

# Robotics 2 Project

Robotics & Control 2

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# Introduction - Problem definition I

- Initialization:** Consider 3 mobile robots (unicycles) starting from two sets of random initial conditions.
- Consensus:** Make them agree on a rendez-vous point.
- Regulation:** Move them towards the consensus point.
- Switch:** When they are close to it (threshold  $\varepsilon = 0.01$ ), switch to the tracking controller.
- Tracking:** Make them follow a circular trajectory centered in the rendez-vous point.



# Introduction - Problem definition II

## Design choices:

- Unicycle as point mass, described by the kinematic model

$$\Sigma : \begin{cases} \dot{x}(t) = v(t) \cos \theta(t) \\ \dot{y}(t) = v(t) \sin \theta(t) \\ \dot{\theta}(t) = \omega(t) \end{cases}$$

- Three robots treated as independent agents and no handle of collision avoidance.
- Average consensus in one step.
- Gains chosen especially by trial and error.

## Implementation choices:

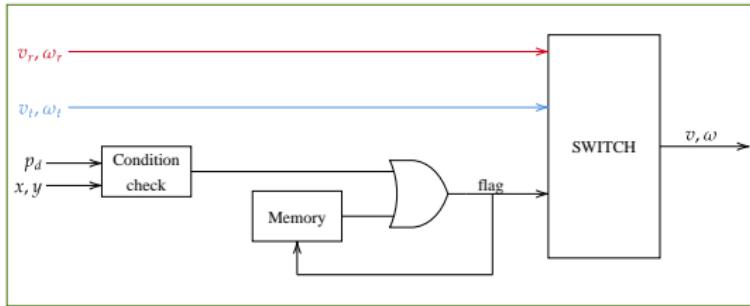
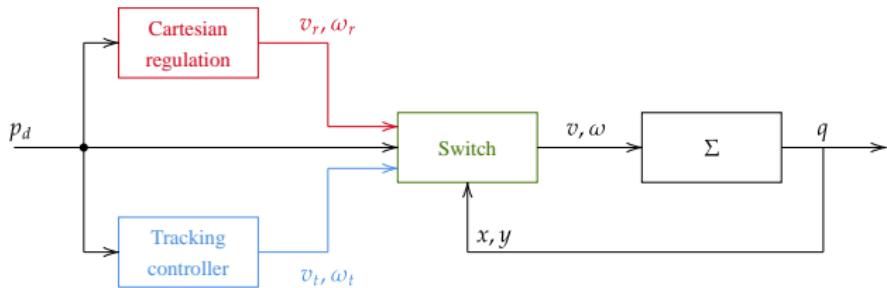
- Derivative implemented as a 1<sup>st</sup> order high-pass filter

$$H(s) = \frac{s}{f_c s + 1}, \quad \text{with } f_c = \frac{1}{2\pi 20}.$$

- Unwrap block placed after the atan2 function.
- Initial conditions  $q_0$  set in the Integrator blocks of the model.



# Introduction - Switch

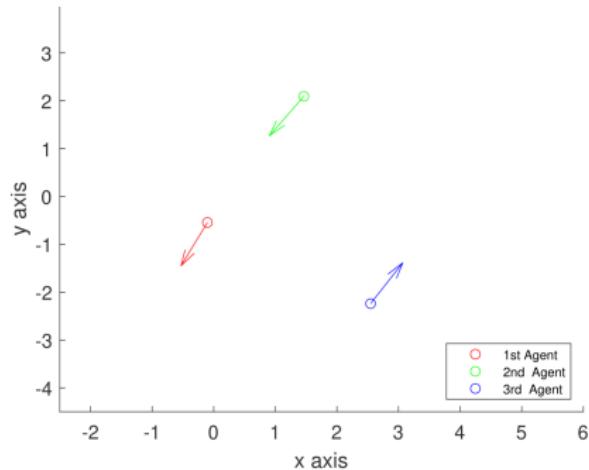


Note: In the first block diagram the output feedback should enter also into the two controllers, though, it has been neglected for clarity.

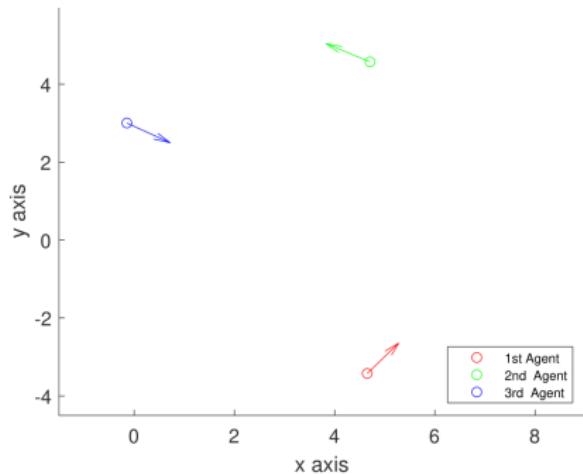


# Introduction - Initial Conditions

Case 1



Case 2



$$\text{Case 1: } q_{0,1} = \begin{bmatrix} -0.10 \\ -0.54 \\ 4.27 \end{bmatrix}, \quad q_{0,2} = \begin{bmatrix} 1.46 \\ 2.09 \\ 4.12 \end{bmatrix}, \quad q_{0,3} = \begin{bmatrix} 2.55 \\ -2.24 \\ 1.02 \end{bmatrix}.$$

$$\text{Case 2: } q_{0,1} = \begin{bmatrix} 4.65 \\ -3.42 \\ 0.89 \end{bmatrix}, \quad q_{0,2} = \begin{bmatrix} 4.71 \\ 4.57 \\ 2.65 \end{bmatrix}, \quad q_{0,3} = \begin{bmatrix} -0.15 \\ 3.00 \\ 5.75 \end{bmatrix}.$$



## Consensus - Algorithm

Given a matrix  $P \in \mathbb{R}^{3 \times 3}$ , the consensus dynamics is  $x_{cons}(k+1) = P x_{cons}(k)$ , initialized

with the initial positions of the agents, with  $x_{cons}(k) = [x_{cons,1}|x_{cons,2}] = \begin{bmatrix} x_1(k) & y_1(k) \\ x_2(k) & y_2(k) \\ x_3(k) & y_3(k) \end{bmatrix}$ .

