PS 3

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Issued: Thu 10/09/2025 Due: Thu 10/23/2025

Problem 1:

We designed a P.D. controller to achieve a point-to-point task with a planar two-link manipulator before.

For impedance control of the manipulator in this problem, we proposed a control law for the joint torque that can achieve in the task space a restoring force F corresponding to the virtual programmable cartesian spring Kp and damper Kd.

With gravity compensation, the control law was formulated in terms of the end-effector cartesian displacement error $x \sim x \sim x$ as:

$$au = g(q) - J^T \left(K_p ilde{x} + K_d \dot{ ilde{x}}
ight)$$

Consider now the case of impedance control of a planar four-link manipulator for achieving a point-to-point task.

In addition to the virtual cartesian spring and damper at the end-effector, let us say we also have a virtual cartesian spring and damper at joint-2 (the joint adjacent to the \shoulder" of the manipulator).

Propose a control law similar to the one shown above for the torque for the case of this four-link manipulator.

- The control law must be written in terms of the end-effector cartesian displacement error ~xe and the joint-2 cartesian displacement error ~x2.
- Neglect the gravity compensation term g(q). (You can find this term easily, we have done a similar exercise as part of Problem 3(b) in Problem Set#2.)
- No simulations are required (i.e. just propose the control law: NO coding is required in this problem!)

[Hint: Your answer should contain two different (why?) JT matrices respectively premultiplying the restoring force vectors corresponding to the mechanical impedances at the end-effector and the joint-2. Explicitly derive expressions for the Jacobian matrices in terms of joint angles and link lengths of the manipulator.]

Answer:

Known:

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Neglect the gravity compensation term g(q):

$$au = J^T \left(K_p ilde{x} + K_d \dot{ ilde{x}}
ight)$$

$$F = (K_p ilde{x} + K_d \dot{ ilde{x}})$$

The displacement error of endpoint and the joint 2:

$$ilde{x_e} = x - x_d$$

$$ilde{x_2} = x_2 - x_2 d$$

The forces of endpoint and the joint 2:

$$F_e = \left(K_p ilde{x_e} + K_d\dot{ ilde{x_e}}
ight)$$

$$F_2 = \left(K_p ilde{x_2} + K_d\dot{ ilde{x_2}}
ight)$$

The Jacobian of endpoint and the joint 2:

1. The end point position:

$$x_e = l1c1 + l2c12 + l3c123 + l4c1234$$

$$y_e = l1s1 + l2s12 + l3s123 + l4s1234$$

The Jacobian matrix:

$$J_e = egin{bmatrix} rac{\partial x_e}{\partial q_1} & rac{\partial x_e}{\partial q_2} & rac{\partial x_e}{\partial q_3} & rac{\partial x_e}{\partial q_4} \ rac{\partial y_e}{\partial q_1} & rac{\partial y_e}{\partial q_2} & rac{\partial y_e}{\partial q_3} & rac{\partial y_e}{\partial q_4} \end{bmatrix}$$

The elements:

$$\begin{split} \frac{\partial x_{e,x}}{\partial q_1} &= -l_1 s_1 - l_2 s_{12} - l_3 s_{123} - l_4 s_{1234} \\ \frac{\partial x_{e,x}}{\partial q_2} &= -l_2 s_{12} - l_3 s_{123} - l_4 s_{1234} \\ \frac{\partial x_{e,x}}{\partial q_3} &= -l_3 s_{123} - l_4 s_{1234} \\ \frac{\partial x_{e,x}}{\partial q_4} &= -l_4 s_{1234} \\ \frac{\partial x_{e,y}}{\partial q_1} &= l_1 c_1 + l_2 c_{12} + l_3 c_{123} + l_4 c_{1234} \\ \frac{\partial x_{e,y}}{\partial q_2} &= l_2 c_{12} + l_3 c_{123} + l_4 c_{1234} \\ \frac{\partial x_{e,y}}{\partial q_3} &= l_3 c_{123} + l_4 c_{1234} \\ \frac{\partial x_{e,y}}{\partial q_4} &= l_4 c_{1234} \\ \end{split}$$

