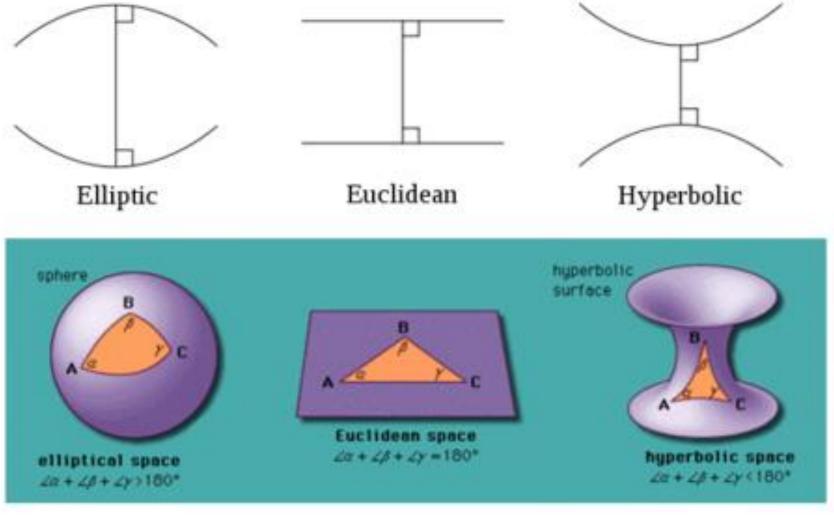
Dynamic Relaxation & Force-Directed Graph Drawing

Dr. Ir. Pirouz Nourian, Ir. Shervin Azadi, Ir. Puck Flikweert

Chair of Design Informatics



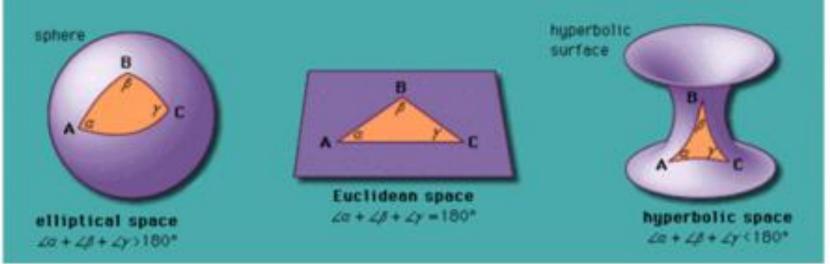
Material-Form-Structure





Material-Form-Structure







Middle: https://www.colourbox.com/image/ancient-fisherman-s-wooden-hut-in-ethnic-park-of-alesund-norway-image-1723627

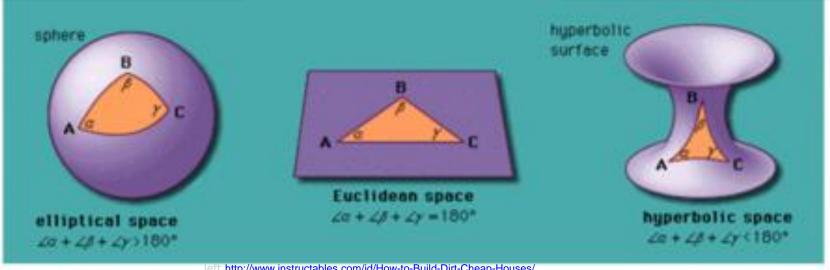
Right: https://www.colourbox.com/image/ancient-fisherman-s-wooden-hut-in-ethnic-park-of-alesund-norway-image-1723627

bottom: http://original.britannica.com/eb/art-322/Contrasting-triangles-in-Euclidean-elliptic-and-hyperbolic-spaces



Material-Form-Structure





left http://www.instructables.com/id/How-to-Build-Dirt-Cheap-Houses/

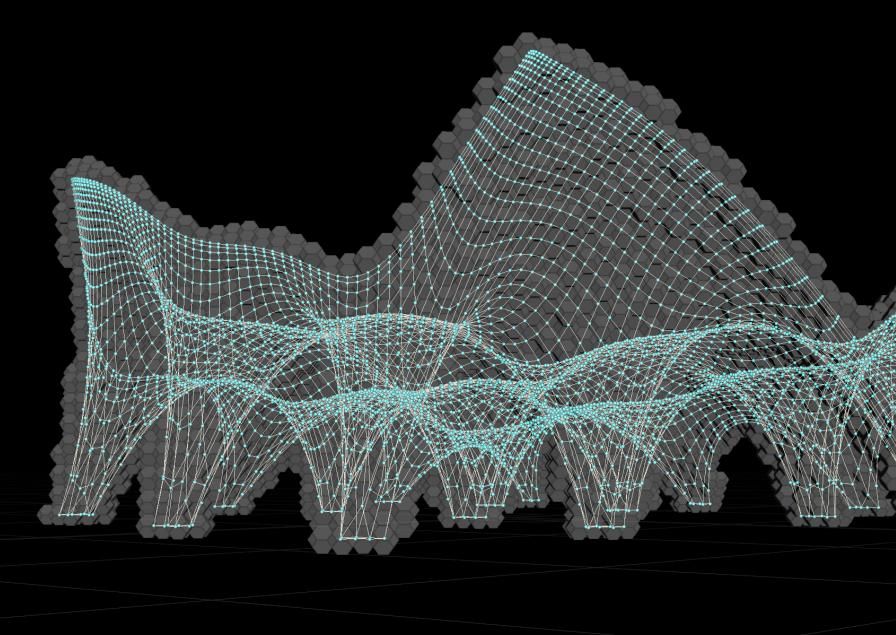
https://www.colourbox.com/image/ancient-fisherman-s-wooden-hut-in-ethnic-park-of-alesund-norway-image-1723627

