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HW#8
Lab 001-B
Date: April 17, 2016

Answer to 17.9(a):

The experiment is a $x \times b$ design. The levels for factor A is $[a_1, a_2, \dots, a_a]$, and the levels for factor B is $[b_1, b_2, \dots, b_b]$

If A and B are both fixed: all the levels of $[a_1, a_2, \dots, a_a]$ for A and all levels of $[b_1, b_2, \dots, b_b]$ for B, are included in the design.

If A and B are both random: out of all the levels of $[a_1, a_2, \dots, a_a]$ for A, only a subset of the $[a_1, a_2, \dots, a_a]$ levels for A is randomly selected and included. For B, only a randomly selected subset of all levels of $[b_1, b_2, \dots, b_b]$ for B, are included in the design.

Answer to 17.13(a):

The mixed effects model can be represented as:

$$y_{ijkl} = \mu + \tau_i + \beta_j + \gamma_k + \tau\beta_{ij} + \tau\gamma_{ik} + \beta\gamma_{jk} + \tau\beta\gamma_{ijk} + \epsilon_{l(ijk)}$$

here $i = 1, 2, 3, j = 1, 2, \dots, 4$, and $k = 1, 2, \dots, 6$,

Furthermore,

y_{ijkl} is the l^{th} observation for the level of i , for factor chemical, the level of j , for factor B, and the level of k , for factor C.

μ = overall mean response which is unknown

τ_i = the random effect corresponding to the i^{th} level of factor A. The τ_i s have independent normal distribution with mean zero and variance σ^2_A

β_j = the fixed effect corresponding to the j^{th} level of factor B.

γ_k = the fixed effect corresponding to the k^{th} level of factor C.

$\tau\beta_{ij}$ = the random effect due to interaction of the i^{th} level of factor A, and the j^{th} level of factor B. The $\tau\beta_{ij}$ s have independent normal distribution with mean zero and variance $\sigma^2_{\tau\beta}$

$\tau\gamma_{ik}$ = the random effect due to interaction of the i^{th} level of factor A, and the k^{th} level of factor C. The $\tau\gamma_{ik}$ s have independent normal distribution with mean zero and variance $\sigma^2_{\tau\gamma}$

$\beta\gamma_{jk}$ = the random effect due to interaction of the j^{th} level of factor B, and the k^{th} level of factor C. The $\beta\gamma_{jk}$ s have independent normal distribution with mean zero and variance $\sigma^2_{\beta\gamma}$

$\tau\beta\gamma_{ijk}$ = the random effect due to interaction for the i^{th} level of factor A, j^{th} level of factor B, and the k^{th} level of factor C. The $\tau\beta\gamma_{ijk}$ s have independent normal distribution with mean zero and variance $\sigma^2_{\tau\beta\gamma}$

$\varepsilon_{l(ijk)}$ = the random error associated with the l^{th} observation and has an independent distribution with mean zero, and variance σ^2

τ_i , $\tau\beta_{ij}$, $\tau\gamma_{ik}$, and $\tau\beta\gamma_{ijk}$ are mutually independent

Answer to 17.13(b):

Source	Expected Mean Square (EMS)	Degrees of Freedom (df)
A	$\sigma^2 + n\sigma^2_{ABC} + nb\sigma^2_{AC} + nc\sigma^2_{AB} + nbc\sigma^2_A$	$a-1=2$
B	$\sigma^2 + n\sigma^2_{ABC} + nc\sigma^2_{AB} + na\varphi^2_B$	$b-1=3$
C	$\sigma^2 + n\sigma^2_{ABC} + nb\sigma^2_{AC} + nab\varphi^2_C$	$c-1=5$
AB	$\sigma^2 + n\sigma^2_{ABC} + nc\sigma^2_{AB}$	$(a-1)(b-1) = 6$
AC	$\sigma^2 + n\sigma^2_{ABC} + nb\sigma^2_{AC}$	$(a-1)(c-1)=10$
BC	$\sigma^2 + n\sigma^2_{ABC} + na\varphi^2_{BC}$	$(b-1)(c-1)=15$
ABC	$\sigma^2 + n\sigma^2_{ABC}$	$(a-1)(b-1)(c-1) = 30$
Error	σ^2	$abc(n-1) = 216$

Answer to 17.13(c):

For random effects of A, σ^2_A :