2. The joint 2 position:

$$x_2=l1c1$$

$$y_2 = l1s1$$

The joint 2 Jacobian:

$$J_2 = egin{bmatrix} rac{\partial x_e}{\partial q_1} & rac{\partial x_e}{\partial q_2} & rac{\partial x_e}{\partial q_3} & rac{\partial x_e}{\partial q_4} \ rac{\partial y_e}{\partial q_1} & rac{\partial y_e}{\partial q_2} & rac{\partial y_e}{\partial q_3} & rac{\partial y_e}{\partial q_4} \end{bmatrix} = egin{bmatrix} -l_1 s1 & 0 & 0 & 0 \ l1c1 & 0 & 0 & 0 \end{bmatrix}$$

Thus, the control law:

$$au = -J_e^T \left(K_{p,e} ilde{x}_e + K_{d,e}\dot{ ilde{x}}_e
ight) - J_2^T \left(K_{p,2} ilde{x}_2 + K_{d,2}\dot{ ilde{x}}_2
ight)$$

Problem 2:

Consider the dynamic equations in the vertical plane for a two degree-of-freedom planar manipulator with two rotational joints

$$H(q)\ddot{q}+C(q,\dot{q})\dot{q}+g(q)= au$$

Where:

$$egin{aligned} q &= egin{bmatrix} heta_1 \ heta_2 \end{bmatrix}, \quad H &= egin{bmatrix} H_{11} & H_{12} \ H_{12} & H_{22} \end{bmatrix}, \quad C &= egin{bmatrix} -h\dot{ heta}_2 & -h\dot{ heta}_1 - h\dot{ heta}_2 \ h\dot{ heta}_1 & 0 \end{bmatrix}, \quad g &= egin{bmatrix} G_1 \ G_2 \end{bmatrix} \end{aligned}$$
 $H_{11} &= m_1 l_{c1}^2 + I_1 + m_2 (l_1^2 + l_{c2}^2 + 2l_1 l_{c2} \cos{ heta}_2) + I_2$
 $H_{22} &= m_2 l_{c2}^2 + I_2$
 $H_{12} &= m_2 l_1 l_{c2} \cos{ heta}_2 + m_2 l_{c2}^2 + I_2$
 $h &= m_2 l_1 l_{c2} \sin{ heta}_2$
 $G_1 &= m_1 l_{c1} g \cos{ heta}_1 + m_2 l_{c2} g \cos({ heta}_1 + { heta}_2) + m_2 l_1 g \cos{ heta}_1$
 $G_2 &= m_2 l_{c2} g \cos({ heta}_1 + { heta}_2)$

Design and simulate an adaptive controller without any initial knowledge of the constant parameters. The desired trajectory is:

$$heta_{d1} = 2(1-e^{-t}), \quad heta_{d2} = 3(1-e^{-2t})$$

(In the simulation, you can choose the real values of the parameters and the initial conditions by yourself.)

Answer:

Known:

$$H(q)\ddot{q}+C(q,\dot{q})\dot{q}+g(q)= au$$
 $q=egin{bmatrix} heta_1 & H_{12} & H_{12} & H_{12} \ heta_2 & H_{12} & H_{22} \end{bmatrix}, \quad C=egin{bmatrix} -h\dot{ heta}_2 & -h\dot{ heta}_1-h\dot{ heta}_2 \ h\dot{ heta}_1 & 0 \end{bmatrix}, \quad g=egin{bmatrix} G_1 \ G_2 \end{bmatrix}$ $H_{11}=m_1l_{c1}^2+I_1+m_2(l_1^2+l_{c2}^2+2l_1l_{c2}\cos\theta_2)+I_2$ $H_{22}=m_2l_{c2}^2+I_2$ $H_{22}=m_2l_{c2}^2+I_2$ $H_{12}=m_2l_1l_{c2}\cos\theta_2+m_2l_{c2}^2+I_2$ $h=m_2l_1l_{c2}\sin\theta_2$ $G_1=m_1l_{c1}g\cos\theta_1+m_2l_{c2}g\cos(\theta_1+\theta_2)+m_2l_1g\cos\theta_1$ $G_2=m_2l_{c2}g\cos(\theta_1+\theta_2)$