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### Algorithm

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```
i = 0, ε = 0.01
flag = false
set P, xcons(0)

while flag = false do
    if i ≥ 100 then
        flag = true
    if |max {xcons,1} - min {xcons,1}| ≤ ε/10 then
        if |max {xcons,2} - min {xcons,2}| ≤ ε/10 then
            flag = true
    xcons(i + 1) = P xcons(i)
    i = i + 1
```

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## Consensus - Theory

### Proposition [Strongly connected and aperiodic digraphs and primitive adjacency matrices]

A matrix  $A \in \mathbb{R}^{n \times n}$  is primitive  $\iff$  The associated digraph  $\mathcal{G}$  is strongly connected and aperiodic.

### Proposition [Sufficient condition for consensus]

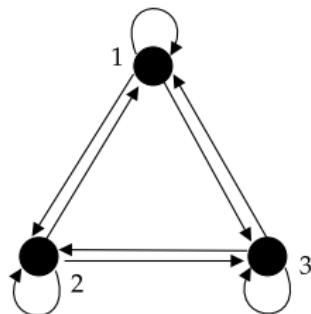
Given the update rule  $x(k+1) = Ax(k)$  with  $A \in \mathbb{R}^{n \times n}$  primitive and row-stochastic, then  $x(k) = P^k x(0)$  reaches consensus for  $k \rightarrow \infty$ .

### Proposition [Sufficient condition for average consensus]

Given the update rule  $x(k+1) = Ax(k)$  with  $A \in \mathbb{R}^{n \times n}$  primitive and doubly-stochastic, then  $x(k) = P^k x(0)$  reaches average consensus for  $k \rightarrow \infty$ .



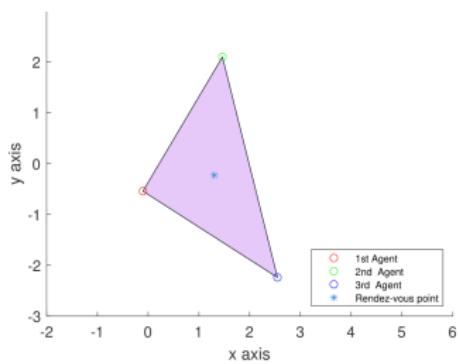
## Consensus - Average Asymptotic Consensus in One Step



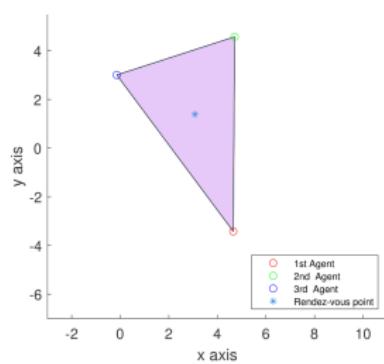
$P$  primitive and doubly stochastic

$$P = \begin{bmatrix} 1/3 & 1/3 & 1/3 \\ 1/3 & 1/3 & 1/3 \\ 1/3 & 1/3 & 1/3 \end{bmatrix}$$

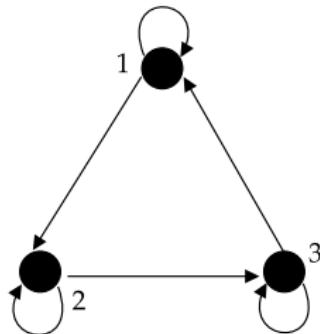
Case 1



Case 2



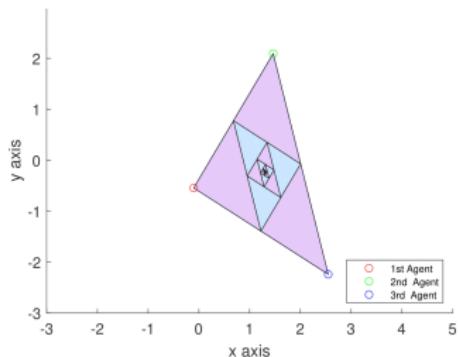
## Consensus - Average Asymptotic Consensus I



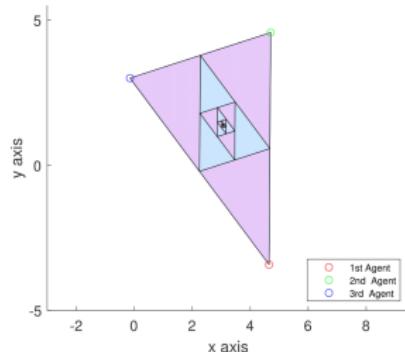