https://www.colourbox.com/image/ancient-fisherman-s-wooden-hut-in-ethnic-park-of-alesund-norway-image-1723627

bottom: http://original.britannica.com/eb/art-322/Contrasting-triangles-in-Euclidean-elliptic-and-hyperbolic-spaces

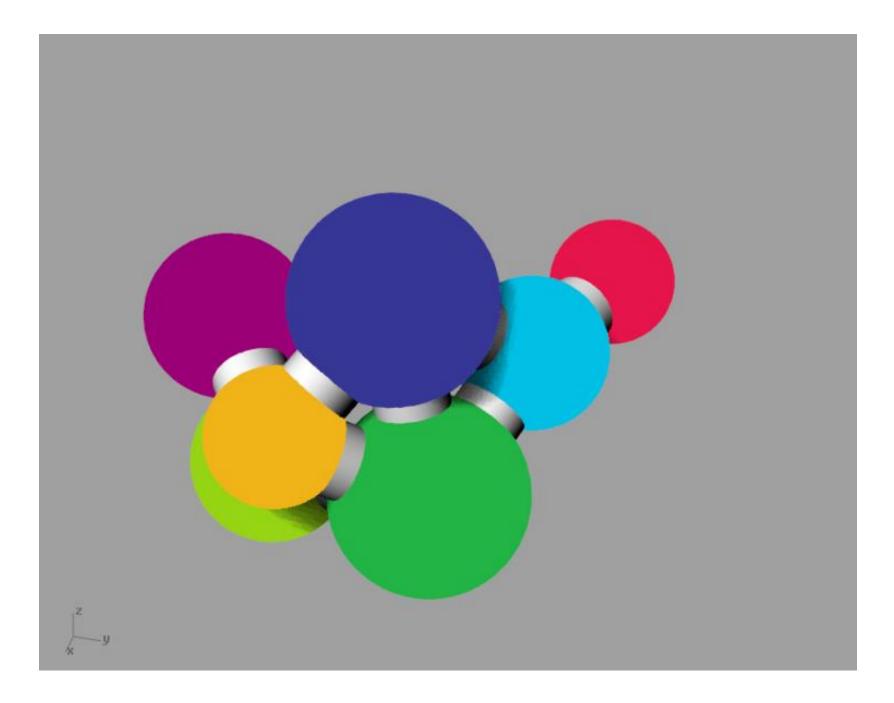


ynamic Relaxation





Force-Directed Graph-Drawing

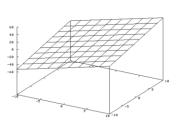


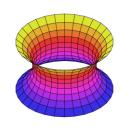


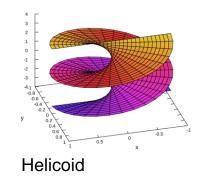
 A surface that minimizes total area subject to some constraint



Classic

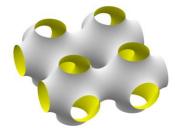


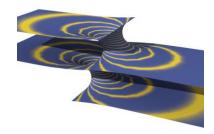




Catenoid

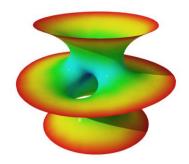
19th Century



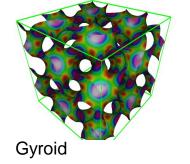


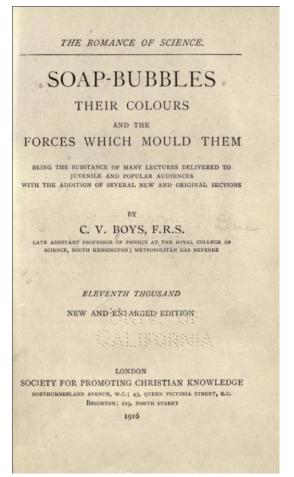
Riemann

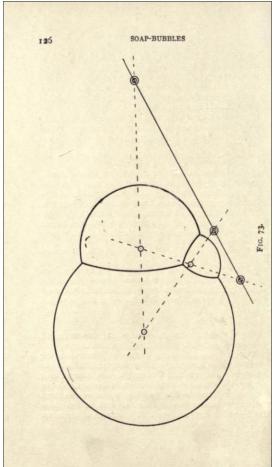
Contemporary

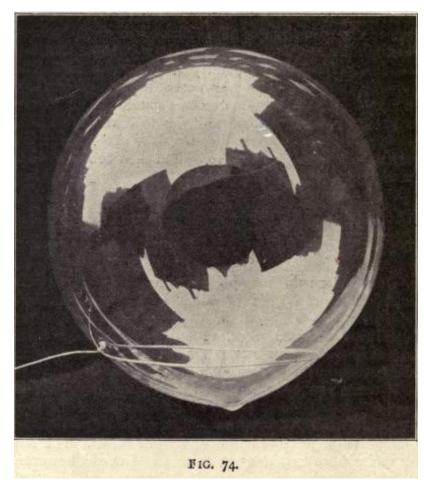














SOAP-BUBBLES

It is easy to show that this is heavy; it is only necessary to drop into the jar a bubble, and so soon as the bubble meets the heavy vapour it stops falling and remains floating upon the surface as a cork does upon water (Fig. 53). Now let me test the bubble and see whether any of the vapour bas passed to the inside. I pick it up