Definition of Tracking Error and Reference Trajectory:

$$egin{aligned} ilde{q} &= q_d - q \ \dot{q}_r &= \dot{q}_d - \Lambda e \ s &= \dot{q} - \dot{q}_r &= \dot{ ilde{q}} + \Lambda ilde{q} \end{aligned}$$

Linear Parameterization:

$$H(q)\ddot{q}+C(q,\dot{q})\dot{q}+g(q)= au$$
 $H(q)\ddot{q}_r+C(q,\dot{q})\dot{q}_r+g(q)=Y(q,\dot{q},\dot{q}_r,\ddot{q}_r)a$

For a:

$$a = egin{bmatrix} a_1 \ a_2 \ a_3 \ a_4 \ a_5 \end{bmatrix} = egin{bmatrix} m_1 l_{c1}^2 + m_2 l_1^2 + I_1 \ m_2 l_{c2}^2 + I_2 \ m_2 l_1 l_{c2} \ m_1 l_{c1} g + m_2 l_1 g \ m_2 l_{c2} g \end{bmatrix}$$

For Y:

$$Y = egin{bmatrix} Y_{11} & Y_{12} & Y_{13} & Y_{14} & Y_{15} \ Y_{21} & Y_{22} & Y_{23} & Y_{24} & Y_{25} \end{bmatrix} = egin{bmatrix} \ddot{q}_{r1} + \ddot{q}_{r2} & 2\cos heta_2\ddot{q}_{r1} + \cos heta_2\ddot{q}_{r2} - \sin heta_2(\dot{ heta}_2\dot{q}_{r1} + (\dot{ heta}_1 + \dot{ heta}_2)\dot{q}_{r2}) & \cos heta_1 \ 0 & \ddot{q}_{r1} + \ddot{q}_{r2} & \cos heta_2\ddot{q}_{r1} + \sin heta_2\dot{ heta}_1\dot{q}_{r1} & 0 \end{pmatrix}$$

Control and Adaption:

$$au = Y\hat{a} - K_d s$$
 $\dot{\hat{a}} = -P\,Y^ op s = \dot{\hat{a}} = -P\,Y(q,\dot{q},\dot{q}_r,\ddot{q}_r)^ op s$

Lyapunov stability analysis:

$$V=1/2(S^THS)+1/2(ilde{a}^TP^{-1} ilde{a})$$
 $\dot{V}=s^TH\dot{s}+rac{1}{2}s^T\dot{H}s+ ilde{a}^TP^{-1}\dot{ ilde{a}}=-s^TK_ds\leq 0$

Since

$$V \geq 0$$
, $\dot{V} \leq 0$, V is radially unbounded

according to Lyapunov stability theory, the system is globally uniformly stable. Moreover,

$$s \to 0$$
 as $t \to \infty$

Because

$$s=\dot{ ilde{q}}+\Lambda ilde{q}$$

it follows that

$$ilde{q}
ightarrow 0, \quad \dot{ ilde{q}}
ightarrow 0 ext{ as } t
ightarrow \infty$$

meaning both the tracking error and its derivative converge to zero.

