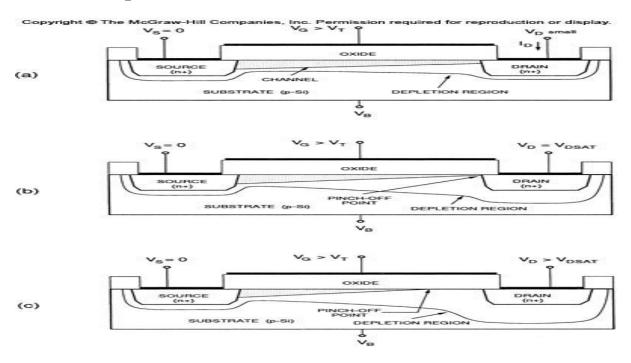
MOS transistors: Structures, MOS system under external bias, operation of MOS transistor (MOSFET),

MOS transistors: Threshold voltage MOSFET current-voltage characteristics (GCA), channel length modulation, substrate bias effect.

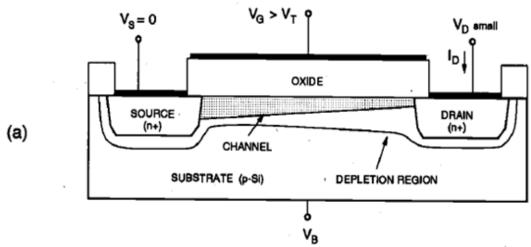
Measurements of parameters – KN, VTP & γ. Short channel effects, Narrow channel effects. Latch up and its prevention. MOSFET capacitances.

MOSFET Operation: A Qualitative View

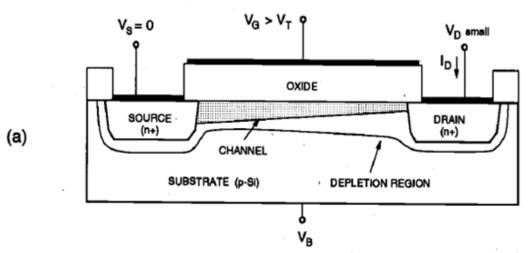


Cross-sectional view of an n-channel (nMOS) transistor, (a) operating in the linear region, (b) operating at the edge of saturation, and (c) operating beyond saturation

Operating in the linear region

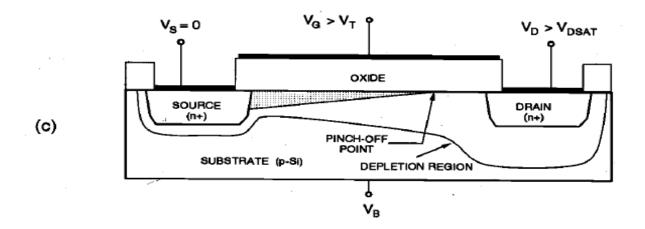


Cross-sectional view of an n-channel (nMOS) transistor operating in the linear region



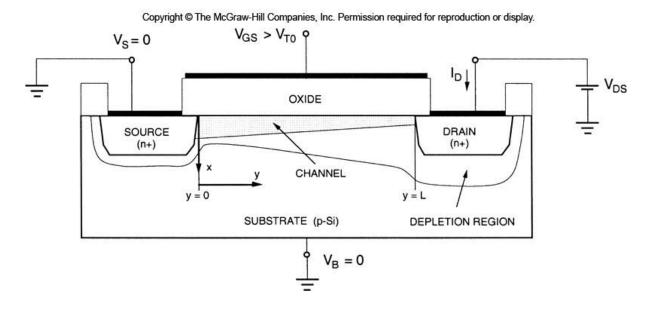
Cross-sectional view of an n-channel (nMOS) transistor operating in the linear region

N-channel (nMOS) transistor operating beyond saturation



MOSFET Current-Voltage Characteristics

- ➤ The analytical derivation of the MOSFET current-voltage relationships for various bias conditions requires that several approximations be made to simplify the problem.
- ➤ Without these simplifying assumptions, analysis of the actual three-dimensional MOS system would become a very complex task and would prevent the derivation of closed form current-voltage equations.
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- ➤ Without these simplifying assumptions, analysis of the actual three-dimensional MOS system would become a very complex task and would prevent the derivation of closed form current-voltage equations.



Gradual Channel Approximation(GCA)

- ➤ The gradual channel approximation (GCA) for establishing the MOSFET current-voltage relationships, effectively reduces the analysis to a one-dimensional current-flow problem.
- ➤ As in every approximate approach, however, the GCA also has its

limitations, especially for small-geometry MOSFETs.