$P$  primitive and doubly stochastic

$$P = \begin{bmatrix} 1/2 & 1/2 & 0 \\ 0 & 1/2 & 1/2 \\ 1/2 & 0 & 1/2 \end{bmatrix}$$

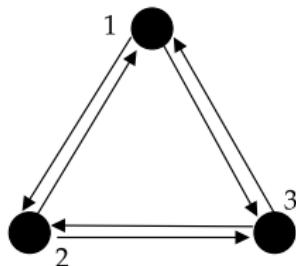
Case 1



Case 2



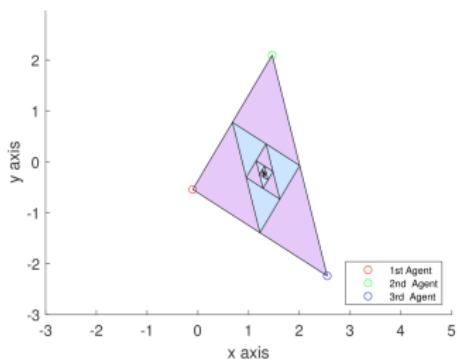
## Consensus - Average Asymptotic Consensus II



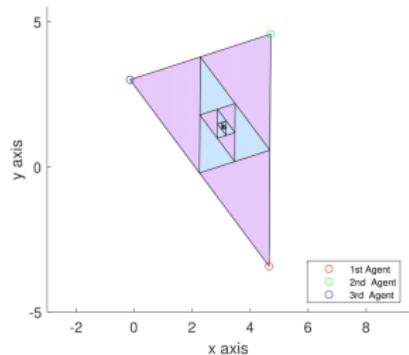
$P$  primitive and doubly stochastic

$$P = \begin{bmatrix} 0 & 1/2 & 1/2 \\ 1/2 & 0 & 1/2 \\ 1/2 & 1/2 & 0 \end{bmatrix}$$

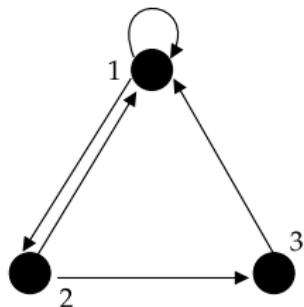
Case 1



Case 2



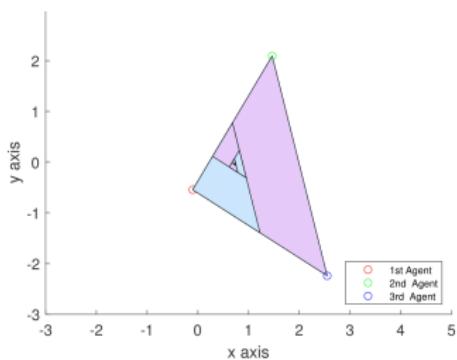
## Consensus - Asymptotic Consensus



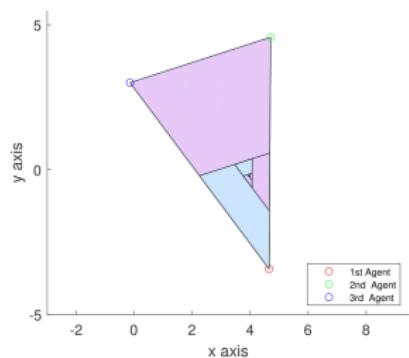
$P$  primitive and row stochastic

$$P = \begin{bmatrix} 1/2 & 1/2 & 0 \\ 1/2 & 0 & 1/2 \\ 1 & 0 & 0 \end{bmatrix}$$

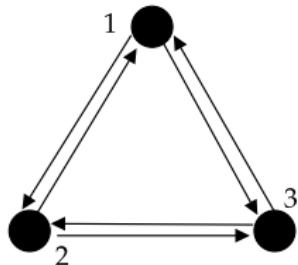
Case 1



Case 2



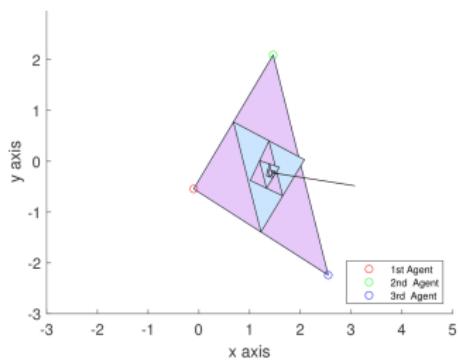
## Consensus - Divergence



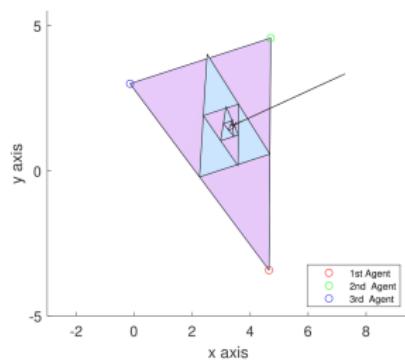
$P$  primitive

$$P = \begin{bmatrix} 0 & 0.55 & 1/2 \\ 1/2 & 0 & 1/2 \\ 1/2 & 1/2 & 0 \end{bmatrix}$$

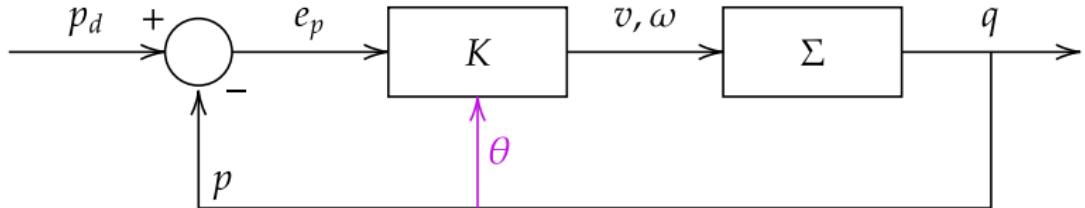
Case 1



Case 2



## Regulation - Cartesian I



Rendez-vous point:  $p_d = [x_d \quad y_d]^T$

Control law:

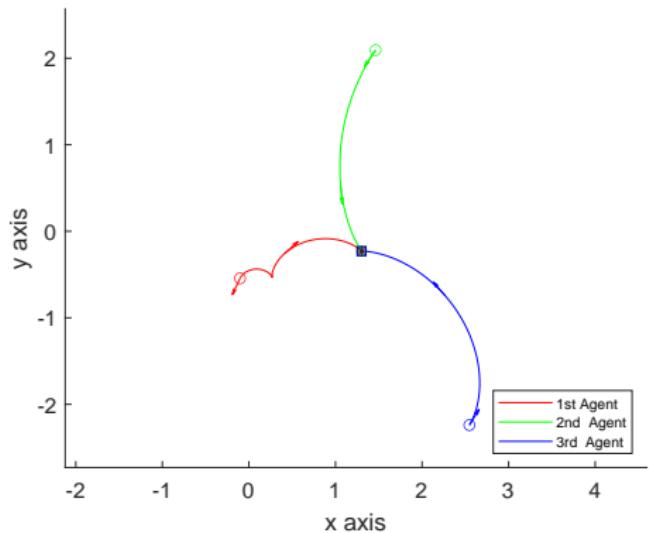
$$\begin{cases} v = -K_v \underbrace{(e_{p,x} \cos \theta + e_{p,y} \sin \theta)}_{= \langle e_p, n \rangle} \\ \omega = -K_\omega \underbrace{(\text{atan2}(e_{p,y}, e_{p,x}) + \pi - \theta)}_{= \gamma} \end{cases}$$

Gains:  $K_v = 3$ ,  $K_\omega = 5$ .

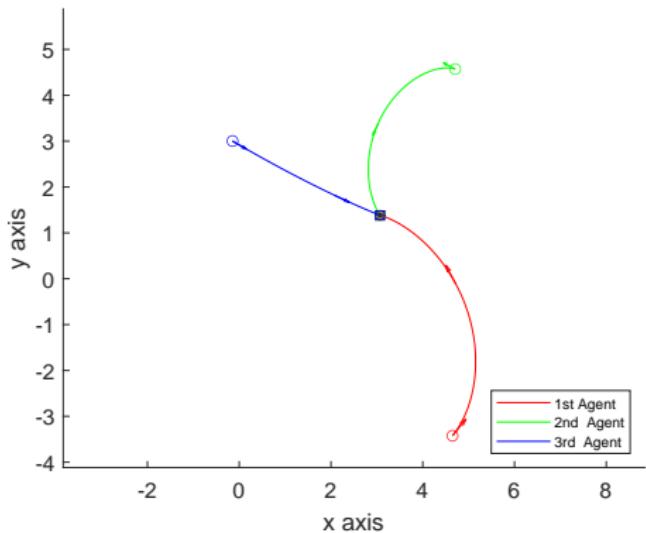


## Regulation - Cartesian II

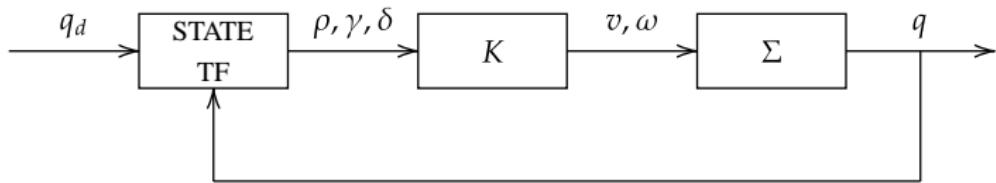
Case 1



Case 2