$H_0: \sigma^2_A = 0$, $H_A: \sigma^2_A > 0$

Under H_0 , $\sigma^2_A = 0$, modified EMS = $\sigma^2 + n\sigma^2_{ABC} + nb\sigma^2_{AC} + nc\sigma^2_{AB}$

This modified EMS is not in the ANOVA table so we need to approximate the F-test is needed, with Satterthwaite's degree of freedom formula. The modified EMS can be obtained from $MS_{AB} + MS_{AC} - MS_{ABC}$

For fixed effects of B, φ^2_B :

$H_0: \varphi^2_B = 0$, $H_A: \varphi^2_B > 0$

Under H_0 , $\varphi^2_B = 0$, modified EMS = $\sigma^2 + n\sigma^2_{ABC} + nc\sigma^2_{AB}$

This modified EMS is in the ANOVA table, as well as with the degrees of freedom so we F-test = MS_B / MS_{AB}

For fixed effects of C, φ^2_C :

$H_0: \varphi^2_C = 0$, $H_A: \varphi^2_C > 0$

Under H_0 , $\varphi^2_C = 0$, modified EMS = $\sigma^2 + n\sigma^2_{ABC} + nb\sigma^2_{AC}$

This modified EMS is in the ANOVA table, as well as with the degrees of freedom so we
 $F\text{-test} = MS_C / MS_{AC}$

For random effects of AB, σ^2_{AB} :

$H_0: \sigma^2_{AB} = 0, H_A: \sigma^2_{AB} > 0$

Under H_0 , $\sigma^2_{AB} = 0$, modified EMS = $\sigma^2 + n\sigma^2_{ABC} + nc\sigma^2_{AB}$

This modified EMS and degrees of freedom is in the ANOVA table. The F-test = MS_{AB}/MS_{ABC}

For random effects of AC, σ^2_{AC} :

$H_0: \sigma^2_{AC} = 0, H_A: \sigma^2_{AC} > 0$

Under H_0 , $\sigma^2_{AC} = 0$, modified EMS = $\sigma^2 + n\sigma^2_{ABC}$

This modified EMS and degrees of freedom is in the ANOVA table. The F-test = MS_{AC}/MS_{ABC}

For random effects of BC, σ^2_{BC} :

$H_0: \sigma^2_{BC} = 0, H_A: \sigma^2_{BC} > 0$

Under H_0 , $\sigma^2_{BC} = 0$, modified EMS = $\sigma^2 + n\sigma^2_{ABC}$

This modified EMS and degrees of freedom is in the ANOVA table. The F-test = MS_{BC}/MS_{ABC}

For random effects of BC, σ^2_{ABC} :

$H_0: \sigma^2_{ABC} = 0, H_A: \sigma^2_{ABC} > 0$

Under H_0 , $\sigma^2_{ABC} = 0$, modified EMS = σ^2

This modified EMS and degrees of freedom is in the ANOVA table. The F-test = MS_{ABC}/MSE

Answer to 17.10(a):

The mixed effects model can be represented as:

$$y_{ijk} = \mu + \tau_i + \beta_j + \tau\beta_{ij} + \varepsilon_{k(ij)}$$

here $i = 1, 2, 3, 4$, and $j = 1, 2, \dots, 5$

Furthermore,

y_{ijk} is the k^{th} observation for the level of i , for factor chemical, the level of j , for factor location.

μ = overall mean response which is unknown

τ_i = the fixed effect corresponding to the i^{th} level of factor 'chemical'.

β_j = the random effect corresponding to the j^{th} level of factor 'location'. The β_j s have independent normal distribution with mean zero and variance $\sigma^2_{\text{location}}$

$\tau\beta_{ij}$ = the random effect due to interaction of the i^{th} level of factor chemical, and the j^{th} level of factor location. The $\tau\beta_{ij}$ s have independent normal distribution with mean zero and variance $\sigma^2_{\tau\beta}$

$\varepsilon_{k(ij)}$ = the random error associated with the k^{th} observation and has an independent distribution with mean zero, and variance σ^2

$\varepsilon_{k(ij)}$, $\tau\beta_{ij}$, and β_j are mutually independent

Answer to 17.10(b):