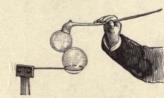


Fig. 54.

out of the jar with a wire ring and carry it to a light, and at once there is a burst of flame. But this is not sufficient to show that the ether vapour has passed to the inside, because it might have condensed in sufficient quantity upon the bubble to make it inflammable. You remember that when I poured some of this vapour upon water (see p. 34), sufficient condensed to so weaken the water-skin that the frame of wire could get

EXPERIMENTS WITH SOAP-BUBBLES

through to the other side. However, I can see whether this is the true explanation or not by blowing a bubble on a wide pipe, and holding it in the vapour for a moment. Now on removing it you notice that the bubble hangs like a heavy drop; it has lost the perfect roundness that it had at first, and this looks as if the vapour had found its way in, but this is made certain by bringing a light to the mouth of the tube, when the vapour, forced out by the elasticity of the bubble, catches fire and burns with a flame five or six inches long (Fig. 5.4). You might also have noticed that when the bubble was re-



moved, the vapour inside it began to pass out again and

fell away in a heavy stream, but this you could only see by looking at the shadow upon the screen.

Experiments with Soap-bubbles

You may have noticed when I made the drops of oil in the mixture of alcohol and water, that when they were brought together they did not at once unite; they pressed against one another and pushed each other away if allowed, just as the water-drops did in the fountain of which I showed you a photograph. You also may have noticed that the drops of water in the paraffin

SOAP-BUBBLES

mixture bounced against one another, or if filled with the paraffin, formed bubbles in which often other small drops, both of water and paraffin, remained floating.

In all these cases there was a thin film of something between the drops which they were unable to squeeze out, namely, water, paraffin, or air, as the case might be.



Fig. 56.

Will two soap-bubbles also when knocked together be unable to squeeze out the air between them? This you can try at home just as well as I can here, but I will perform the experiment at once. I have blown a pair of bubbles, and now when I hit them together they remain distinct and separate (Fig. 55).

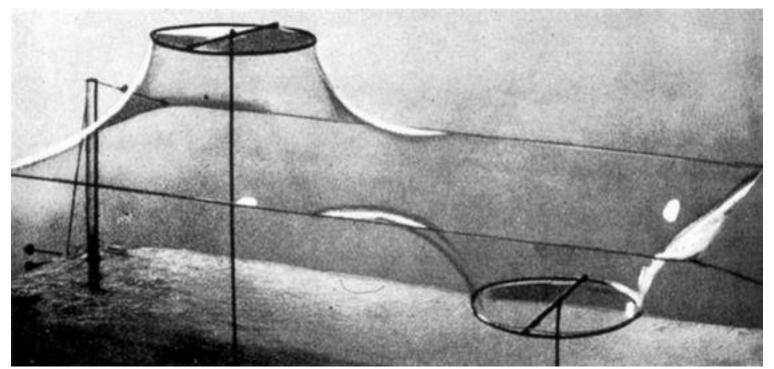
I shall next place a bubble on a ring, which it is just too large to get through. In my hand I hold a ring, on





ArchDaily













Newton's Laws of Motion

And what they actually mean...

- 1. Inertness: movement does not require force, in the absence of forces, an object is inert, i.e. it keeps its velocity, whether zero or non-zero
- 2. Acceleration: the vector sum of forces on an object cause an acceleration inversely proportional to the mass of the object
- 3. Action and Reaction: When one body exerts a force on a second body, the second body simultaneously exerts a force equal in magnitude and opposite in direction on the first body.
- 4. Superposition: Forces add up like vectors



Newton's Laws of Motion

And what they actually mean...

Why do we say velocity and not speed? Is this just a fancy word?

- 1. Inertness: movement doe not require force, in the absence of forces, an object is inert, i.e. it keeps its velocity, whether zero or non-zero.
- 2. Acceleration: the vector sum of forces on an object cause an acceleration inversely proportional to the mass of the object.
- 3. Action and Reaction: When one body exerts a force on a second body, the second body simultaneously exerts a force equal in magnitude and opposite in direction on the first body.
- 4. Superposition: Forces add up like vectors.

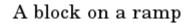
Yes sir Newton, but what does this mean for structures? Where does the so-called surface reaction force come from?