# Regulation - Posture with singularity at the rendez-vous point |



Regulation desired point:  $q_d = [x_d \quad y_d \quad \theta_d]^T$ , with  $x_d, y_d$  rendez-vous point and  $\theta_d$  arbitrary

State Transformation:

$$\begin{cases} \rho = \sqrt{e_{q,x}^2 + e_{q,y}^2} \\ \gamma = \text{atan2}(e_{q,y}, e_{q,x}) + \pi - \theta \\ \delta = \gamma + e_{q,\theta} \end{cases}$$

Control law:

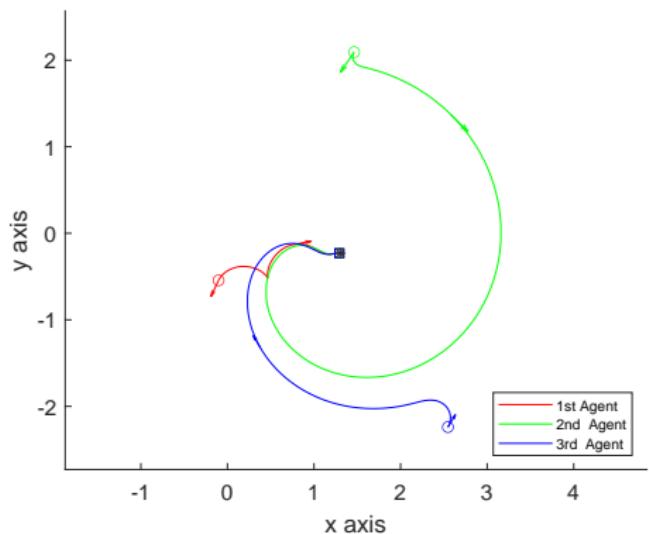
$$\begin{cases} v = K_1 \frac{\langle e_p, n \rangle}{\rho \cos \gamma} \\ \omega = K_2 \gamma + K_1 \frac{\sin \gamma \cos \gamma}{\gamma} (\gamma + K_3 \delta) \end{cases}$$

Gains:  $K_1 = K_2 = K_3 = 5$ .

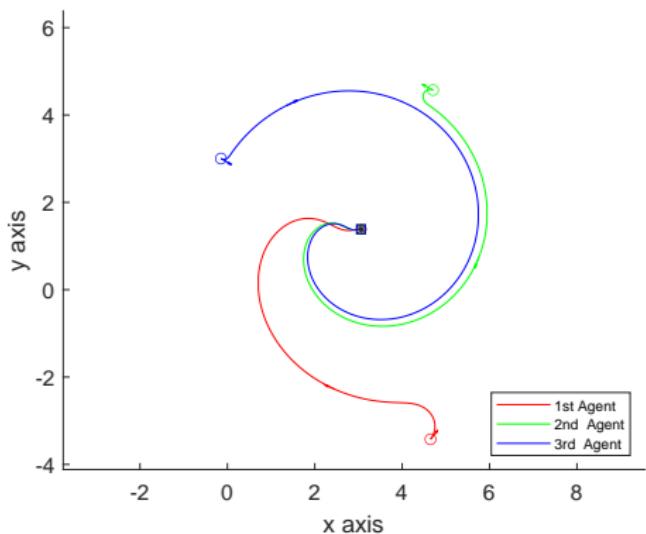


## Regulation - Posture with singularity at the rendez-vous point II

Case 1

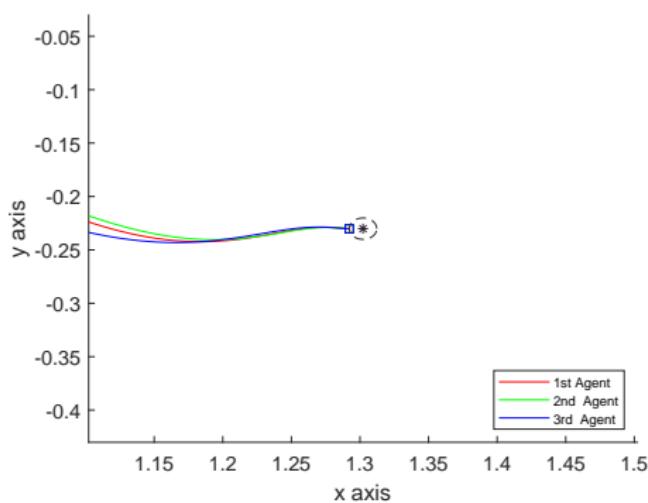


Case 2

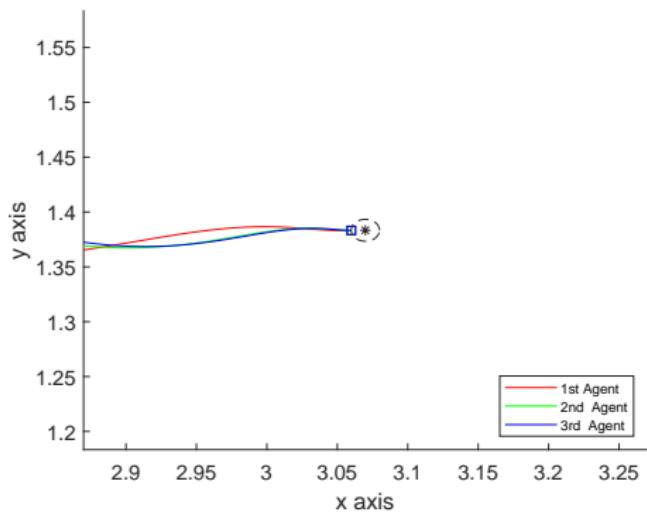


## Regulation - Posture with singularity at the rendez-vous point III

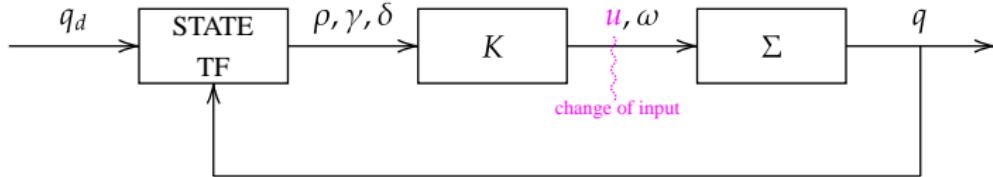
Case 1



Case 2



# Regulation - Posture without singularity at the rendez-vous point |



Regulation desired point:  $q_d = [x_d \quad y_d \quad \theta_d]^T$ , with  $x_d, y_d$  rendez-vous point and  $\theta_d$  arbitrary

State Transformation:

$$\begin{cases} \rho = \sqrt{e_{q,x}^2 + e_{q,y}^2} \\ \gamma = \text{atan2}(e_{q,y}, e_{q,x}) + \pi - \theta \\ \delta = \gamma + e_{q,\theta} \end{cases}$$

Control law:

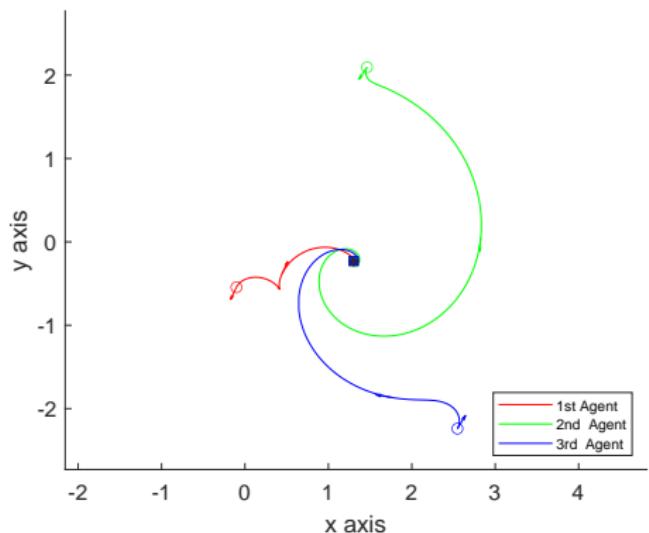
$$\begin{cases} u = \frac{v}{\rho} = K_1 \cos \gamma \\ \omega = K_2 \gamma + K_1 \frac{\sin \gamma \cos \gamma}{\gamma} (\gamma + K_3 \delta) \end{cases}$$

Gains:  $K_1 = K_2 = 3$ ,  $K_3 = 2$ .

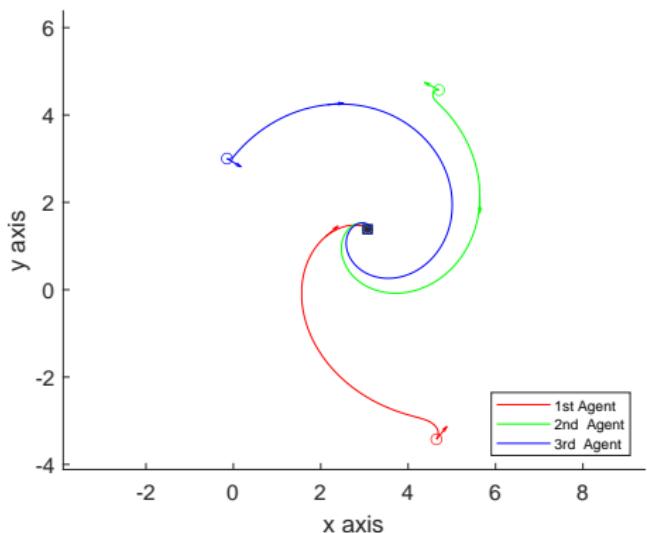


## Regulation - Posture without singularity at the rendez-vous point II

Case 1