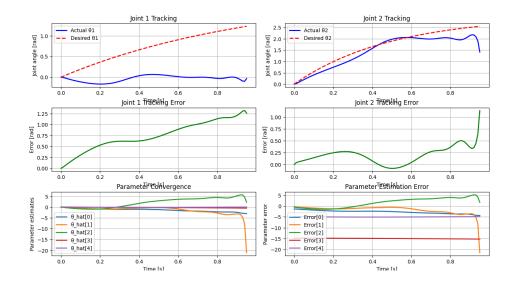
Simulation with:

```
import numpy as np
from scipy.integrate import solve_ivp
import matplotlib.pyplot as plt
#design parameters
m1, m2 = 1.0, 1.0
11, 12 = 1.0, 1.0
Ic1, Ic2 = 0.5, 0.5
11, 12 = 0.1, 0.1
g = 9.81
phi_true = np.array([
  m1*lc1**2 + m2*l1**2 + l1,
  m2*lc2**2 + I2,
  m2*I1*Ic2,
  m1*lc1*g + m2*l1*g,
  m2*lc2*g
print("True parameters:")
for i in range(5):
  print(f''\pi\{i+1\} = \{phi\_true[i]:.3f\}'')
def qd(t):
  theta1 = 2*(1 - np.exp(-t))
  theta2 = 3*(1 - np.exp(-2*t))
  return np.array([theta1, theta2])
def qd_dot(t):
  return np.array([2*np.exp(-t), 6*np.exp(-2*t)])
def qd_ddot(t):
  return np.array([-2*np.exp(-t), -12*np.exp(-2*t)])
def H_matrix(q):
  th1, th2 = q
  H11 = m1*lc1**2 + l1 + m2*(l1**2 + lc2**2 + 2*l1*lc2*np.cos(th2)) + l2
  H12 = m2*I1*Ic2*np.cos(th2) + m2*Ic2**2 + I2
  H22 = m2*lc2**2 + I2
  return np.array([[H11, H12],[H12, H22]])
def C_matrix(q, q_dot):
  th1, th2 = q
  dth1, dth2 = q_dot
  h = m2*I1*Ic2*np.sin(th2)
  return np.array([[-h*dth2, -h*(dth1 + dth2)],
            [h*dth1, 0]])
def g_vector(q):
  th1, th2 = q
  G1 = m1*lc1*g*np.cos(th1) + m2*lc2*g*np.cos(th1 + th2) + m2*l1*g*np.cos(th1)
```

```
G2 = m2*lc2*g*np.cos(th1 + th2)
  return np.array([G1, G2])
Lambda = np.diag([5.0, 5.0])
K = np.diag([10.0, 10.0])
Gamma = np.diag([0.1, 0.1, 0.1, 0.1, 0.1])
def Y_matrix(q, q_dot, q_r_dot, q_r_dot):
  th1, th2 = q
  dth1, dth2 = q_dot
  dqr1, dqr2 = q_r_dot
  ddqr1, ddqr2 = q_r_ddot
  Y = np.zeros((2, 5))
  Y[0, 0] = ddqr1
  Y[0, 1] = ddqr1 + ddqr2
  Y[0, 2] = 2*np.cos(th2)*ddqr1 + np.cos(th2)*ddqr2 - np.sin(th2)*(dth2*dqr1 + (dth1 + dth2)*dqr2)
  Y[0, 3] = np.cos(th1)
  Y[0, 4] = np.cos(th1 + th2)
  Y[1, 0] = 0
  Y[1, 1] = ddqr1 + ddqr2
  Y[1, 2] = np.cos(th2)*ddqr1 + np.sin(th2)*dth1*dqr1
  Y[1, 3] = 0
  Y[1, 4] = np.cos(th1 + th2)
  return Y
def dynamics(t, state):
  q = state[0:2]
  q_dot = state[2:4]
  theta_hat = state[4:9]
  q_d = qd(t)
  q_d_d = q_d_d (t)
  q_d=ddot = qd_dot(t)
  q_tilde = q_d - q
  q_r_dot = q_d_dot - Lambda @ q_tilde
  q_{tilde_{dot}} = q_{d_{dot}} - q_{dot}
  q_r_ddot = q_d_ddot - Lambda @ q_tilde_dot
  s = q_dot - q_r_dot
  Y = Y_matrix(q, q_dot, q_r_dot, q_r_ddot)
  tau = Y @ theta_hat - K @ s
  H = H_matrix(q)
  C = C_{matrix}(q, q_{dot})
  g_{vec} = g_{vector}(q)
  q_ddot = np.linalg.inv(H) @ (tau - C @ q_dot - g_vec)
```

```
theta_hat_dot = -Gamma @ Y.T @ s
  return np.concatenate([q_dot, q_ddot, theta_hat_dot])
q0 = np.array([0.0, 0.0])
q_dot0 = np.array([0.0, 0.0])
theta_hat0 = np.zeros(5)
state0 = np.concatenate([q0, q_dot0, theta_hat0])