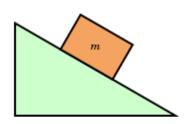


Free-Body Diagrams and the mysterious N

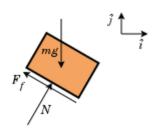
Where does this force N come from in reality?

https://en.wikipedia.org/wiki/Free_body_diagram





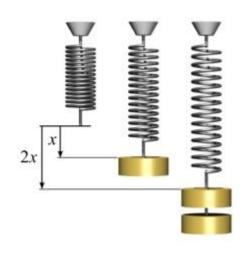
Free body diagram of just the block





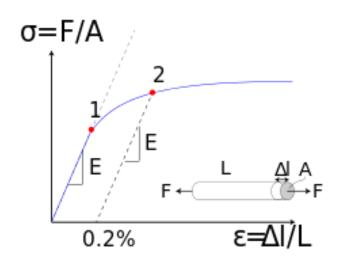
Hooke's Law

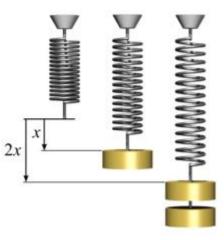
$$f = k\Delta x$$





Hooke's Law and the Stress-Strain Relation



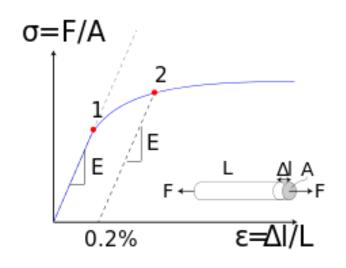


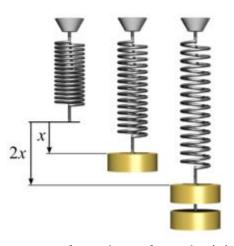
Stress–strain curve showing typical yield behavior for nonferrous alloys. Stress (σ) is shown as a function of strain (ϵ)

- 1: Elastic (proportionality) limit
- 2: Offset yield strength (0.2% proof strength)



Hooke's Law and the Stress-Strain Relation





Stress–strain curve showing typical yield behavior for nonferrous alloys. Stress (σ) is shown as a function of strain (ϵ)

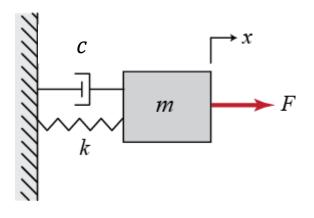
- 1: Elastic (proportionality) limit
- 2: Offset yield strength (0.2% proof strength)



$$m\ddot{u} + c\dot{u} + ku = f$$

$$f = f_{ext} - kx - c\frac{dx}{dt} = ma = m\frac{d^2x}{dt^2}$$

$$f = f_{ext} - kx - c\frac{dx}{dt} = ma = m\frac{d^2x}{dt^2}$$

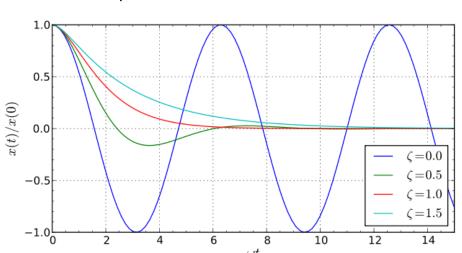


$$m\ddot{u} + c\dot{u} + ku = f$$

$$f = f_{ext} - kx - c\frac{dx}{dt} = ma = m\frac{d^2x}{dt^2}$$

No external forces
$$\rightarrow$$
 $m \frac{d^2x}{dt^2} + 2\zeta\omega_0 \frac{dx}{dt} + \omega_0^2 x = 0$

$$\omega_0 = \sqrt{\frac{k}{m}} \qquad \zeta = \frac{c}{2\sqrt{mk}}$$



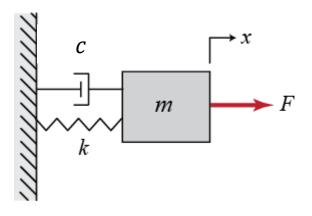




Image Credits:

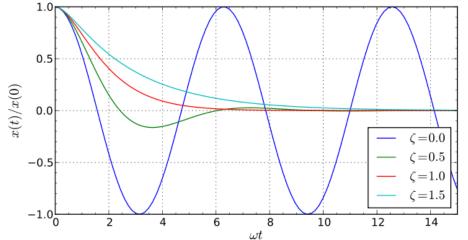
$$m\ddot{u} + c\dot{u} + ku = f$$

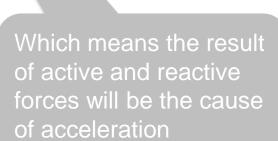
$$f = f_{ext} - kx - c\frac{dx}{dt} = ma = m\frac{d^2x}{dt^2}$$

No external forces
$$\Rightarrow m \frac{d^2x}{dt^2} + 2\zeta\omega_0 \frac{dx}{dt} + \omega_0^2 x = 0$$

Which means the system is going to start move to balance itself

$$\omega_0 = \sqrt{\frac{k}{m}} \qquad \zeta = \frac{c}{2\sqrt{mk}}$$





m



$$m\ddot{u} + c\dot{u} + ku = f$$

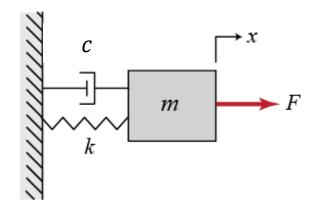
$$f = f_{ext} - kx - c\frac{dx}{dt} = ma = m\frac{d^2x}{dt^2}$$