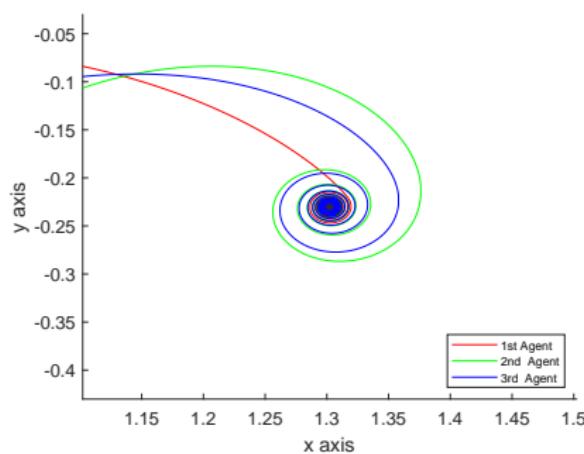


Case 2

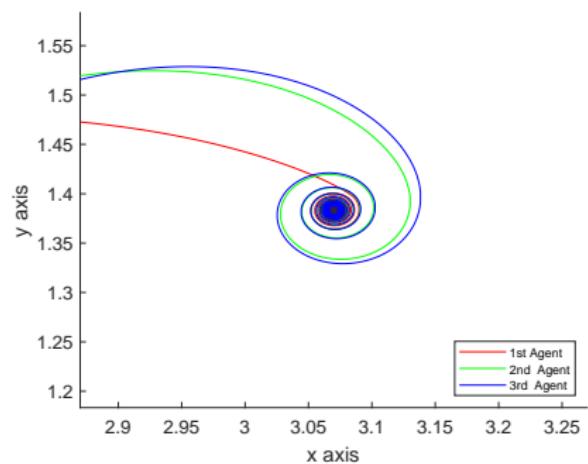


## Regulation - Posture without singularity at the rendez-vous point III

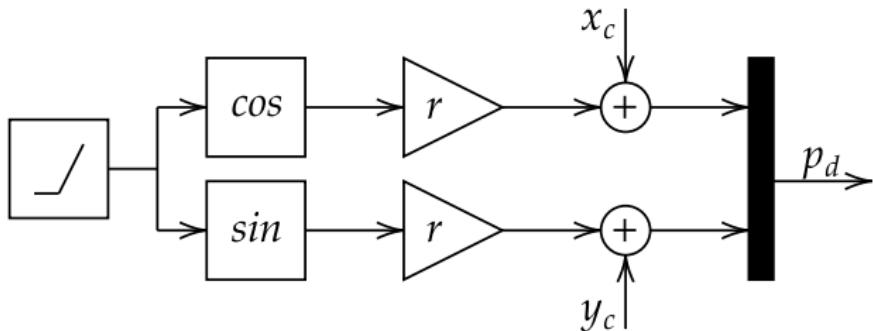
Case 1



Case 2



## Tracking - Circular trajectory



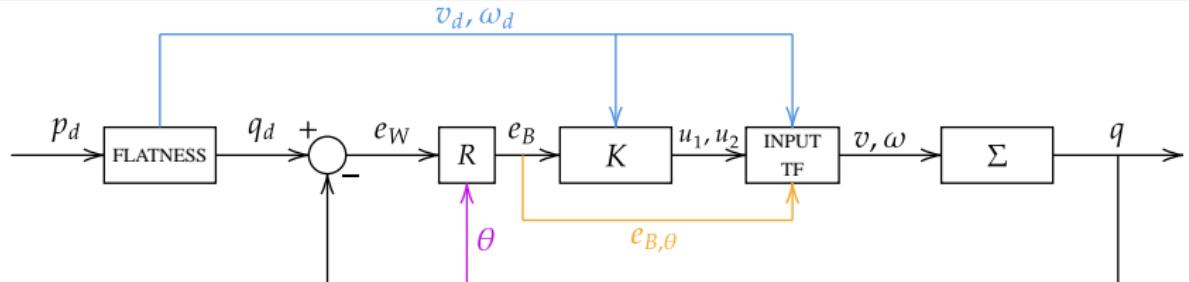
Center:  $[x_c \quad y_c]^T = \text{rendez-vous point}, \quad \text{Radius: } r = 5 \text{ [m]}$

Phases:  $\varphi_1 = 0, \quad \varphi_2 = \frac{2}{3}\pi, \quad \varphi_3 = \frac{4}{3}\pi$

Trajectory:  $p_d = \begin{cases} x_d(t) = x_c + r \cos(\theta(t) + \varphi_i) \\ y_d(t) = y_c + r \sin(\theta(t) + \varphi_i) \end{cases}, \quad \theta(t) = \text{ramp}(t) + \varphi_i, \quad i = 1, 2, 3.$



# Tracking - Linearization of state error dynamics I



Flatness:  $\begin{cases} v_d = \sqrt{\dot{x}_d^2 + \dot{y}_d^2} \\ \omega_d = \frac{\dot{x}_d \dot{y}_d - \ddot{x}_d \dot{y}_d}{\dot{x}_d^2 + \dot{y}_d^2} \end{cases}$ , W2B transformation:  $\begin{bmatrix} e_{B,x} \\ e_{B,y} \\ e_{B,\theta} \end{bmatrix} = \underbrace{\begin{bmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{= R} \underbrace{\begin{bmatrix} x_d - x \\ y_d - y \\ \theta_d - \theta \end{bmatrix}}_{= e_w}$

Control law:  $\begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \underbrace{\begin{bmatrix} -K_1 & 0 & 0 \\ 0 & -K_2 & -K_3 \end{bmatrix}}_{= K} \underbrace{\begin{bmatrix} e_{B,x} \\ e_{B,y} \\ e_{B,\theta} \end{bmatrix}}_{= e_B}$

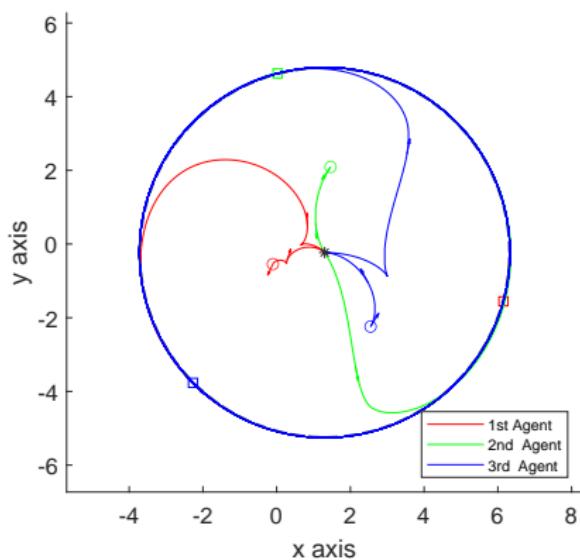
Input Transformation:  $\begin{cases} v = v_d \cos e_{B,\theta} - u_1 \\ \omega = \omega_d - u_2 \end{cases}$

Gains:  $K_1 = K_3 = 2\xi a$ ,  $K_2 = \frac{a^2 - \omega_d^2}{v_d}$  and  $a = 3$ ,  $\xi = 0.9$ .