- 1. Consider the cross-sectional view of the n-channel MOSFET operating in the linear mode, as shown in the figure. Here, the source and the substrate terminals are connected to ground, i.e., Vs = VB = 0.
- 2. The gate-to-source voltage (VGS) and the drain-to-source voltage (VDS) are the external parameters controlling the drain (channel) current ID.
- 3. *The gate-to-source voltage is set to be larger than the* threshold voltage VT0 to create a conducting inversion layer between the source and the drain.
- 4. The channel voltage with respect to the source is denoted by Vc(y).
- 5. Assumption: The threshold voltage VT0 is constant along the entire channel region, between y = 0 and y = L.
- 6. (In reality, the threshold voltage changes along the channel since the channel voltage is not constant)
- 7. Assumption: The electric field component *Ey along the y-coordinate is dominant compared to the electric field component Ex along the x-coordinate.*
- 8. (*This* assumption will allow us to reduce the current-flow problem in the channel to the y dimension only)

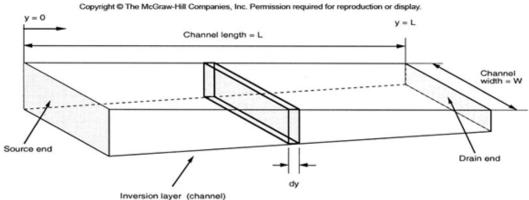
The boundary conditions for the channel voltage Vc are:

$$V_c(y=0) = V_S = 0$$
$$V_c(y=L) = V_{DS}$$

Assumption: The entire channel region between the source and the drain is inverted, i.e.,

$$\begin{aligned} V_{GS} &\geq V_{T0} \\ V_{GD} &= V_{GS} - V_{DS} \geq V_{T0} \end{aligned}$$

➤The thickness of the inversion layer tapers off as we move from the source to the drain, since the gate-to-channel voltage causing surface inversion is smaller at the drain end.



Simplified geometry of the surface inversion layer (channel region)

ightharpoonupLet $Q_I(y)$ be the total mobile electron charge in the surface inversion layer. This charge can be expressed as a function of the gate-to-source voltage V_{GS} and of the channel voltage $V_{C}(y)$ as follows

$$Q_{I}(y) = -C_{ox} \cdot [V_{GS} - V_{c}(y) - V_{T0}]$$
 (15)

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$$\begin{split} V_{GS} &\geq V_{T0} \\ V_{GD} &= V_{GS} - V_{DS} \geq V_{T0} \end{split}$$

The incremental resistance \underline{dR} of the differential channel segment can be expressed as

(assuming constant *surface mobility* μ_n of all mobile electrons in the inversion layer)

$$dR = -\frac{dy}{W \cdot \mu_n \cdot Q_I(y)} \tag{16}$$

The minus sign is due to the negative polarity of the inversion layer charge $Q_I(y) = qnx_c(y)$ [per unit W - y area; x_c = channel depth at y]

$$\rho = \frac{1}{\sigma} = \frac{1}{q\mu_n n}$$

Applying Ohm's law for this segment yields the voltage drop along the incremental segment *dy*, in the y direction.

$$dV_c = I_D \cdot dR = -\frac{I_D}{W \cdot \mu_n \cdot Q_I(y)} \cdot dy \tag{17}$$

MOSFET Drain Current Equation(GCA)

The incremental resistance <u>dR</u> of the differential channel segment can be expressed as

(assuming constant surface mobility μ_n of all mobile electrons in the inversion layer)

 $dR = -\frac{dy}{W \cdot \mu_n \cdot Q_I(y)} \tag{16}$

The minus sign is due to the negative polarity of the inversion layer charge $Q_I(y) = qnx_c(y)$ [per unit W - y area; x_c = channel depth at y]

$$\rho = \frac{1}{\sigma} = \frac{1}{q\mu_n n}$$

Applying Ohm's law for this segment yields the voltage drop along the incremental segment *dy*, in the y direction.

$$dV_c = I_D \cdot dR = -\frac{I_D}{W \cdot \mu_n \cdot Q_I(y)} \cdot dy \tag{17}$$

Integrating along the Channel

$$\int_{0}^{L} I_{D} \cdot dy = -W \cdot \mu_{n} \int_{0}^{V_{DS}} Q_{I}(y) \cdot dV_{c}$$
 (18)

$$I_D \cdot L = W \cdot \mu_n \cdot C_{ox} \int_0^{V_{DS}} \left(V_{GS} - V_c - V_{T0} \right) \cdot dV_c \tag{19}$$

$$I_D = \frac{\mu_n \cdot C_{ox}}{2} \cdot \frac{W}{L} \cdot \left[2 \cdot \left(V_{GS} - V_{T0} \right) V_{DS} - V_{DS}^2 \right]$$
 (20)

