omega_{2} - \frac{k_{1}k_{8}}{k_{1}k_{6} - k_{5}k_{2}} \frac{\Theta_{2}}{k_{1}k_{6} - k_{5}k_{2}} - \frac{k_{4}}{k_{1}k_{6} - k_{5}k_{2}} \frac{k_{4}}{k_{4}} V_{IN}
 W1 = - k2 k3 k5 W1 + k2 k7 W2 + k2 k8 W2 + k2 k8 W2 + k2 k8 W2 + k1 (k1 k6 - k2 k5) VIN - k3 W1 + k4 VIN
```

 $\omega_{1} = -\frac{\kappa_{2} k_{5} k_{5} + \kappa_{3} (\kappa_{3} \kappa_{6} - \kappa_{2} k_{5})}{\kappa_{1} (\kappa_{3} \kappa_{6} - \kappa_{2} k_{5})} \omega_{1} + \frac{\kappa_{2} k_{7}}{\kappa_{1} \kappa_{6} - \kappa_{2} \kappa_{5}} \omega_{2} + \frac{\kappa_{2} \kappa_{8}}{\kappa_{1} \kappa_{6} - \kappa_{2} \kappa_{5}} \theta_{2} + \left(\frac{\kappa_{4} (\kappa_{1} \kappa_{6} - \kappa_{2} \kappa_{5}) + \kappa_{2} k_{5} \kappa_{5}}{\kappa_{1} (\kappa_{1} \kappa_{6} - \kappa_{2} \kappa_{5})}\right) V_{N}$

$$\frac{\dot{\Theta}_{1} = \omega_{1}}{\dot{\Theta}_{2} = \omega_{2}}$$

$$\frac{\dot{\Theta}_{2} = \omega_{2}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\theta_{2} - \frac{k_{3}k_{6}}{k_{3}k_{6} - k_{2}k_{5}}}{k_{3}k_{6} - k_{2}k_{5}} \frac{\omega_{1} + \frac{k_{2}k_{7}}{k_{1}k_{6} - k_{2}k_{5}}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{2} + \frac{k_{4}k_{6}}{k_{1}k_{6} - k_{2}k_{5}}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{1} + \frac{k_{2}k_{7}}{k_{1}k_{6} - k_{2}k_{5}}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{2} - \frac{k_{4}k_{5}}{k_{1}k_{6} - k_{2}k_{5}}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{1}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{2}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{2}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{1}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{2}}{k_{1}k_{6} - k_{2}k_{5}} \frac{\omega_{2}}{k_{1}k_{$$

vociabili pii stato
$$X = \begin{cases} \Theta_1 \\ \Theta_2 \\ \omega_4 \\ \omega_2 \end{cases}$$

$$\frac{h_{2}k_{8}}{k_{1}k_{6}-k_{2}k_{5}} - \frac{k_{3}k_{6}}{k_{3}k_{6}-k_{2}k_{5}} - \frac{k_{2}k_{7}}{k_{1}k_{6}-k_{2}k_{5}}$$

$$- \frac{k_{1}k_{8}}{k_{3}k_{6}-k_{2}k_{5}} - \frac{k_{3}k_{7}}{k_{3}k_{6}-k_{2}k_{5}} - \frac{k_{4}k_{7}}{k_{3}k_{6}-k_{2}k_{5}}$$

$$C = \begin{bmatrix} 1 & 0 & 9 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \qquad D = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

Experiment #01: fixed oz. No spring

$$\Theta_4 = \omega_4$$
 $\omega_4 = \Theta_4$

K1 W1 + K3 W1 = KA VIN

$$A = \begin{bmatrix} 0 & -\frac{K3}{k1} \\ 0 & 4 \end{bmatrix} \qquad B = \begin{bmatrix} K4/k1 \\ 0 \end{bmatrix} \qquad C = \begin{bmatrix} 1 & 0 \end{bmatrix} \qquad D = 0$$