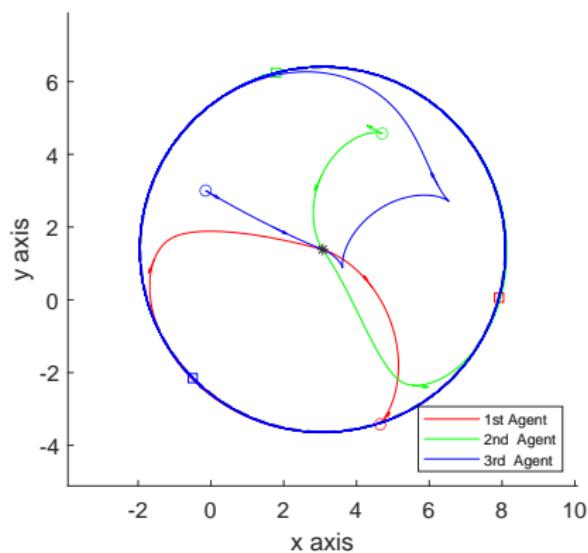


## Tracking - Linearization of state error dynamics II

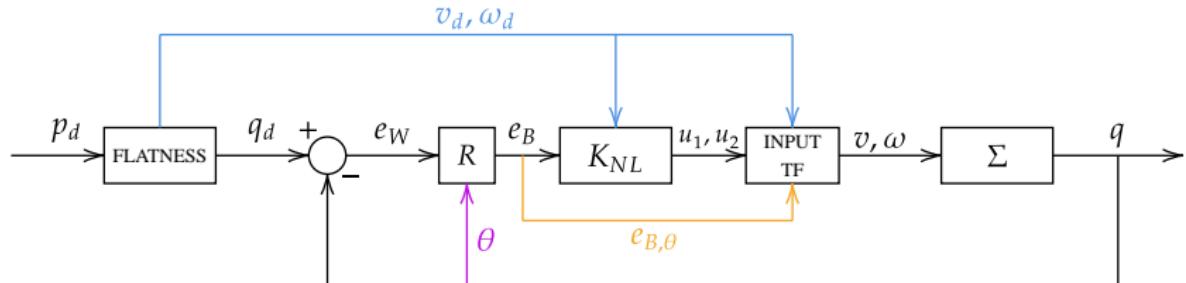
Case 1



Case 2



# Tracking - Non-Linear controller of state error dynamics I



Flatness:  $\begin{cases} v_d = \sqrt{\dot{x}_d^2 + \dot{y}_d^2} \\ \omega_d = \frac{\dot{x}_d \ddot{y}_d - \ddot{x}_d \dot{y}_d}{\dot{x}_d^2 + \dot{y}_d^2} \end{cases}$ , W2B transformation:

$$\begin{bmatrix} e_{B,x} \\ e_{B,y} \\ e_{B,\theta} \end{bmatrix} = \underbrace{\begin{bmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{= R} \underbrace{\begin{bmatrix} x_d - x \\ y_d - y \\ \theta_d - \theta \end{bmatrix}}_{= e_w}$$

Control law:  $\begin{cases} u_1 = -K_1 e_{B,x} \\ u_2 = -K_2 \left( v_d \frac{\sin e_{B,\theta}}{e_{B,\theta}} \right) e_{B,y} - K_3 e_{B,\theta} \end{cases}$

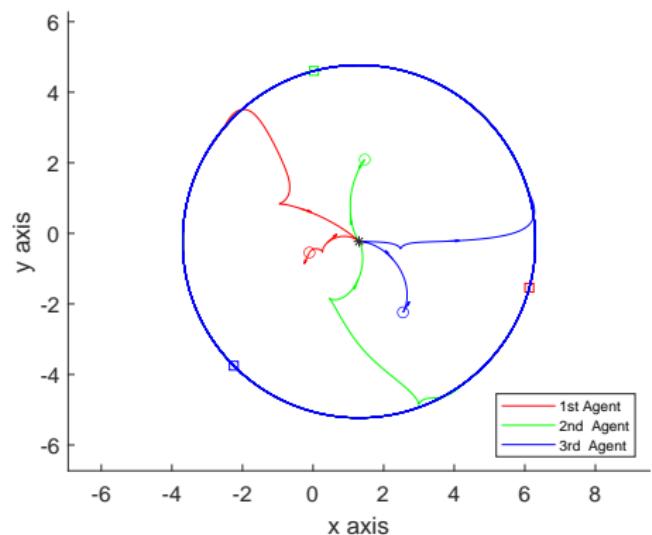
Input Transformation:  $\begin{cases} v = v_d \cos e_{B,\theta} - u_1 \\ \omega = \omega_d - u_2 \end{cases}$

Gains:  $K_1 = K_3 = 2\xi \sqrt{b v_d + \omega_d^2}$ ,  $K_2 = b$ , with  $b = 20$ ,  $\xi = 0.8$ .

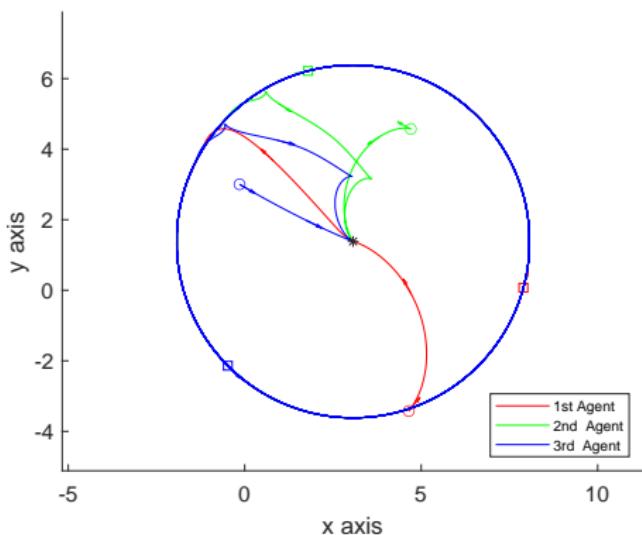


## Tracking - Non-Linear controller of state error dynamics II

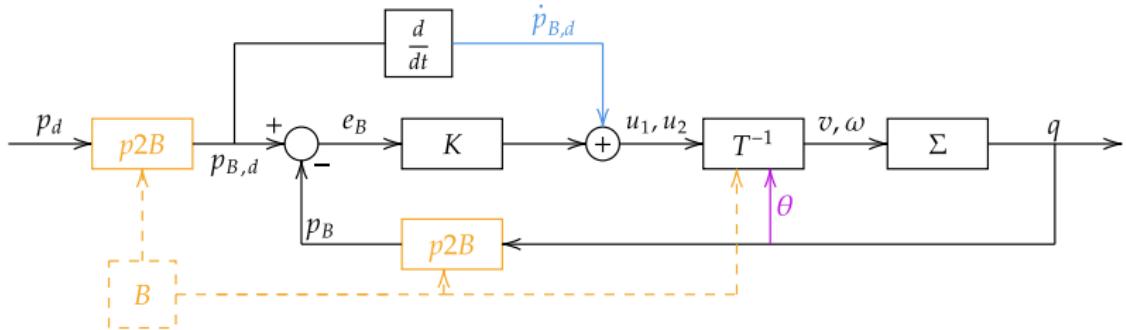
Case 1



Case 2



# Tracking - Output Feedback Linearization based on a reference point on the sagittal axis I



p2B transformation:  $\begin{cases} x_B = x + b \cos \theta \\ y_B = y + b \sin \theta \end{cases}$ , with  $b = 0.01 \text{ [m]}$ , New dynamics:  $\begin{cases} \dot{x}_B = u_1 \\ \dot{y}_B = u_2 \end{cases}$

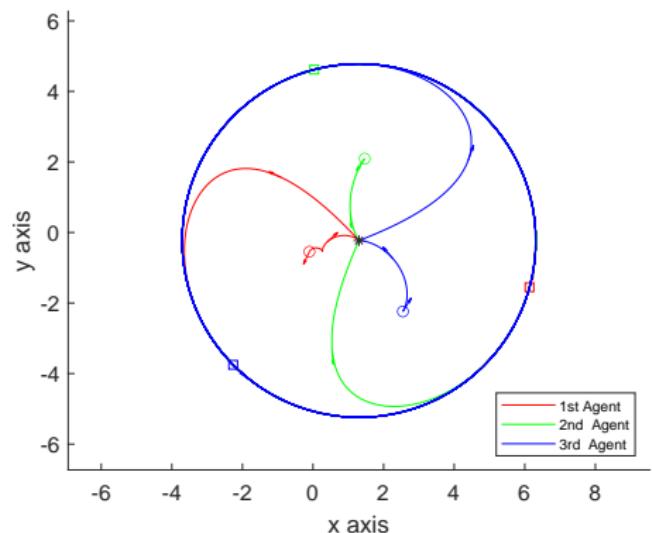