Integrating along the Channel

$$\int_{0}^{L} I_{D} \cdot dy = -W \cdot \mu_{n} \int_{0}^{V_{DS}} Q_{I}(y) \cdot dV_{c}$$
 (18)

$$I_D \cdot L = W \cdot \mu_n \cdot C_{ox} \int_0^{V_{DS}} \left(V_{GS} - V_c - V_{T0} \right) \cdot dV_c \tag{19}$$

$$I_{D} = \frac{\mu_{n} \cdot C_{ox}}{2} \cdot \frac{W}{L} \cdot \left[2 \cdot \left(V_{GS} - V_{T0} \right) V_{DS} - V_{DS}^{2} \right]$$
 (20)

Equation (20) represents the drain current ID as a simple second-order function of the two external voltages, VGS and VDS.

This current equation can also be rewritten as

$$I_{D} = \frac{k'}{2} \cdot \frac{W}{L} \cdot \left[2 \cdot \left(V_{GS} - V_{T0} \right) V_{DS} - V_{DS}^{2} \right]$$
 (21)

or

$$I_D = \frac{k}{2} \cdot \left[2 \cdot \left(V_{GS} - V_{T0} \right) V_{DS} - V_{DS}^2 \right] \tag{22}$$

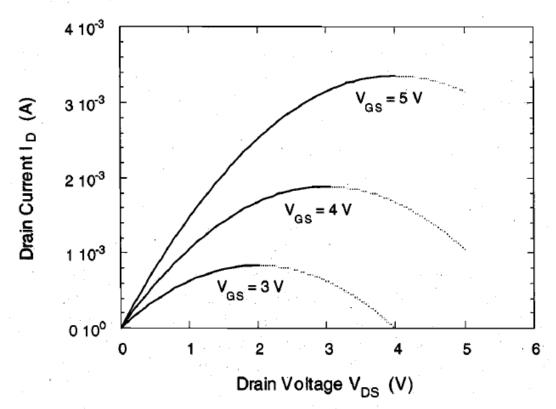
where the parameters k and k' are defined as

$$k' = \mu_n \cdot C_{ox}$$
 process transconductance parameter

$$k = k' \cdot \frac{W}{L}$$
 gain factor

Current-voltage relationship is affected by to the process dependent constants k', $V\tau_0$, and is also affected by the device dimensions, W and L.

Region of Validity of the Equation



The second-order current-voltage equation given above produces a set of inverted parabolas for each constant *VGS value*.

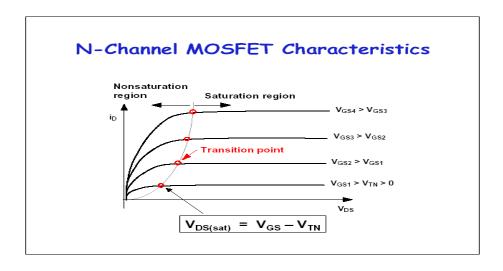
The drain current-drain voltage curves shown above reach their peak value for VDS = VGS - VTO

Beyond this maximum, each curve exhibits a negative differential conductance, which is not observed in actual MOSFET current-voltage measurements (section shown by the dashed lines) **Validity of the Equation (Linear Region)**

We must remember now that the drain current equation (20) has been derived under the following voltage assumptions,

$$\begin{split} V_{GS} &\geq V_{T0} \\ V_{GD} &= V_{GS} - V_{DS} \geq V_{T0} \end{split}$$

which guarantee that the entire channel region between the source and the drain is inverted. This condition corresponds to the *linear operating mode for the MOSFET* Hence, the current equation (20) is valid only for the linear mode operation.



Current Equation for Saturation Region

Beyond the linear region boundary, i.e., for V_{DS} values larger than V_{GS} - V_{TO} , the MOS transistor is assumed to be in saturation.

$$Q_I(y=L)=-C_{ox}(V_{GS}-V_{T0}-V_{DSAT})=0$$

$$\Rightarrow V_{DSAT}=V_{GS}-V_{T0} \qquad \text{Definition}$$

$$V_{DS}\geq V_{DSAT}=V_{GS}-V_{T0} \qquad \text{Condition for Saturation}$$
 When
$$V_{DS}=V_{DSAT}$$

$$I_{D}(sat) = \frac{\mu_{n} \cdot C_{ox}}{2} \cdot \frac{W}{L} \cdot \left[2 \cdot (V_{GS} - V_{T0}) \cdot (V_{GS} - V_{T0}) - (V_{GS} - V_{T0})^{2} \right]$$

$$= \frac{\mu_{n} \cdot C_{ox}}{2} \cdot \frac{W}{L} \cdot (V_{GS} - V_{T0})^{2}$$
(23)

This expression indicates that the saturation drain current has no dependence on $V_{\text{DS}}\,$