Source	df	Sum of Squares	Mean Square	Expected mean Square	Error term	Error DF	F Value	p-value
Chemical	3	180.123	60.044	Var(Residual) + 2 Var (chemical*location) + Q(chemical)	MS (chemical*location)	12	44.59	< 0.0001
Location	4	3.811	0.952	Var(Residual) + 2 Var (chemical*location) + 8 Var (location)	MS (chemical*location)	12	0.71	0.6020
Chemical*location	12	16.158	1.346	Var(Residual) + 2 Var (chemical*location)	MS(Residual)	20	3.89	0.0037
Error	20	6.925	0.346	Var(Residual)				

Answer to 17.11:

Fixed effects for chemical:

$H_0: \varphi^2_{\text{chemical}} = 0$, $H_A: \varphi^2_{\text{chemical}} > 0$

Decision: With 5% significance level, we reject the null hypothesis

Conclusion: There is significantly sufficient evidence that there is variability amongst the i^{th} levels of chemical.

Random effects for location:

$H_0: \sigma^2_{\text{location}} = 0$, $H_A: \sigma^2_{\text{location}} > 0$

Decision: With 5% significance level, we fail to reject the null hypothesis

Conclusion: There is not significantly sufficient evidence that there is variability amongst the j^{th} levels of location.

Random effects for interaction due to chemical*location:

$H_0: \sigma^2_{\text{chemical} * \text{location}} = 0$, $H_A: \sigma^2_{\text{chemical} * \text{location}} > 0$

Decision: With 5% significance level, we reject the null hypothesis

Conclusion: There is significantly sufficient evidence that there is variability amongst the interaction due to j^{th} levels of location and i^{th} levels of chemical.

Answer to 17.27(a):

The mixed effects model can be represented as:

$$y_{ijk} = \mu + \tau_i + \beta_j + \tau\beta_{ij} + \varepsilon_{k(ij)}$$

here $i = 1, 2, 3, 4$, and $j = 1, 2, 3$

Furthermore,

y_{ijk} is the k^{th} observation for the level of i , for factor machine, the level of j , for factor operator.

μ = overall mean response which is unknown

τ_i = the random effect corresponding to the i^{th} level of factor 'machine'. The τ_i s have independent normal distribution with mean zero and variance $\sigma^2_{\text{machine}}$

β_j = the random effect corresponding to the j^{th} level of factor 'operator'. The β_j s have independent normal distribution with mean zero and variance $\sigma^2_{\text{operator}}$

$\tau\beta_{ij}$ = the random effect due to interaction of the i^{th} level of factor machine, and the j^{th} level of factor operator. The $\tau\beta_{ij}$ s have independent normal distribution with mean zero and variance $\sigma^2_{\tau\beta}$

$\varepsilon_{k(ij)}$ = the random error associated with the k^{th} observation and has an independent distribution with mean zero, and variance σ^2

$\varepsilon_{k(ij)}$, $\tau\beta_{ij}$, and τ_i, β_j are mutually independent

Answer to 17.27(b):

Source	d f	Sum of Squares	Mean Square	Expected mean Square	Error term	Error DF	F Value	p- value
Machine	3	12.4583	60.044	Var(Residual) + 2 Var (machine*operator) + 6 Var (machine)	MS (machine*operator)	6	0.56	0.6619
Operator	2	160.333	0.952	Var(Residual) + 2 Var (machine*operator) + 8 Var (operator)	MS (machine*operator)	6	10.77	0.0103
Machine*Operator	6	44.6667	1.346	Var(Residual) + 2 Var (machine*operator)	MS(Residual)	12	1.96	0.1507
Error	12	45.506	0.346	Var(Residual)				

Answer to 17.27(c):

Random effects for machine:

$H_0: \sigma^2_{\text{machine}} = 0$, $H_A: \sigma^2_{\text{machine}} > 0$, p-value = 0.6619

Decision: With 5% significance level, we fail to reject the null hypothesis

Conclusion: There is not significantly sufficient evidence that there is variability amongst the i^{th} levels of machine.

Random effects for operator:

$H_0: \sigma^2_{\text{operator}} = 0$, $H_A: \sigma^2_{\text{operator}} > 0$, p-value = 0.0103

Decision: With 5% significance level, we reject the null hypothesis

Conclusion: There is not significantly sufficient evidence that there is variability amongst the j^{th} levels of operator.

Random effects for interaction due to machine*operator:

$H_0: \sigma^2_{\text{machine} * \text{operator}} = 0$, $H_A: \sigma^2_{\text{machine} * \text{operator}} > 0$, p-value = 0.1507

Decision: With 5% significance level, we fail to reject the null hypothesis

Conclusion: There is significantly sufficient evidence that there is variability amongst the interaction due to j^{th} levels of operator and i^{th} levels of machine.