Control law:  $\begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \underbrace{\begin{bmatrix} K_1 & 0 \\ 0 & K_2 \end{bmatrix}}_K \underbrace{\begin{bmatrix} x_{B,d} - x_B \\ y_{B,d} - y_B \end{bmatrix}}_{=e_B} + \underbrace{\begin{bmatrix} \dot{x}_{B,d} \\ \dot{y}_{B,d} \end{bmatrix}}_{=\dot{p}_{B,d}}$

Input transformation:  $\begin{bmatrix} v \\ \omega \end{bmatrix} = \underbrace{\begin{bmatrix} \cos \theta & \sin \theta \\ -\frac{\sin \theta}{b} & \frac{\cos \theta}{b} \end{bmatrix}}_{=T^{-1}} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$ , Gains:  $K_1 = K_2 = 3$ .

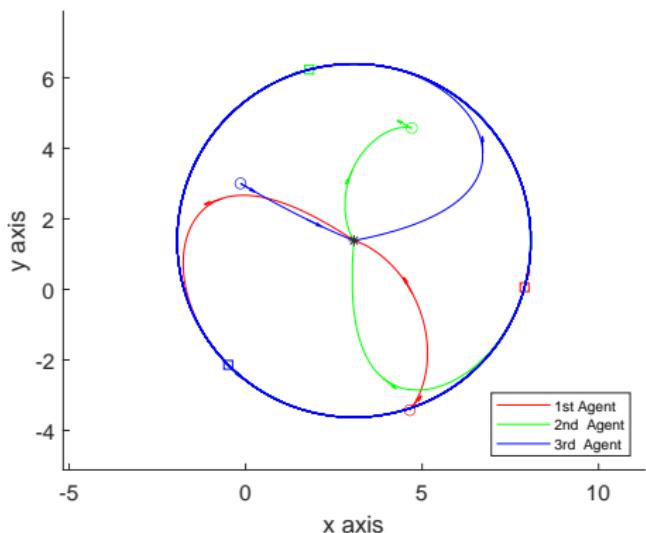


## Tracking - Output Feedback Linearization based on a reference point on the sagittal axis II

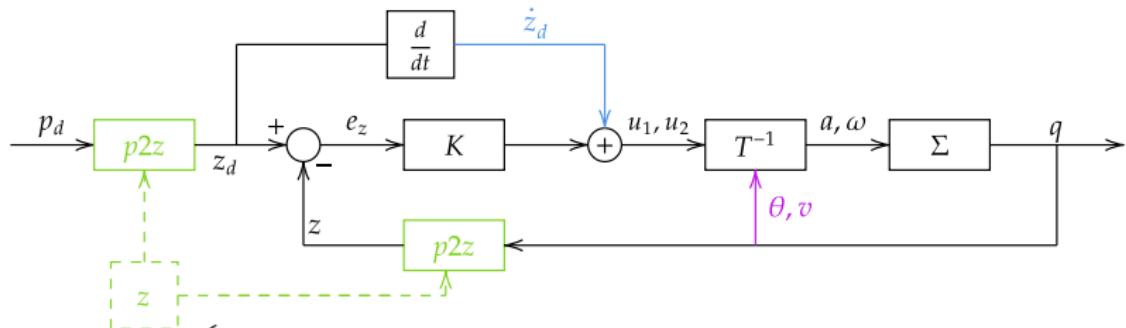
Case 1



Case 2



# Tracking - Output Feedback Linearization based on second order derivatives I



p2z transformation:  $\begin{cases} z_1 = x \\ z_2 = y \\ z_3 = \dot{x} \\ z_4 = \dot{y} \end{cases}$ , New dynamics:  $\begin{cases} \ddot{z}_1 = u_1 \\ \ddot{z}_2 = u_2 \end{cases}$

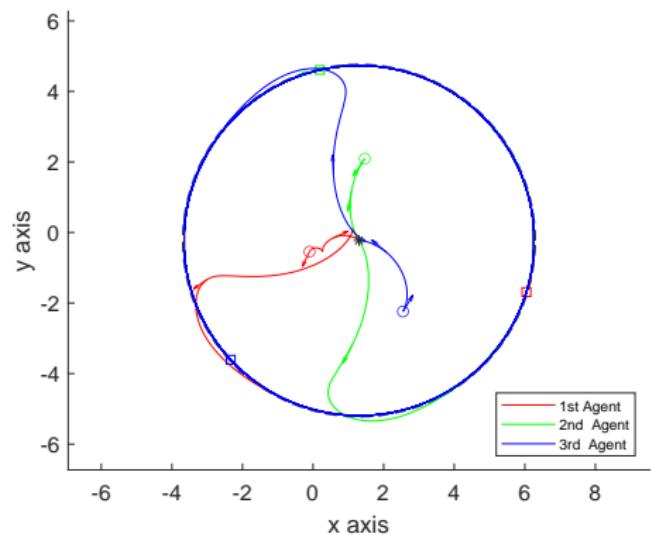
Control law:  $\begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \underbrace{\begin{bmatrix} K_1 & 0 & K_3 & 0 \\ 0 & K_2 & 0 & K_4 \end{bmatrix}}_{=K} \underbrace{\begin{bmatrix} x_d - x \\ y_d - y \\ \dot{x}_d - \dot{x} \\ \dot{y}_d - \dot{y} \end{bmatrix}}_{=e_z} + \begin{bmatrix} \ddot{x}_d \\ \ddot{y}_d \end{bmatrix}, v = \sqrt{\dot{x}^2 + \dot{y}^2}$

Input Transformation:  $\begin{bmatrix} a \\ w \end{bmatrix} = \underbrace{\begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \\ \hline v & v \end{bmatrix}}_{=T^{-1}} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$ , Gains:  $K_1 = K_2 = 30, K_3 = K_4 = 5$

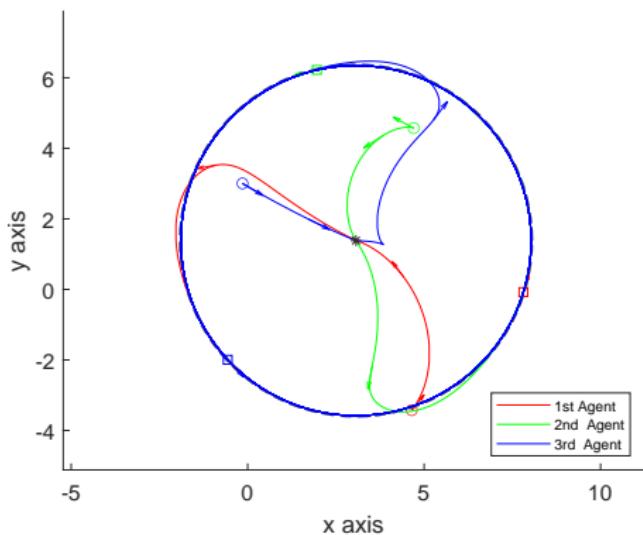