print("Starting adaptive control simulation...")
t_{span} = (0, 10)
t_eval = np.linspace(0, 10, 2000)
sol = solve_ivp(dynamics, t_span, state0, t_eval=t_eval, method='RK45', rtol=1e-6)
print("Simulation completed!")
t_sol = sol.t
q_sol = sol.y[0:2, :]
q_dot_sol = sol.y[2:4, :]
theta_hat_sol = sol.y[4:9, :]
q_d=0 = np.array([qd(t) for t in t_sol]).T
q_d_{ot} = np.array([qd_{ot}(t) for t in t_{sol}]).T
q_tilde_sol = q_d_sol - q_sol
s_sol = q_dot_sol - (q_d_dot_sol - Lambda @ q_tilde_sol)
plt.figure(figsize=(15, 12))
plt.subplot(3, 2, 1)
plt.plot(t_sol, q_sol[0, :], 'b-', linewidth=2, label='Actual \theta1')
plt.plot(t_sol, q_d_sol[0, :], 'r--', linewidth=2, label='Desired \theta1')
plt.xlabel('Time [s]')
plt.ylabel('Joint angle [rad]')
plt.title('Joint 1 Tracking')
plt.legend()
plt.grid(True)
plt.subplot(3, 2, 2)
plt.plot(t_sol, q_sol[1, :], 'b-', linewidth=2, label='Actual θ2')
plt.plot(t_sol, q_d_sol[1, :], 'r--', linewidth=2, label='Desired \theta2')
plt.xlabel('Time [s]')
plt.ylabel('Joint angle [rad]')
plt.title('Joint 2 Tracking')
plt.legend()
plt.grid(True)
plt.subplot(3, 2, 3)
plt.plot(t_sol, q_tilde_sol[0, :], 'g-', linewidth=2)
plt.xlabel('Time [s]')
plt.ylabel('Error [rad]')
plt.grid(True)
```

```
plt.subplot(3, 2, 4)
plt.plot(t_sol, q_tilde_sol[1, :], 'g-', linewidth=2)
plt.xlabel('Time [s]')
plt.ylabel('Error [rad]')
plt.title('Joint 2 Tracking Error (q2)')
plt.grid(True)
plt.subplot(3, 2, 5)
plt.plot(t_sol, s_sol[0, :], 'm-', linewidth=2, label='s_1')
plt.plot(t_sol, s_sol[1, :], 'c-', linewidth=2, label='s_2')
plt.xlabel('Time [s]')
plt.ylabel('Sliding variable')
plt.title('Sliding Variables')
plt.legend()
plt.grid(True)
plt.subplot(3, 2, 6)
for i in range(5):
  plt.plot(t_sol, theta_hat_sol[i, :], linewidth=2, label=f'â[{i+1}]')
  plt.axhline(y=phi_true[i], color=plt.gca().lines[-1].get_color(), linestyle='--', alpha=0.5)
plt.xlabel('Time [s]')
plt.ylabel('Parameter estimates')
plt.title('Parameter Convergence (dashed: true values)')
plt.legend()
plt.grid(True)
plt.tight_layout()
plt.show()
print("\nPerformance Analysis:")
print(f"Final Joint 1 Error: {q_tilde_sol[0, -1]:.6f} rad")
print(f"Final Joint 2 Error: {q_tilde_sol[1, -1]:.6f} rad")
print(f"RMS Joint 1 Error: {np.sqrt(np.mean(q_tilde_sol[0, :]**2)):.6f} rad")
print(f"RMS Joint 2 Error: {np.sqrt(np.mean(q_tilde_sol[1, :]**2)):.6f} rad")
print("\nFinal Parameter Estimates vs True Values:")
for i in range(5):
  error = theta_hat_sol[i, -1] - phi_true[i]
  print(f"â[{i+1}] = {theta_hat_sol[i, -1]:.4f} (True: {phi_true[i]:.4f}, Error: {error:.4f})")
```