Answer to 17.28(a):

Co-variance estimates from Type III:

Machine = -0.5486
Operator = 9.0903
Machine * operator = 1.8264
Residual = 3.7917

Co-variance estimates from REML:

Machine = 0
Operator = 9.2275
Machine * operator = 1.2777
Residual = 3.7917

REML is preferred as it includes adjustments needed for degree of freedom for estimating the mean squares. We also see from the output that the co-variance estimates for REML is different to that of Type III. For Type III the co-variance estimate is negative for machine.

Answer to 17.28(c):

The confidence interval for average solder strength = (199.43, 215.16)
This value states that with 95% statistical confidence we can state that the true average solder strength lies between 199.43, and 215.16.

/*
Akond Rahman

Date: April 14, 2016

Section 001B

Title: 17.10 and 17.11 problem for HW#8

*/

/*Loading data*/

data fire_ant_killer;

input chemical location @ ;

do k = 1 to 2;

input kill_count @;

output;

end;

cards;

1 1 7.2 9.6

1 2 8.5 9.6

1 3 9.1 8.6

1 4 8.2 9.0

1 5 7.8 8.0

2 1 4.2 3.5

2 2 2.9 3.3

2 3 1.8 2.4

2 4 3.6 4.4

2 5 3.7 3.9

3 1 9.5 9.3

3 2 8.8 9.2

3 3 7.6 7.1

3 4 7.3 7.0

3 5 9.2 8.3

4 1 5.4 3.9

4 2 6.3 6.0

4 3 6.1 5.6

4 4 5.0 5.4

4 5 6.5 6.9

;

run;

quit;

proc mixed data = fire_ant_killer method = type3 ;

class chemical location; /* chemical and location are the two factors*/

model kill_count = chemical ; /*chemical is the fixed factor, kill_count is the response*/

random location location*chemical; /* location*chemical, and location are the random factors*/

run;

The SAS System

The Mixed Procedure

Model Information	
Data Set	WORK.FIRE_ANT_KILLER
Dependent Variable	kill_count
Covariance Structure	Variance Components
Estimation Method	Type 3
Residual Variance Method	Factor
Fixed Effects SE Method	Model-Based
Degrees of Freedom Method	Containment

Class Level Information		
Class	Levels	Values
chemical	4	1 2 3 4
location	5	1 2 3 4 5

Dimensions	
Covariance Parameters	3
Columns in X	5
Columns in Z	25
Subjects	1
Max Obs Per Subject	40

Number of Observations	
Number of Observations Read	40
Number of Observations Used	40
Number of Observations Not Used	0

Type 3 Analysis of Variance								
Source	DF	Sum of Squares	Mean Square	Expected Mean Square	Error Term	Error DF	F Value	Pr > F
chemical	3	180.132750	60.044250	Var(Residual) + 2 Var (chemical*location) + Q(chemical)	MS (chemical*location)	12	44.59	<.0001
location	4	3.811500	0.952875	Var(Residual) + 2 Var (chemical*location) + 8 Var (location)	MS (chemical*location)	12	0.71	0.6020
chemical*location	12	16.158500	1.346542	Var(Residual) + 2 Var (chemical*location)	MS(Residual)	20	3.89	0.0037
Residual	20	6.925000	0.346250	Var(Residual)

Covariance Parameter Estimates	
Cov Parm	Estimate
location	-0.04921
chemical*location	0.5001

Covariance Parameter Estimates	
Cov Parm	Estimate
Residual	0.3462

Fit Statistics	
-2 Res Log Likelihood	93.5
AIC (smaller is better)	99.5
AICC (smaller is better)	100.3
BIC (smaller is better)	98.4

Type 3 Tests of Fixed Effects				
Effect	Num DF	Den DF	F Value	Pr > F
chemical	3	12	44.59	<.0001