## Tracking - Output Feedback Linearization based on second order derivatives II

Case 1



Case 2



# Conclusions I

## Regulation

<i>Cartesian</i>	Easy to implement	No orientation control
<i>Posture w/ singularity</i>	Orientation control	Singularity in $e_p = 0$
<i>Posture w/out singularity</i>	Orientation control	Spiraling approach to $q_d$ No deceleration approaching $q_d$

## Tracking

<i>Linearization</i>	Linear dynamics	W2B transformation of $e$
	Poles allocation	Local approximation around $e = 0$ Differential flatness
<i>NonLinear</i>	No approximation around $e = 0$	W2B transformation of $e$ Differential flatness
<i>B-Point</i>	Simple implementation	Translation of $b \neq 0$
	Linearized and decoupled dynamics	Smoothness of trajectory
	$\theta_d$ not required	$\theta$ not directly controllable
<i>2<sup>nd</sup> Derivatives</i>	Linearized and decoupled dynamics	2 <sup>nd</sup> derivatives computations
	$\theta_d$ not required	$\theta$ not directly controllable
		$v \neq 0$



## Conclusions II

In this specific scenario the most suitable controllers are:

- Regulation task: Cartesian controller;
- Tracking task: Either the B-Point or the Non-Linear controller. However, the former requires a perfect knowledge of the model, hence in a non-ideal case the performances could worsen.

Some possible future improvements or further work could be:

- Exploit the posture regulation to position the robots with the appropriate orientation in order to follow the circular trajectory;
- Consider real-world applications, implementing saturation blocks, collision avoidance and gain tuning to satisfy given performance specifications, even in presence of noise.



# Thank you for your attention