Problem 3:

Consider the dynamic equations of a robot manipulator

$$H(q)\ddot{q}+C(q,\dot{q})\dot{q}+D\dot{q}+g(q)= au$$

where the matrix D is constant symmetric positive definite. Consider an adaptive P.D. controller for such a robot with the control law

$$au = Y\hat{a} - K_d\dot{ ilde{q}} - K_p ilde{q}$$

and the adaptation law

$$\dot{\hat{a}} = -PY^Ts$$

where

$$egin{split} Ya &= H(q)\ddot{q}_r + C(q,\dot{q})\dot{q}_r + D\dot{q}_r + g(q) \ & s &= \dot{q} - \dot{q}_r = \dot{ ilde{q}} + \lambda ilde{q} \ & ilde{q} &= q - q_d \end{split}$$

The adaptation and controller gain matrices $P, K_d and K_p$ are all symmetric positive definite.

Show that this controller will force the tracking error \tilde{q} to converge to zero.

[Hint: You may want to use the Lyapunov function candidate

$$V = rac{1}{2} s^T H s + rac{1}{2} ilde{a}^T P^{-1} ilde{a} + rac{1}{2} ilde{q}^T (K_p + \lambda K_d) ilde{q}$$

Answer:

Known:

$$egin{aligned} H(q)\ddot{q}+C(q,\dot{q})\dot{q}+D\dot{q}+g(q)&= au\ & au=Y\hat{a}-K_d\dot{ ilde{q}}-K_p ilde{q} \end{aligned}$$
 $Ya=H(q)\ddot{q}_r+C(q,\dot{q})\dot{q}_r+D\dot{q}_r+g(q)$

Definition of Tracking Error and Reference Trajectory:

$$egin{aligned} ilde{q} &= q - q_d \ s &= \dot{ ilde{q}} + \lambda ilde{q} &= \dot{q} - \dot{q}_r \ \dot{q}_r &= \dot{q}_d - \lambda ilde{q} \end{aligned}$$

Adaptive:

$$\dot{\hat{a}} = -PY^Ts$$

Known Lyapunov function candidate:

$$V = rac{1}{2} s^T H s + rac{1}{2} ilde{a}^T P^{-1} ilde{a} + rac{1}{2} ilde{q}^T (K_p + \lambda K_d) ilde{q}$$

Thus:

$$\dot{V} = s^T H \dot{s} + rac{1}{2} s^T \dot{H} s - ilde{a}^T P^{-1} \dot{\hat{a}} + ilde{q}^T (K_p + \lambda K_d) \dot{ ilde{q}}$$

Fort the $s^T H \dot{s}$:

$$au = Y\hat{a} - K_d\dot{ ilde{q}} - K_p ilde{q} = H\dot{s} + Cs + Ds$$
 $s^TH\dot{s} = s^T(Y ilde{a} - Cs - Ds - K_d\dot{ ilde{q}} - K_p ilde{q})$

For the $\tilde{a}^TP^{-1}\dot{\hat{a}}$:

$$\dot{\hat{a}} = -PY^Ts$$
 $\tilde{a}^TP^{-1}\dot{\tilde{a}} = -\tilde{a}^TY^Ts = -s^TY\tilde{a}$

Because $H^{\boldsymbol{\cdot}}(q) - 2C(q,q^{\boldsymbol{\cdot}})$ is skew-symmetric matrix:

$$rac{1}{2}s^T\dot{H}s-s^TCs=0$$

Thus:

$$\dot{V} = -s^T D s - s^T K_d \dot{ ilde{q}} - s^T K_p ilde{q} + ilde{q}^T (K_p + \lambda K_d) \dot{ ilde{q}}$$