No external forces
$$\rightarrow$$
 $m \frac{d^2x}{dt^2} + c \frac{dx}{dt} + kx(t) = 0$

If
$$x(t) = e^{\lambda t}$$

Then
$$m\lambda^2 e^{\lambda t} + c\lambda e^{\lambda t} + ke^{\lambda t} = 0$$

Then
$$m\lambda^2 + c\lambda + k = 0 \Rightarrow \lambda = \frac{-c \pm \sqrt{c^2 - 4mk}}{2m}$$



for $c=0, c^2-4mk<0$ and so, the system has strictly imaginary eigevalues and the response is oscillatory (no friction) for $c>2\sqrt{mk}, c^2-4mk>0$ and so, the system has strictly real eigevalues and the response is steadily convergent to zero



$$m\ddot{u} + c\dot{u} + ku = f$$





A+ BE: Architecture and the Built Environment 6 (14), 1-348

Force-Directed Graph Drawing

Given the graph $\Gamma = (V, E)$, $E = (V_i, V_i)$ if V_i is linked to V_i

Do

- For Each vertex $u \in V$
 - Resulting_Forces= $\sum Attraction_Forces(u) + \sum Repulsion_Forces(u)$
 - *u=u* moved by the Resulting_Forces
- Next
- Recompute Continuance_Condition: $\forall (i,j) \in E, x_{ij} \neq (R_i + R_j) \mp ErrorTolerance$
- Iteration_Count=Iteration_Count+1

Until (Continuance_Condition=False Or Iteration_Count>MaximumIterations)

Attraction_Forces=
$$AF_{ij} = k_a \Delta x_{ij}$$
, if $(I, j) \in E$, $k_a = \text{attraction strength factor}$, $\Delta x_{ij} = Distance \ V_i \ to \ V_j - RestLength(i, j)$ $RestLength(i, j) = R_i + R_j$ Repulsion_Forces= $RF_{ij} = \frac{k_r}{x_{ij}}$, for all (I, j) if $x_{ij} < RestLength(i, j)$

$$k_r$$
 = repulsion strength factor
 x_{ij} = Distance V_i to V_j
RestLength (i,j) = $R_i + R_j$

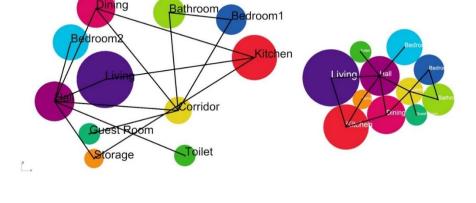






Image Credit:

For each coordinate x,y, or z:

$$P_{ix} - K_{ix}\delta_{ix}^t - C_i v_{ix}^t = M_i \dot{v}_{ix}^t$$





For each coordinate x,y, or z:

$$P_{ix} - K_{ix}\delta_{ix}^t - C_i v_{ix}^t = M_i \dot{v}_{ix}^t$$

 P_{ix} Applied force at node *i* in direction *x*

 K_{ix} Stiffness term at node *i* in direction *x*

 δ_{ix}^{t} Total displacement of node *i* in direction *x* at time *t*

 C_i Viscous Damping constant at node i

 v_{ix}^{t} Velocity of node *i* in direction *x* at time *t*

 M_i Lumped fictitious mass at node *i* chosen to optimise convergence

 \dot{v}_{ix}^{t} Acceleration at node *i* in direction *x* at time *t*



For each coordinate x,y, or z:

$$P_{ix} - K_{ix}\delta_{ix}^t - C_i v_{ix}^t = M_i \dot{v}_{ix}^t$$

$$R_{ix}^t = P_{ix} - K_{ix}\delta_{ix}^t = M_i\dot{v}_{ix}^t + C_iv_{ix}^t$$

 R_{ix}^{t} Residual (or resultant) of the applied and structural member forces at node i in direction x at time t



For each coordinate x,y, or z we do the followings:

$$P_{ix} - K_{ix}\delta^t_{ix} - C_i v^t_{ix} = M_i \dot{v}^t_{ix}$$

$$R_{ix}^t = P_{ix} - K_{ix}\delta_{ix}^t = M_i\dot{v}_{ix}^t + C_iv_{ix}^t$$

 R_{ix}^{t} Residual (or resultant) of the applied and structural member forces at node i in direction x at time t



For each coordinate x,y, or z we do the followings:

$$P_{ix} - K_{ix}\delta^t_{ix} - C_i v^t_{ix} = M_i \dot{v}^t_{ix}$$

$$R_{ix}^t = P_{ix} - K_{ix}\delta_{ix}^t = M_i\dot{v}_{ix}^t + C_iv_{ix}^t$$

acceleration as an apaproximate derivative of velocity:

$$\dot{v}_{ix}^t = \frac{v_{ix}^{t+\Delta t/2} - v_{ix}^{t-\Delta t/2}}{\Delta t}$$

velocity of a moment in time as an average of two half moments before and after:

$$v_{ix}^{t} = \frac{v_{ix}^{t + \Delta t/2} + v_{ix}^{t - \Delta t/2}}{2}$$

$$R_{ix}^{t} = M_{i}\dot{v}_{ix}^{t} + C_{i}v_{ix}^{t} = M_{i}\left(\frac{v_{ix}^{t+\Delta t/2} - v_{ix}^{t-\Delta t/2}}{\Delta t}\right) + C_{i}\left(\frac{v_{ix}^{t+\Delta t/2} + v_{ix}^{t-\Delta t/2}}{2}\right)$$