Akond Rahman

Date: April 14, 2016

Section 001B

Title: 17.27 and 17.28 problem for HW#8

```
*/
/*Loading data*/
data strength_data;
  input machine operator @ ;
  do k = 1 to 2;
    input strength @;
    output;
  end;
cards;
1 1 204 205
1 2 205 207
1 3 211 209
2 1 205 210
2 2 205 206
2 3 207 210
3 1 203 204
3 2 206 204
3 3 209 214
4 1 205 203
4 2 209 207
4 3 215 212
;
run;
quit;
/*Using Type III method*/
proc mixed data = strength_data method = type3 ;
  class machine operator; /* machine and operator are the two factors*/
  model strength =; /* strength is the response*/
  random machine operator machine*operator; /* machine*operator, machine and operator are the random
run;
/* Ans.to 17.28 (a) */
/*Using REML method*/
proc mixed data = strength_data method = reml ;
  class machine operator; /* machine and operator are the two factors*/
  model strength = / ddfm = satterth cl ; /* strength is the response, used Satterwieth's adjustment
  random machine operator machine*operator; /* machine*operator, machine and operator are the random
  estimate 'Avg. solder strength' intercept 1 / cl; * get CI of the estimate of the avg. solder stren
run;
```

The SAS System

The Mixed Procedure

Model Information	
Data Set	WORK.STRENGTH_DATA
Dependent Variable	strength
Covariance Structure	Variance Components
Estimation Method	Type 3
Residual Variance Method	Factor
Fixed Effects SE Method	Model-Based
Degrees of Freedom Method	Containment

Class Level Information		
Class	Levels	Values
machine	4	1 2 3 4
operator	3	1 2 3

Dimensions	
Covariance Parameters	4
Columns in X	1
Columns in Z	19
Subjects	1
Max Obs Per Subject	24

Number of Observations	
Number of Observations Read	24
Number of Observations Used	24
Number of Observations Not Used	0

Type 3 Analysis of Variance								
Source	DF	Sum of Squares	Mean Square	Expected Mean Square	Error Term	Error DF	F Value	Pr > F
machine	3	12.458333	4.152778	Var(Residual) + 2 Var (machine*operator) + 6 Var (machine)	MS (machine*operator)	6	0.56	0.6619
operator	2	160.333333	80.166667	Var(Residual) + 2 Var (machine*operator) + 8 Var (operator)	MS (machine*operator)	6	10.77	0.0103
machine*operator	6	44.666667	7.444444	Var(Residual) + 2 Var (machine*operator)	MS(Residual)	12	1.96	0.1507
Residual	12	45.500000	3.791667	Var(Residual)

Covariance Parameter Estimates	
Cov Parm	Estimate
machine	-0.5486
operator	9.0903

Covariance Parameter Estimates	
Cov Parm	Estimate
machine*operator	1.8264
Residual	3.7917

Fit Statistics	
-2 Res Log Likelihood	109.5
AIC (smaller is better)	117.5
AICC (smaller is better)	119.7
BIC (smaller is better)	115.1

The SAS System

The Mixed Procedure

Model Information	
Data Set	WORK.STRENGTH_DATA
Dependent Variable	strength
Covariance Structure	Variance Components
Estimation Method	REML
Residual Variance Method	Profile
Fixed Effects SE Method	Model-Based
Degrees of Freedom Method	Satterthwaite

Class Level Information		
Class	Levels	Values
machine	4	1 2 3 4
operator	3	1 2 3

Dimensions	
Covariance Parameters	4
Columns in X	1
Columns in Z	19
Subjects	1
Max Obs Per Subject	24

Number of Observations	
Number of Observations Read	24
Number of Observations Used	24
Number of Observations Not Used	0

Iteration History			
Iteration	Evaluations	-2 Res Log Like	Criterion
0	1	124.48875799	
1	3	109.85258730	0.00025935
2	1	109.84333612	0.00000208
3	1	109.84326553	0.00000000

Convergence criteria met.

Covariance Parameter Estimates	
Cov Parm	Estimate
machine	0
operator	9.2275
machine*operator	1.2777

Covariance Parameter Estimates	
Cov Parm	Estimate
Residual	3.7917

Fit Statistics	
-2 Res Log Likelihood	109.8
AIC (smaller is better)	115.8
AICC (smaller is better)	117.1
BIC (smaller is better)	114.0

Solution for Fixed Effects								
Effect	Estimate	Standard Error	DF	t Value	Pr > t	Alpha	Lower	Upper
Intercept	207.29	1.8277	2	113.42	<.0001	0.05	199.43	215.16

Estimates								
Label	Estimate	Standard Error	DF	t Value	Pr > t	Alpha	Lower	Upper
Avg. solder strength	207.29	1.8277	2	113.42	<.0001	0.05	199.43	215.16