As
$$s=\dot{ ilde{q}}+\lambda ilde{q}=\dot{q}-\dot{q}_r$$

$$egin{aligned} -s^T K_d \dot{ ilde{q}} &= -\dot{ ilde{q}}^T K_d \dot{ ilde{q}} - \lambda ilde{q}^T K_d \dot{ ilde{q}} \ &- s^T K_p ilde{q} &= -\dot{ ilde{q}}^T K_p ilde{q} - \lambda ilde{q}^T K_p ilde{q} \ & ilde{q}^T (K_p + \lambda K_d) \dot{ ilde{q}} &= ilde{q}^T K_p \dot{ ilde{q}} + \lambda ilde{q}^T K_d \dot{ ilde{q}} \end{aligned}$$

Thus:

$$\dot{V} = -s^T D s - \dot{ ilde{q}}^T K_d \dot{ ilde{q}} - \lambda ilde{q}^T K_p ilde{q} \leq 0$$

Because the the adaptation and controller gain matrices $P, K_d and K_p$ are all symmetric positive definite, so $V^\star \leq 0$.

Problem 4:

Consider the following dynamics equation from the lecture:

$$J\ddot{q}+b\dot{q}|\dot{q}|+mgl\sin q= au$$
 $a_1=J$ $a_2=b$ $a_3=mgl$

with unknown but constant parameters $a=[a_1,a_2,a_3]^\mathsf{T}$. From the lecture and the previous problems, you should be able to design a control law and an adaptation law for this system, assuming no prior knowledge of the actual values of a_1,a_2,a_3 .

Now assume that we know that parameters a_1 , a_2 satisfy $a_1, a_2 > 0$ and parameter a_3 satisfies $a_3 > c$ for some known constant c > 0. How can we exploit this knowledge in the adaptation law? State the adaptation law, and show that the controller will still force the tracking error \tilde{q} to zero.

Answer:

Know:

$$J\ddot{q} + b\dot{q}|\dot{q}| + mgl\sin q = au$$

$$a=egin{bmatrix} a_1\ a_2\ a_3 \end{bmatrix},\quad a_1,a_2>0,\quad a_3>c>0$$

Definition of Tracking Error:

$$egin{aligned} ilde{q} &= q - q_d \ \dot{q}_r &= \dot{q}_d - \lambda ilde{q} \ s &= \dot{ ilde{q}} + \lambda ilde{q} &= \dot{q} - \dot{q}_r \ \dot{s} &= \ddot{q} - \ddot{q}_r \ \ddot{q}_r &= \ddot{q}_d - \lambda \dot{ ilde{q}} \end{aligned}$$

Option1, If Define:

$$V=rac{1}{2}s^2$$

Thus:

$$\dot{V}=s\dot{s}=s(\ddot{q}-\ddot{q}_r)$$

$$\ddot{q}=J^{-1}(au-b\dot{q}|\dot{q}|-mgl\sin q)$$
 $\dot{V}=s\dot{s}=s(au-J\ddot{q}r-b\dot{q}|\dot{q}|-mgl\sin q))=s(au-Ya)$

Design control and adaptation law:

$$au = Y\hat{a} - ks$$

Thus:

$$\dot{V}=s(Y\hat{a}-ks-Ya)=sY(\hat{a}-a)-ks^2$$
 $\dot{V}=-ks^2\leq 0$

Option2, If Define:

$$V=rac{1}{2}Js^2+rac{1}{2} ilde{a}^TP^{-1} ilde{a}\geq 0$$

Thus:

$$\dot{V}=sJ\dot{s}+ ilde{a}^TP^{-1}\dot{ ilde{a}}=-ks^2+\left(sY ilde{a}+ ilde{a}^TP^{-1}\dot{ ilde{a}}
ight)$$

Design control and adaptation law:

$$au = Y\hat{a} - ks$$

$$\dot{\hat{a}} = -PY^Ts$$

Thus:

$$\dot{V}=-ks2\leq 0$$

The controller will still force the tracking error \tilde{q} to zero.