For each coordinate x,y, or z we do the followings:

$$P_{ix} - K_{ix}\delta_{ix}^t - C_i v_{ix}^t = M_i \dot{v}_{ix}^t$$

$$R_{ix}^t = P_{ix} - K_{ix}\delta_{ix}^t = M_i\dot{v}_{ix}^t + C_iv_{ix}^t$$

acceleration as an apaproximate derivative of velocity:

$$\dot{v}_{ix}^{t} = \frac{v_{ix}^{t+\Delta t/2} - v_{ix}^{t-\Delta t/2}}{\Delta t}$$

velocity of a moment in time as an average of two half moments before and after:

$$v_{ix}^{t} = \frac{v_{ix}^{t + \Delta t/2} + v_{ix}^{t - \Delta t/2}}{2}$$

$$R_{ix}^{t} = M_{i}\dot{v}_{ix}^{t} + C_{i}v_{ix}^{t} = M_{i}\left(\frac{v_{ix}^{t+\Delta t/2} - v_{ix}^{t-\Delta t/2}}{\Delta t}\right) + C_{i}\left(\frac{v_{ix}^{t+\Delta t/2} + v_{ix}^{t-\Delta t/2}}{2}\right)$$

Damping proportionate to masses:

$$C_i = M_i C$$

$$R_{ix}^{t} = M_{i}\dot{v}_{ix}^{t} + C_{i}v_{ix}^{t} = M_{i}\left(\frac{v_{ix}^{t+\Delta t/2} - v_{ix}^{t-\Delta t/2}}{\Delta t}\right) + CM_{i}\left(\frac{v_{ix}^{t+\Delta t/2} + v_{ix}^{t-\Delta t/2}}{2}\right)_{31}$$



For each coordinate x,y, or z we do the followings:

$$P_{ix} - K_{ix}\delta_{ix}^t - C_i v_{ix}^t = M_i \dot{v}_{ix}^t$$

$$R_{ix}^t = P_{ix} - K_{ix}\delta_{ix}^t = M_i\dot{v}_{ix}^t + C_iv_{ix}^t$$

https://gitlab.com/Pirouz-Nourian/Earthy/blob/master/Intensive%20Programming%20Workshops/Dynamic%20Relaxation/DynamicRelaxation.py

Damping proportionate to masses:

$$C_i = M_i C$$

$$R_{ix}^{t} = M_{i}\dot{v}_{ix}^{t} + C_{i}v_{ix}^{t} = M_{i}\left(\frac{v_{ix}^{t+\Delta t/2} - v_{ix}^{t-\Delta t/2}}{\Delta t}\right) + CM_{i}\left(\frac{v_{ix}^{t+\Delta t/2} + v_{ix}^{t-\Delta t/2}}{2}\right)$$

Long story short:

$$A = \frac{1}{1 + C\Delta t} \quad B = \frac{1 - C\Delta t}{1 + C\Delta t} \quad v_{ix}^{t + \Delta t/2} = A \frac{\Delta t}{M_i} R_{ix}^t + B v_{ix}^{t - \Delta t/2}$$



For each coordinate x,y, or z we do the followings:

$$P_{ix} - K_{ix}\delta_{ix}^t - C_i v_{ix}^t = M_i \dot{v}_{ix}^t$$

$$R_{ix}^t = P_{ix} - K_{ix}\delta_{ix}^t = M_i \dot{v}_{ix}^t + C_i v_{ix}^t$$

https://gitlab.com/Pirouz-Nourian/Earthy/blob/master/Intensive%20Programming%20Workshops/Dynamic%20Relaxation/DynamicRelaxation.py

$$A = \frac{1}{1 + C\Delta t}$$
 $B = \frac{1 - C\Delta t}{1 + C\Delta t}$

$$A = \frac{1}{1 + C\Delta t} \quad B = \frac{1 - C\Delta t}{1 + C\Delta t} \quad v_{ix}^{t + \Delta t/2} = A \frac{\Delta t}{M_i} R_{ix}^t + B v_{ix}^{t - \Delta t/2}$$

Now, from the definition of velocity:



$$v_{ix}^{t+\Delta t/2} = \frac{x_i^{t+\Delta t} - x_i^t}{\Delta t} \rightarrow x_i^{t+\Delta t} = x_i^t + v_{ix}^{t+\Delta t/2} \Delta t$$

For each coordinate x,y, or z we do the followings:

$$P_{ix} - K_{ix}\delta_{ix}^t - C_i v_{ix}^t = M_i \dot{v}_{ix}^t$$

$$R_{ix}^t = P_{ix} - K_{ix}\delta_{ix}^t = M_i\dot{v}_{ix}^t + C_iv_{ix}^t$$

https://gitlab.com/Pirouz-Nourian/Earthy/blob/master/Intensive%20Programming%20Workshops/Dynamic%20Relaxation/DynamicRelaxation.py

$$A = \frac{1}{1 + C\Delta t}$$
 $B = \frac{1 - C\Delta t}{1 + C\Delta t}$

$$A = \frac{1}{1 + C\Delta t} \quad B = \frac{1 - C\Delta t}{1 + C\Delta t} \quad v_{ix}^{t + \Delta t/2} = A \frac{\Delta t}{M_i} R_{ix}^t + B v_{ix}^{t - \Delta t/2}$$

$$v_{ix}^{t+\Delta t/2} = \frac{x_i^{t+\Delta t} - x_i^t}{\Delta t} \rightarrow x_i^{t+\Delta t} = x_i^t + v_{ix}^{t+\Delta t/2} \Delta t$$

Longer story: Hooke's law, graph theory, and cosines, projecting stiffness forces along the edges onto principal axes:

where t is not an exponent but an addicator of time step,
$$f_{\{i,j\}}$$
 is the lasticity force along the edge (i,j) , and l_{ij} is the length of that edge. The division by this length in every direction

$$R_{ix}^{t} = P_{ix} + \sum_{i \sim j} \left(\frac{f_{i,j}}{l_{i,j}} \right)^{t} \left(x_i - x_j \right)^{t}$$

1)
$$R_{ix}^t = P_{ix} + \sum_{i \sim j} \left(\frac{f_{i,j}}{l_{i,j}} \right)^t \left(x_i - x_j \right)^t$$

2)
$$v_{ix}^{t+\Delta t/2} = A \frac{\Delta t}{M_i} R_{ix}^t + B v_{ix}^{t-\Delta t/2}$$

$$x_i^{t+\Delta t} = x_i^t + v_{ix}^{t+\Delta t/2} \Delta t$$

$$A = \frac{1}{1 + C\Delta t} \quad B = \frac{1 - C\Delta t}{1 + C\Delta t}$$



1)
$$R_{ix}^{t} = P_{ix} + \sum_{i \sim j} \left(\frac{f_{i,j}}{l_{i,j}}\right)^{t} \left(x_{i} - x_{j}\right)^{t}$$

Well, this is problematic for an algorithm with a discrete time set to Δt

$$v_{ix}^{t+\Delta t/2} = A \frac{\Delta t}{M_i} R_{ix}^t + B v_{ix}^{t-\Delta t/2}$$

$$x_i^{t+\Delta t} = x_i^t + v_{ix}^{t+\Delta t/2} \Delta t$$

$$A = \frac{1}{1 + C\Delta t} \quad B = \frac{1 - C\Delta t}{1 + C\Delta t}$$



$$R_{ix}^{t} = P_{ix} + \sum_{i \sim j} \left(\frac{f_{i,j}}{l_{i,j}}\right)^{t} \left(x_{i} - x_{j}\right)^{t}$$

 $\left| R_{ix}^t = P_{ix} + \sum_{i \sim j} \left(\frac{f_{i,j}}{l_{i,j}} \right)^t \left(x_i - x_j \right)^t \right|$ We, therefore, consider the discrete time of the algorithm as $\Delta t' = 2\Delta t$ or $\Delta t = 0.5\Delta t'$ in all formulae, where $\Delta t'$ is the algorithm's iteration time interval:

2)
$$v_{ix}^{t+0.25\Delta t'} = 0.5A \frac{\Delta t'}{M_i} R_{ix}^t + B v_{ix}^{t-0.25\Delta t'}$$

3)
$$x_i^{t+0.5\Delta t'} = x_i^t + 0.5v_{ix}^{t+0.25\Delta t'} \Delta t'$$

$$A = \frac{1}{1 + 0.5C\Delta t'}$$
 $B = \frac{1 - 0.5C\Delta t'}{1 + 0.5C\Delta t'}$



1)
$$R_{ix}^t = P_{ix} + \sum_{i \sim j} \left(\frac{f_{i,j}}{l_{i,j}} \right)^t \left(x_i - x_j \right)^t$$

$$v_{ix}^{t+\Delta t'} = 2A \frac{\Delta t'}{M_i} \frac{R_{ix}^t}{R_{ix}^t} + B v_{ix}^{t-\Delta t'}$$

We could, in principle, also consider the discrete time of the algorithm as $\Delta t' = 0.5 \Delta t$ or $\Delta t = 2 \Delta t'$ in all formulae, where $\Delta t'$ is the algorithm's iteration time interval. However, using these formulae, the velocities will be large and thus likely to entangle the graph. Thus we implement the algorithm as in previous page.

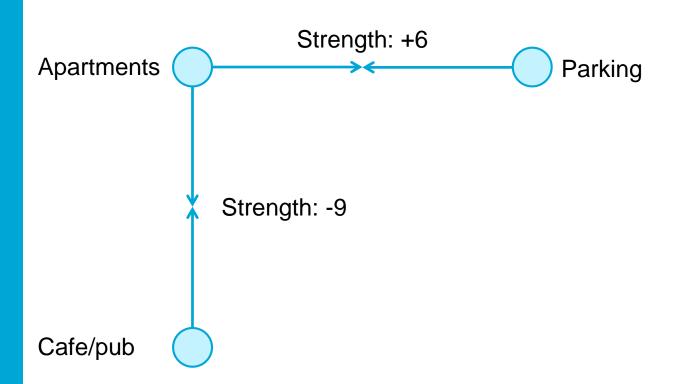
$$x_i^{t+2\Delta t'} = x_i^t + 2v_{ix}^{t+\Delta t'} \Delta t'$$

$$A = \frac{1}{1 + 2C\Delta t'} \qquad B = \frac{1 - 2C\Delta t'}{1 + 2C\Delta t'}$$



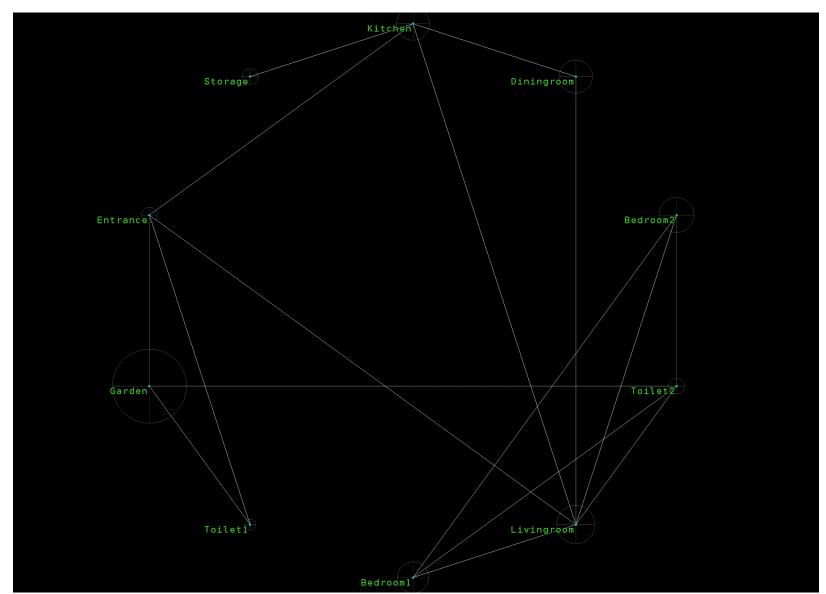
Force-directed graph drawing

- Same principle as dynamic relaxation, but then applied to a graph
- Connected nodes in a graph are attracted to each other with a certain strength



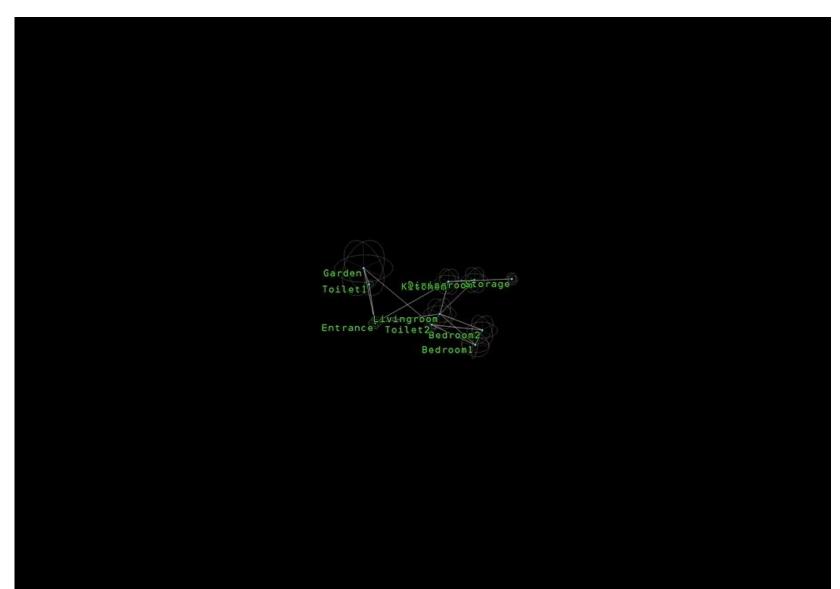


2D Force-Directed graph drawing (houdini)





3D Force-Directed graph drawing (houdini)





Example input requirements (graph)

- All nodes are given a size based on area
- All relationships are assigned a strength (attracting or repelling)

Nodes

Node	Name	Area (m2)
1	Entrance	4
2	Bedroom	12
3	Garden	12
4	Bathroom	9
5	Kitchen	9

Relationships

Node1	Node2	Strength
2	4	6
3	5	4
1	2	-4



Tasks

- Change .csv input files with your data
- Try to understand what is happening in the Python code
- Extend Python scripts in Grasshopper:
 - How to deal with different strengths between 2 nodes?
 - Make it work in 3D as well
 - Make it work in a voxel grid (nodes can only be located at the centers of voxels, and balls change to groups of voxels)



Questions: p.nourian@tudelft.nl

